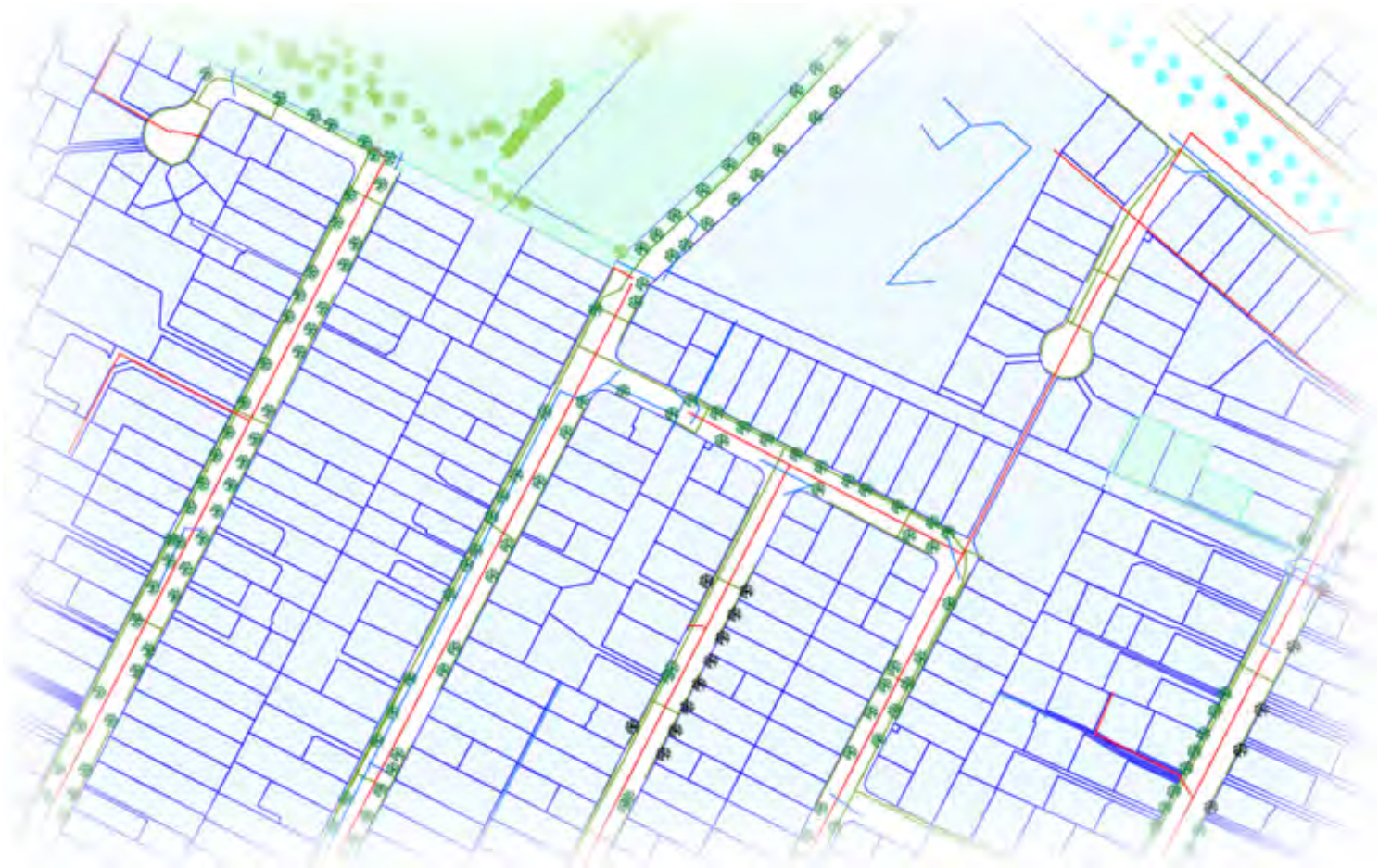


# Land Information Memorandum



Property address:  
511 Halswell Road

LIM number: 70247280  
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Christchurch City Council  
53 Hereford Street, PO Box 73015  
Christchurch 8154, New Zealand  
Tel 64 3 941 8999  
Fax 64 3 941 8984  
[www.ccc.govt.nz](http://www.ccc.govt.nz)

## Application details

Please supply to YOURSECTION RS LTD  
Client reference RIVERSTONE  
Phone number  
Fax number  
Date issued 18 June 2021  
Date received 10 June 2021

## Property details

Property address 511 Halswell Road  
Valuation roll number 23562 09200  
Valuation information Capital Value: \$5650000  
Land Value: \$5600000  
Improvements Value: \$50000  
*Please note: these values are intended for Rating purposes*  
Legal description Pt RS 1593 Canterbury Dist  
Pt RS 1593 Canterbury Dist  
Existing owner Yoursection RS Limited  
PO Box 9301  
TOWER JUNCTION  
CHRISTCHURCH 8149

## Council references

Debtor number 4188171  
Rate account ID 73054377  
LIM number 70247280  
Property ID 1022691

## Document information

This Land Information Memorandum (LIM) has been prepared for the purpose of section 44A of the Local Government Official Information and Meetings Act 1987 (LGOIMA). It is a summary of the information that we hold on the property. Each heading or "clause" in this LIM corresponds to a part of section 44A.

Sections 1 to 10 contain all of the information known to the Christchurch City Council that must be included under section 44A(2) LGOIMA. Any other information concerning the land as the Council considers, at its discretion, to be relevant is included at section 11 of this LIM (section 44A(3) LGOIMA). If there are no comments or information provided in these sections this means that the Council does not hold information on the property that corresponds to that part of section 44A.

The information included in this LIM is based on a search of Council records only and there may be other information relating to the land which is unknown to the Council. Please note that other agencies may also hold information relevant to the property, or administer legislation relevant to the use of the land, for example, the Regional Council (Ecan), Heritage New Zealand Pouhere Taonga, and Land Information New Zealand.

Council records may not show illegal or unauthorised building or works on the property. The applicant is solely responsible for ensuring that the land is suitable for a particular purpose.

A LIM is only valid at the date of issue as information is based only upon information the Council held at the time of that LIM request being made.

## Property file service

This Land Information Memorandum does not contain all information held on a property file. Customers may request property files by phoning the Council's Customer Call Centre on (03) 941 8999, or visiting any of the Council Service Centres. For further information please visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

To enable the Council to measure the accuracy of this LIM document based on our current records, we would appreciate your response should you find any information contained therein which may be considered to be incorrect or omitted. Please telephone the Customer Call Centre on (03) 941 8999.

A search of records held by the Council has revealed the following information:

## 1. Special features and characteristics of the land

*Section 44A(2)(a) LGOIMA. This is information known to the Council but not apparent from the district scheme under the Town and Country Planning Act 1977 or a district plan under the Resource Management Act 1991. It identifies each (if any) special feature or characteristic of the land concerned, including but not limited to potential erosion, avulsion, falling debris, subsidence, slippage, alluvion, or inundation, or likely presence of hazardous contaminants.*

( For enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### ┆ Consultant Report Available

The Tonkin & Taylor Darfield Earthquake 4 September 2010 Geotechnical Land Damage Assessment & Reinstatement Stage 1 Report indicates areas of observed surface manifestations of liquefaction resulting from the earthquake. This property is within one of the identified areas. The report can be viewed at [www.eqc.govt.nz/canterbury-quake/stage-one/stage1.aspx](http://www.eqc.govt.nz/canterbury-quake/stage-one/stage1.aspx)

### ┆ Consultant Report Available

Land Information New Zealand (LINZ) engaged Tonkin and Taylor to provide a Geotechnical Report on Ground Movements that occurred as a result of the Canterbury Earthquake Sequence. The report indicates this property may have been effected by a degree of earthquake induced subsidence. The report obtained by LINZ can be accessed on their website at <https://www.linz.govt.nz/land/surveying/earthquakes/canterbury-earthquakes/information-for-canterbury-surveyors>

### ┆ Liquefaction Vulnerability

Christchurch City Council holds indicative information on liquefaction hazard for Christchurch. Information on liquefaction, including an interactive web tool, can be found on the Council website at [ccc.govt.nz/liquefaction](http://ccc.govt.nz/liquefaction). Depending on the liquefaction potential of the area that the property is in, the Council may require site-specific investigations before granting future subdivision or building consent for the property.

### ┆ Property Affected by a Spring

Council records show a spring on the property.

## Related information

- ┆ There is attached a sub division soil investigation report covering this property.
- ┆ There are attached hazard/special site characteristics supplementary sheet/s.

## 2. Private and public stormwater and sewerage drains

Section 44A(2)(b) LGOIMA. This is information about private and public stormwater and sewerage drains as shown in the Council's records.

( For stormwater and sewerage enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### 1 Property within Local Pressurised Sewer System Zone

This property is in a local pressure sewer system catchment within the Christchurch wastewater network. If there is a house on the property, there will already be a wastewater pressure pump and tank. If a house is yet to be built, a new wastewater pressure pump and tank will need to be installed. General information about pressure sewer systems can be found on the Council website. More detailed information can be obtained by contacting Council Customer Services on 03 941 8999.

### Related information

- 1 The property is shown to be served by an on-site septic tank disposal system.
- 1 No details of the private stormwater system serving this property are shown on the plan or on Council records.
- 1 This property has been identified as being in a pressurised wastewater system zone and attached is a copy of the systems user guide. For more information you can refer to <https://ccc.govt.nz/services/water-and-drainage/wastewater/about-wastewater/types-of-wastewater-systems> or contact Christchurch City Councils 3 waters unit on (03) 941-8999.

### 3. Drinking Water Supply

*Section 44A(2)(ba) and (bb) LGOIMA. This is information notified to the Council about whether the land is supplied with drinking water, whether the supplier is the owner of the land or a networked supplier, any conditions that are applicable, and any information the Council has about the supply.*

Please note the council does not guarantee a particular water quality to its customers. If you require information on current water quality at this property please contact the Three Waters & Waste Unit.

( For water supply queries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

#### Water Supply

Christchurch City Council is the networked supplier of water to this property. This property is connected to the Christchurch City Council Water Supply. The conditions of supply are set out in the Christchurch City Council Water Supply, Wastewater & Stormwater Bylaw (2014), refer to [www.ccc.govt.nz](http://www.ccc.govt.nz).

## 4. Rates

Section 44A(2)(c) LGOIMA. This is information on any rates owing in relation to the land.

( For rates enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (a) Annual rates

Annual rates to 30/06/2021: \$ 33,271.48

	Instalment Amount	Date Due
Instalment 1	\$ 8,317.78	31/08/2020
Instalment 2	\$ 8,317.78	30/11/2020
Instalment 3	\$ 8,317.78	28/02/2021
Instalment 4	\$ 8,318.14	31/05/2021

Rates owing as at 18/06/2021: \$ 0.00

### (b) Excess water charges

\$ 0.00

( For water charge enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (c) Final water meter reading required?

Reading is Required

( To arrange a final water meter reading, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

## 5. Consents, certificates, notices, orders, or requisitions affecting the land and buildings

*Section 44A(2)(d) LGOIMA. This is information concerning any consent, certificate, notice, order, or requisition, affecting the land or any building on the land, previously issued by the Council. The information in this section may also cover building consent and/or code compliance information issued by building certifiers under the Building Act 1991 and building consent authorities that are not the Council under the Building Act 2004.*

You can check the property file to identify whether any consent or certificate was issued by a building certifier under the Building Act 1991.

*Section 44A(2)(da) LGOIMA. The information required to be provided to a territorial authority under section 362T(2) of the Building Act 2004. There is currently no information required to be provided by a building contractor to a territorial authority under section 362T(2) of the Building Act 2004. The Building (Residential Consumer Rights and Remedies) Regulations 2014 only prescribed the information that must be given to the clients of a building contractor.*

( For building enquiries, please phone (03) 941 8999, email [EPADutyBCO@ccc.govt.nz](mailto:EPADutyBCO@ccc.govt.nz) or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (a) Consents

- | BCN/1956/4315 Applied: 12/11/1956 Status: Completed  
511 Halswell Road Halswell  
Permit issued 13/11/1956  
SEPTIC TANK & ASSOCIATED DRAINAGE- Historical Reference PER56560372
- | BCN/1982/2860 Applied: 26/04/1982 Status: Completed  
511 Halswell Road Halswell  
Permit granted 27/04/1982  
Permit issued 27/04/1982  
KENT LOG FIRE - WETBACK- Historical Reference PER82127340
- | BCN/1989/4560 Applied: 26/06/1989 Status: Completed  
511 Halswell Road Halswell  
Permit granted 04/07/1989  
Permit issued 04/07/1989  
IMPLEMENT & STORAGE SHED- Historical Reference PER89136326
- | BCN/2010/4221 Applied: 11/05/2010 Status: Completed  
511 Halswell Road Halswell  
Accepted for processing 11/05/2010  
Building consent granted 28/05/2010  
Building consent issued 28/05/2010  
PIM Granted 28/05/2010  
PIM Issued 28/05/2010  
Code Compliance Certificate Granted 19/07/2010  
Code Compliance Certificate Issued 19/07/2010  
FIRENZO FORTE AQUALUX AG INBUILT WETBACK WOODBURNER CLEAN AIR CERTIFICATION: 102107-  
Historical Reference ABA10102903

### (b) Certificates

*Note: Code Compliance Certificates were only issued by the Christchurch City Council since January 1993.*

### (c) Notices

### (d) Orders

### (e) Requisitions

Property address:  
511 Halswell Road

LIM number: 70247280  
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Christchurch City Council  
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Christchurch 8154, New Zealand  
Tel 64 3 941 8999  
Fax 64 3 941 8984  
[www.ccc.govt.nz](http://www.ccc.govt.nz)



## Related information

- 1 Council holds no record of building permit/consent for dwelling at this address. No information is held by Council relating to the materials, construction or year the dwelling was built.

## 6. Certificates issued by a building certifier

Section 44A(2)(e) LGOIMA. This is information notified to the Council concerning any certificate issued by a building certifier pursuant to the Building Act 1991 or the Building Act 2004.

( For building enquiries, please phone (03) 941 8999, email [EPADutyBCO@ccc.govt.nz](mailto:EPADutyBCO@ccc.govt.nz) or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

Property address:  
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LIM number: 70247280  
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## 7. Weathertightness

*Section 44A(2)(ea) LGOIMA. This is information notified to the Council under section 124 of the Weathertight Homes Resolution Services Act 2006.*

( For weathertight homes enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

*If there is no information below this means Council is unaware of any formal Weathertight Homes Resolution Services claim lodged against this property.*

## 8. Land use and conditions

Section 44A(2)(f) LGOIMA. This is information relating to the use to which the land may be put and conditions attached to that use. The planning information provided below is not exhaustive and reference to the Christchurch District Plan and any notified proposed changes to that plan is recommended: <https://ccc.govt.nz/the-council/plans-strategies-policies-and-bylaws/plans/christchurch-district-plan/>.

There maybe some provisions of the Christchurch City Plan or Banks Peninsula District Plan that affect this property that are still operative.

( For planning queries, please phone (03) 941 8999, email [DutyPlanner@ccc.govt.nz](mailto:DutyPlanner@ccc.govt.nz) or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### Regional plan or bylaw

There may be objectives, policies or rules in a regional plan or a regional bylaw that regulate land use and activities on this site. Please direct enquiries to Canterbury Regional Council (Environment Canterbury).

### Waterway Provisions for Other Councils

A resource consent or permit may also be required from the Canterbury Regional Council or other territorial authority, particularly with respect to water bodies managed by those authorities. Please refer to the relevant regional plan and any relevant bylaws, and contact the Christchurch City Council if you are uncertain which authority manages the water body in question.

## (a) (i) Christchurch City Plan & Banks Peninsula District Plan

### (ii) Christchurch District Plan

#### High Flood Hazard Management Area

This property or parts of, are within the High Flood Hazard Management Area (HFHMA) in the Christchurch District Plan. A resource consent is likely to be required for new buildings or to subdivide this property. Further information can be found at [www.ccc.govt.nz/hfhma](http://www.ccc.govt.nz/hfhma).

#### Liquefaction Management Area (LMA)

Property or part of property within the Liquefaction Management Area (LMA) Overlay which is operative.

#### Outline Development Plan

Property or part of property is within an Outline Development Plan area which is affected by specific provisions that are operative.

#### Remainder Slope Instability Management Area

Property or part of property within the Christchurch District Plan Remainder of Port Hills and Banks Peninsula Slope Instability Management Area overlay.

#### Waterway Provisions

This property or part of this property is close to at least one waterway. It may be within the setback for an Environmental Asset Waterway. Within that setback, District Plan rules apply to activities including buildings, earthworks, fences and impervious surfacing. Any part of the property within the setback will be affected by those rules.

## Waterway Provisions

This property or part of this property is close to at least one waterway. It may be within the setback for a Downstream Waterway. Within that setback, District Plan rules apply to activities including buildings, earthworks, fences and impervious surfacing. Any part of the property within the setback will be affected by those rules.

## Flood Management Area

Property or part of property within the Flood Management Area (FMA) Overlay which is operative.

## District Plan Zone

Property or part of property within the Residential New Neighbourhood Zone which is operative.

## District Plan Zone

Property or part of property within the Rural Urban Fringe Zone which is operative.

## (b) Resource consents

If there are any land use resource consents issued for this property the Council recommends that you check those resource consents on the property file. There may be conditions attached to those resource consents for the property that are still required to be complied with.

- | RMA/2020/163 - Land Use Consent  
511 Halswell Road Halswell  
Earthworks for residential development  
Status: Processing complete  
Applied 28/01/2020  
Granted 10/02/2020  
Decision issued 10/02/2020
  
- | RMA/2020/2770 - Land Use Consent  
511 Halswell Road Halswell  
To conduct earthworks and stockpiling on site  
Status: Processing complete  
Applied 27/11/2020  
Granted 27/01/2021  
Decision issued 27/01/2021
  
- | RMA/2020/3076 - Combined subdivision / land use consent  
511 Halswell Road Halswell  
To subdivide 4 allotments to create 87 residential allotments. Land use consent for earthworks and under the NES for contaminated land.  
Status: On hold - waiting for response from applicant  
Applied 22/12/2020

- | RMA/2021/733 - Land Use Consent  
511 Halswell Road Halswell  
Earthworks - Associated with the formation of vehicle crossings  
Status: Processing complete  
Applied 24/03/2021  
Granted 11/06/2021  
Decision issued 11/06/2021

## Related information

- | Council records show that there are current/on hold monitoring job in our system. This monitoring is to ensure that the resource consent conditions have been met. For further information you can contact the Compliance & Investigation team A on 941 8999 or email: [rcmon@ccc.govt.nz](mailto:rcmon@ccc.govt.nz) and reference to resource consent RMA/2021/733 & RMA/2020/2770.

## 9. Other land and building classifications

*Section 44A(2)(g) LGOIMA. This is information notified to the Council by any statutory organisation having the power to classify land or buildings for any purpose.*

( For land and building enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

Please refer to Section 1 for details

## 10. Network utility information

*Section 44A(2)(h) LGOIMA. This is information notified to the Council by any network utility operator pursuant to the Building Act 1991 or the Building Act 2004.*

( For network enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

! **None recorded for this property**



## 11. Other information

Section 44A(3) LGOIMA. This is information concerning the land that the Council has the discretion to include if it considers it to be relevant.

( For any enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (a) Kerbside waste collection

- | Your recycling is collected Fortnightly on the Week 2 collection cycle on a Tuesday. Please leave your recycling at the Kerbside by 6:00 a.m. Your nearest recycling depot is the Parkhouse Road EcoDrop.
- | Your refuse is collected Fortnightly on the Week 2 collection cycle on a Tuesday. Please leave your rubbish at the Kerbside by 6:00 a.m. Your nearest rubbish depot is the Parkhouse Road EcoDrop.
- | Your organics are collected Weekly on Tuesday. Please leave your organics at the Kerbside by 6:00 a.m.

### (b) Other

#### | Floor Levels Information

Christchurch City Council holds a variety of information relevant to building/property development across the city. This includes minimum finished floor levels that need to be set to meet the surface water requirements in clause E1.3.2 of the building code (where this applies), and the requirements of the Christchurch District Plan (where a property is in the Flood Management Area). Where this information has been processed for your site, it can be viewed at <https://ccc.govt.nz/floorlevelmap/>, otherwise site specific advice can be obtained by emailing [floorlevels@ccc.govt.nz](mailto:floorlevels@ccc.govt.nz).

#### | Community Board

Property located in Halswell-Hornby-Riccarton Community Board.

#### | Guest Accommodation

Guest accommodation (including whole unit listings on Airbnb; BookaBach; etc.) generally requires a resource consent in this zone when the owner is not residing on the site. For more information, please refer to: <https://ccc.govt.nz/providing-guest-accommodation/>.

#### | Tsunami Evacuation Zone

This property is not in a tsunami evacuation zone. It is not necessary to evacuate in a long or strong earthquake or during an official Civil Defence tsunami warning. Residents may wish to offer to open their home to family or friends who need to evacuate from a tsunami zone, and should plan with potential guests to do so in advance. More information can be found at <https://ccc.govt.nz/services/civil-defence/hazards/tsunami-evacuation-zones-and-routes/>

#### | Electoral Ward

Property located in Halswell Electoral Ward

#### | Listed Land Use Register

Property address:  
511 Halswell Road

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Christchurch City Council  
53 Hereford Street, PO Box 73015  
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Hazardous activities and industries involve the use, storage or disposal of hazardous substances. These substances can sometimes contaminate the soil. Environment Canterbury identifies land that is used or has been used for hazardous activities and industries. This information is held on a publically available database called the Listed Land Use Register (LLUR). The Christchurch City Council may not hold information that is held on the LLUR. Therefore, it is recommended that you check Environment Canterbury's online database at [www.llur.ecan.govt.nz](http://www.llur.ecan.govt.nz)

## I **Spatial Query Report**

A copy of the spatial query report is attached at the end of this LIM. The spatial query report lists land use resource consents that have been granted within 100 metres of this property.

# Geotechnical Investigation and Assessment Report for Subdivision

Riverstone Subdivision, 2 & 4 Glovers Road, Halswell, Christchurch

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Issue Date: **20 October 2020**

Document Ref: **200357-RP-001[A]**



Prepared for: **Yoursection Ltd**



**Report Tracking - 2 & 4 Glovers Road, Halswell, Christchurch**

Revision	Status	Date	Prepared by	Reviewed by
A	Final	20 October 2020	C. Gibbens	A. Giannakogiorgos

**Authorisation**

<b>Author's Signature</b>		<b>Approver's Signature</b>	
<b>Name</b>	Clem Gibbens	<b>Name</b>	Andreas Giannakogiorgos
<b>Title</b>	Engineering Geologist BSc MSc (Hons) MEngNZ	<b>Title</b>	Chartered Professional Engineer (Geotechnical) BSc MSc DIC CMEngNZ CPEng IntPE (NZ)

**Miyamoto International New Zealand Ltd**  
Level 1, 236 Hereford Street | Christchurch 8011

[www.miyamoto.nz](http://www.miyamoto.nz)

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## Executive Summary

Miyamoto International NZ Ltd (MINZ) has been engaged by Yoursection Ltd to undertake a geotechnical land suitability assessment for the proposed residential subdivision at 2 & 4 Glovers Road, Halswell, Christchurch. The key findings of our evaluation and assessment are outlined below.

<b>GROUND CONDITIONS</b>	<b>Ground profile</b>	The sub-surface conditions comprise mainly topsoil over sand-silt mixtures underlain by soft clayey silts and shallow gravel. The ground conditions are variable in horizontal and vertical spread.	
	<b>Soil classification as per NZS 1170.5:2004</b>	Residential Subdivision Area: Class 'D' (deep or soft soil site)	
	<b>Depth to water table</b>	Perched water tables and shallow saturated soils were encountered within the top 1.0 to 2.0m bgl. Permanent ground water is anticipated below the soft silts within the underlying sands and gravels.	
<b>SEISMIC ASSESSMENT</b>	<b>Design Earthquake Event</b>	<b>SLS/SLS2</b>	<b>ULS</b>
	<b>Estimated "free-field" Index post-liquefaction volumetric settlements</b>	< 50mm	< 80mm
	<b>Liquefaction Severity Number (LSN) Value</b>	< 15 Little to minor expression of liquefaction	< 25 Little to moderate expression of liquefaction
	<b>MBIE Technical Categorization (TC)</b>	<b>Mapped MBIE</b>	Rural & Unmapped
<b>Site Specific Foundation TC</b>		TC2	
<b>GEOTECHNICAL CONSIDERATIONS</b>	<p>Our assessment of the site under RMA Section 106 found that the subsidence hazard is present on-site due to presence of soft/loose soil layers and liquefiable deposits, though these hazards can be mitigated by the options listed in this report.</p> <p>As the site is located within an FMA set out by CCC, a portion of the site will require filling to raise the ground level to a suitable level for the proposed development by around 1.0m close to Green's Stream. Filling of the site will likely cause static some consolidation settlements in the soft compressible soils underlying the site, though this is not expected to be a significant risk to the development, based on the pre-loading trial undertaken by MINZ previously. A period of monitoring of the site filling works during the raising of the site levels and for a period (~6 months) is advised to be safeguard against the anticipated static settlements.</p>		

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10. References .....	15

### Appendices

- A. Updated Indicative Subdivision Plan (Davie Lovell Smith)
- B. ECan Listed Land Use Register Files
- C. Geotechnical Investigation Results
- D. Southern Geophysical MASW and GPR Report
- E. Geotechnical Cross Sections
- F. Liquefaction Analyses

## 1. Introduction

Miyamoto International NZ Ltd (Miyamoto) has been engaged by Yoursection Ltd to undertake a geotechnical evaluation and assessment as part of a land suitability assessment for the proposed new extension of the residential Riverstone Subdivision at 2 & 4 Glovers Road, Halswell, Christchurch.

Miyamoto have previously completed a geotechnical assessment for resource consenting purposes for the initial stage of the Riverstone Subdivision located at 511 Halswell Road, Christchurch (190666-RP-001[A] – 511 Halswell Road, dated 10 October 2019), as well as undertaking a trial pre-load assessment for the same property (190666-TM-001[A]\_511 Halswell Road\_Pre-load Trial, dated 28 January 2020). Both documents are referenced as part of this assessment, with this report supplementing and expanding on the work already undertaken.

The scope of this geotechnical engineering assessment was to evaluate the geotechnical conditions at the site and to provide preliminary recommendations for development of the sections. This assessment comprised the following:

- Research of the available information from the New Zealand Geotechnical Database (NZGD), Christchurch City Council (CCC) and Environment Canterbury (ECan);
- Site walkover inspection of the land;
- Shallow field investigation comprising hand-augered boreholes (HA) with associated dynamic cone penetrometer (DCP) and shear vane (SV) tests;
- Deep field investigation comprising Cone Penetration Tests (CPT) with accompanying Dynamic Probe Super Heavy (DPSH) testing;
- Multichannel Analysis of Surface Waves (MASW) geophysical survey;
- Ground Penetrating Radar (GPR) geophysical survey;
- Liquefaction analyses using CPT-based liquefaction triggering procedures;
- Reporting of the findings.

The geotechnical investigation and assessment were carried out considering the Ministry of Business, Innovation & Employment (MBIE) Guidance documents “Planning and engineering guidance for potentially liquefaction-prone land” - Version 1, dated September 2017, “Repairing and rebuilding houses affected by the Canterbury earthquakes” - Version 3, dated December 2012, and “Earthquake geotechnical engineering practice - Modules 2 & 3”. This report presents our findings and conclusions which are provided to facilitate the development of the extended subdivision plan for the site.

## 2. Site Description

The site, legally described as Lot 1 (2 Glovers) and Lot 2 (4 Glovers) DP 83635, is in Halswell, Christchurch and is approximately 8.3 hectares (ha) in total area. There is an approximate elevation change of 2.0m over 460m at an average gradient of 0.4%. The site generally slopes from north to south, with the low point at the southern boundary of both sections. The property is bound by Glovers Road along the northern boundaries and is bound by rural

properties on the south and east boundaries, and the 511 Halswell Road section to the west. Green's Stream runs through the southern end of both sections.

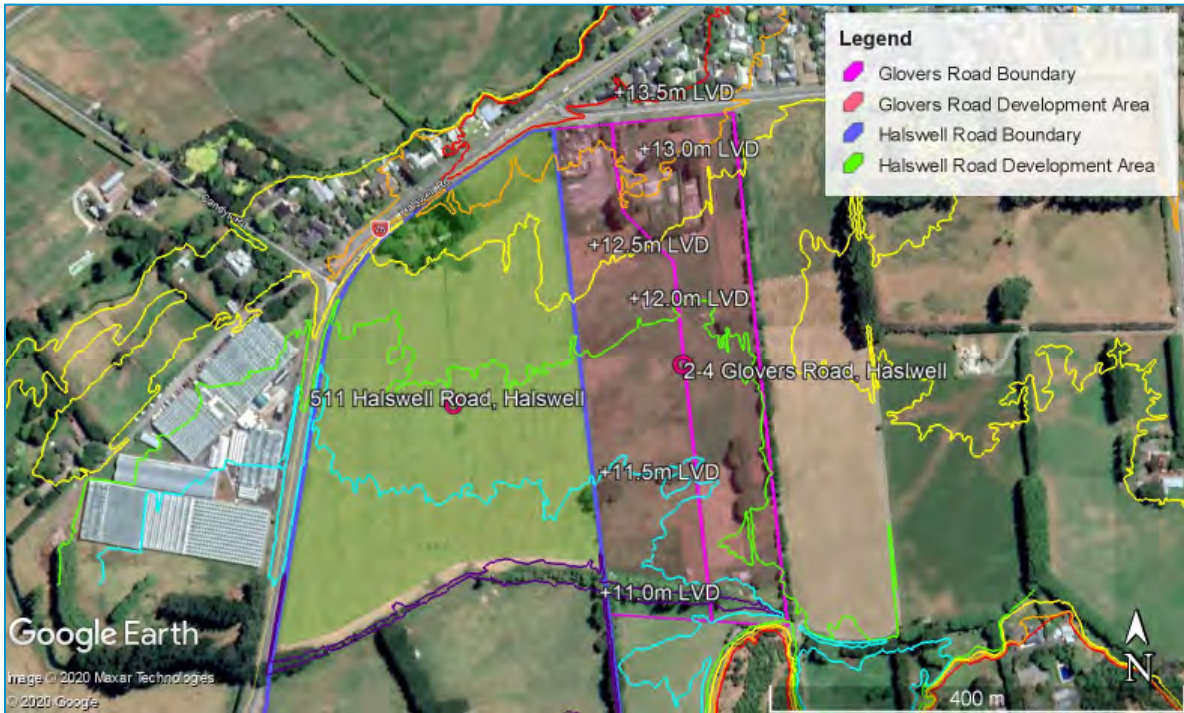


Figure 1: Proposed Site Layout with (Scale as Shown)

The property is located within the “Rural and Unmapped” category listed under the MBIE Technical Categories Map. The site location with reference to the MBIE Technical Categories is shown in Figure 2.

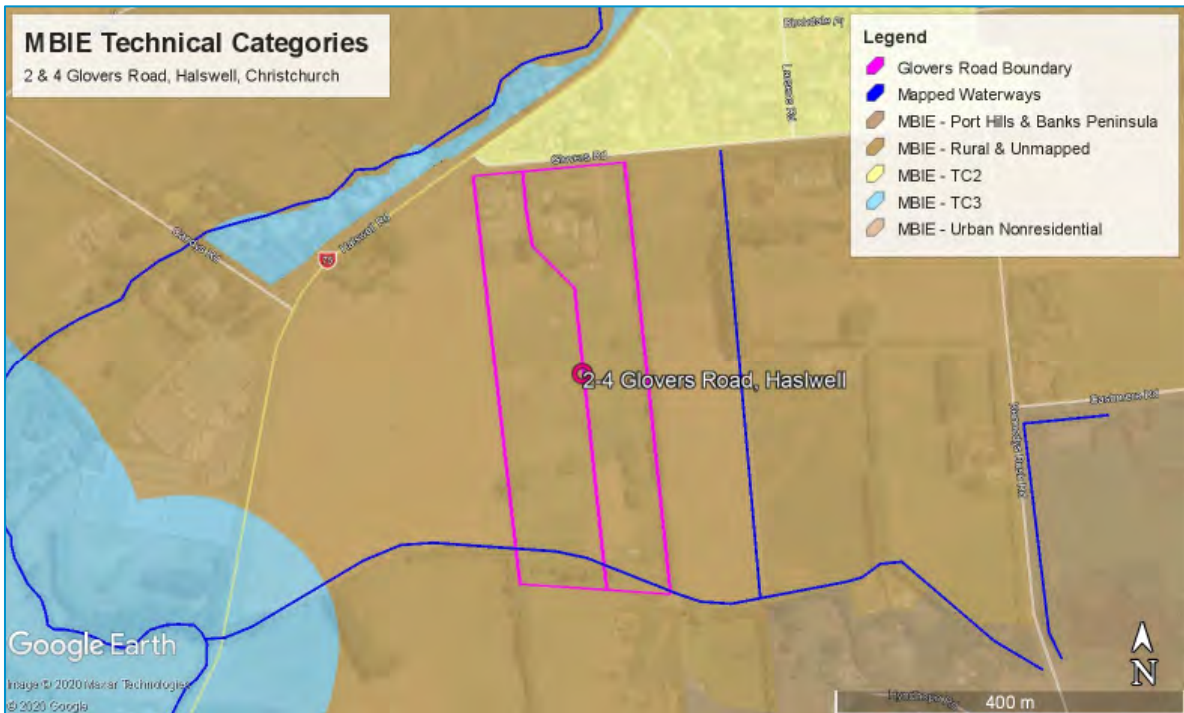


Figure 2: Site Location Plan Showing MBIE Technical Categories and Mapped Waterways (Scale as Shown)



The Riverstone Subdivision is proposed to, currently, be comprised of 239 residential lots with reserves located throughout. A draft plan of the subdivision, including the Glovers Road properties, is presented in Appendix A.

### 3. Desk Study

The following sources of third-party information were considered and are referenced in this report:

- New Zealand Geotechnical Database (NZGD);
- Environment Canterbury (ECan);
- Christchurch City Council (CCC).

#### New Zealand Geotechnical Database

The NZGD website was reviewed to identify any additional information related to the extent of land damage after the CES on the site and in the immediate surrounding areas. The results of this review indicate that no significant land damage was observed across the site. Table 1 provides a summary of the information obtained from our review of the NZGD.

Table 1: Desk Study Information Summary (NZGD)

	September 2010 (M <sub>w</sub> 7.1)	February 2011 (M <sub>w</sub> 6.2)	June 2011 (M <sub>w</sub> 6.0)	December 2011 (M <sub>w</sub> 5.9)
<i>Aerial Photography Review</i>	Outside of photographed area	Areas of likely ejecta identified in the central and northern areas of both properties, though mainly confined to 2 Glovers Road	Outside of photographed area	Outside of photographed area
<i>Land damage observations</i>	Minor ground cracking but no observed ejected liquefied material was recorded on the properties on the opposite side of Glovers Road in the September 2010 CES event and along Halswell Road and sections of Glovers Road during the June 2011 CES event.			
<i>Observed ground cracking</i>	No cracks mapped on the properties, 10mm – 200mm ground cracks mapped ~65m west of the northernmost boundary of the site within the residential area on the opposite side of Halswell Road			
<i>PGA (g) ± SD</i>	0.294 ± 0.390	0.356 ± 0.435	0.145 ± 0.465	0.139 ± 0.250
<i>Scaled PGA<sub>7.5</sub> PGA<sub>16%ile</sub> to PGA<sub>84%ile</sub><sup>(1)</sup> (g)</i>	0.179 to 0.394	0.164 to 0.391	0.061 to 0.156	0.071 to 0.117

(1) Scaled to M7.5 using Idriss and Boulanger recommendations (2008); 68% confidence PGA<sub>7.5</sub> range

## Contaminated Land Considerations

The ECan Listed Land Use Register (LLUR) was reviewed and holds records of potentially Hazardous Activities and Industrial List (HAIL) sites. At this time, a small area that intersects the southern end of both sections is listed as a potential HAIL site. The LLUR lists this small area (in the vicinity of a storage shed) as an A10-classified area, which relates to “persistent pesticide bulk storage or use including sports turfs, market gardens, orchards, glass houses or spray sheds”, though this has not been investigated by ECan. The property reports for both sections are included in Appendix B.

An environmental assessment is outside the scope of this assessment and has been undertaken by others.

## Flood Hazard

Christchurch is a low-lying city and there have always been areas that are prone to flooding during heavy rainfall. The CES has worsened flood risk in many areas of the city through damage to waterways and land. Flood Management Areas (FMAs) have been identified by CCC in the District Plan and take into consideration the impacts of the CES.

At the time of writing this report the site is located within a FMA as indicated by the CCC District Plan.

It is understood that a Finished Floor Level (FFL) of 21.25m above Christchurch Drainage Datum (CDD) is a requirement for development of the site.

## Ground Motion

Using the MBIE and Bradley & Hughes (2012) procedures, we have found that the site was “sufficiently tested” to the Serviceability Limit State (SLS) level of earthquake demand during the September 2010 and February 2011 events of the CES. This indicates that land and building damage in a future SLS event is likely to be similar to these individual events.

Additionally, based on the SLS2 level of shaking ( $M_w$  6.0 and PGA of 0.19g) which was introduced by MBIE following the updated liquefaction triggering CPT-based procedure by Boulanger & Idriss (2014), it is our opinion the site was “sufficiently tested” to the SLS2 level of earthquake demand during the September 2010 and February 2011 events of the CES.

Utilising a derivation of the Bradley and Hughes method, we can suggest that the site was not tested to Ultimate Limit State (ULS) level of shaking during the CES. Based on the probabilistic analysis of the PGAs experienced at the site, the nature of land and building damage is likely to be more severe during a future ULS event than that already experienced during the individual CES events.

## 4. Subsurface Conditions

### Geological Setting

The geological map of the area (GNS 1:250,000 QMap) indicates that most of the site has surface geology consisting of “modern (Quaternary) river floodplain and low-level degradation terraces (<2° slopes) comprised of unweathered, variably sorted gravel/sand/silt/clay”.

## Field Investigations

The NZGD website was reviewed to identify relevant geotechnical investigations completed within the site vicinity, additional to the data identified for use in the original site assessment for the neighbouring section, though nothing for inclusion was identified.

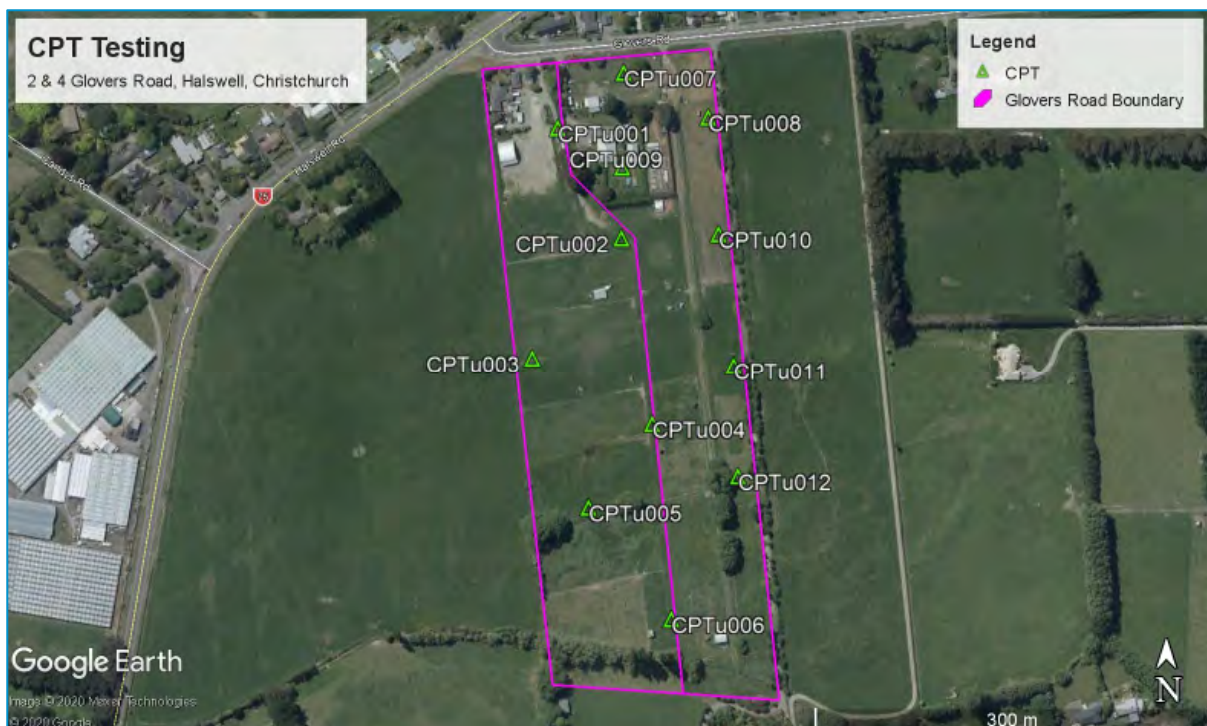
Miyamoto undertook the following site-specific ground investigations and testing:

- Five (5) hand-augered boreholes (referenced HA1 to HA5) with in-situ shear vane testing;
- Five (5) Dynamic Cone Penetrometer (DCP) tests (referenced DCP1 to DCP5);
- Laboratory testing including fines content (FC) and Atterberg Limits;
- Twelve (12) Cone Penetration Tests (CPTu) with porewater pressure measurements;
- Multichannel Analysis of Surface Waves (MASW) geophysical survey;
- Ground Penetrating Radar (GPR) geophysical survey.

The general details of the ground investigations are summarised in Table 2, the test locations are shown in Figure 3 and Figure 4, and the HA/DCP logs and CPT plots are presented in Appendix C and the geophysical survey report is presented in Appendix D.

**Table 2: Summary of Ground Investigations**

Test Ref.	Source	Source Ref.	Test Type	Depth (m bgl)
HA1/DCP1 to HA5/DCP5	MINZ	200357	Hand Auger/ DCP	1.8 to 3.9
CPTu001 to CPTu012	LandTest	19096	CPT	10.0 to 15.0
MASW 1 to MASW 3	Southern Geophysical Ltd	2050	MASW	Up to 40.0
GPR 1 to GPR 11			GPR	Up to 4.0



**Figure 3: CPT Investigation Location Plan (Scale as Shown)**

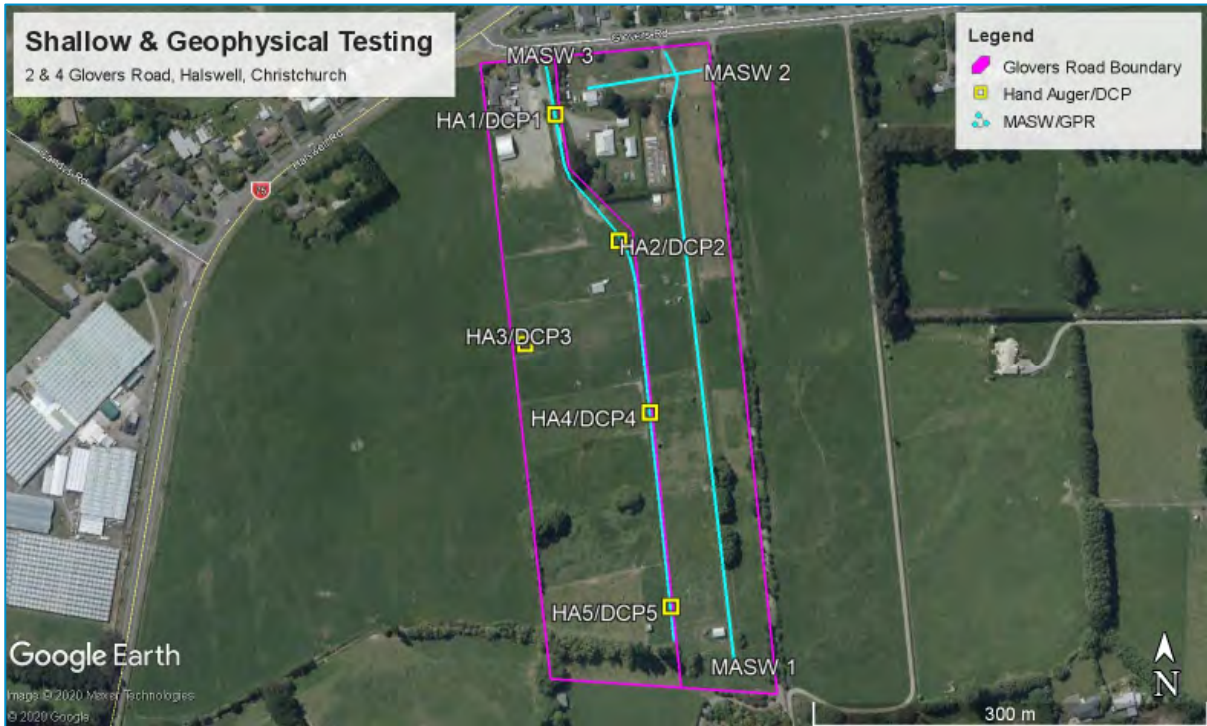


Figure 4: Other Geotechnical Investigation Location Plan (Scale as Shown)

### Laboratory Test Results

Laboratory testing was undertaken on samples obtained from our shallow ground investigation to assess the soil characteristics across the site. The testing undertaken includes wet sieving to determine the fines content, and Atterberg limits tests to determine the plastic and liquid limits. A summary of the test results is presented in Table 3, with the full results presented in Appendix C.

Table 3: Laboratory Test Results

Sample Ref.	Depth of sample (m)	Soil Description	Plasticity Index	% Passing		
				0.3 mm	0.15 mm	0.063 mm
C20-319	HA1 1.5m – 2.3m	Silty SAND, brownish grey, wet, non-plastic	-	100	90	49
C20-320	HA1 2.3m – 3.8m	Silty SAND, brownish grey, saturated, non-plastic	-	100	91	49
C20-321	HA2 2.7m – 4.0m	Silty CLAY, some sand, dark grey, saturated, low plasticity	9	99	96	85
C20-312	HA3 2.0m – 3.4m	Sandy SILT, dark grey, saturated, non-plastic	NP	100	99	59
C20-323	HA5 1.5m – 1.8m	Silty SAND, brownish grey, wet, non-plastic	-	99	77	42

## Ground Conditions

The ground conditions interpreted from the existing data and investigations undertaken as part of this assessment are presented graphically in the geotechnical cross sections included in Appendix E and the basic soil descriptions are outlined in Table 4.

A near-surface paleo-feature (old river terrace or paleochannel) was identified during the site testing with the CPT's completed at the southern end of the site (CPTu004 to CPTu006 and CPTu012) refusing in dense soils within the upper 5m, before testing was continued with the DPSH. The shallow investigation (HA5/DCP5) also refused at a shallow depth due to dense soils. The testing at the northern end of the site all reached the target depths and were consistent in their findings.

Table 4: Ground Conditions Summary

Layer	Soil Name
a	Silty SAND and Sandy SILT, loose to firm
b	Clayey SILT, soft to firm, medium plasticity
c	Silty SAND, medium dense to dense with increasing depth
GS	Gravelly SAND to Sandy GRAVEL, dense
d	Clayey SILT to silty CLAY, firm
e	Medium dense SAND with silt and gravels
f	Clayey SILT, firm to stiff
S	Silty SAND to Sandy SILT, medium dense to very stiff

## MASW & GPR Geophysical Survey

The shear wave velocity ( $V_s$ ) measurement was assessed with a MASW survey. The results of the survey were used to refine the boundaries and extents between the shallow, softer soils and denser sandy/gravelly layers with the MASW survey reflecting the findings of the intrusive investigations, with 2 clearly defined areas for the north and south of the site. The soils in the northern part of the site had a generally lower shear wave velocity ( $V_s < 180\text{m/s}$ ) to approximately 20.0m depth, though discrete layers of denser, higher  $V_s$  soils were identified above this depth before becoming lower velocity again. For the southern part of the site, the lower  $V_s$  soils are generally terminated shallower (<5m depth) before the  $V_s$  increased in the gravelly dense material.

Additionally, the measured cone tip resistance ( $q_c$ ) and interpreted shear wave velocity from the CPT data generally shows a consistent pattern with the recorded values from the MASW survey as seen in the CPT profiles in Appendix C. It should be noted that due to the high velocity layers towards the south, thin lower velocity layers were not picked up as seen in the DPSH data. This is reflected in the cross sections presented in Appendix E.

The GPR survey was undertaken to further supplement the MASW surveys for the near-surface soils. The primary objective of this survey was to assist in identifying softer or denser layers that may not have been picked up in the MASW survey. The results generally show a consistent correlation with the MASW survey. The softer soils generally had a poor reflection, with denser material showing a clearer reflection. The shallow gravelly soils at the southern end of the site were also clear within the upper 4.0m of the soil profile.

## Groundwater

Our site-specific shallow investigation encountered groundwater levels between 1.0m and 1.8m bgl, however the cohesive soils below the recorded depth were noted to not be saturated, indicating that a perched water table is likely present on-site. The CPT data shows variable piezometric conditions indicating a groundwater table depth between 0.7m and 2.4m bgl, due to the differing depth of cohesive soils in the upper soil profile and different elevations. The shallower groundwater depths were generally confined to the lower elevations of the property.

Based on the above, a groundwater depth range of between 0.7m to 2.4m bgl was adopted for the liquefaction triggering and free-field settlement assessment, depending on the location of the test across the site.

## Site Subsoil Class

Based on the site-specific investigation, geological maps and other available information, the site is classified as a Class D (deep or soft soil) site.

## Shallow Soils

The geotechnical investigations indicate the existence of low velocity ( $V_s \leq 180\text{m/s}$ ), soils between approximately 4.0m and 20.0m depth, with the lower  $V_s$  soils encountered at greater depths towards the north of the sections. There are also locations where denser pockets of material were identified within these lower  $V_s$  layers. Those layers have lower strength and have the potential for long-term consolidation settlements from loads, such as residential dwellings. This is further discussed later in this report.

# 5. Liquefaction Assessment

## Methodology

An assessment of the earthquake-induced free-field post-liquefaction volumetric settlement at the site has been carried out in accordance with the MBIE Guidance and using proprietary liquefaction assessment software, for SLS and ULS earthquake scenarios.

The seismic design requirements adopted for use in the analyses are defined in MBIE/NZGS Earthquake Geotechnical Engineering Practice Module 3 (May 2016), and Part C of the MBIE Guidelines “Repairing and rebuilding houses affected by the Canterbury earthquakes” and its subsequent updates - clarifications. These are:

- Buildings of normal use (Importance Level 2);
- Deep or soft soil sites (Class D) as specified previously;

- Boulanger and Idriss (2014) methodology for liquefaction triggering, as per the MBIE Guidance subsequent updates (Issue 7, October 2014);
- Zhang et al. (2002) post-liquefaction volumetric strain calculation for estimating the free-field settlements;

Calculations were performed for the full depth of the CPTs and the upper 10m of the soil profile (as per the MBIE Guidance “index value” estimations). It should be noted that the settlement estimates only account for the free-field component of the expected settlement. Actual total settlements under SLS or ULS earthquake loading may be greater or less.

The Liquefaction Severity Number (LSN<sup>1</sup>) has been calculated and used in our assessment as it tends to better reflect the more damaging effects of shallow liquefaction, which is more critical for shallow founded structures. The level of ground damage associated with LSN is summarised in Table 5.

**Table 5: Liquefaction Severity Number Ranges and Related Effects**

LSN Value	Observed Performance
<10	Little to no expression of liquefaction, minor effects
10 – 20	Minor expression of liquefaction, some sand boils
20 – 30	Moderate expression of liquefaction, with sand boils and some structural damage
30 – 40	Moderate to severe expression of liquefaction, settlement can cause structural damage
40 – 50	Major expression of liquefaction, undulations and damage to ground surface, sever total and differential settlement of structures
>50	Severe damage, extensive evidence of liquefaction at surface, sever total and differential settlements affecting structures, damage to services

### Liquefaction Assessment Results

Due to the rapid changes at the interface between fine and coarse-grained soils, a layer correction was applied. The cone tip penetration, and subsequently, the ability to resist liquefaction of a sandy material, is reduced by the surrounding silty layers, while the  $I_c^2$  of the silt layers is reduced due to the presence of the surrounding sandy layers and hence the susceptibility of the fine layers is overestimated. For our analysis, an  $I_c$  change of >0.05 per 10mm has been adopted, which eliminates the liquefaction potential for the layer.

The results of our liquefaction triggering analyses utilising the CPT data are presented in Appendix F and summarised in Table 6.

<sup>1</sup> **LSN = Liquefaction Severity Number.** LSN (van Ballegooy et al., 2014) is a vulnerability indicator (damage index) quantifying liquefaction-induced damage developed to reflect more damaging effects of shallow liquefaction on residential land and foundations following the Canterbury Earthquakes (2010-11). LSN considers depth weighted calculated volumetric densification strain within soil layers as a proxy for the severity of liquefaction land damage likely at the ground surface.

<sup>2</sup>  **$I_c$  = Soil Behaviour Classification Index** - Robertson & Wride 1998.

Table 6: Estimated “Free-Field” Post-Liquefaction Volumetric Ground Surface Settlements

Earthquake scenario	Moment magnitude ( $M_w$ ) / PGA (g)	MBIE “Index Value” (mm)	MBIE Technical Category	LSN Values
GWD = varying (in-situ) and 0.5m to 1.2m (earthquake); Layer transition applied				
SLS	7.5/0.13	< 35	TC2	1 – 5
SLS2	6.0/0.19	5 – 50	TC2	2 – 16
ULS	7.5/0.35	5 – 80	TC2	5 – 25

In accordance with the MBIE Guidance, the analysis indicates that under SLS and ULS loading conditions the predicted index value settlements fall within the expected future land performance values for a TC2 category site. The higher settlements were located on the land at the northern area of the 2 Glovers Road section, which generally correlates with observed liquefaction ejecta in the aerial photographs.

Based on the LSN estimated for the design events, ‘little to minor’ expression of liquefaction may be expected for a future SLS design event, and ‘little to moderate’ expression of liquefaction may be expected for a future ULS design event. The values of LSN at the upper end of the ranges estimated are generally located in the central portion of the development area (where ejecta has been observed following the CES events).

### Lateral Spreading

Given the generally flat topography of the site, and the assumption that the site will be levelled further during the development of the subdivision, there is unlikely to be significant height differences, apart from the area immediately adjacent to Green’s Stream. As the area needs to be developed with the FMA in mind, and land levels lifted, there is the potential for a more pronounced ‘free-face’ that could create a risk of lateral spreading. Options to address this are discussed later in the report.

## 6. Site Designation Assessment

Based on the findings of our desk study, our site-specific ground investigation and observations, and assessment of the performance of the land, we consider the MBIE TC2 category generally appropriate for the site. Despite the deformation characteristics of TC2, the land does not meet the definition of ‘Good Ground’ as per the New Zealand Standards without modification to standard foundation systems and specific engineering design to account for this due to the soft soils.

## 7. Geotechnical Considerations for Subdivision

### Geotechnical Hazards

The most significant geotechnical hazards at the site comprise the potential for earthquake-induced soil liquefaction and potential static subsidence of the soft compressible soils. These hazards can be partly mitigated by providing strengthened foundations, which reduce the potential for differential settlement of the buildings and are designed to be re-levellable.

However, as part of the land development it is understood that, in order to meet the CCC FFL requirements, the site grade will need to be raised by filling. Site filling works can induce



additional loading of the underlying soft compressible deposits and potentially lead to consolidation settlement of the fill and / or construction above. To assess the likely influence of filling, a pre-load trial was undertaken by Miyamoto. This trial indicates that static settlements are not believed to pose a significant risk to the Halswell Road section of the development. Given the similar soil conditions found, it is our professional opinion that this statement also applies to the Glovers Road properties. It is still recommended that settlement plates are installed during the site filling works and these should be founded at the base of the fill with upstands extending through the top of the fill. It is advised that the settlement plates are monitored during the raising of the site levels and for a period (up to 6 months) to assess any static settlements and ensure performance is in line with the pre-loading trial findings.

The current subdivision plan for the entire site is not currently finalised and until it is further developed, specific detailed recommendations cannot be provided, however, the following sections outline general considerations for future development.

### Development Considerations

Based on the land survey data (provided by others), a maximum level of approximately 22.3m CDD was identified at the northern extent of property. The land drops to approximately 19.6m CDD next to Green's Stream, though the development does not extend to this point. The low point of the development area is at approximately 20.4m CDD. As discussed above, the site will require filling to meet the CCC FFL requirements (FFL = 21.25m CDD based on the Halswell Road site), particularly if the preferred foundation options comprise concrete slab foundations. It is anticipated that maximum filling would be in the proximity of 1.2m.

Currently, there is no indication of cutting or removal of material to the north of the site. All earthworks should be undertaken in accordance with NZS 4431:1989 (code of practice for earth fill for residential development) prior to the construction of any foundations. The monitoring scheme (mentioned earlier) should be fully developed once the final details of the proposed earthworks are known.

The southern extent of the filling (in proximity of Green's Stream) will be the maximum height of fill required and will require detailed design to ensure stability. It is our understanding the development area is to extend to within 15m of Green's Stream. A shallow vegetated slope is considered suitable given the height of filling is not likely to exceed 1.2m, and provided the slope is not at a gradient exceeding 1.0m vertical to 2.0m horizontal.

Based on the above and the previously completed works, the following foundation solutions would be considered suitable for the construction of NZS3604 compliant structures for the subdivision:

- MBIE TC2 (Options 1 to 4) enhanced foundation slab;
- Specifically designed, enhanced NZS 3604 perimeter foundation wall and shallow piles.

Based on development works proposed, a geotechnical ultimate bearing capacity of 200kPa can be assumed at a high level, though this value is indicative only. The available bearing capacity must be confirmed on-site prior to construction works at the time of any building consent application.

The foundation types detailed above are also preliminary and should be further developed and optimised in collaboration with the structural engineer once further details of any proposed structure are finalised.

### Stormwater Management

Stormwater management is outside the scope of our works. However, it is understood the southern section of the Halswell Road site (area south of Green's Stream) will be utilised for stormwater detention and treatment for the Riverstone subdivision as a whole, with shallow basins excavated through this area. As mentioned in the initial assessment undertaken, this material is unlikely to be suitable for filling of the development area.

### Services

Buried services are vulnerable to ground deformations when located within and/or in proximity of potentially liquefiable and compressible soils. Services for the residential development should be designed by a suitably qualified person in collaboration with the geotechnical engineers to accommodate the likelihood of future ground deformations.

### Pavement/Roading Infrastructure

As for the services at the site, pavements will require detailed design by a suitably experienced person in collaboration with the geotechnical engineer, the finished ground levels and compaction characteristics of the filling material.

It is currently understood that the new areas of development will link into the Halswell Road property as well as having its own access onto Glovers Road, and it is assumed that filling in this area will be required to raise the grade. The underlying soils in this area are generally typical for the site with the upper 1.0m comprising topsoil over soft silt (loosely corresponding to a CBR of ~2 to 3 below the topsoil).

## 8. Assessment Against RMA Section 106

As per the requirements of Section 106 of the Resource Management Act (RMA) (2017), we have undertaken a high-level assessment of the significant geotechnical hazards that may affect the site, outside of the hazards already discussed in this report (i.e. static and earthquake-induced subsidence, and lateral spreading). These hazards include, but are not limited to:

- Erosion;
- Falling debris;
- Slippage;
- Inundation.

At the time of our site visit, there was no evidence of erosion. Likewise, no evidence was observed to suggest that lateral movement is an issue on the site, given the site is generally

flat. Rock Fall or slope movement are also not considered a risk to this area of the development.

As part of the site is identified as being within a Flood Management Area (FMA) as defined by the CCC, inundation is likely to be a risk, as the site currently stands. If the site is built up to ensure the FFLs set by the CCC are met and suitable stormwater drainage is in place, then inundation is not considered an imminent risk to the development.

Based on our assessment, we consider that the “significant” geotechnical hazards may be mitigated to an acceptable standard, provided that the geotechnical recommendations given in this report are followed, and the appropriate engineering measures implemented, we consider that the development is unlikely to be affected nor worsen, accelerate or result in material damage.

## 9. Limitations

This report is subject to the following limitations:

- This report has been prepared by Miyamoto for the Client for the purpose/s agreed with the Client (Purpose). Miyamoto accepts no responsibility for the validity, appropriateness, sufficiency or consequences of the Client using the report for purposes other than for the Purpose.
- This report is not intended for general publication or circulation. This report is not to be reproduced by the Client except in relation to the Purpose, without Miyamoto’s prior written permission. Miyamoto disclaims all risk and all responsibility to any third party.
- This report is provided based on the various assumptions contained in the report.
- Miyamoto’s professional services are performed using a degree of care and skill reasonably exercised by reputable consultants providing the same or similar services as at the date of this report.
- The Client is responsible for ensuring that the design of any foundations ensures the functionality of the building under SLS level loads.
- The sub surface information has been obtained from investigation carried out at discrete locations, which by their nature only provide information about a relatively small volume of subsoils. While Miyamoto has taken reasonable skill and care in carrying out the investigation to determine the subsoil condition, the subsoil condition could differ substantially from the results of any sampling investigation. Miyamoto is not responsible for and does not accept any liability in respect of any difference between the actual subsoil conditions and the results of our investigation.
- Any susceptibility analysis carried out in respect of liquefaction is based on Miyamoto’s current understanding as an experienced professional engineering consultant of the data, methods etc. Future seismic events may change our understanding of liquefaction and its affects, which may affect the content of this report. Miyamoto is not responsible for and does not accept any liability where the content of this report is changed due to a change in industry knowledge of matters relating to liquefaction.
- This report specifically excludes assessment or advice relating to hazardous materials, such as asbestos.

- Where the Client provides information to Miyamoto, including design calculations and drawings of the as-built structure, or where the report indicates that we have obtained and/or relied upon information provided from a third party, Miyamoto has not made any independent verification of this information except as expressly stated in the report. Miyamoto assumes no responsibility for any inaccuracies in, or omissions to, that information.
- A change in circumstances, facts, information after the report has been provided may affect the adequacy or accuracy of the report. Miyamoto is not responsible for the adequacy or accuracy of the report as a result of any such changes.
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If you have any queries or you require any further clarification on any aspects of this report, please do not hesitate to contact Miyamoto International (NZ) Ltd.

## 10. References

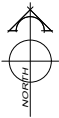
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## Appendices



**A. Updated Indicative Subdivision Plan (Davie Lovell Smith)**





**DRAFT**

AMENDMENT	DATE	DESCRIPTION



Total Area : 23.1161 ha  
 Comprised in: RT's CB108/654, CB48C/117 & CB48C/118

**DAVE LOVELL-SMITH**  
 PLANNING SURVEYING ENGINEERING

116 Wrights Road P O Box 679 Christchurch 8140, New Zealand  
 Telephone: 03 379-0793 Website: www.dls.co.nz E-mail: office@dls.co.nz

JOB TITLE: **Halswell Road**

SHEET TITLE: **Proposed Subdivision of  
 Pt RS 1593, RS 772 &  
 Lots 1 & 2 DP 83635**

DRAWING STATUS: **For Discussion Purposes**

SCALE: 1:1000@A1 DATE: October 2020  
 1:2000@A3  
 CAD FILE: J:\2017\Concept\_R4.dwg REVISION:  
 DRAWING No: **C20017** SHEET No: 1 OF 1 **R6**

- NOTES:
1. Areas and dimensions are approximate only and are subject to final survey and deposit of plans.
  2. Service easements to be created as required.
  3. This plan has been prepared for discussion purposes only. No liability is accepted if the plan is used for any other purposes.
  4. The position of Greens Drain is approximate and subject to survey.

Pt RS 5786

Lot 2  
DP 490383

Lot 3  
DP 83635



## B. ECan Listed Land Use Register Files



Dear Sir/Madam

Thank you for submitting your property enquiry in regards to our Listed Land Use Register (LLUR) which holds information about sites that have been used, or are currently used for activities which have the potential to have caused contamination.

The LLUR statement provided indicates the location of the land parcel(s) you enquired about and provides information regarding any LLUR sites within a radius specified in the statement of this land.

Please note that if a property is not currently entered on the LLUR, it does not mean that an activity with the potential to cause contamination has never occurred, or is not currently occurring there. The LLUR is not complete, and new sites are regularly being added as we receive information and conduct our own investigations into current and historic land uses.

The LLUR only contains information held by Environment Canterbury in relation to contaminated or potentially contaminated land; other information relevant to potential contamination may be held in other files (for example consent and enforcement files).

If your enquiry relates to a farm property, please note that many current and past activities undertaken on farms may not be listed on the LLUR. Activities such as the storage, formulation and disposal of pesticides, offal pits, foot rot troughs, animal dips and underground or above ground fuel tanks have the potential to cause contamination.

Please contact and Environment Canterbury Contaminated Sites Officer if you wish to discuss the contents of the LLUR statement, or if you require additional information. For any other information regarding this land please contact Environment Canterbury Customer Services.

Yours sincerely

**Contaminated Sites Team**

# Property Statement from the Listed Land Use Register

Visit [www.ecan.govt.nz/HAIL](http://www.ecan.govt.nz/HAIL) for more information about land uses.



Customer Services  
P. 03 353 9007 or 0800 324 636

PO Box 345  
Christchurch 8140

P. 03 365 3828  
F. 03 365 3194  
E. [ecinfo@ecan.govt.nz](mailto:ecinfo@ecan.govt.nz)

[www.ecan.govt.nz](http://www.ecan.govt.nz)

Date:	13 October 2020	
Land Parcels:	Lot 1 DP 83635	Valuation No(s): 2356209300



*The information presented in this map is specific to the property you have selected. Information on nearby properties may not be shown on this map, even if the property is visible.*

## Summary of sites:

Site ID	Site Name	Location	HAIL Activity(s)	Category
26587	26587	Halswell West	A10 - Persistent pesticide bulk storage or use;	Not Investigated

*Please note that the above table represents a summary of sites and HAILS intersecting the area of enquiry only.*

## Information held about the sites on the Listed Land Use Register

**Site 26587: 26587** (Intersects enquiry area.)

Site Address:	Halswell West
Legal Description(s):	Lot 1 DP 83635, Lot 2 DP 83635

<b>Site Category:</b>	Not Investigated
<b>Definition:</b>	Verified HAIL has not been investigated.

Land Uses (from HAIL):	Period From	Period To	HAIL land use
	Pre 1994	Pre 2004	Persistent pesticide bulk storage or use including sports turfs, market gardens, orchards, glass houses or spray sheds

**Notes:**

17 Oct 2013                      Area defined from: 1994-2004 ECan Aerial Photographs  
 Note: Multiple glass houses were noted in aerial photographs reviewed.

**Investigations:**

There are no investigations associated with this site.

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**Information held about other investigations on the Listed Land Use Register**

For further information from Environment Canterbury, contact Customer Services and refer to enquiry number ENQ265562.

**Disclaimer:**            *The enclosed information is derived from Environment Canterbury’s Listed Land Use Register and is made available to you under the Local Government Official Information and Meetings Act 1987 and Environment Canterbury’s Contaminated Land Information Management Strategy (ECan 2009).*

*The information contained in this report reflects the current records held by Environment Canterbury regarding the activities undertaken on the site, its possible contamination and based on that information, the categorisation of the site. Environment Canterbury has not verified the accuracy or completeness of this information. It is released only as a copy of Environment Canterbury's records and is not intended to provide a full, complete or totally accurate assessment of the site. It is provided on the basis that Environment Canterbury makes no warranty or representation regarding the reliability, accuracy or completeness of the information provided or the level of contamination (if any) at the relevant site or that the site is suitable or otherwise for any particular purpose. Environment Canterbury accepts no responsibility for any loss, cost, damage or expense any person may incur as a result of the use, reference to or reliance on the information contained in this report.*

*Any person receiving and using this information is bound by the provisions of the Privacy Act 1993.*

Dear Sir/Madam

Thank you for submitting your property enquiry in regards to our Listed Land Use Register (LLUR) which holds information about sites that have been used, or are currently used for activities which have the potential to have caused contamination.

The LLUR statement provided indicates the location of the land parcel(s) you enquired about and provides information regarding any LLUR sites within a radius specified in the statement of this land.

Please note that if a property is not currently entered on the LLUR, it does not mean that an activity with the potential to cause contamination has never occurred, or is not currently occurring there. The LLUR is not complete, and new sites are regularly being added as we receive information and conduct our own investigations into current and historic land uses.

The LLUR only contains information held by Environment Canterbury in relation to contaminated or potentially contaminated land; other information relevant to potential contamination may be held in other files (for example consent and enforcement files).

If your enquiry relates to a farm property, please note that many current and past activities undertaken on farms may not be listed on the LLUR. Activities such as the storage, formulation and disposal of pesticides, offal pits, foot rot troughs, animal dips and underground or above ground fuel tanks have the potential to cause contamination.

Please contact and Environment Canterbury Contaminated Sites Officer if you wish to discuss the contents of the LLUR statement, or if you require additional information. For any other information regarding this land please contact Environment Canterbury Customer Services.

Yours sincerely

**Contaminated Sites Team**

# Property Statement from the Listed Land Use Register

Visit [www.ecan.govt.nz/HAIL](http://www.ecan.govt.nz/HAIL) for more information about land uses.

Customer Services  
P. 03 353 9007 or 0800 324 636

PO Box 345  
Christchurch 8140

P. 03 365 3828  
F. 03 365 3194  
E. [ecinfo@ecan.govt.nz](mailto:ecinfo@ecan.govt.nz)

[www.ecan.govt.nz](http://www.ecan.govt.nz)

<b>Date:</b>	13 October 2020	
<b>Land Parcels:</b>	Lot 2 DP 83635	Valuation No(s): 2356209301



*The information presented in this map is specific to the property you have selected. Information on nearby properties may not be shown on this map, even if the property is visible.*

## Summary of sites:

Site ID	Site Name	Location	HAIL Activity(s)	Category
26587	26587	Halswell West	A10 - Persistent pesticide bulk storage or use;	Not Investigated

*Please note that the above table represents a summary of sites and HAILS intersecting the area of enquiry only.*

## Information held about the sites on the Listed Land Use Register

**Site 26587: 26587** (Intersects enquiry area.)

<b>Site Address:</b>	Halswell West
<b>Legal Description(s):</b>	Lot 1 DP 83635, Lot 2 DP 83635

<b>Site Category:</b>	Not Investigated
<b>Definition:</b>	Verified HAIL has not been investigated.

Land Uses (from HAIL):	Period From	Period To	HAIL land use
	Pre 1994	Pre 2004	Persistent pesticide bulk storage or use including sports turfs, market gardens, orchards, glass houses or spray sheds

**Notes:**

17 Oct 2013                    Area defined from: 1994-2004 ECan Aerial Photographs  
 Note: Multiple glass houses were noted in aerial photographs reviewed.

**Investigations:**

There are no investigations associated with this site.

---

**Information held about other investigations on the Listed Land Use Register**

For further information from Environment Canterbury, contact Customer Services and refer to enquiry number ENQ265560.

**Disclaimer:**        *The enclosed information is derived from Environment Canterbury’s Listed Land Use Register and is made available to you under the Local Government Official Information and Meetings Act 1987 and Environment Canterbury’s Contaminated Land Information Management Strategy (ECan 2009).*

*The information contained in this report reflects the current records held by Environment Canterbury regarding the activities undertaken on the site, its possible contamination and based on that information, the categorisation of the site. Environment Canterbury has not verified the accuracy or completeness of this information. It is released only as a copy of Environment Canterbury’s records and is not intended to provide a full, complete or totally accurate assessment of the site. It is provided on the basis that Environment Canterbury makes no warranty or representation regarding the reliability, accuracy or completeness of the information provided or the level of contamination (if any) at the relevant site or that the site is suitable or otherwise for any particular purpose. Environment Canterbury accepts no responsibility for any loss, cost, damage or expense any person may incur as a result of the use, reference to or reliance on the information contained in this report.*

*Any person receiving and using this information is bound by the provisions of the Privacy Act 1993.*

## C. Geotechnical Investigation Results

MINZ Shallow Investigation Logs

Laboratory Soil Sample Test Results

LandTest CPT/DPSH Plot





## SHALLOW GROUND INVESTIGATION LOG

HA1/DCP1

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 2.9 mbgl
<b>PROCESSED BY:</b> CG	<b>HOLE DIAMETER:</b> 50 mm
<b>LOCATION:</b> REFER TO SITE PLAN	<b>DRILLING METHOD:</b> Hand Auger
	<b>SHEAR VANE NUMBER:</b> 2102
	<b>GROUNDWATER LEVEL:</b> 1.65 mbgl
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size				WC (%)	UW
							LL	PL	PI	Gr	Sa	FC			
0.0 - 0.1	1			SILT: low plasticity, dark brown, moist, with minor rootlets (TOPSOIL)	[Cross-hatch pattern]										
0.1 - 0.2	1														
0.2 - 0.3	1														
0.3 - 0.4	1														
0.4 - 0.5	3			SILT: low plasticity, brown, moist, with minor fine sand	[X pattern]										
0.5 - 0.6	2														
0.6 - 0.7	1														
0.7 - 0.8	2														
0.8 - 0.9	1														
0.9 - 1.0	2														
1.0 - 1.1	2														
1.1 - 1.2	2														
1.2 - 1.3	2														
1.3 - 1.4	2														
1.4 - 1.5	1														
1.5 - 1.6	2			Silty SAND: fine to medium, brown-grey, wet	[Dotted pattern]										
1.6 - 1.7	2														
1.7 - 1.8	2														
1.8 - 1.9	2														
1.9 - 2.0	2														
2.0 - 2.1	3			at 2.0m: becomes blue-grey, saturated											
2.1 - 2.2	3														
2.2 - 2.3	2														
2.3 - 2.4	1														
2.4 - 2.5	1														
2.5 - 2.6	2														
2.6 - 2.7	2														
2.7 - 2.8	3														
2.8 - 2.9	4														
2.9 - 3.0	5														

...contd on next page

### LEGEND

**ABBREVIATIONS**

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 ∇... STANDING GWL

**NOTES**

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA1/DCP1 (contd.)

PROJECT:	2 & 4 Glovers Road, Halswell, Christchurch				
LOGGED BY:	CG	TOTAL DEPTH OF HOLE:	3.9 mbgl	HOLE DIAMETER:	50 mm
PROCESSED BY:	CG	DRILLING METHOD:	Hand Auger	SHEAR VANE NUMBER:	2102
LOCATION:	REFER TO SITE PLAN	GROUNDWATER LEVEL:	1.65 mbgl	This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size				WC (%)	UW
							LL	PL	PI	Gr	Sa	FC			
3.5	9 9 9 9 7 6 6 7 7	1.65m bgl →		Silty SAND: fine to medium, blue-grey, saturated (contd.)		DIST. SAMPLE					51%	49%			
4.0				SILT: low plasticity, blue-grey, saturated											
4.5				EOH (Target Depth Reached)											
5.0															
5.5															

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
GWL GROUNDWATER LEVEL  
mbgl METERS BELOW GROUND LEVEL  
WC WATER CONTENT

HA HAND AUGER  
UTP UNABLE TO PENETRATE  
EOH END OF HOLE  
UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
PL PLASTIC LIMIT  
PI PLASTICITY INDEX  
NE NOT ENCOUNTERED

Gr GRAVEL  
Sa SAND  
FC FINES CONTENT  
...▽... STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA2/DCP2

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 3.9 mbgl
<b>PROCESSED BY:</b> CG	<b>DRILLING METHOD:</b> Hand Auger
<b>LOCATION:</b> REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b> 1.3 mbgl
<b>HOLE DIAMETER:</b> 50 mm	
<b>SHEAR VANE NUMBER:</b> 2102	
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing							Vane shear strength (kPa) peak/remoulded	
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size			WC (%)		UW
							LL	PL	PI	Gr	Sa	FC			
1	1	▽		SILT: non-plastic, dark brown, moist, with some sand and rootlets (TOPSOIL)										66 / 16	
2	2			SILT: low plasticity, yellow-brown, moist, with some sand											
0.5	2														
	3														
	3				SAND: fine to medium, orange-brown, moist, with trace of silt										
1.0	2														
	2														
	4														
	3														
	2														
	3														
	2														
1.5	2														
	3				Clayey SILT: low to medium plasticity, grey, moist, with some sand										
	4														
	3														
	3			at 1.9m: becomes wet, mottled orange											
2.0	Self Weight														
	1														
	3														
	3			at 2.2m: mottling absent											
	3														
	4			at 2.3m: becomes saturated											
2.5	4														
	4														
	5														
	5														
	7														
	7														
...contd on next page						DIST. SAMPLE	29	20	9	-	15%	85%			

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 ▽ STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA2/DCP2 (contd.)

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 3.9 mbgl
<b>PROCESSED BY:</b> CG	<b>DRILLING METHOD:</b> Hand Auger
<b>LOCATION:</b> REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b> 1.3 mbgl
<b>HOLE DIAMETER:</b> 50 mm	
<b>SHEAR VANE NUMBER:</b> 2102	
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded			
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size				WC (%)	UW	
							LL	PL	PI	Gr	Sa	FC				
7	7	1.3m bgl -->		Clayey SILT: low to medium plasticity, grey, saturated, with some sand (contd.)		DIST. SAMPLE										
7	7															
8	8															
7	7															
3.5	7															
	6															
	7															
	8															
	7															
4.0																
				EOH (Target Depth Reached)												
4.5																
5.0																
5.5																

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
GWL GROUNDWATER LEVEL  
mbgl METERS BELOW GROUND LEVEL  
WC WATER CONTENT

HA HAND AUGER  
UTP UNABLE TO PENETRATE  
EOH END OF HOLE  
UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
PL PLASTIC LIMIT  
PI PLASTICITY INDEX  
NE NOT ENCOUNTERED

Gr GRAVEL  
Sa SAND  
FC FINES CONTENT  
...▽... STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

**SHALLOW GROUND INVESTIGATION LOG**

**HA3/DCP3**

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
LOGGED BY: CG	TOTAL DEPTH OF HOLE: 4.1 mbgl
PROCESSED BY: CG	HOLE DIAMETER: 50 mm
LOCATION: REFER TO SITE PLAN	DRILLING METHOD: Hand Auger
	SHEAR VANE NUMBER: 2102
	GROUNDWATER LEVEL: 1.8 mbgl
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size					
							LL	PL	PI	Gr	Sa	FC		WC (%)	UW
2				SILT: non-plastic, dark brown, dry, with some sand and rootlets (TOPSOIL)											
1				SILT: low plasticity, light brown, moist											
2				SAND: fine to medium, orange brown, moist											
0.5				SAND: fine to medium, orange brown, moist											
2				SAND: fine to medium, orange brown, moist											
2				SAND: fine to medium, orange brown, moist											
1.0				SAND: fine to medium, orange brown, moist											
2				SAND: fine to medium, orange brown, moist											
2				SAND: fine to medium, orange brown, moist											
3				SAND: fine to medium, orange brown, moist											
1.5				Sandy SILT: low plasticity, orange brown, wet											
2				Sandy SILT: low plasticity, orange brown, wet											
3				SILT: medium plasticity, brown, wet											
3				SILT: medium plasticity, brown, wet											
3				SILT: medium plasticity, brown, wet											
5				SILT: medium plasticity, brown, wet											
2.0				Sandy SILT: non-plastic, dark grey, saturated											
2				Sandy SILT: non-plastic, dark grey, saturated											
2				Sandy SILT: non-plastic, dark grey, saturated											
3				Sandy SILT: non-plastic, dark grey, saturated											
4				Sandy SILT: non-plastic, dark grey, saturated											
2.5				Sandy SILT: non-plastic, dark grey, saturated		DIST. SAMPLE									
4				Sandy SILT: non-plastic, dark grey, saturated			Non-Plastic								
4				Sandy SILT: non-plastic, dark grey, saturated											
5				Sandy SILT: non-plastic, dark grey, saturated											
5				Sandy SILT: non-plastic, dark grey, saturated											
5				Sandy SILT: non-plastic, dark grey, saturated											
2				Sandy SILT: non-plastic, dark grey, saturated											
4				Sandy SILT: non-plastic, dark grey, saturated											
5				Sandy SILT: non-plastic, dark grey, saturated											

...contd on next page

**LEGEND**

ABBREVIATIONS				NOTES			
DCP	DYNAMIC CONE PENETROMETER	HA	HAND AUGER	LL	LIQUID LIMIT	Gr	GRAVEL
GWL	GROUNDWATER LEVEL	UTP	UNABLE TO PENETRATE	PL	PLASTIC LIMIT	Sa	SAND
mbgl	METERS BELOW GROUND LEVEL	EOH	END OF HOLE	PI	PLASTICITY INDEX	FC	FINES CONTENT
WC	WATER CONTENT	UW	UNIT WEIGHT (kN/m <sup>3</sup> )	NE	NOT ENCOUNTERED		STANDING GWL

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

### HA3/DCP3 (contd.)

<b>PROJECT:</b>	2 & 4 Glovers Road, Halswell, Christchurch				
<b>LOGGED BY:</b>	CG	<b>TOTAL DEPTH OF HOLE:</b>	4.1 mbgl	<b>HOLE DIAMETER:</b>	50 mm
<b>PROCESSED BY:</b>	CG	<b>DRILLING METHOD:</b>	Hand Auger	<b>SHEAR VANE NUMBER:</b>	2102
<b>LOCATION:</b>	REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b>	1.8 mbgl	This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded	
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size				
							LL	PL	PI	Gr	Sa	FC		WC (%)
5	5	1.8m bgl →		Sandy SILT: non-plastic, dark grey, saturated (contd.)	XXXXXX	DIST. SAMPLE	Non-Plastic			-	41%	59%		
7	7				XXXXXX									
8	8				XXXXXX									
8	8				XXXXXX									
8	8				XXXXXX									
3.5	7				XXXXXX									
	8				XXXXXX									
	9				XXXXXX									
	10				XXXXXX									
4.0					EOH (Target Depth Reached)		XXXXXX							
4.5														
5.0														
5.5														

#### LEGEND

##### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 ∇... STANDING GWL

##### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA4/DCP4

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 2.9 mbgl
<b>PROCESSED BY:</b> CG	<b>DRILLING METHOD:</b> Hand Auger
<b>LOCATION:</b> REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b> 1.2 mbgl
<b>HOLE DIAMETER:</b> 50 mm	
<b>SHEAR VANE NUMBER:</b> 2102	
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing							Vane shear strength (kPa) peak/remoulded	
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size			WC (%)		UW
							LL	PL	PI	Gr	Sa	FC			
0.0 - 0.2	2			Sandy SILT: non-plastic, brown, moist, with minor rootlets (TOPSOIL)	[Cross-hatch pattern]										
0.2 - 0.8	2			SAND: fine to medium, grey, moist, with some silt	[Dotted pattern]										
0.8 - 1.2	2			at 0.8m: becomes wet	[Dotted pattern]										
1.2 - 1.9	3	▽		Sandy SILT: low plasticity, brown-grey, wet, sand is fine	[Cross-hatch pattern]										
1.9 - 2.0	3			at 1.2m: becomes saturated	[Cross-hatch pattern]										
2.0 - 2.2	3			SILT: low to medium plasticity, blue-grey, saturated	[Cross-hatch pattern]										
2.2 - 2.4	4			Silty SAND: fine to medium, grey, saturated	[Dotted pattern]										
2.4 - 2.5	4				[Dotted pattern]										
			EOH (Target Depth Reached)												

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
GWL GROUNDWATER LEVEL  
mbgl METERS BELOW GROUND LEVEL  
WC WATER CONTENT

HA HAND AUGER  
UTP UNABLE TO PENETRATE  
EOH END OF HOLE  
UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
PL PLASTIC LIMIT  
PI PLASTICITY INDEX  
NE NOT ENCOUNTERED

Gr GRAVEL  
Sa SAND  
FC FINES CONTENT  
▽ STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA5/DCP5

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
LOGGED BY: CG	TOTAL DEPTH OF HOLE: 1.9 mbgl
PROCESSED BY: CG	HOLE DIAMETER: 50 mm
LOCATION: REFER TO SITE PLAN	DRILLING METHOD: Hand Auger
	SHEAR VANE NUMBER: 2102
	GROUNDWATER LEVEL: 1.0 mbgl
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing							Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size			WC (%)		UW	
							LL	PL	PI	Gr	Sa	FC				
0.0 - 0.2	2	1.0		SILT: low plasticity, brown, moist, with minor fine sand (TOPSOIL)												
0.2 - 0.4	1			Sandy SILT: low plasticity, grey, moist, sand is fine												
0.4 - 0.6	2															
0.6 - 0.8	2															
0.8 - 1.0	2															
1.0 - 1.2	1			at 1.0m: becomes wet												
1.2 - 1.4	1		at 1.2m: becomes saturated													
1.4 - 1.6	2			Silty SAND: fine to medium, grey, saturated												
1.6 - 1.8	2			at 1.8m: with minor fine to medium gravel		DIST. SAMPLE					58%	42%				
1.8 - 2.0	5															
2.0 - 2.2	11			EOH (Practical Refusal on Gravel)												

### LEGEND

ABBREVIATIONS				NOTES			
DCP	DYNAMIC CONE PENETROMETER	HA	HAND AUGER	LL	LIQUID LIMIT	Gr	GRAVEL
GWL	GROUNDWATER LEVEL	UTP	UNABLE TO PENETRATE	PL	PLASTIC LIMIT	Sa	SAND
mbgl	METERS BELOW GROUND LEVEL	EOH	END OF HOLE	PI	PLASTICITY INDEX	FC	FINES CONTENT
WC	WATER CONTENT	UW	UNIT WEIGHT (kN/m³)	NE	NOT ENCOUNTERED		STANDING GWL

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth



**SITE INVESTIGATION PLAN**

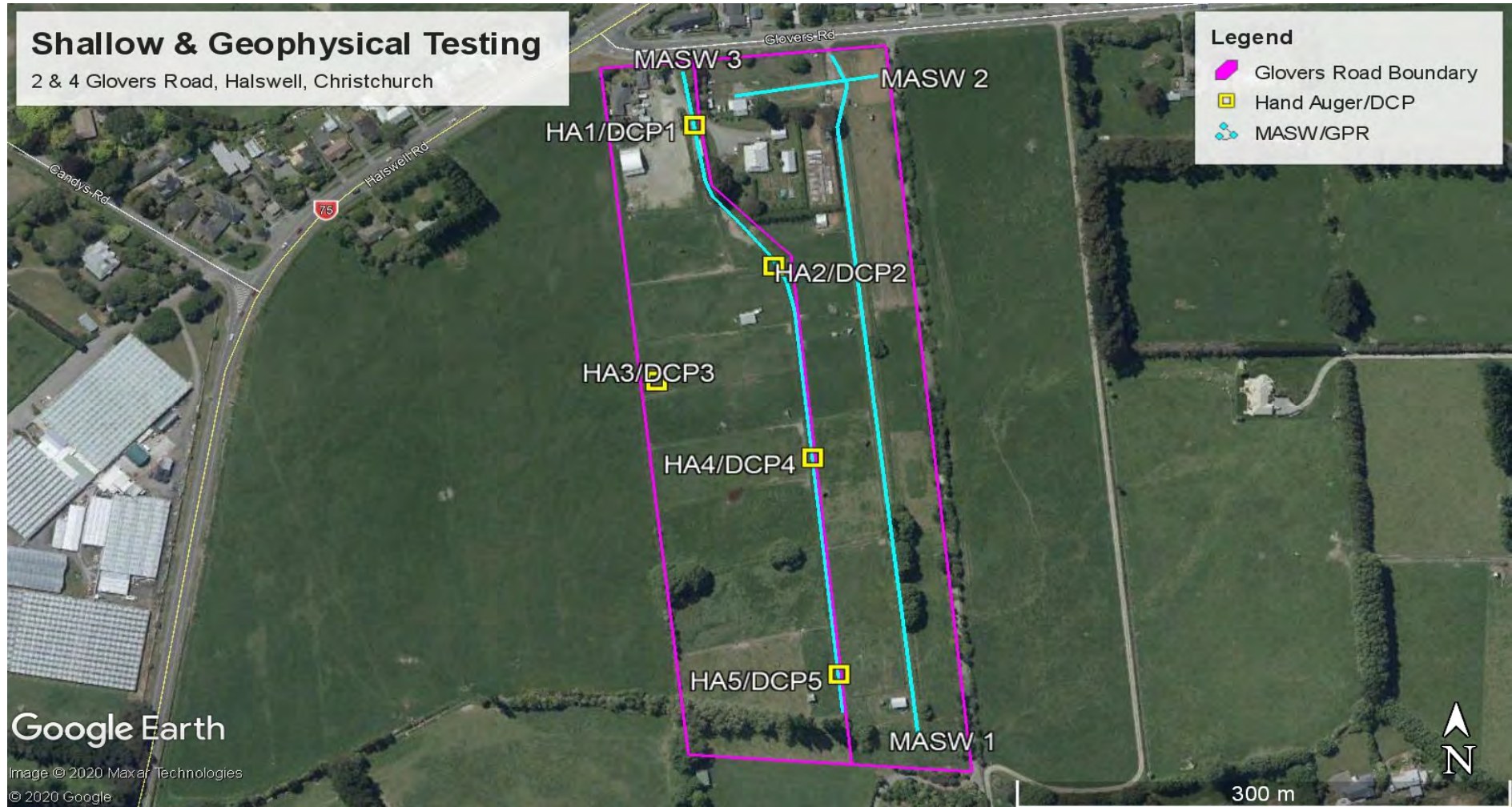
2 & 4 Glovers Road, Halswell, Christchurch

**Shallow & Geophysical Testing**

2 & 4 Glovers Road, Halswell, Christchurch

**Legend**

- Glovers Road Boundary
- Hand Auger/DCP
- MASW/GPR



## TEST REPORT

Lab Job No: 8378-032  
Your ref.: -  
Date of Issue: 14/09/2020  
Date of Re-Issue: -  
Page: 1 of 8

### Test Report

#### C20-450

PROJECT: 2 Glovers Road – Laboratory Testing  
CLIENT: Miyamoto International NZ Ltd,  
518 Colombo Street,  
Christchurch, 8011  
ATTENTION: Clem Gibbens  
INSTRUCTIONS: Determination of Particle-Size Distribution-Wet Sieving method  
Determination of the Liquid & Plastic Limits, Plasticity Index and Water Content  
Determination of the Water Content of Soils  
TEST METHOD: NZS 4402:1986 Test 2.8.1  
NZS 4402:1986 Tests 2.2, 2.3, 2.4  
NZS 4402:1986 Test 2.1  
SAMPLING METHOD: Client - SNA  
TEST RESULTS: As per Laboratory sheets attached



Jeremy Brokenshire  
Laboratory Technician



Nick van Warmerdam  
Approved Signatory



All tests reported herein  
have been performed in  
accordance with the  
laboratory's scope of  
accreditation

-CPT – Aggregates – Soil – Roadings-

This report shall not be reproduced except in full, without written approval of the laboratory



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Middleton, Christchurch  
E: info@geocivil.co.nz  
M: 027 6565 317

DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH

NZS 4402: 1986 Test 2.8.1, 2.8.2

Lab Job No: 8378-032  
Client: Miyamoto International NZ Ltd  
Location: 2 Glovers Road  
HA01 (1.5-2.3m)  
Date Received: 8/09/2020  
Report No: C20-450  
REF: -

Sample No: C20-319  
Tested By: D.P  
Date: 9/09/2020  
Checked By: J.B  
Date: 14/09/2020  
Page: 2 of 8

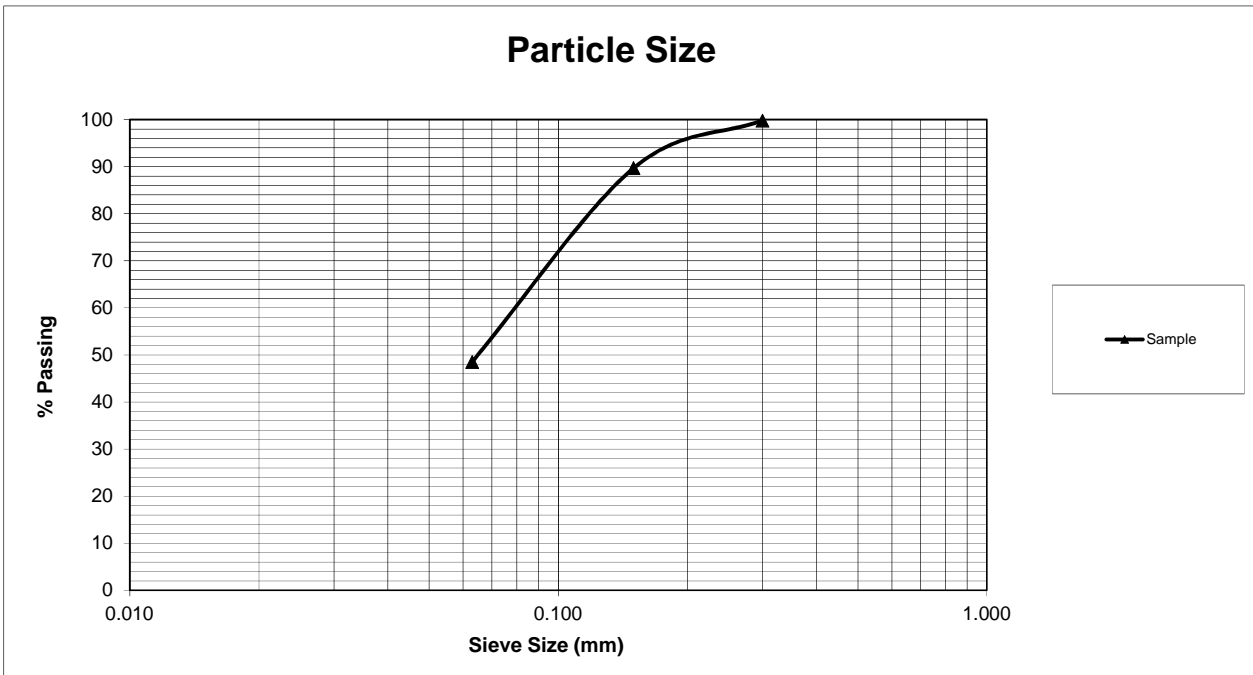
Sampling Method: Sampled by client - SNA  
Date Sampled: 4/09/2020

Sampled By: Client

Test Details: Wet sieving method  
History: Natural

Description of Sample: Silty SAND, brownish grey, wet, no plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	100
0.150	-	-	90
0.063	-	-	49



\*The percentage passing the finest sieve was obtained by difference.

N. van Warmerdam  
Approved Signatory



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**DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH**

NZS 4402: 1986 Test 2.8.1, 2.8.2

**Lab Job No:** 8378-032  
**Client:** Miyamoto International NZ Ltd  
**Location:** 2 Glovers Road  
HA01 (2.3-3.8m)  
**Date Received:** 8/09/2020  
**Report No:** C20-450  
**REF:** -

**Sample No:** C20-320  
**Tested By:** D.P  
**Date:** 9/09/2020  
**Checked By:** J.B  
**Date:** 14/09/2020  
**Page:** 3 of 8

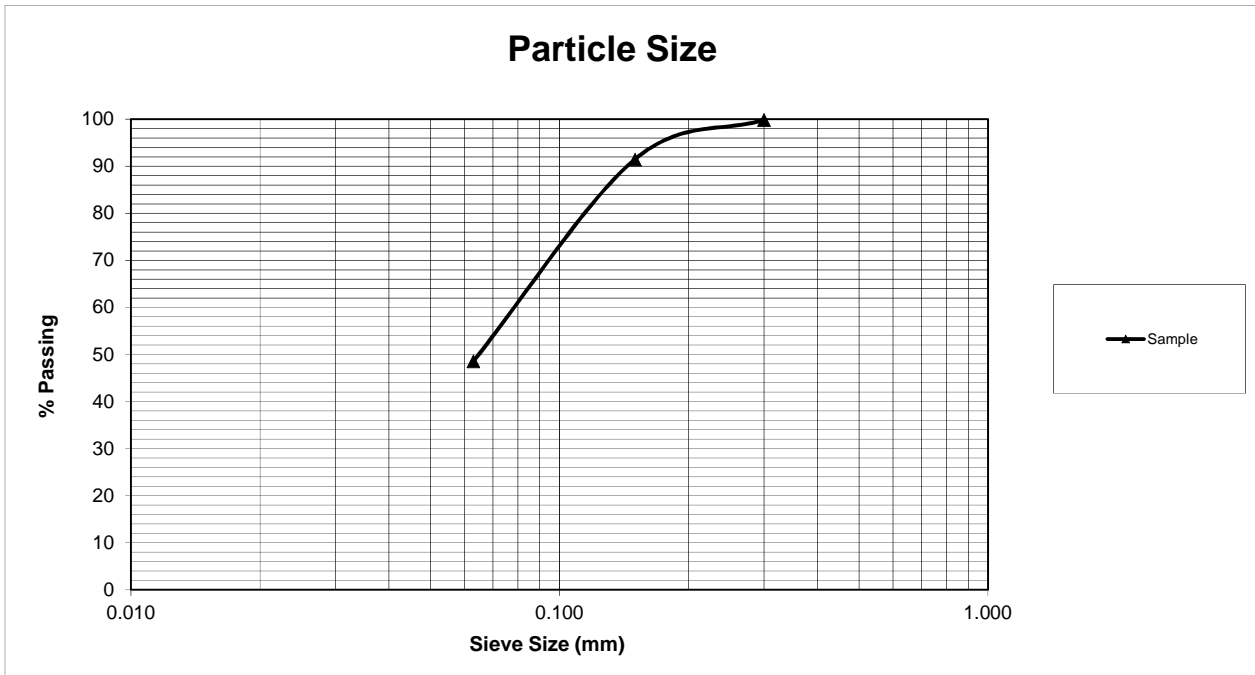
**Sampling Method:** Sampled by client - SNA  
**Date Sampled:** 4/09/2020

**Sampled By:** Client

**Test Details:** Wet sieving method  
**History:** Natural

**Description of Sample:** Silty SAND, brownish grey, saturated, no plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	100
0.150	-	-	91
0.063	-	-	49



\*The percentage passing the finest sieve was obtained by difference.



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**DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH**

NZS 4402: 1986 Test 2.8.1, 2.8.2

Lab Job No: 8378-032  
Client: Miyamoto International NZ Ltd  
Location: 2 Glovers Road  
HA02 (2.7-4.0m)  
Date Received: 8/09/2020  
Report No: C20-450  
REF: -

Sample No: C20-321  
Tested By: D.P  
Date: 9/09/2020  
Checked By: J.B  
Date: 14/09/2020  
Page: 4 of 8

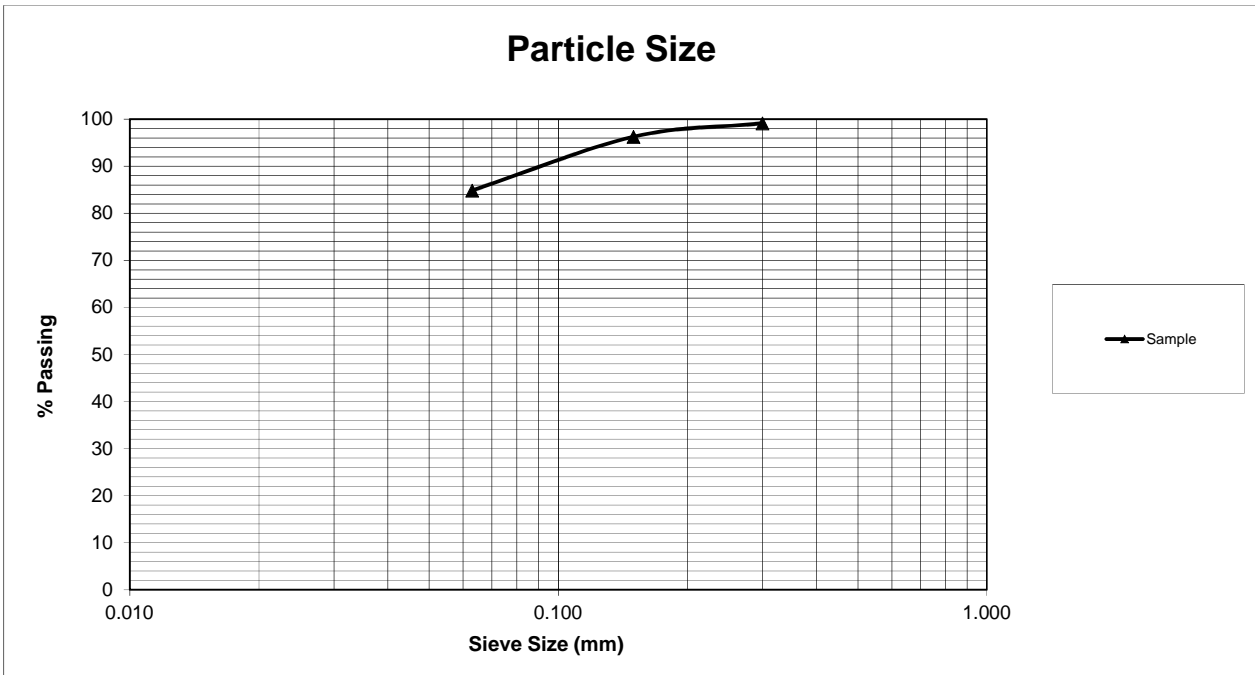
Sampling Method: Sampled by client - SNA  
Date Sampled: 4/09/2020

Sampled By: Client

Test Details: Wet sieving method  
History: Natural

Description of Sample: Silty CLAY, some sand, dark grey saturated, low plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	99
0.150	-	-	96
0.063	-	-	85



\*The percentage passing the finest sieve was obtained by difference.

N. van Warmerdam  
Approved Signatory

**DETERMINATION OF THE LIQUID & PLASTIC LIMITS,  
PLASTICITY INDEX & WATER CONTENT**

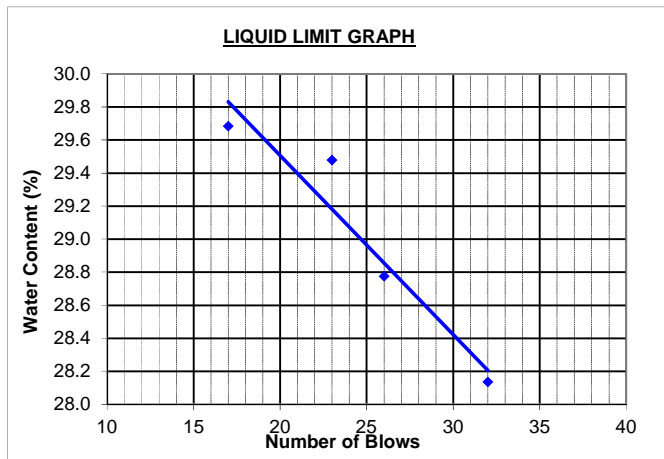
NZS 4402: 1986 Test 2.2, 2.3, 2.4

<b>Lab Job No:</b>	8378-032	<b>Sample No.:</b>	C20-321
<b>Client:</b>	Miyamoto International NZ Ltd	<b>Tested By:</b>	S.P.S
<b>Location:</b>	2 Glovers Road HA02 (2.7-4.0m)	<b>Date Tested:</b>	11/09/2020
<b>Date Received:</b>	8/09/2020	<b>Checked By:</b>	J.B
<b>Report No:</b>	C20-450	<b>Date Checked:</b>	14/09/2020
<b>REF:</b>	-	<b>Page:</b>	5 of 8
<b>Sampling Method:</b>	Sampled by client - SNA	<b>Sampled By:</b>	Client
<b>Date Sampled:</b>	4/09/2020		

**Test Details:**  
 Test performed on: Fraction passing 425mm sieve  
 Sample history: Natural state

**Description of Sample:** Silty CLAY, some sand, dark grey saturated, low plasticity

Liquid Limit				Plastic Limit		NWC	30.5
No. of blows	17	23	26	32		Liquid Limit	29
Water content (%)	29.7	29.5	28.8	28.1	20.0	19.2	20
						Plasticity Index	9





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DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH

NZS 4402: 1986 Test 2.8.1, 2.8.2

Lab Job No: 8378-032  
Client: Miyamoto International NZ Ltd  
Location: 2 Glovers Road  
HA03 (2.0-3.4m)  
Date Received: 8/09/2020  
Report No: C20-450  
REF: -

Sample No: C20-322  
Tested By: D.P  
Date: 9/09/2020  
Checked By: J.B  
Date: 14/09/2020  
Page: 6 of 8

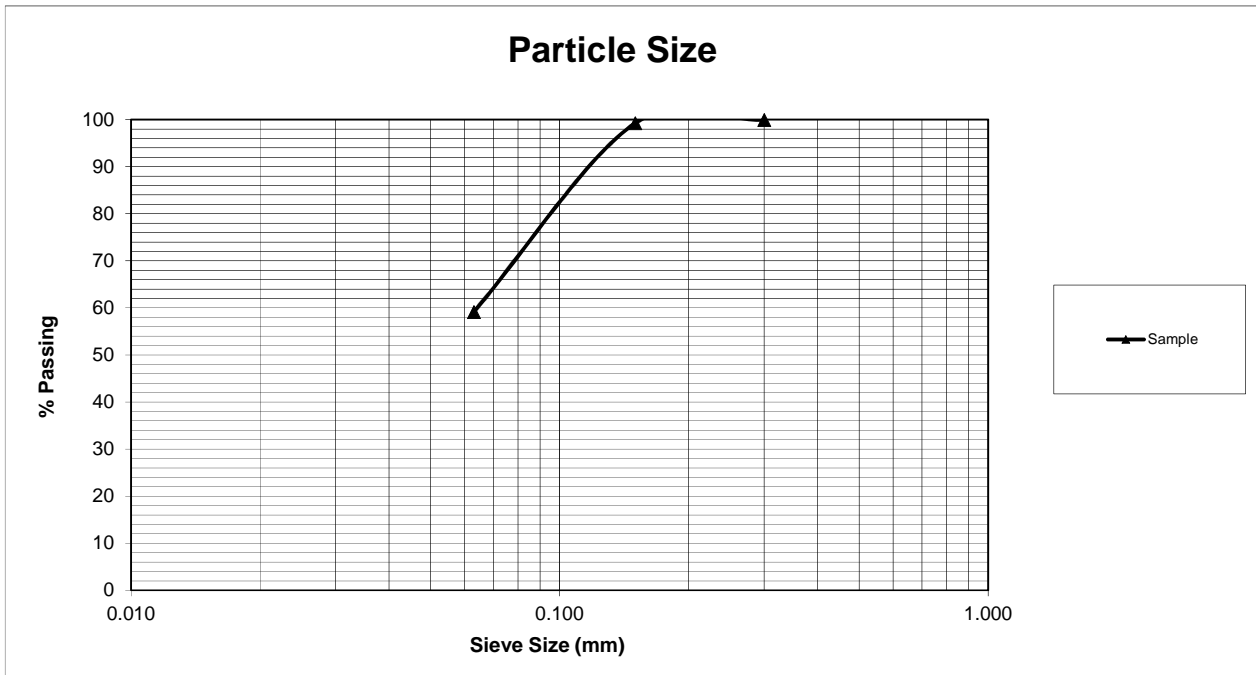
Sampling Method: Sampled by client - SNA  
Date Sampled: 4/09/2020

Sampled By: Client

Test Details: Wet sieving method  
History: Natural

Description of Sample: Sandy SILT, dark grey, saturated, no plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	100
0.150	-	-	99
0.063	-	-	59



\*The percentage passing the finest sieve was obtained by difference.

N. van Warmerdam  
Approved Signatory

**DETERMINATION OF THE LIQUID & PLASTIC LIMITS,  
PLASTICITY INDEX & WATER CONTENT**

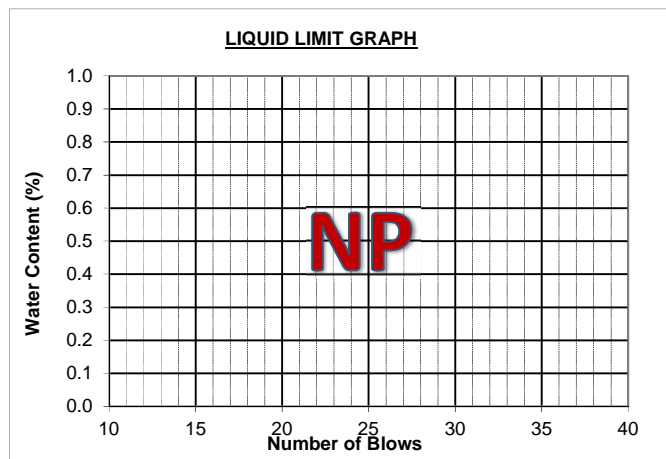
NZS 4402: 1986 Test 2.2, 2.3, 2.4

<b>Lab Job No:</b>	8378-032	<b>Sample No.:</b>	C20-322
<b>Client:</b>	Miyamoto International NZ Ltd	<b>Tested By:</b>	S.P.S
<b>Location:</b>	2 Glovers Road HA03 (2.0-3.4m)	<b>Date Tested:</b>	11/09/2020
<b>Date Received:</b>	8/09/2020	<b>Checked By:</b>	J.B
<b>Report No:</b>	C20-450	<b>Date Checked:</b>	14/09/2020
<b>REF:</b>	-	<b>Page:</b>	7 of 8
<b>Sampling Method:</b>	Sampled by client - SNA	<b>Sampled By:</b>	Client
<b>Date Sampled:</b>	4/09/2020		

**Test Details:**  
 Test performed on: Fraction passing 425mm sieve  
 Sample history: Natural state

**Description of Sample:** Sandy SILT, dark grey, saturated, no plasticity

	<b>Liquid Limit</b>	<b>Plastic Limit</b>	<b>NWC</b>	<b>28.9</b>
<b>No. of blows</b>	<b>NP</b>	<b>NP</b>	<b>Liquid Limit</b>	-
<b>Water content (%)</b>			<b>Plastic Limit</b>	-
			<b>Plasticity Index</b>	-



\*Unable to obtain Liquid Limit or Plastic Limit.





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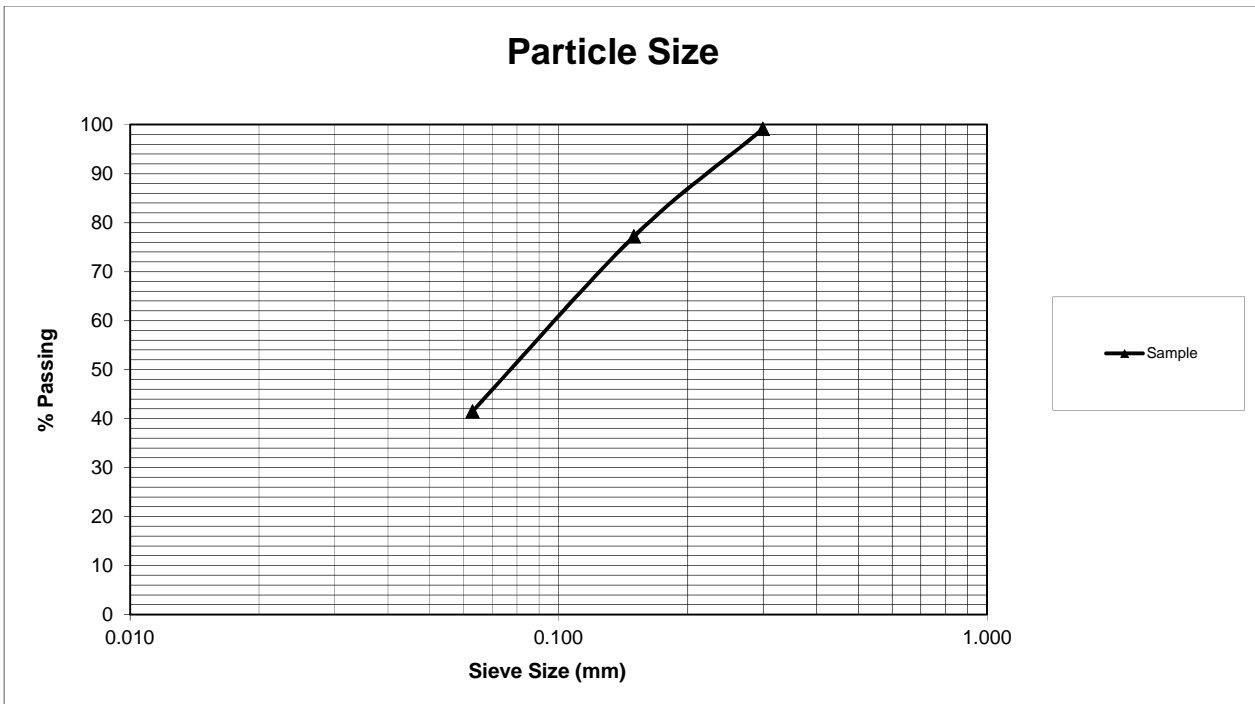
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M: 027 6565 317

**DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH**

NZS 4402: 1986 Test 2.8.1, 2.8.2

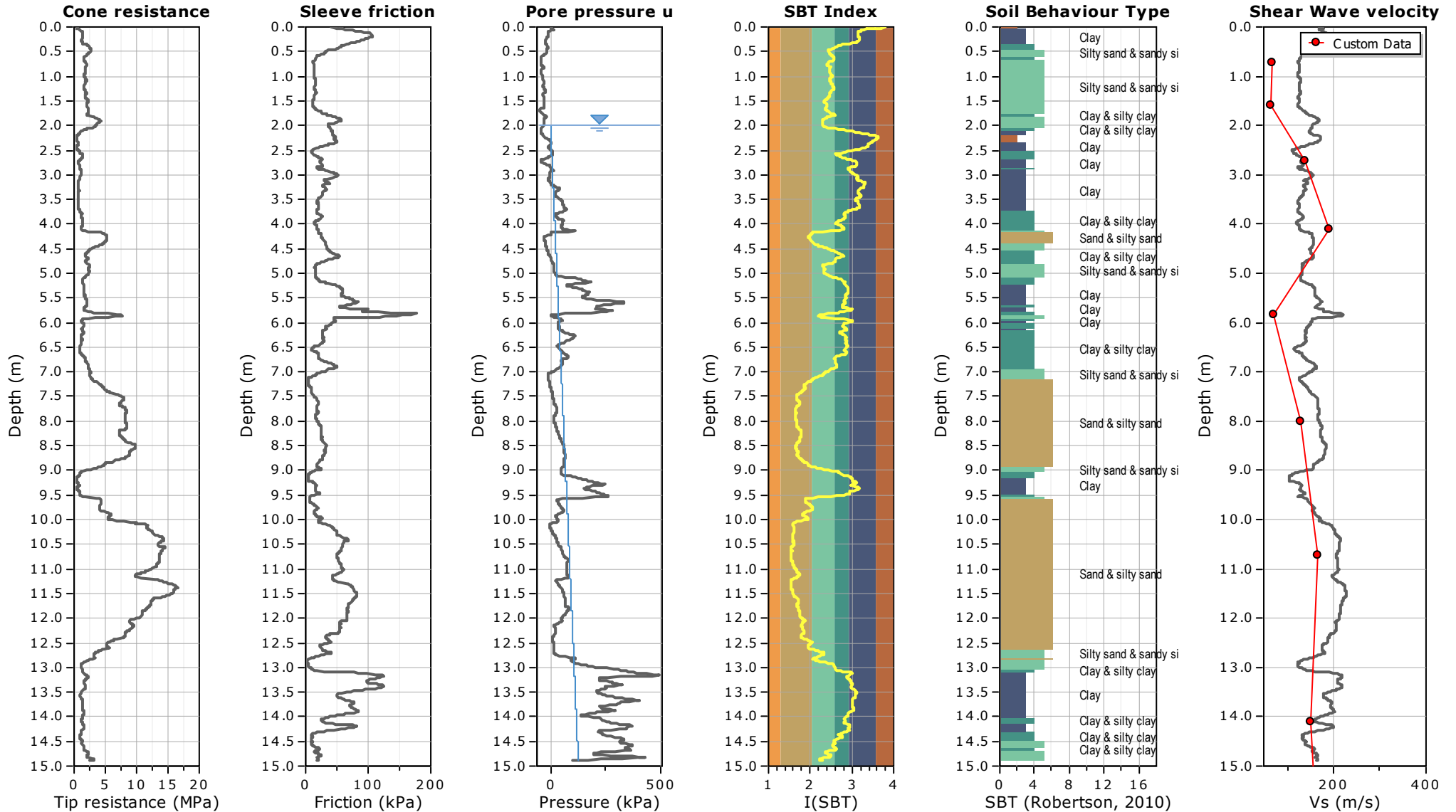
<b>Lab Job No:</b>	8378-032	<b>Sample No:</b>	C20-323
<b>Client:</b>	Miyamoto International NZ Ltd	<b>Tested By:</b>	D.P
<b>Location:</b>	2 Glovers Road HA05 (1.5-1.8m)	<b>Date:</b>	9/09/2020
<b>Date Received:</b>	8/09/2020	<b>Checked By:</b>	J.B
<b>Report No:</b>	C20-450	<b>Date:</b>	14/09/2020
<b>REF:</b>	-	<b>Page:</b>	8 of 8
<b>Sampling Method:</b>	Sampled by client - SNA	<b>Sampled By:</b>	Client
<b>Date Sampled:</b>	4/09/2020		
<b>Test Details:</b>	Wet sieving method		
<b>History:</b>	Natural		
<b>Description of Sample:</b>	Silty SAND, brownish grey, wet, no plasticity		

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	99
0.150	-	-	77
0.063	-	-	42

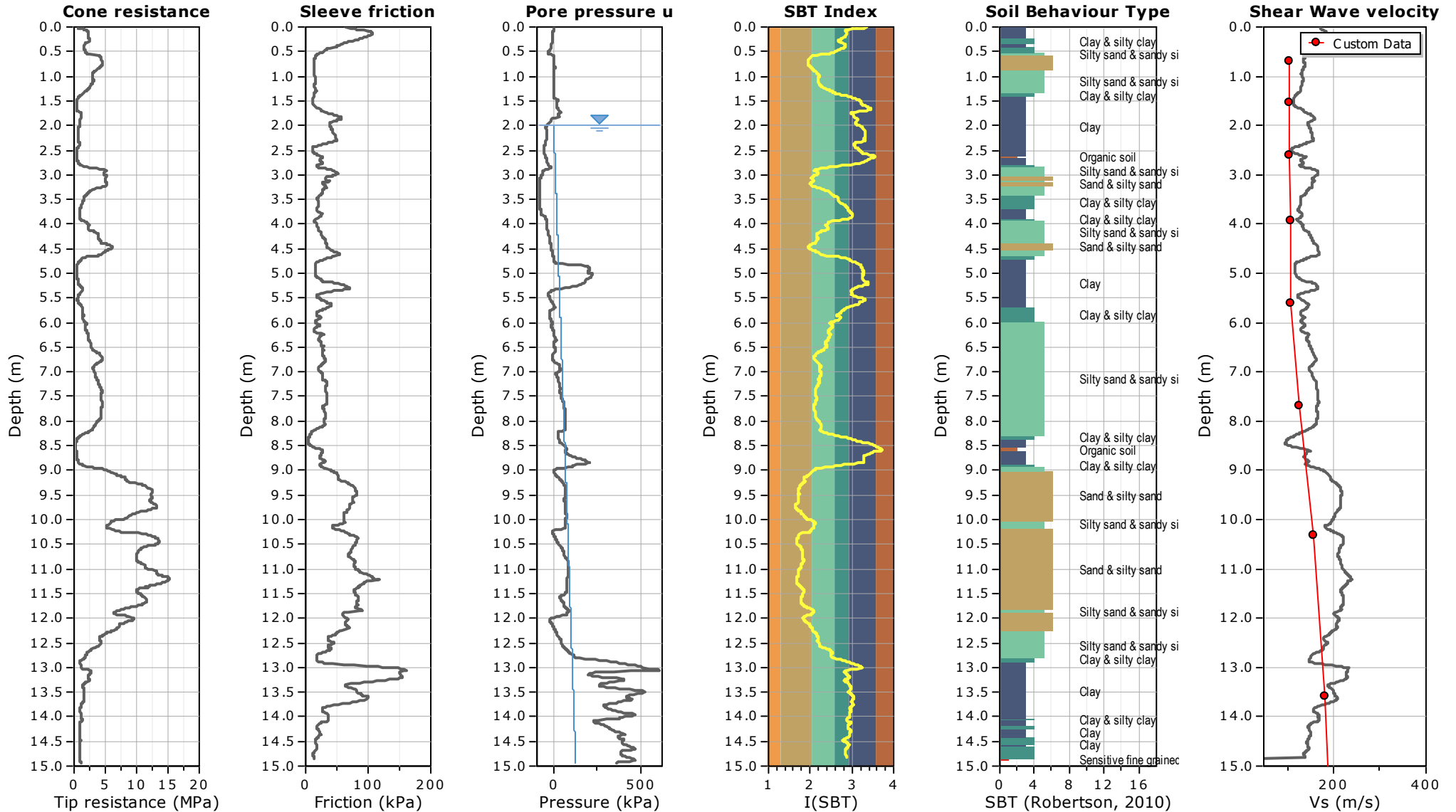


\*The percentage passing the finest sieve was obtained by difference.

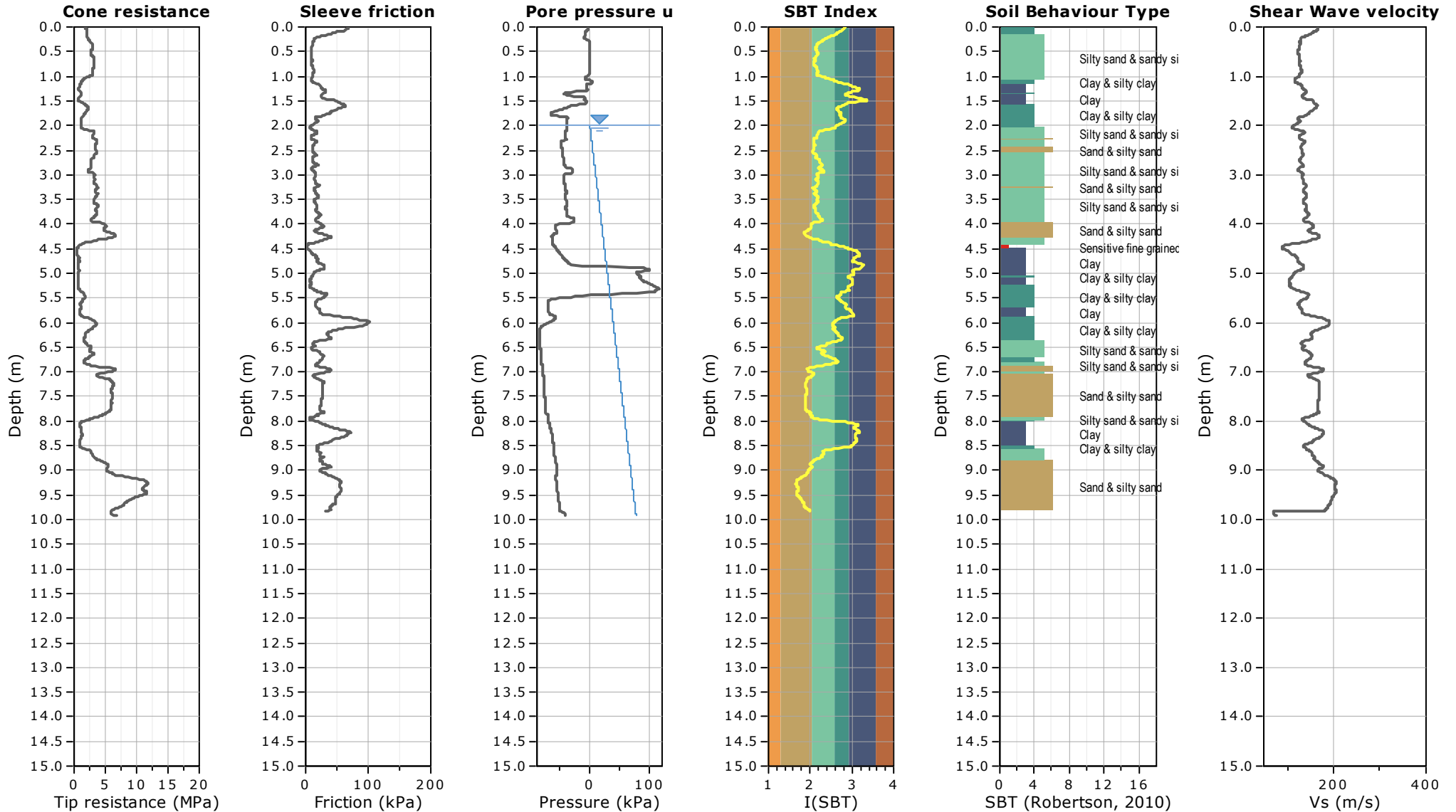
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



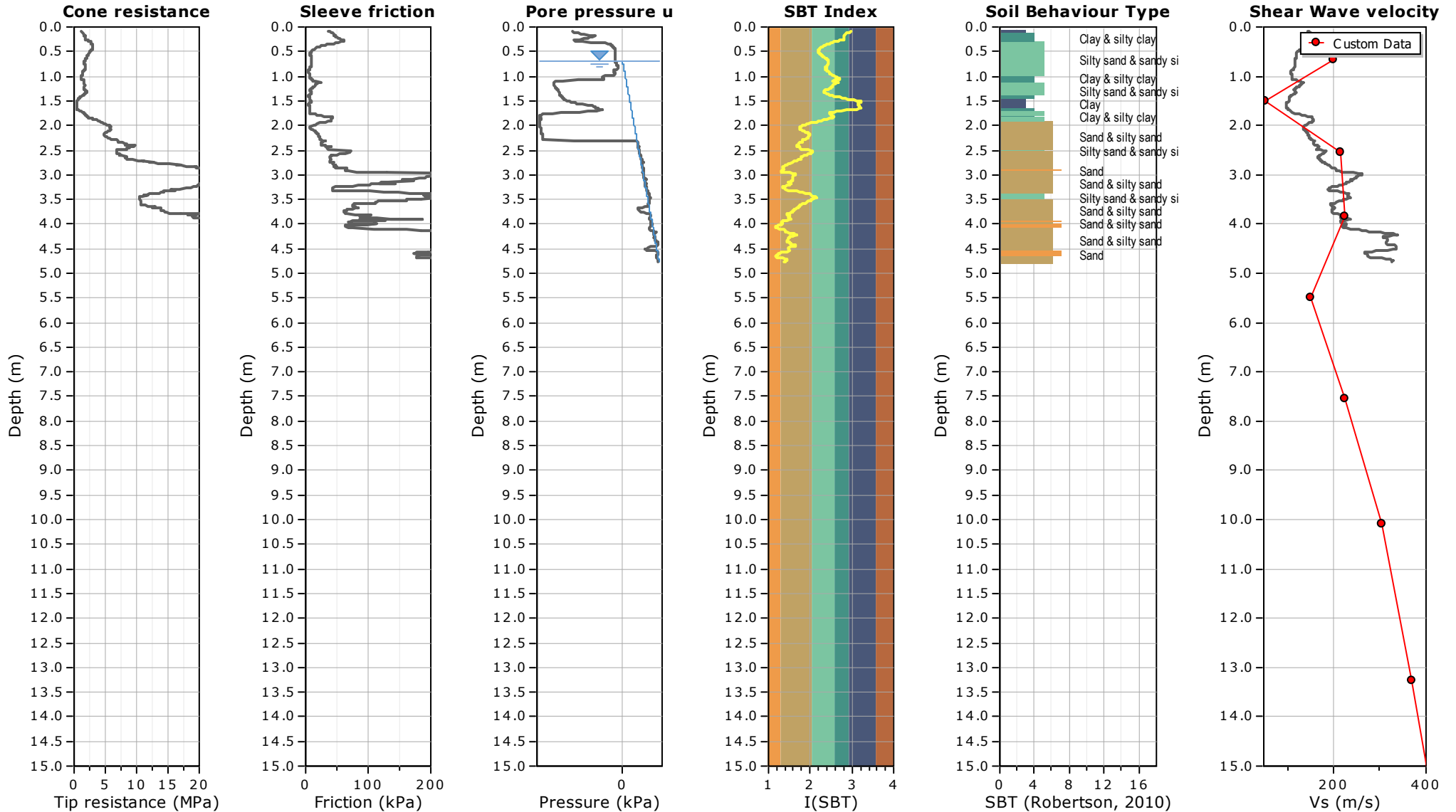
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



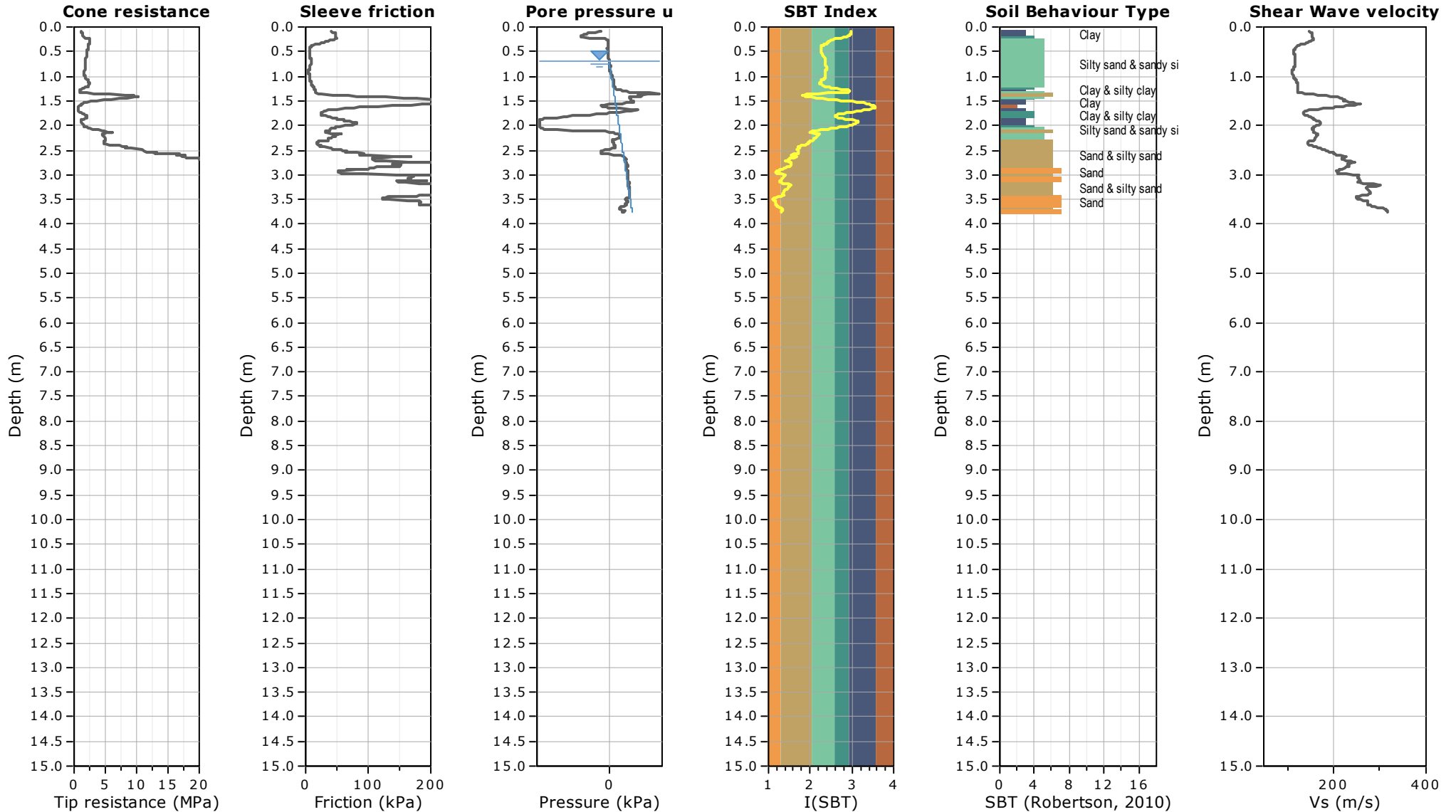
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



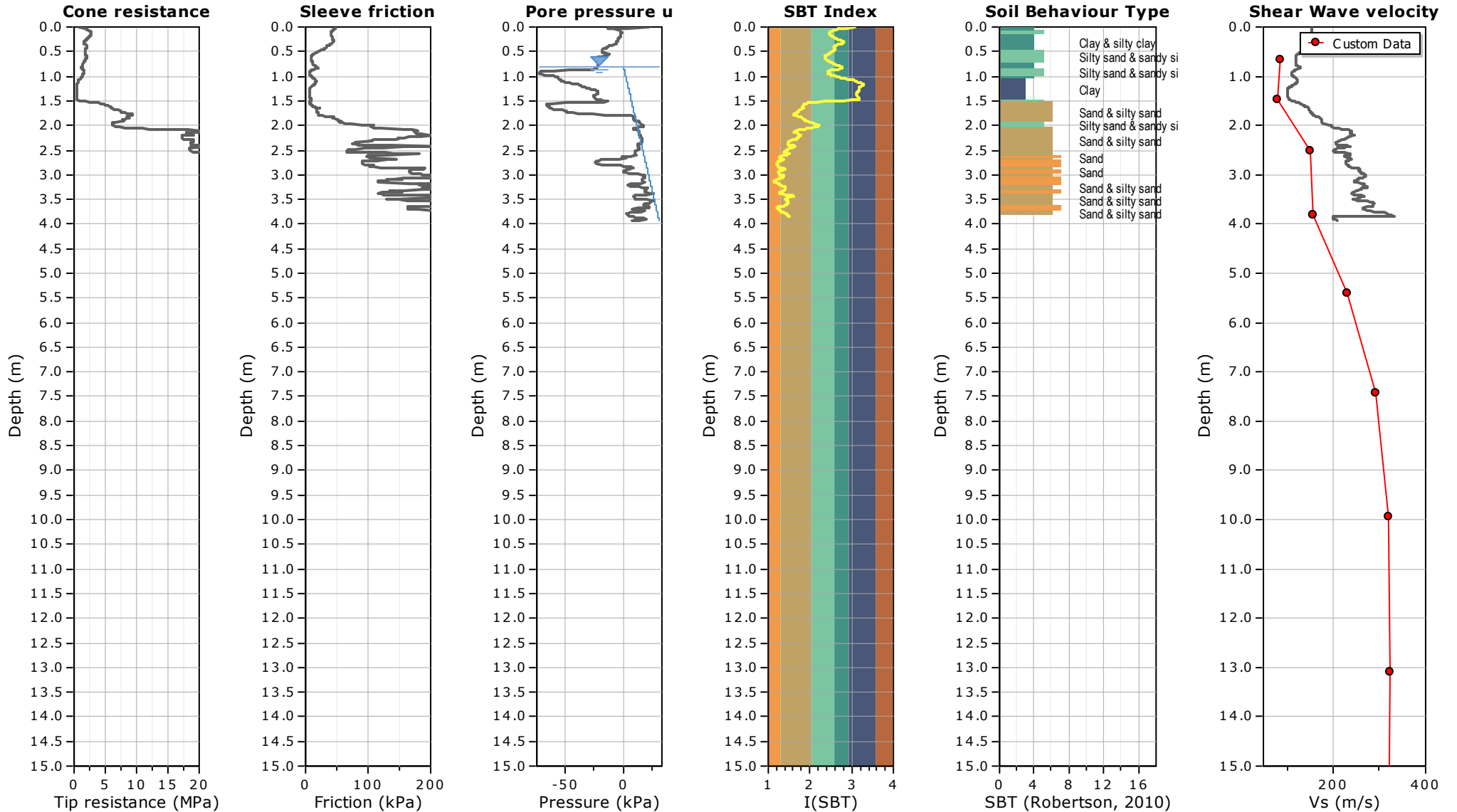
**Project: MINZ200357 - Geotechnical Investigation and Assessment**  
**Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch**



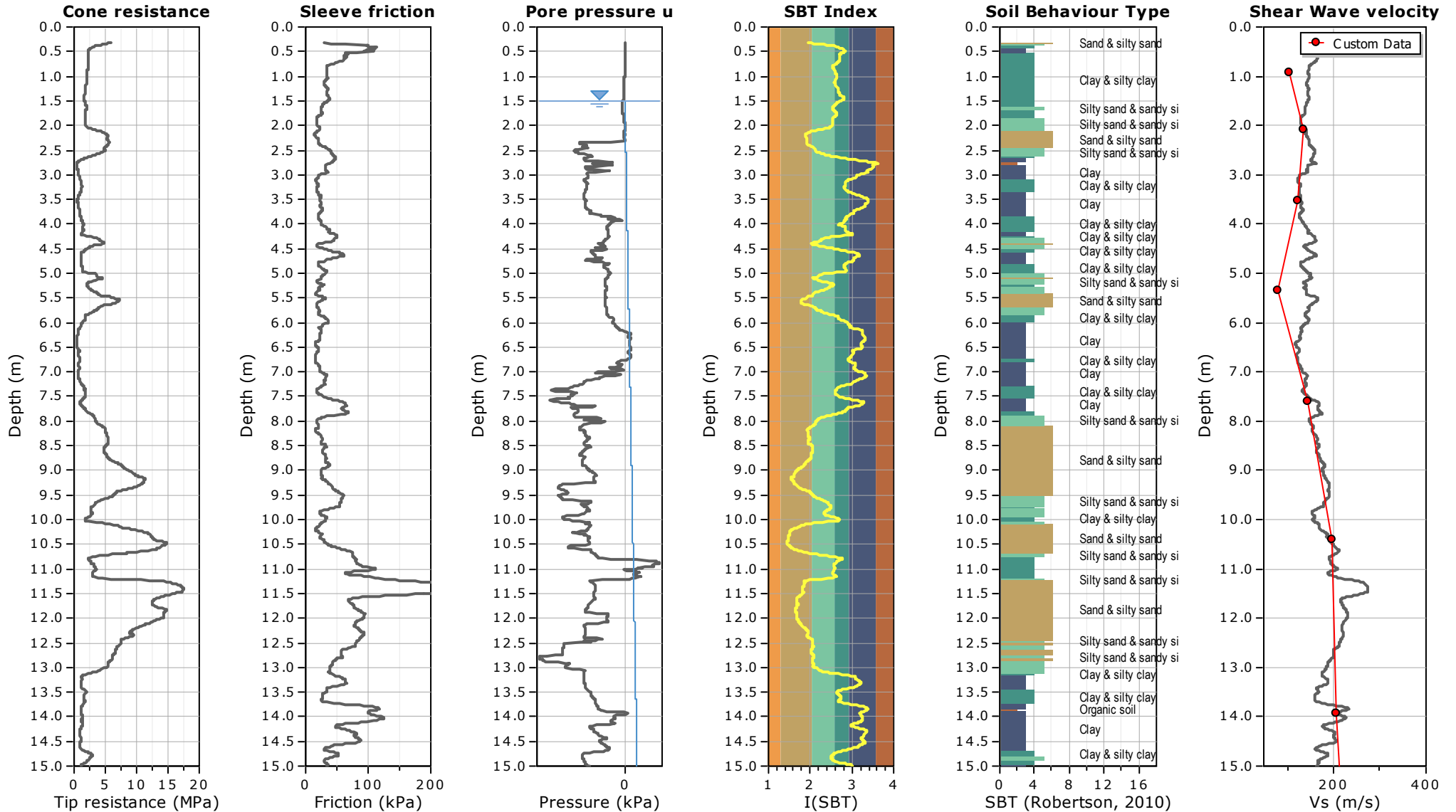
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch

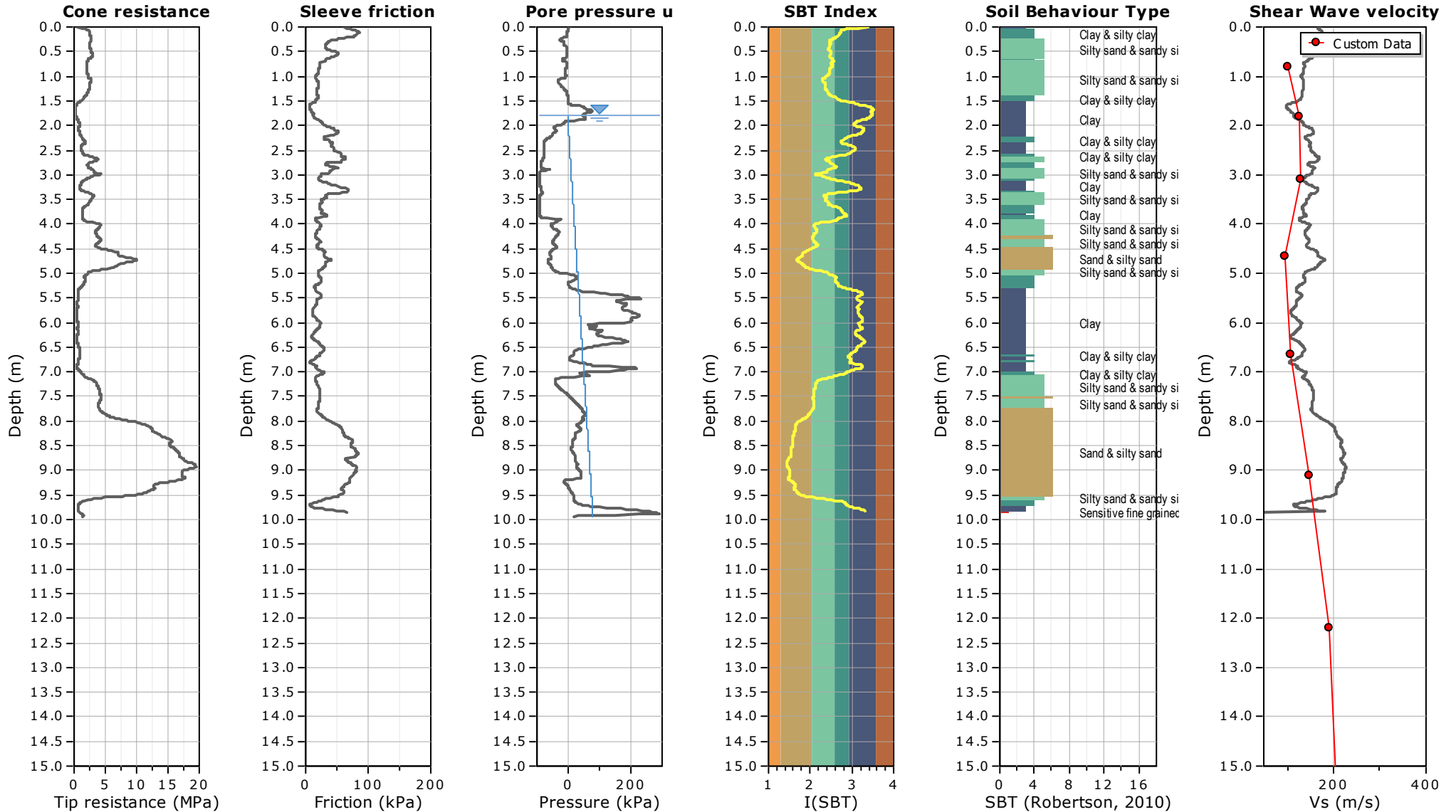


Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch

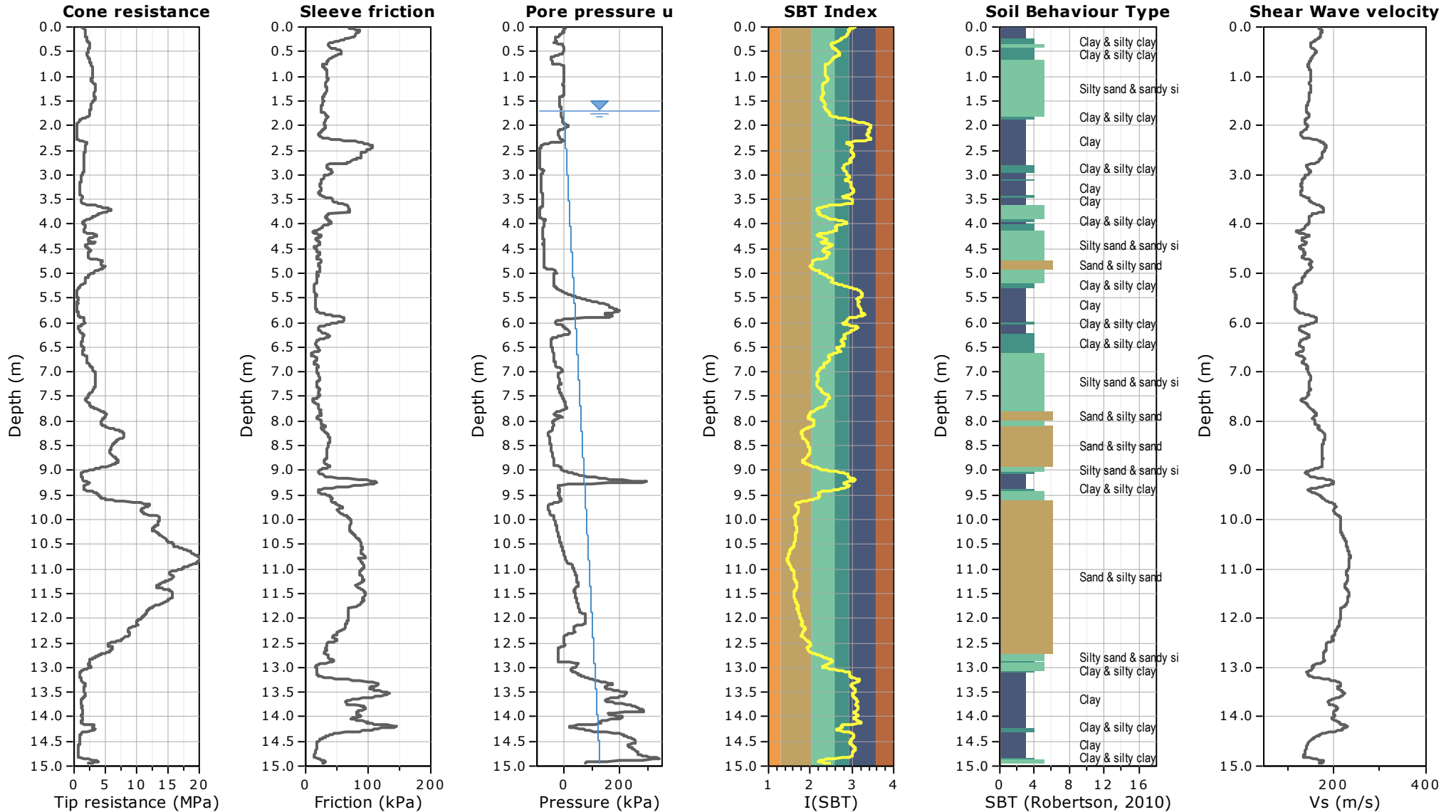




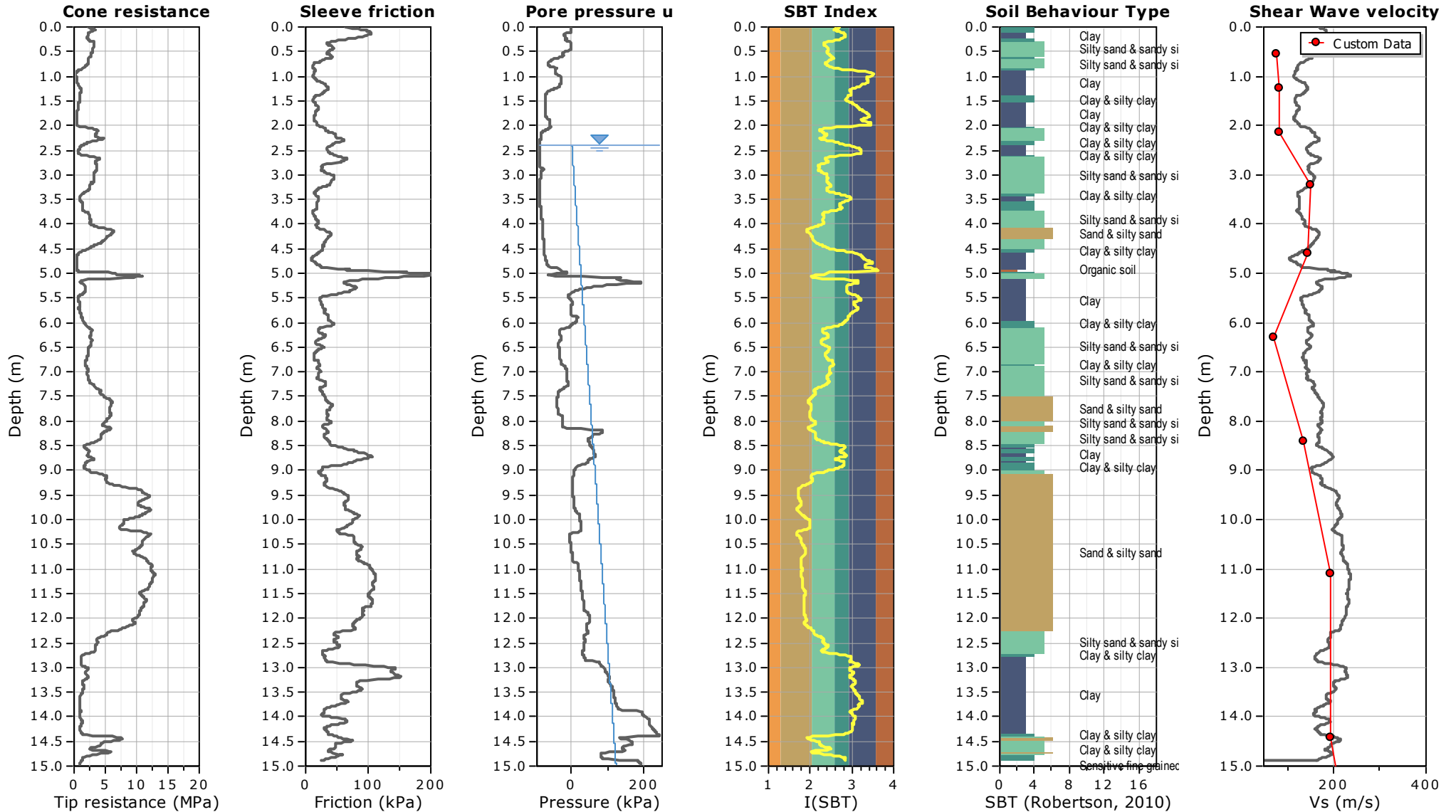
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



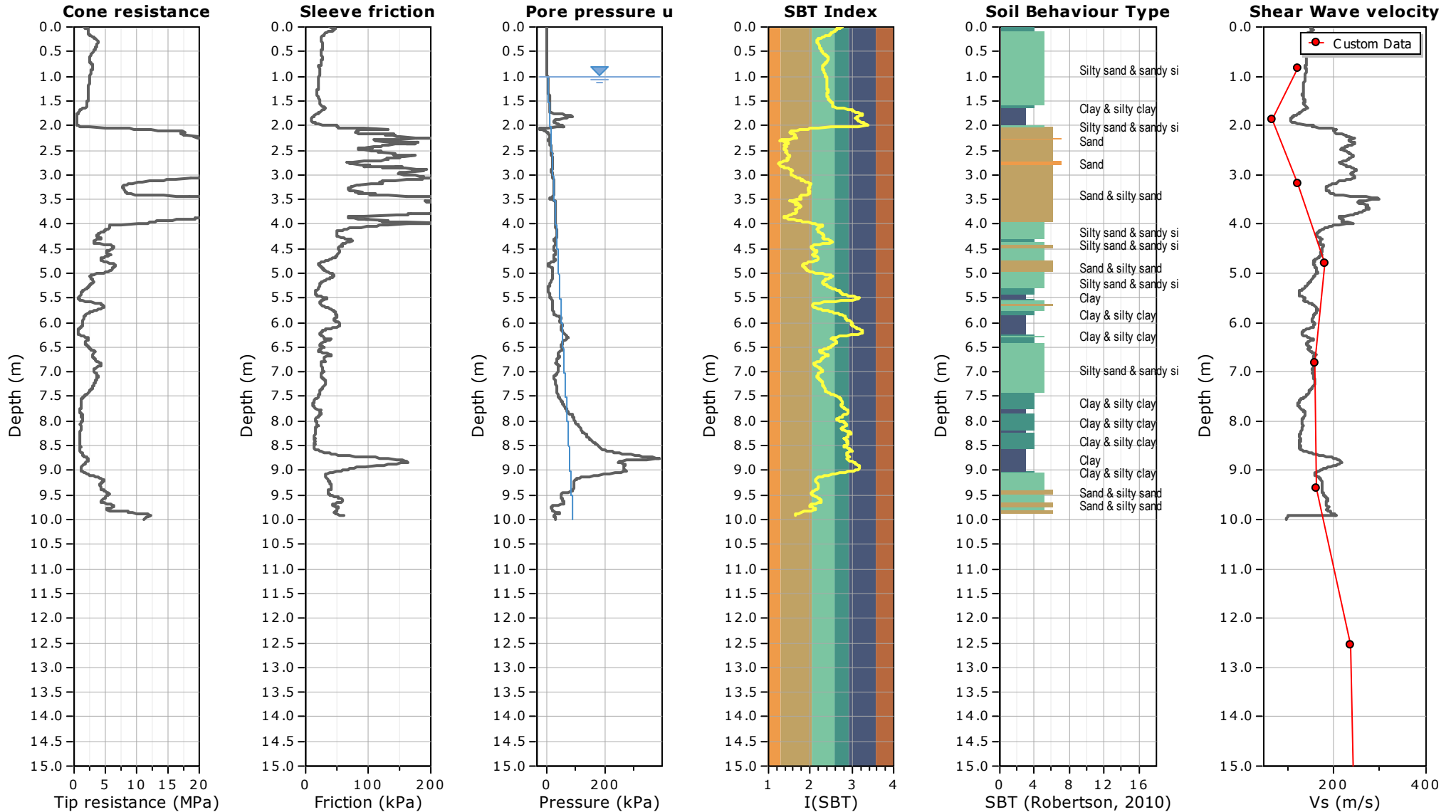
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



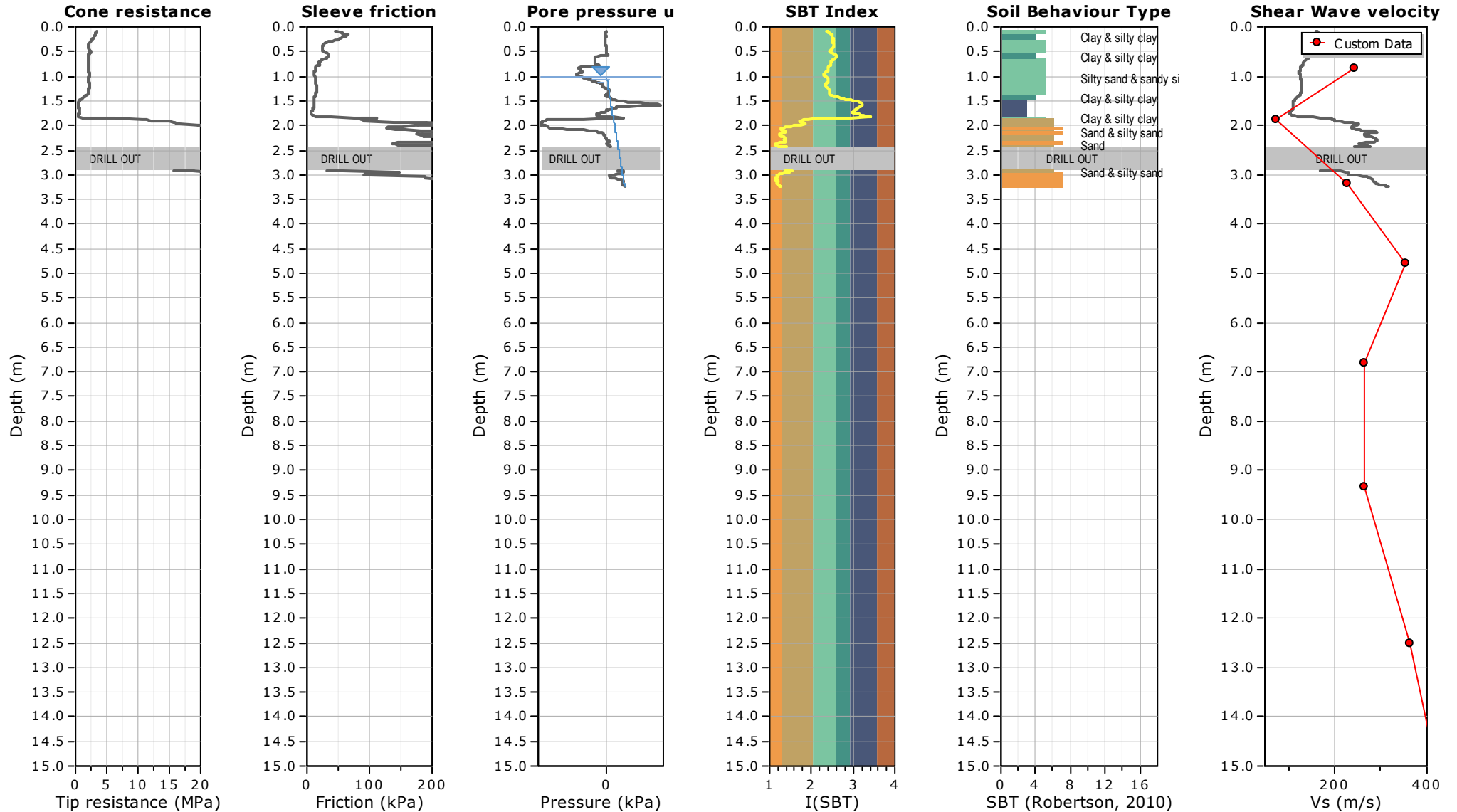
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



# **CONE PENETRATION TEST (CPT) REPORT**

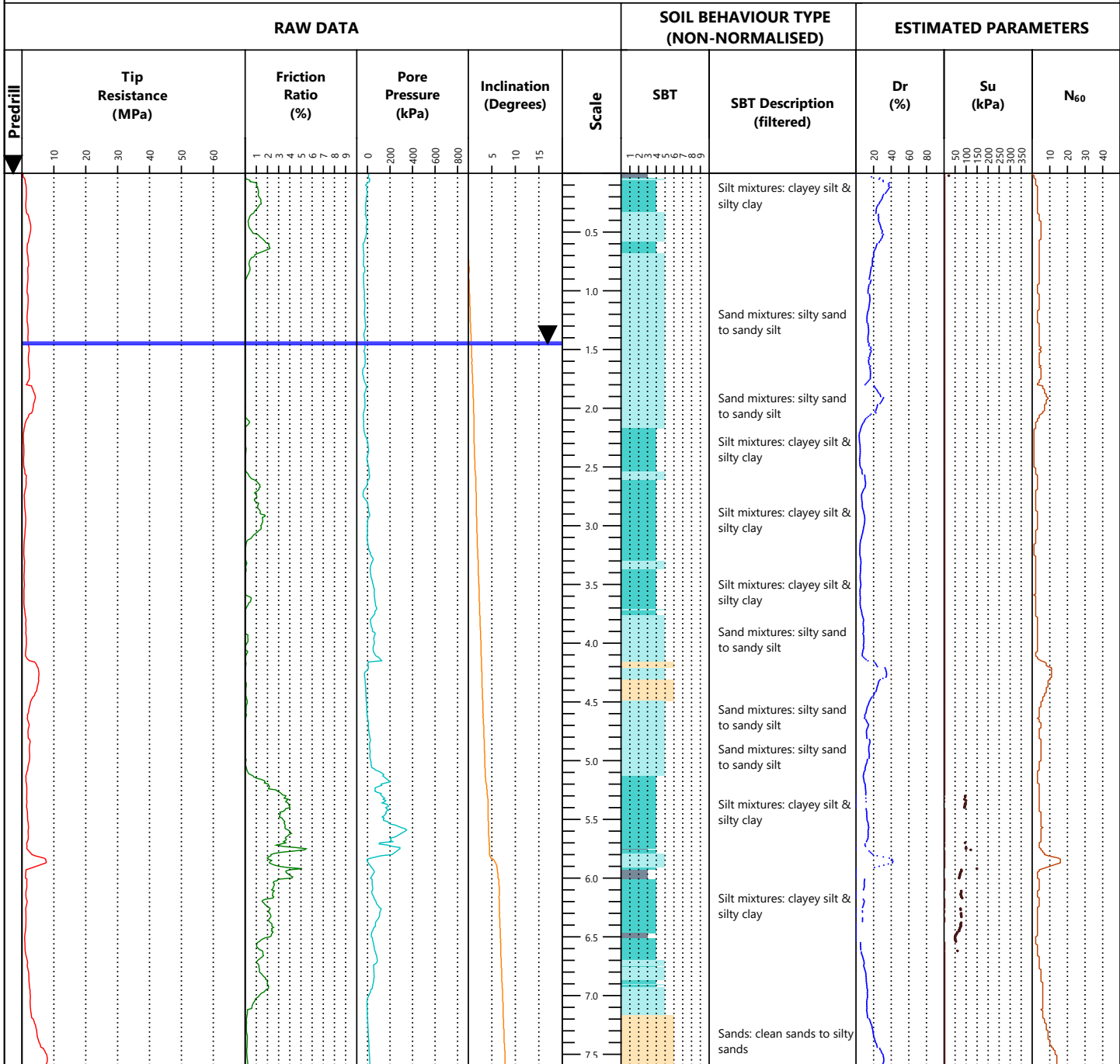


**Client: Miyamoto International NZ**

**Location: 2 Glovers Road, Christchurch**

**Printed: 20/08/2020**

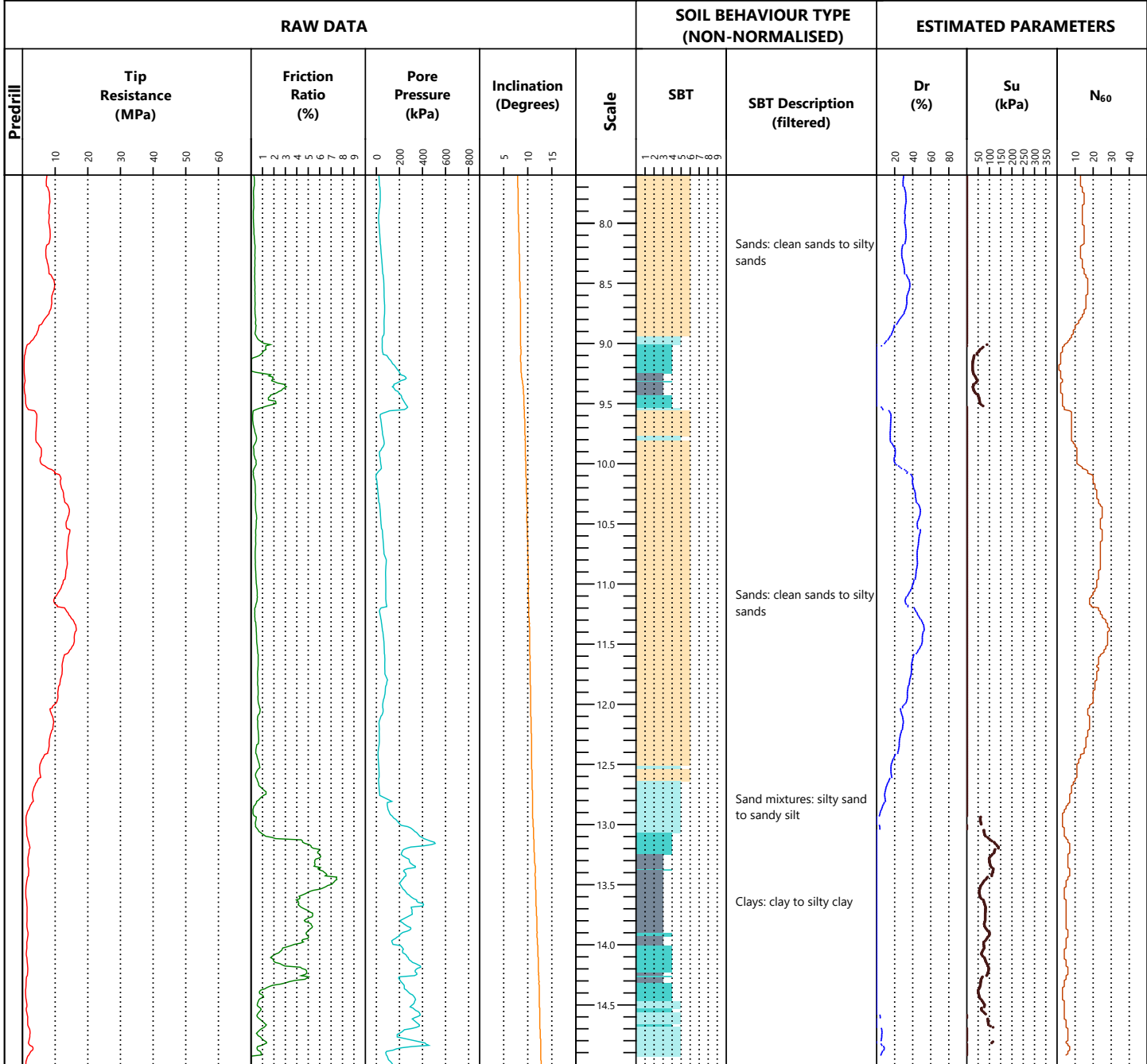
**Site Location:** 2 Glovers Road, Christchurch **Date:** 18/8/2020  
**Grid Reference:** 1564920.46m E, 5173116.23m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Equipment:** Pagani TG63-150  
**Datum:** Ground



<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKS711 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012	<b>Predrill:</b> - <b>Water Level:</b> 1.45m <b>Collapse:</b> 1.60m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table style="width:100%; border: none;"> <tr> <td style="width: 20%; border: 1px solid black; text-align: center;">0</td> <td>Undefined</td> <td style="width: 20%; border: 1px solid black; text-align: center;">5</td> <td>Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td style="border: 1px solid black; text-align: center;">1</td> <td>Sensitive fine-grained</td> <td style="border: 1px solid black; text-align: center;">6</td> <td>Sands: clean sands to silty sands</td> </tr> <tr> <td style="border: 1px solid black; text-align: center;">2</td> <td>Clay - organic soil</td> <td style="border: 1px solid black; text-align: center;">7</td> <td>Dense sand to gravelly sand</td> </tr> <tr> <td style="border: 1px solid black; text-align: center;">3</td> <td>Clays: clay to silty clay</td> <td style="border: 1px solid black; text-align: center;">8</td> <td>Stiff sand to clayey sand</td> </tr> <tr> <td style="border: 1px solid black; text-align: center;">4</td> <td>Silt mixtures: clayey silt &amp; silty clay</td> <td style="border: 1px solid black; text-align: center;">9</td> <td>Stiff fine-grained</td> </tr> </table>	0	Undefined	5	Sand mixtures: silty sand to sandy silt	1	Sensitive fine-grained	6	Sands: clean sands to silty sands	2	Clay - organic soil	7	Dense sand to gravelly sand	3	Clays: clay to silty clay	8	Stiff sand to clayey sand	4	Silt mixtures: clayey silt & silty clay	9	Stiff fine-grained
0	Undefined	5	Sand mixtures: silty sand to sandy silt																				
1	Sensitive fine-grained	6	Sands: clean sands to silty sands																				
2	Clay - organic soil	7	Dense sand to gravelly sand																				
3	Clays: clay to silty clay	8	Stiff sand to clayey sand																				
4	Silt mixtures: clayey silt & silty clay	9	Stiff fine-grained																				
<table style="width:100%; border: none;"> <tr> <td style="width: 30%;"><b>Zero load outputs (MPa)</b></td> <td style="width: 35%;"><b>Before test</b></td> <td style="width: 35%;"><b>After test</b></td> </tr> <tr> <td><b>Tip Resistance</b></td> <td>20.4528</td> <td>20.369</td> </tr> <tr> <td><b>Local Friction</b></td> <td>0.2535</td> <td>0.2535</td> </tr> <tr> <td><b>Pore Pressure</b></td> <td>3.0597</td> <td>3.0579</td> </tr> </table>	<b>Zero load outputs (MPa)</b>	<b>Before test</b>	<b>After test</b>	<b>Tip Resistance</b>	20.4528	20.369	<b>Local Friction</b>	0.2535	0.2535	<b>Pore Pressure</b>	3.0597	3.0579	<b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>										
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	<b>After test</b>																					
<b>Tip Resistance</b>	20.4528	20.369																					
<b>Local Friction</b>	0.2535	0.2535																					
<b>Pore Pressure</b>	3.0597	3.0579																					

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>  <div style="text-align: right;">Sheet 1 of 2</div>
--	--

**Site Location:** 2 Glovers Road, Christchurch **Date:** 18/8/2020  
**Grid Reference:** 1564920.46m E, 5173116.23m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



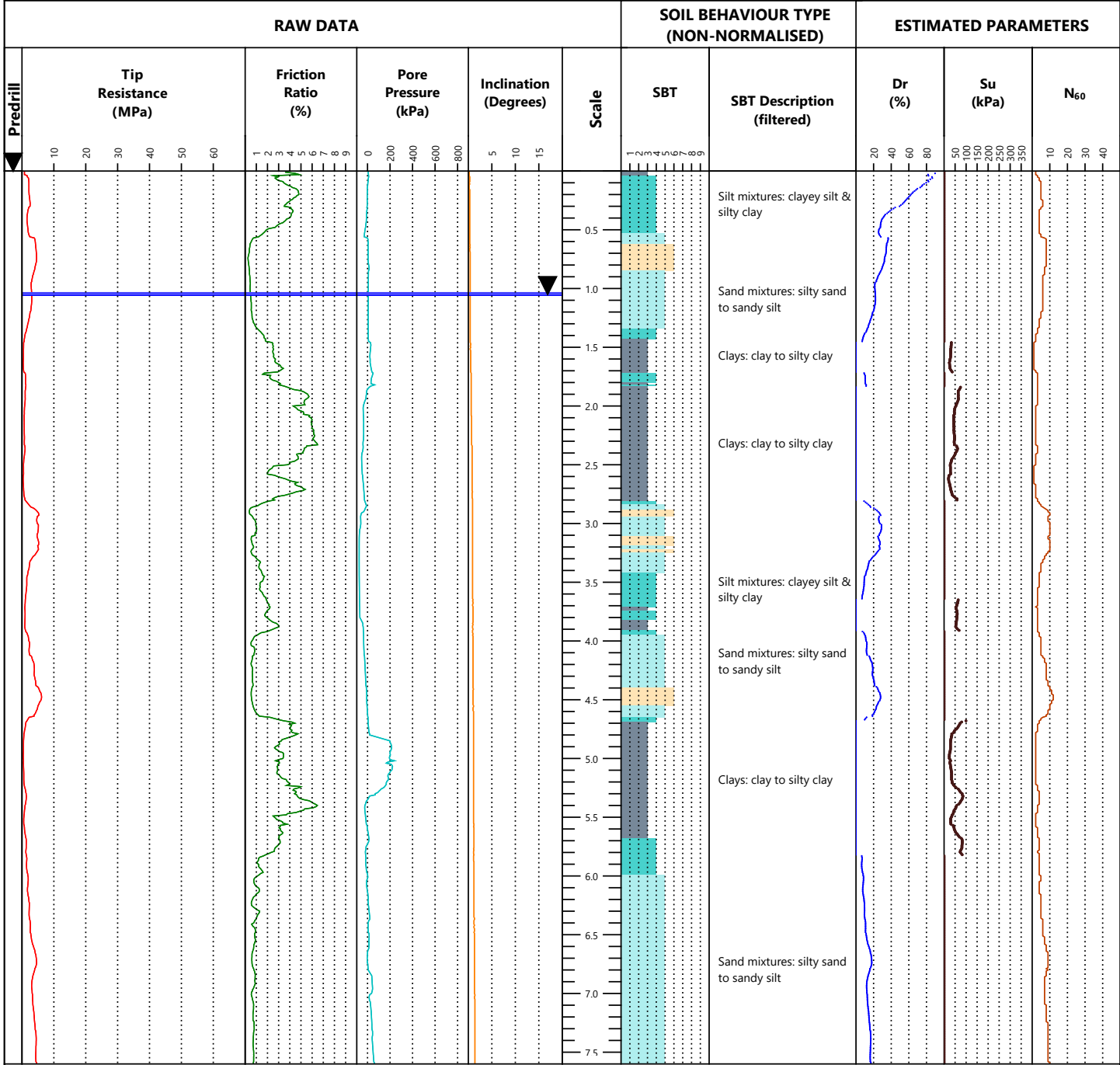
<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKS711	<b>Water Level:</b> 1.45m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 1.60m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	<b>After test</b>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	20.4528	20.369	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.2535	0.2535	<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	3.0597	3.0579	<b>6</b> Sands: clean sands to silty sands
			<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**



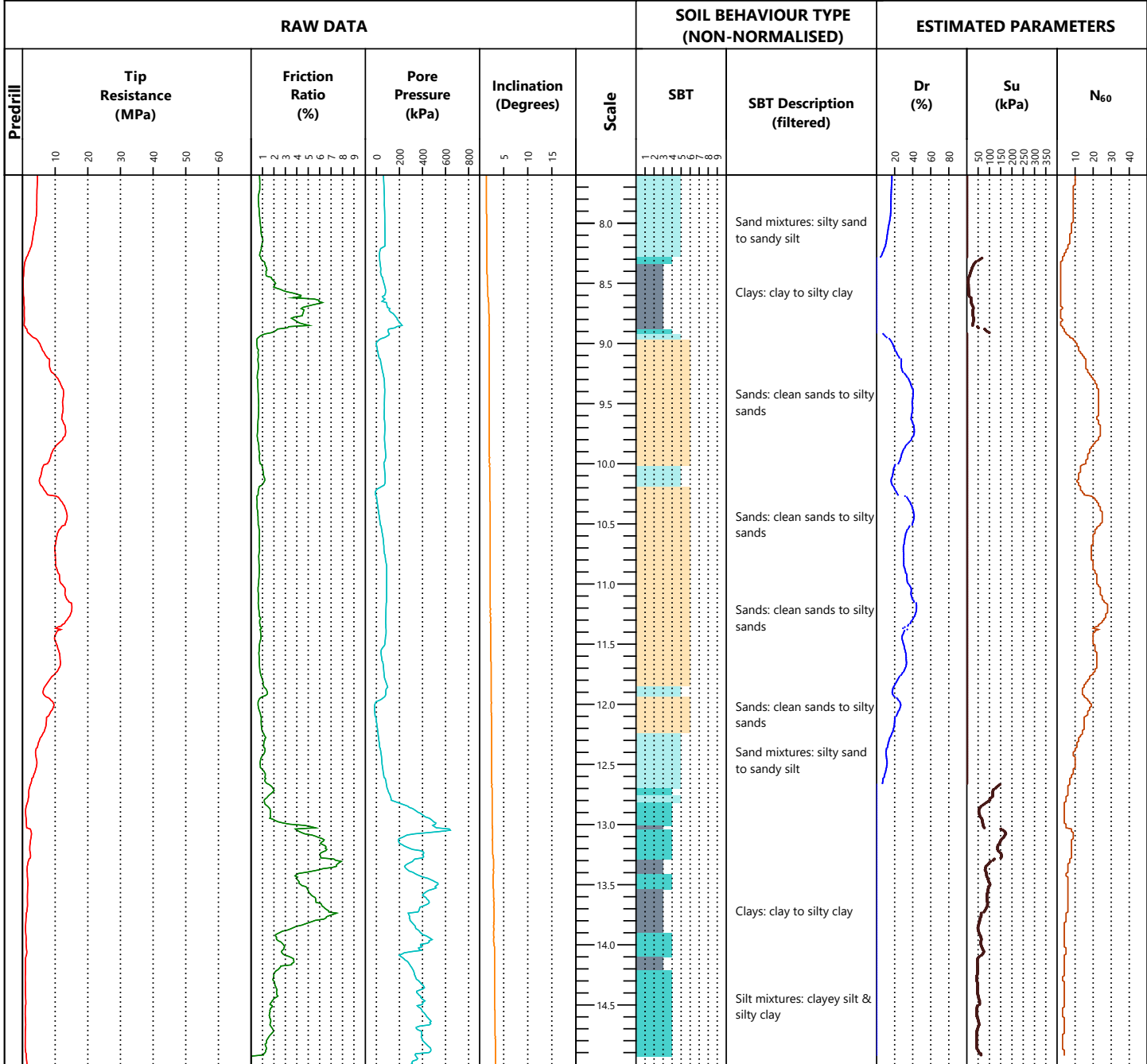
**Site Location:** 2 Glovers Road, Christchurch **Date:** 17/8/2020  
**Grid Reference:** 1564969.32m E, 5173033.19m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<p><b>Cone Type:</b> Pagani Piezocone - Compression  <b>Cone Reference:</b> MKS711  <b>Cone Area Ratio:</b> 0.79  <b>Standards:</b> ISO 22476-1:2012</p> <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>Zero load outputs (MPa)</th> <th>Before test</th> <th>After test</th> </tr> <tr> <td>Tip Resistance</td> <td>20.4004</td> <td>20.348</td> </tr> <tr> <td>Local Friction</td> <td>0.2537</td> <td>0.2536</td> </tr> <tr> <td>Pore Pressure</td> <td>3.0612</td> <td>3.0605</td> </tr> </table>	Zero load outputs (MPa)	Before test	After test	Tip Resistance	20.4004	20.348	Local Friction	0.2537	0.2536	Pore Pressure	3.0612	3.0605	<p><b>Predrill:</b> -  <b>Water Level:</b> 1.05m  <b>Collapse:</b> 2.45m</p> <p><b>Termination</b>  <b>Target Depth:</b> <input checked="" type="checkbox"/></p> <p><b>Effective Refusal</b>          Tip: <input type="checkbox"/>          Gauge: <input type="checkbox"/>          Inclinator: <input type="checkbox"/></p>	<p><b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b></p> <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td style="background-color: black; color: white;">0</td> <td>Undefined</td> <td style="background-color: #90EE90;">5</td> <td>Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td style="background-color: #FF6347;">1</td> <td>Sensitive fine-grained</td> <td style="background-color: #FFD700;">6</td> <td>Sands: clean sands to silty sands</td> </tr> <tr> <td style="background-color: #FF8C00;">2</td> <td>Clay - organic soil</td> <td style="background-color: #8B4513;">7</td> <td>Dense sand to gravelly sand</td> </tr> <tr> <td style="background-color: #4682B4;">3</td> <td>Clays: clay to silty clay</td> <td style="background-color: #808080;">8</td> <td>Stiff sand to clayey sand</td> </tr> <tr> <td style="background-color: #40E0D0;">4</td> <td>Silt mixtures: clayey silt &amp; silty clay</td> <td style="background-color: #404040;">9</td> <td>Stiff fine-grained</td> </tr> </table>	0	Undefined	5	Sand mixtures: silty sand to sandy silt	1	Sensitive fine-grained	6	Sands: clean sands to silty sands	2	Clay - organic soil	7	Dense sand to gravelly sand	3	Clays: clay to silty clay	8	Stiff sand to clayey sand	4	Silt mixtures: clayey silt & silty clay	9	Stiff fine-grained
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<p><b>Notes &amp; Limitations</b>          Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.</p>	<p><b>Remarks</b></p> <p style="text-align: right;">Sheet 1 of 2</p>
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**Site Location:** 2 Glovers Road, Christchurch **Date:** 17/8/2020  
**Grid Reference:** 1564969.32m E, 5173033.19m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



EOH: 15m

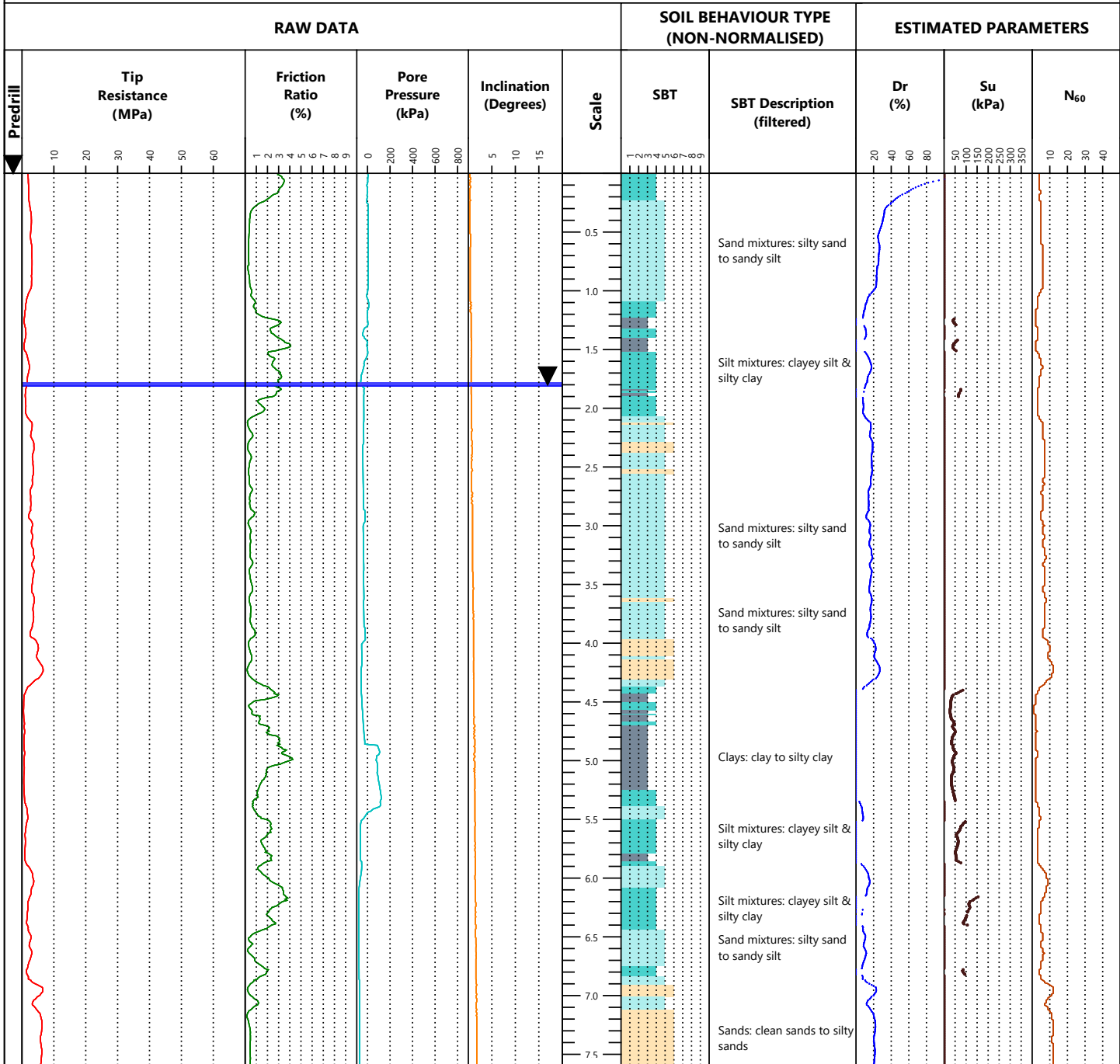
<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKS711 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012	<b>Predrill:</b> - <b>Water Level:</b> 1.05m <b>Collapse:</b> 2.45m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> 0 Undefined 1 Sensitive fine-grained 2 Clay - organic soil 3 Clays: clay to silty clay 4 Silt mixtures: clayey silt & silty clay 5 Sand mixtures: silty sand to sandy silt 6 Sands: clean sands to silty sands 7 Dense sand to gravelly sand 8 Stiff sand to clayey sand 9 Stiff fine-grained
<b>Zero load outputs (MPa)</b> <b>Tip Resistance</b> Before test: 20.4004 After test: 20.348 <b>Local Friction</b> 0.2537 0.2536 <b>Pore Pressure</b> 3.0612 3.0605	<b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>		

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

Sheet 2 of 2

**Site Location:** 2 Glovers Road, Christchurch **Date:** 13/8/2020  
**Grid Reference:** 1564902m E, 5172941.77m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



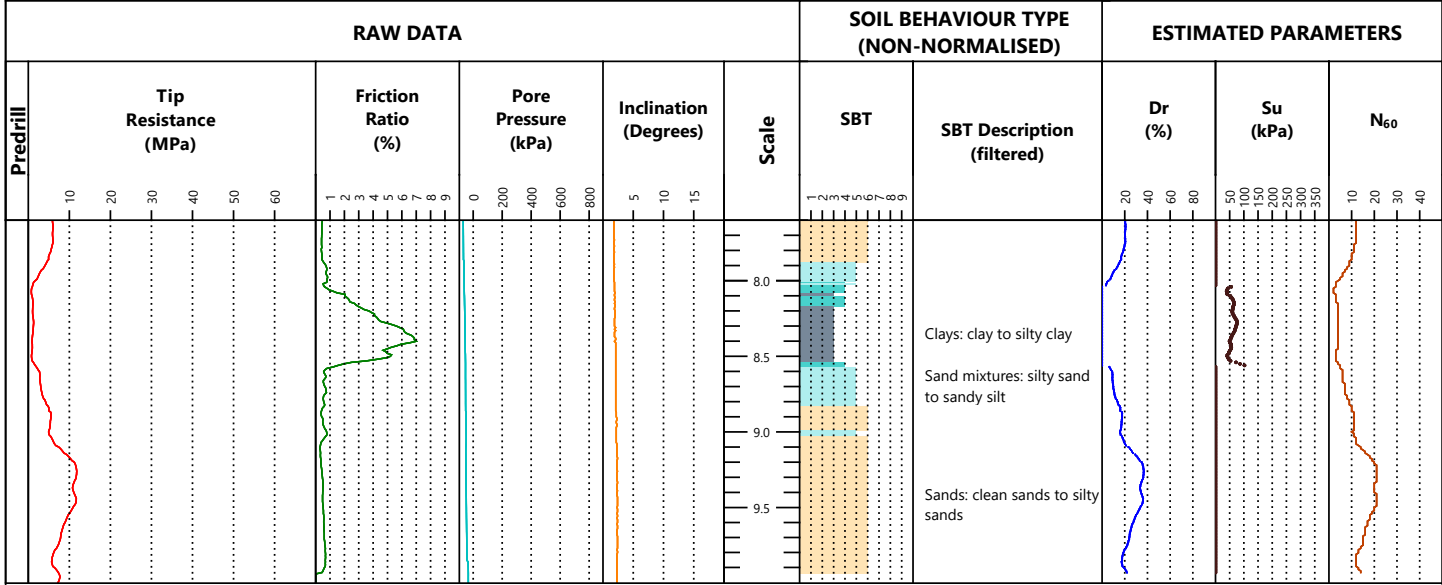
<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 1.8m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 2.70m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3554	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1187		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9596		<b>6</b> Sands: clean sands to silty sands
	0.9557		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
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**Remarks**

<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu003</b>
<b>Project:</b>	2 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

**Site Location:** 2 Glovers Road, Christchurch **Date:** 13/8/2020  
**Grid Reference:** 1564902m E, 5172941.77m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
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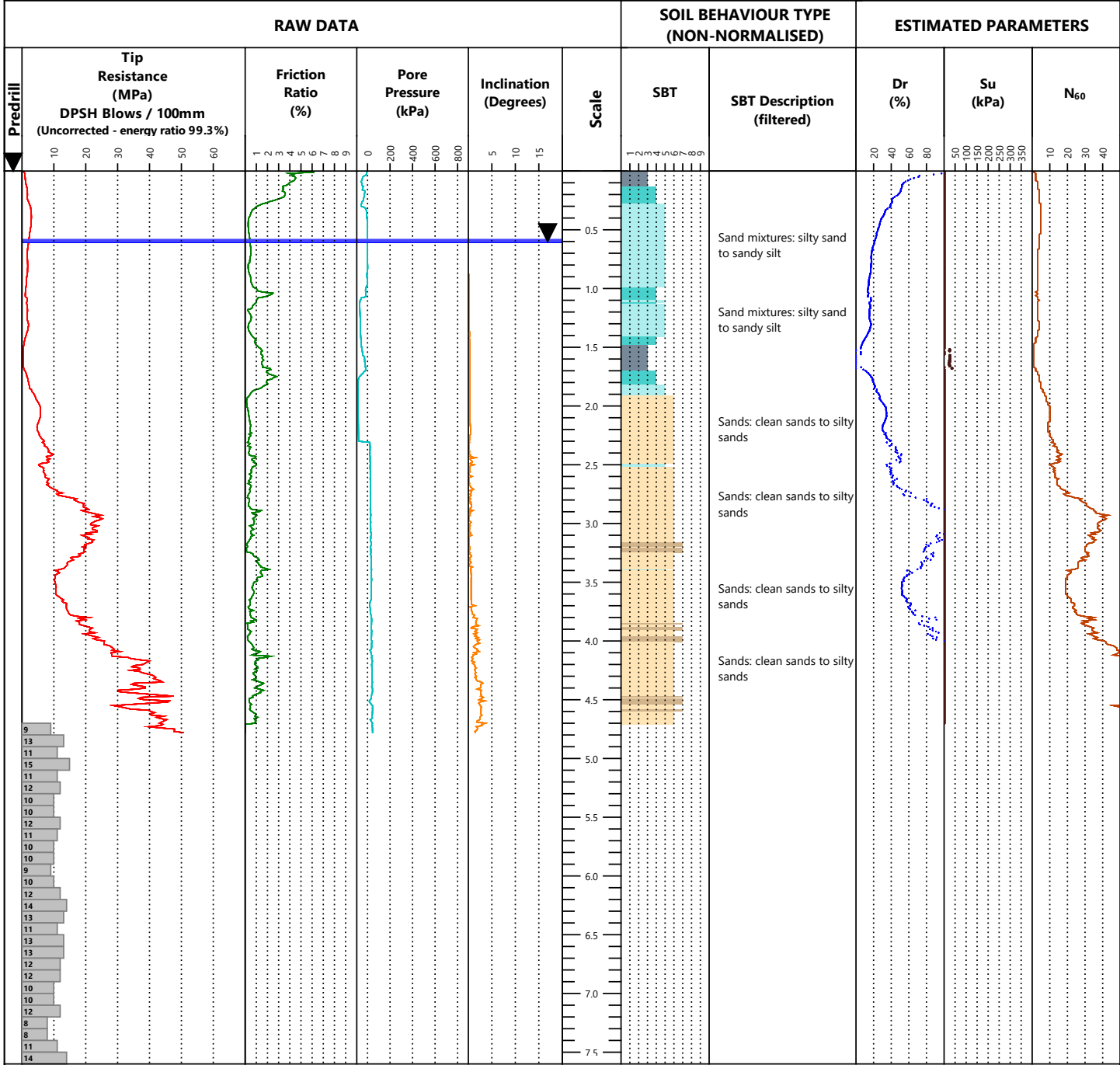


EOH: 10m

<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ328 <b>Cone Area Ratio:</b> 0.80 <b>Standards:</b> ISO 22476-1:2012  <b>Zero load outputs (MPa)</b> <table border="1"> <tr> <th>Before test</th> <th>After test</th> </tr> <tr> <td>Tip Resistance</td> <td>11.3554</td> </tr> <tr> <td>Local Friction</td> <td>0.1187</td> </tr> <tr> <td>Pore Pressure</td> <td>0.9596</td> </tr> </table>	Before test	After test	Tip Resistance	11.3554	Local Friction	0.1187	Pore Pressure	0.9596	<b>Predrill:</b> - <b>Water Level:</b> 1.8m <b>Collapse:</b> 2.70m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>  <b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="1"> <tr> <td>0</td> <td>Undefined</td> <td>5</td> <td>Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td>1</td> <td>Sensitive fine-grained</td> <td>6</td> <td>Sands: clean sands to silty sands</td> </tr> <tr> <td>2</td> <td>Clay - organic soil</td> <td>7</td> <td>Dense sand to gravelly sand</td> </tr> <tr> <td>3</td> <td>Clays: clay to silty clay</td> <td>8</td> <td>Stiff sand to clayey sand</td> </tr> <tr> <td>4</td> <td>Silt mixtures: clayey silt &amp; silty clay</td> <td>9</td> <td>Stiff fine-grained</td> </tr> </table>	0	Undefined	5	Sand mixtures: silty sand to sandy silt	1	Sensitive fine-grained	6	Sands: clean sands to silty sands	2	Clay - organic soil	7	Dense sand to gravelly sand	3	Clays: clay to silty clay	8	Stiff sand to clayey sand	4	Silt mixtures: clayey silt & silty clay	9	Stiff fine-grained
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**Site Location:** 2 Glovers Road, Christchurch **Date:** 19/8/2020  
**Grid Reference:** 1564993.47m E, 5172892.27m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.6m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.95m	<b>Effective Refusal</b>	<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>6</b> Sands: clean sands to silty sands
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>7</b> Dense sand to gravelly sand
<b>Tip Resistance</b>	11.3452	Inclinometer: <input type="checkbox"/>	<b>8</b> Stiff sand to clayey sand
<b>Local Friction</b>	0.1186		<b>9</b> Stiff fine-grained
<b>Pore Pressure</b>	0.9595		

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>
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**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150

RAW DATA					SOIL BEHAVIOUR TYPE (NON-NORMALISED)		ESTIMATED PARAMETERS			
Predrill	Tip Resistance (MPa) DPSH Blows / 100mm (Uncorrected - energy ratio 99.3%)	Friction Ratio (%)	Pore Pressure (kPa)	Inclination (Degrees)	Scale	SBT	SBT Description (filtered)	ESTIMATED PARAMETERS		
								Dr (%)	Su (kPa)	N <sub>60</sub>
9	10	1	0	5	8.0	5		20	50	10
12	10	1	0	5	8.0	5		40	100	20
13	10	1	0	5	8.0	5		60	150	30
12	10	1	0	5	8.0	5		80	200	40
5	10	1	0	5	8.0	5			250	
7	10	1	0	5	8.0	5			300	
6	10	1	0	5	8.0	5			350	
3	10	1	0	5	8.0	5				
1	10	1	0	5	8.0	5				
2	10	1	0	5	8.0	5				
2	10	1	0	5	8.0	5				
2	10	1	0	5	8.0	5				
3	10	1	0	5	8.0	5				
3	10	1	0	5	8.0	5				
3	10	1	0	5	8.0	5				
4	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
11	10	1	0	5	8.0	5				
11	10	1	0	5	8.0	5				
9	10	1	0	5	8.0	5				
10	10	1	0	5	8.0	5				
9	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
4	10	1	0	5	8.0	5				
4	10	1	0	5	8.0	5				
4	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
4	10	1	0	5	8.0	5				
4	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
9	10	1	0	5	8.0	5				
9	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
3	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
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5	10	1	0	5	8.0	5				
5	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
11	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
9	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				

EOH: 15m

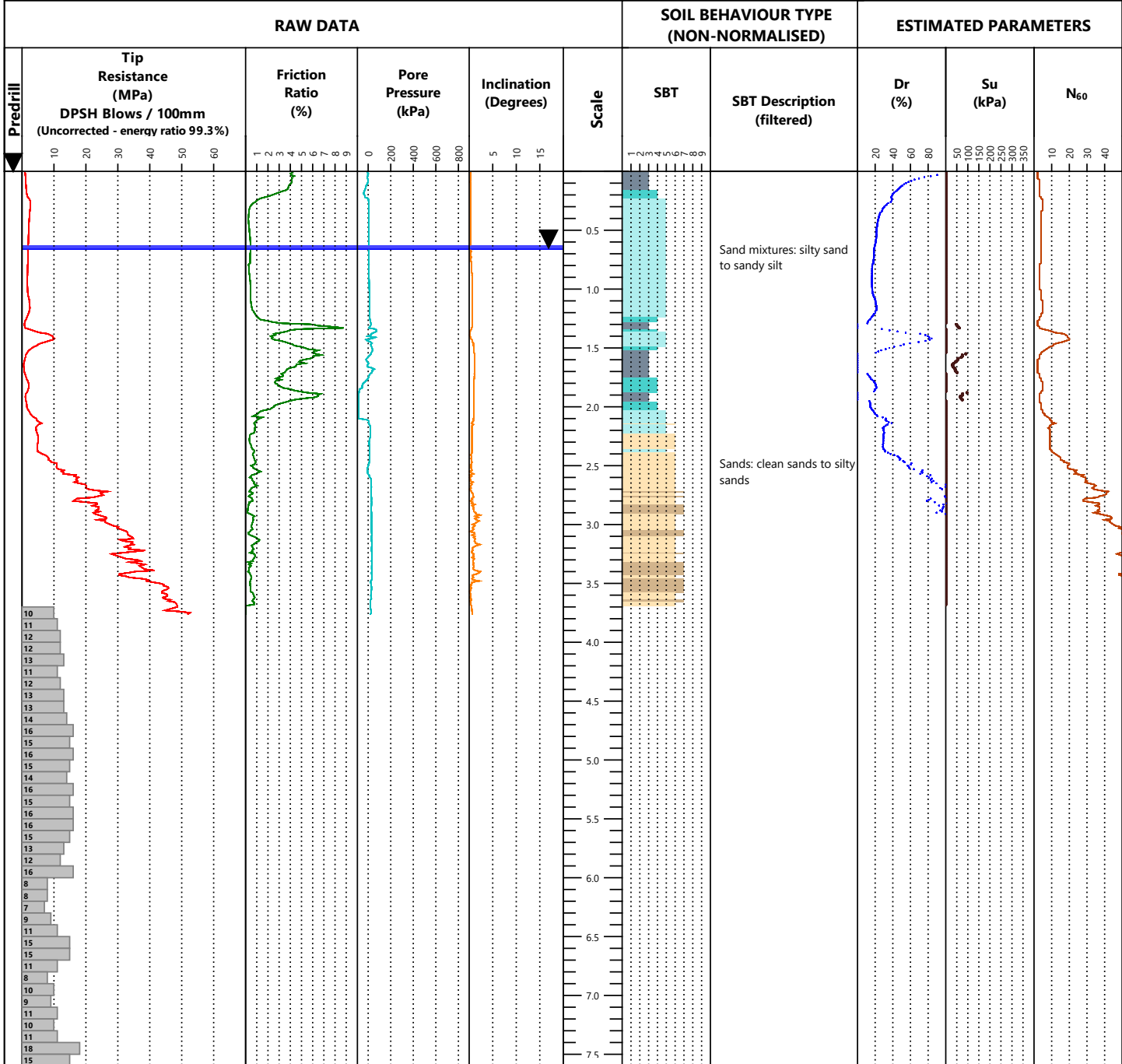
<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.6m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.95m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3452	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1186		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9595		<b>6</b> Sands: clean sands to silty sands
	0.9554		<b>7</b> Dense sand to gravelly sand
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**Remarks**

Generated with Core-GS by Geroc

**Site Location:** 2 Glovers Road, Christchurch **Date:** 19/8/2020  
**Grid Reference:** 1564945.37m E, 5172828.71m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.65m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.45m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.4066	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1183		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9587		<b>6</b> Sands: clean sands to silty sands
	0.9583		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
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 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**



<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu005</b>
<b>Project:</b>	2 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

<b>Site Location:</b> 2 Glovers Road, Christchurch	<b>Date:</b> 19/8/2020
<b>Grid Reference:</b> 1564945.37m E, 5172828.71m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> B. Wilson
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150

RAW DATA					SOIL BEHAVIOUR TYPE (NON-NORMALISED)		ESTIMATED PARAMETERS					
Predrill	Tip Resistance (MPa) DPSH Blows / 100mm (Uncorrected - energy ratio 99.3%)		Friction Ratio (%)	Pore Pressure (kPa)	Inclination (Degrees)	Scale	SBT	SBT Description (filtered)	Dr (%)		Su (kPa)	N <sub>60</sub>
	10	20	1	0	5				20	40	60	80
13	10					8.0						
12	10											
11	10											
8	10											
4	10											
2	10											
2	10											
5	10											
4	10											
10	10					8.5						
14	10											
12	10											
12	10											
12	10					9.0						
10	10											
10	10											
9	10											
12	10											
12	10					9.5						
14	10											
15	10											
17	10											
15	10											

EOH: 10m

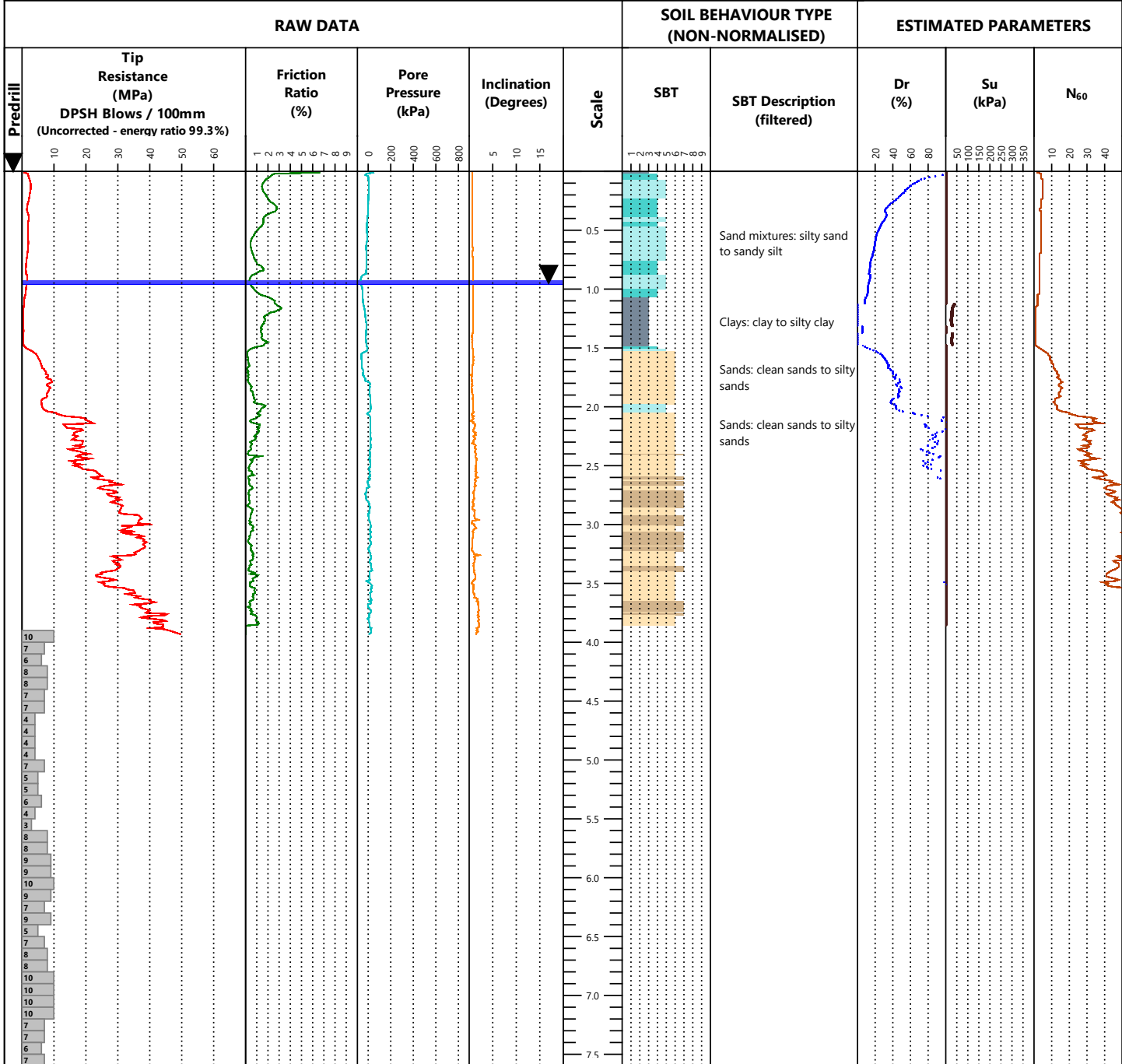
<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ328 <b>Cone Area Ratio:</b> 0.80 <b>Standards:</b> ISO 22476-1:2012  <b>Zero load outputs (MPa)</b> <table border="1"> <tr> <th>Before test</th> <th>After test</th> </tr> <tr> <td><b>Tip Resistance</b> 11.4066</td> <td>11.2583</td> </tr> <tr> <td><b>Local Friction</b> 0.1183</td> <td>0.1192</td> </tr> <tr> <td><b>Pore Pressure</b> 0.9587</td> <td>0.9583</td> </tr> </table>	Before test	After test	<b>Tip Resistance</b> 11.4066	11.2583	<b>Local Friction</b> 0.1183	0.1192	<b>Pore Pressure</b> 0.9587	0.9583	<b>Predrill:</b> - <b>Water Level:</b> 0.65m <b>Collapse:</b> 1.45m	<b>Termination</b> <b>Target Depth:</b> <input type="checkbox"/> <b>Effective Refusal</b> Tip: <input checked="" type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="1"> <tr> <td>0</td> <td>Undefined</td> <td>5</td> <td>Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td>1</td> <td>Sensitive fine-grained</td> <td>6</td> <td>Sands: clean sands to silty sands</td> </tr> <tr> <td>2</td> <td>Clay - organic soil</td> <td>7</td> <td>Dense sand to gravelly sand</td> </tr> <tr> <td>3</td> <td>Clays: clay to silty clay</td> <td>8</td> <td>Stiff sand to clayey sand</td> </tr> <tr> <td>4</td> <td>Silt mixtures: clayey silt &amp; silty clay</td> <td>9</td> <td>Stiff fine-grained</td> </tr> </table>	0	Undefined	5	Sand mixtures: silty sand to sandy silt	1	Sensitive fine-grained	6	Sands: clean sands to silty sands	2	Clay - organic soil	7	Dense sand to gravelly sand	3	Clays: clay to silty clay	8	Stiff sand to clayey sand	4	Silt mixtures: clayey silt & silty clay	9	Stiff fine-grained
Before test	After test																														
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<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>  <p style="text-align: right;">Sheet 2 of 2</p>
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Generated with Core-GS by Geroc



<b>Site Location:</b> 2 Glovers Road, Christchurch	<b>Date:</b> 13/8/2020
<b>Grid Reference:</b> 1565008.77m E, 5172744.63m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> B. Wilson
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.95m	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.40m	<b>0</b> Undefined
<b>Standards:</b> ISO 22476-1:2012	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Zero load outputs (MPa)</b>	<b>Tip:</b> <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Before test</b>	<b>Gauge:</b> <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>After test</b>	<b>Inclinometer:</b> <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Tip Resistance</b> 11.3708 11.2634		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Local Friction</b> 0.1178 0.119		<b>6</b> Sands: clean sands to silty sands
<b>Pore Pressure</b> 0.9592 0.9542		<b>7</b> Dense sand to gravelly sand
		<b>8</b> Stiff sand to clayey sand
		<b>9</b> Stiff fine-grained

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>
	Sheet 1 of 2



<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu006</b>
<b>Project:</b>	2 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

<b>Site Location:</b> 2 Glovers Road, Christchurch	<b>Date:</b> 13/8/2020
<b>Grid Reference:</b> 1565008.77m E, 5172744.63m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> B. Wilson
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150

RAW DATA					SOIL BEHAVIOUR TYPE (NON-NORMALISED)		ESTIMATED PARAMETERS			
Predrill	Tip Resistance (MPa) DPSH Blows / 100mm (Uncorrected - energy ratio 99.3%)	Friction Ratio (%)	Pore Pressure (kPa)	Inclination (Degrees)	Scale	SBT	SBT Description (filtered)	ESTIMATED PARAMETERS		
								Dr (%)	Su (kPa)	N <sub>60</sub>
5	10	1	0	5	8.0	5		20	50	10
6	10	1	0	5	8.0	5		40	100	20
7	10	1	0	5	8.0	5		60	150	30
7	10	1	0	5	8.0	5		80	200	40
11	10	1	0	5	8.0	5			250	
9	10	1	0	5	8.0	5			300	
10	10	1	0	5	8.0	5			350	
8	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
9	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
9	10	1	0	5	8.0	5				
10	10	1	0	5	8.0	5				
9	10	1	0	5	8.0	5				
9	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
4	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
9	10	1	0	5	8.0	5				
6	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
7	10	1	0	5	8.0	5				
8	10	1	0	5	8.0	5				
12	10	1	0	5	8.0	5				
12	10	1	0	5	8.0	5				
12	10	1	0	5	8.0	5				
10	10	1	0	5	8.0	5				
11	10	1	0	5	8.0	5				
14	10	1	0	5	8.0	5				
13	10	1	0	5	8.0	5				
16	10	1	0	5	8.0	5				
17	10	1	0	5	8.0	5				
14	10	1	0	5	8.0	5				
15	10	1	0	5	8.0	5				
17	10	1	0	5	8.0	5				
16	10	1	0	5	8.0	5				
17	10	1	0	5	8.0	5				
21	10	1	0	5	8.0	5				

EOH: 12.7m

<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.95m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.40m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3708	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1178		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9592		<b>6</b> Sands: clean sands to silty sands
	0.9542		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

<b>Notes &amp; Limitations</b>	<b>Remarks</b>
Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	

## TEST DETAIL

PointID: CPTu001  
Sounding: 1

**Operator:** E. Diaz  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKS711  
**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	20.4528	20.369
<b>Local Friction</b>	0.2535	0.2535
<b>Pore Pressure</b>	3.0597	3.0579

**Date:** 18/8/2020  
**Predrill:** -  
**Water Level:** 1.45m  
**Collapse:** 1.60m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu002  
Sounding: 1

**Operator:** E. Diaz  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKS711  
**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	20.4004	20.348
<b>Local Friction</b>	0.2537	0.2536
<b>Pore Pressure</b>	3.0612	3.0605

**Date:** 17/8/2020  
**Predrill:** -  
**Water Level:** 1.05m  
**Collapse:** 2.45m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu003  
Sounding: 1

**Operator:** B. Wilson  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKJ328  
**Cone Area Ratio:** 0.80

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.3554	11.3094
<b>Local Friction</b>	0.1187	0.1186
<b>Pore Pressure</b>	0.9596	0.9557

**Date:** 13/8/2020  
**Predrill:** -  
**Water Level:** 1.8m  
**Collapse:** 2.70m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu004  
Sounding: 1

**Operator:** B. Wilson  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKJ328  
**Cone Area Ratio:** 0.80

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.3452	11.2685
<b>Local Friction</b>	0.1186	0.1191
<b>Pore Pressure</b>	0.9595	0.9554

**Date:** 19/8/2020  
**Predrill:** -  
**Water Level:** 0.6m  
**Collapse:** 1.95m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu005  
Sounding: 1

**Operator:** B. Wilson  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKJ328  
**Cone Area Ratio:** 0.80

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.4066	11.2583
<b>Local Friction</b>	0.1183	0.1192
<b>Pore Pressure</b>	0.9587	0.9583

**Date:** 19/8/2020  
**Predrill:** -  
**Water Level:** 0.65m  
**Collapse:** 1.45m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

# TEST DETAIL

---

PointID: CPTu006

Sounding: 1

**Operator:** B. Wilson

**Cone Type:** Pagani Piezocone - Compression

**Cone Reference:** MKJ328

**Cone Area Ratio:** 0.80

**Date:** 13/8/2020

**Predrill:** -

**Water Level:** 0.95m

**Collapse:** 1.40m

**Termination**

**Target Depth:**

**Effective Refusal**

Tip:

Gauge:

Inclinometer:

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.3708	11.2634
<b>Local Friction</b>	0.1178	0.119
<b>Pore Pressure</b>	0.9592	0.9542

# CPT CALIBRATION AND TECHNICAL NOTES

These notes describe the technical specifications and associated calibration references pertaining to the Pagani piezocone types measuring cone resistance, sleeve friction, inclination and pore pressure (piezocone, 10cm<sup>2</sup>)

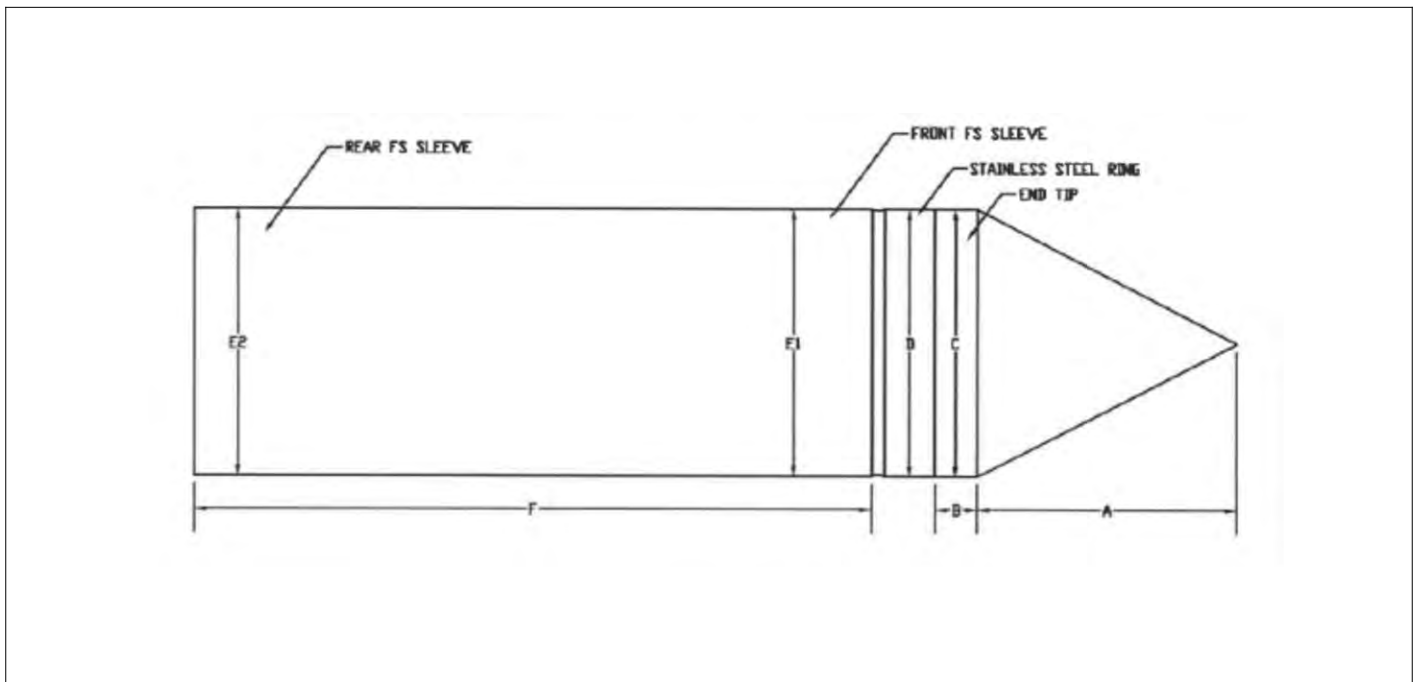
## Dimensions

Dimensional specifications are detailed below. All tolerances are routinely checked prior to testing and measurements taken are electronically recorded. All records are kept on file and available on request.

## Technical specifications

	Tip	Friction	Pore Pressure	Inclination
<b>Maximum Measuring Range:</b>	50 - 100 MPa	1.60 MPa	2.50 MPa	0° - 20°
<b>Resolution:</b>	24 bit	24 bit	24 bit	12 bit
<b>Accuracy:</b>	0.005 MPa	0.04 MPa	0.04 MPa	0.5°

<b>Length:</b>	320 mm	<b>Weight:</b>	1.8 kg
<b>Diameter:</b>	35.8 mm	<b>Opening angle of bit:</b>	60°
<b>Cone base area:</b>	10 cm <sup>2</sup>	<b>Side sleeve surfaces:</b>	150 cm <sup>2</sup>
<b>Cone area ratio:</b>	0.80	<b>Tip and Local Friction sensor displacement:</b>	80 mm



# CONE CERTIFICATES



## CONE CALIBRATION CERTIFICATE N° Z087/19

Calibrated system (Sistema tarato):  
 Serial number **Mkj328**  
 Sensor  
 Max. Capacity [MPa]: **100**  
 Scaling Factor: **195500**  
 Tip net area ratio ( $a_p$ ): **0,80**  
 Sleeve net ratio ( $b_p$ ): **0,00**

Addressee (destinatario):  
 LANDTEST  
 307 Cashel street, Christchurch  
 New Zealand

Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 200 kN  
 Serial Number 138913  
 Power press:  
 Manufacturer Easydur Italiana  
 Model Aura 20T  
 Serial Number 29084

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)

Last verification date: 15/01/2019  
 Certificate N. LAT 091 2019-014  
 Temperature of calibration 22°C  
 Humidity 53%

Factory calibration in accordance with ASTM D5778-13



## CONE CALIBRATION CERTIFICATE N° Z087/19

Calibrated system (Sistema tarato):  
 Serial number **Mkj328**  
 Sensor  
 Max. Capacity [kPa]: **1600**  
 Scaling Factor: **30696**

Addressee (destinatario):  
 LANDTEST  
 307 Cashel street, Christchurch  
 New Zealand

Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 50 kN  
 Serial Number 65495  
 Power press:  
 Manufacturer Easydur Italiana  
 Model Aura 10T  
 Serial Number 29002

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)

The adapted calibration procedure has been developed according to the suggestions given by Prof. Paul W. Mayne (Georges Institute of Technology) and Prof. Diego La Presti (University of Pisa)

Cone calibrated by **Cludio**

Date of issue 27/06/2019



## CONE CALIBRATION CERTIFICATE N° Z087/19

Calibrated system (Sistema tarato):  
 Serial number **Mkj328**  
 Sensor  
 Max. Capacity [kPa]: **2500**  
 Scaling Factor: **16963**  
 Sensor  
 Max. Inclination [°]: **20**  
 Scaling Factor: **140137**

Addressee (destinatario):  
 LANDTEST  
 307 Cashel street, Christchurch  
 New Zealand

Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Pressure Generator:  
 Manufacturer AEP transducers  
 Model GPM500  
 Digital Indicator:  
 Manufacturer AEP transducers  
 Model LAB DMM  
 Serial Number 301796

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)

The adapted calibration procedure has been developed according to the suggestions given by Prof. Paul W. Mayne (Georges Institute of Technology) and Prof. Diego La Presti (University of Pisa)

Date of issue 27/06/2019

# CONE CERTIFICATES



## CONE CALIBRATION CERTIFICATE N° Z024/20

Calibrated system (Sistema tarato):  
 Serial number **Mks711**  
 Sensor  
 Max. Capacity [MPa]: **100**  
 Sealing Factor: **190780**  
 Tip net area ratio (a<sub>b</sub>): **0,79**  
 Sleeve net ratio (b<sub>s</sub>): **0,00**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 200 kN  
 Serial Number 138913  
 Power press: Easydur Italiana  
 Model Aura 20T  
 Serial Number 29084

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 Certificate N. LAT 091 2020-015  
 Temperature of calibration 22°C  
 Humidity 45%  
 Factory calibration in accordance with ASTM D5778-12



## CONE CALIBRATION CERTIFICATE N° Z024/20

Calibrated system (Sistema tarato):  
 Serial number **Mks711**  
 Sensor  
 Max. Capacity [kPa]: **1600**  
 Sealing Factor: **31343**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 50 kN  
 Serial Number 65495  
 Power press: Easydur Italiana  
 Model Aura 10T  
 Serial Number 29002

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 The adopted calibration procedure has been developed acc Prof. Paul W. Mayne (Georgia Institute of technology) and  
 Cone calibrated by



## CONE CALIBRATION CERTIFICATE N° Z024/20

Calibrated system (Sistema tarato):  
 Serial number **Mks711**  
 Sensor  
 Max. Capacity [kPa]: **2500**  
 Sealing Factor: **10298**  
 Sensor  
 Max. Inclination [°]: **20**  
 Sealing Factor: **280277**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Pressure Generator:  
 Manufacturer MENSOR  
 Model CPC 4000  
 Serial Number 41000V56  
 Sensor Descr Silicon Pressure Transducer  
 Sensor Serial Number 41000SYF

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 28/02/2019  
 Certificate N. 162632  
 Temperature of calibration 22°C  
 Humidity 45%  
 Factory calibration in accordance with ASTM D5778-12

# **CONE PENETRATION TEST (CPT) REPORT**



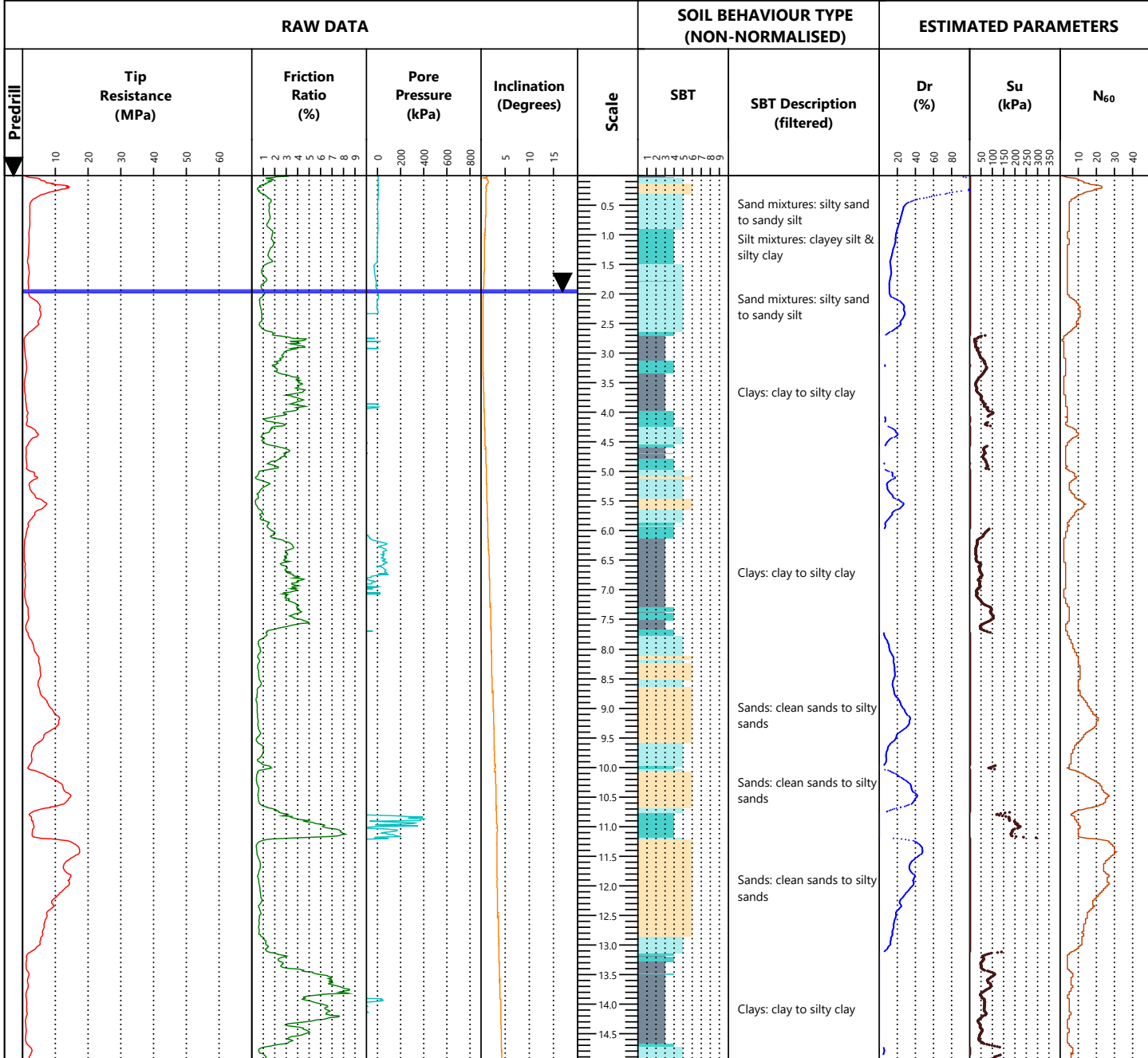
**Client: Miyamoto International NZ**

**Location: 2-4 Glovers Road, Christchurch**

**Printed: 29/09/2020**



**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 24/9/2020  
**Grid Reference:** 1564970.4m E, 5173158.32m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



EOH: 15m

<b>Cone Type:</b> Pagani Piezocone - Compression		<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>	
<b>Cone Reference:</b> MKJ329		<b>Water Level:</b> 1.96m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined	<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Cone Area Ratio:</b> 0.79		<b>Collapse:</b> 2.0m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained	<b>6</b> Sands: clean sands to silty sands
<b>Standards:</b> ISO 22476-1:2012			Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil	<b>7</b> Dense sand to gravelly sand
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	<b>After test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay	<b>8</b> Stiff sand to clayey sand
<b>Tip Resistance</b>	11.9412	11.8737	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay	<b>9</b> Stiff fine-grained
<b>Local Friction</b>	0.1606	0.161			
<b>Pore Pressure</b>	1.4594	1.262			

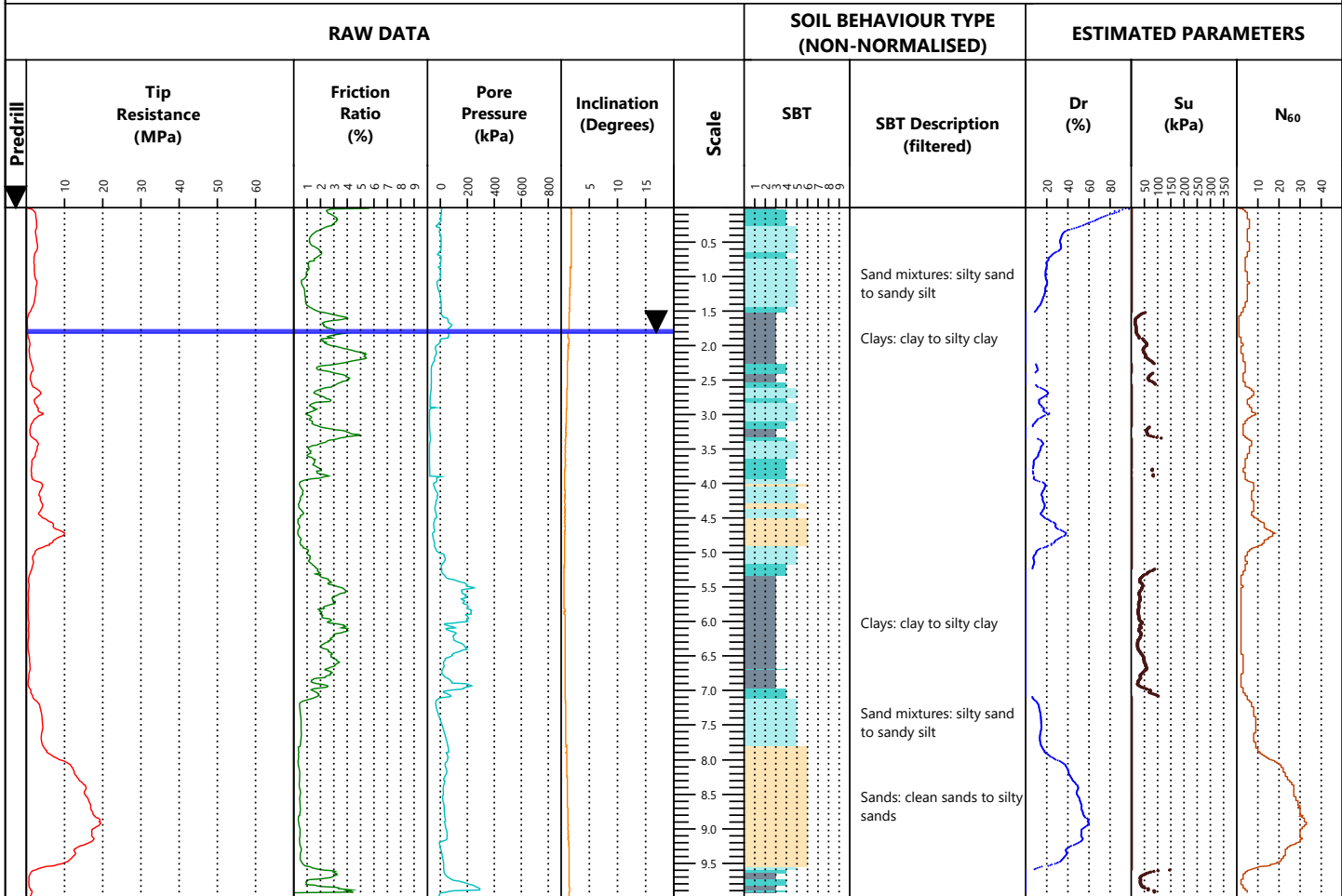
**Notes & Limitations**  
Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**  
Invalid pore water pressure data from 2.33m.

Sheet 1 of 1

<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu008</b>
<b>Project:</b>	2-4 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 24/9/2020  
**Grid Reference:** 1565034.78m E, 5173124.87m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



EOH: 10m

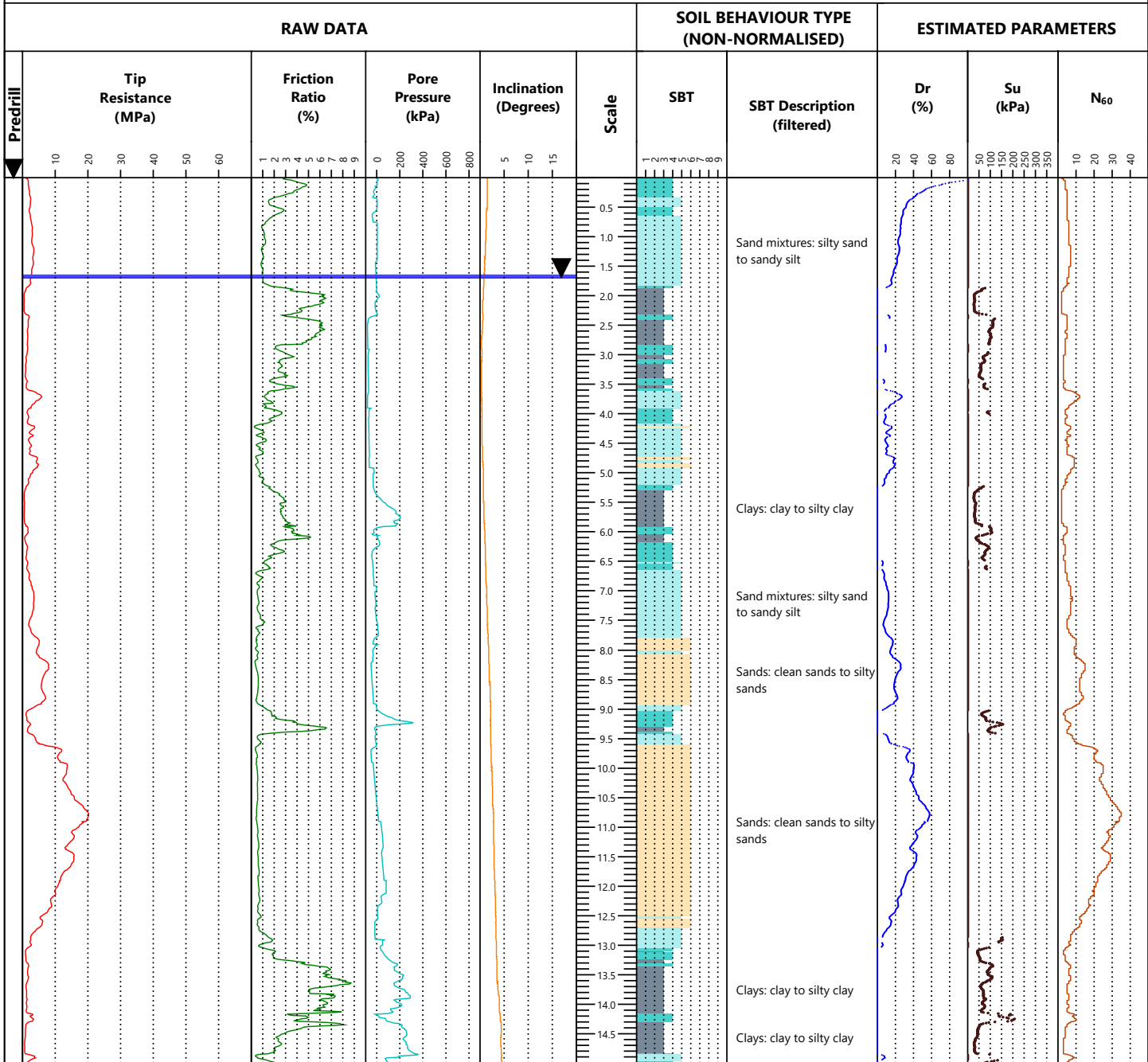
<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ329 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012	<b>Predrill:</b> - <b>Water Level:</b> 1.8m <b>Collapse:</b> 2.2m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> 0 Undefined 1 Sensitive fine-grained 2 Clay - organic soil 3 Clays: clay to silty clay 4 Silt mixtures: clayey silt & silty clay 5 Sand mixtures: silty sand to sandy silt 6 Sands: clean sands to silty sands 7 Dense sand to gravelly sand 8 Stiff sand to clayey sand 9 Stiff fine-grained
<b>Zero load outputs (MPa)</b> <b>Tip Resistance</b> 11.9516 <b>Local Friction</b> 0.1609 <b>Pore Pressure</b> 1.459	<b>Before test</b> 11.8425 0.1614 1.4561	<b>After test</b> 11.8425 0.1614 1.4561	<b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

Sheet 1 of 1

**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 24/9/2020  
**Grid Reference:** 1564969.64m E, 5173086.81m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150

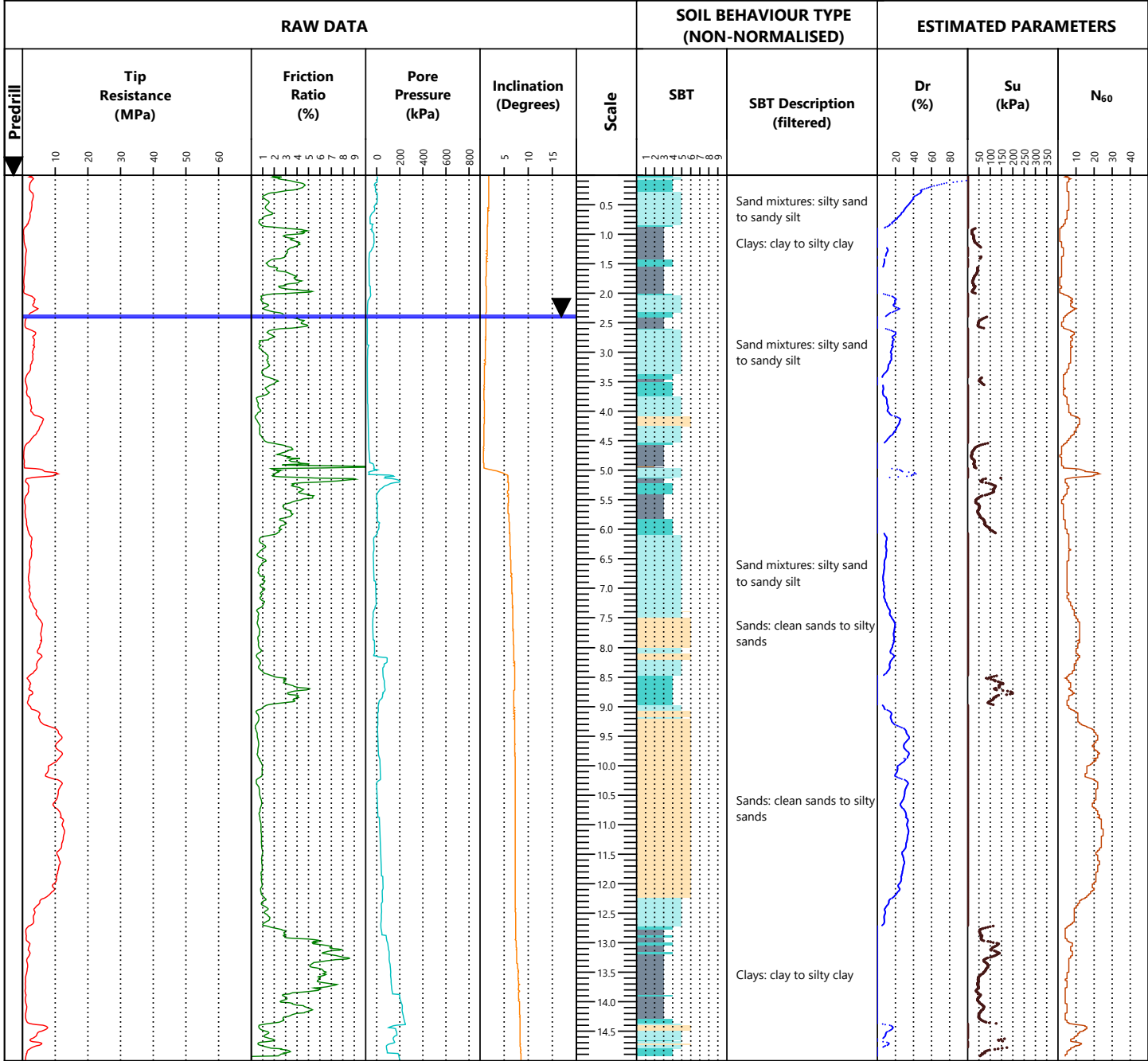


<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ329	<b>Water Level:</b> 1.68m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 1.80m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.9464	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1604		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	1.4592		<b>6</b> Sands: clean sands to silty sands
	1.4568		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

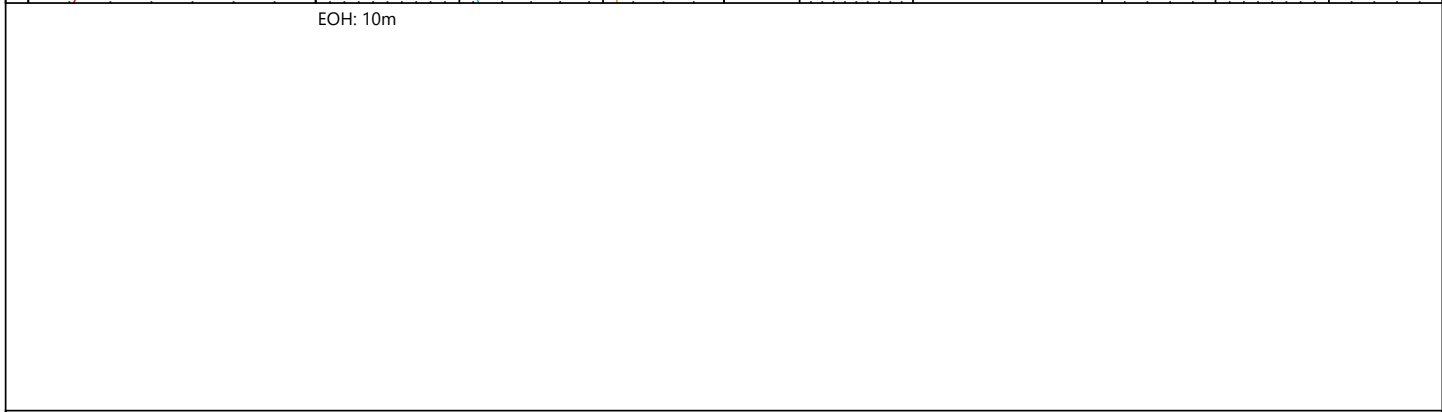
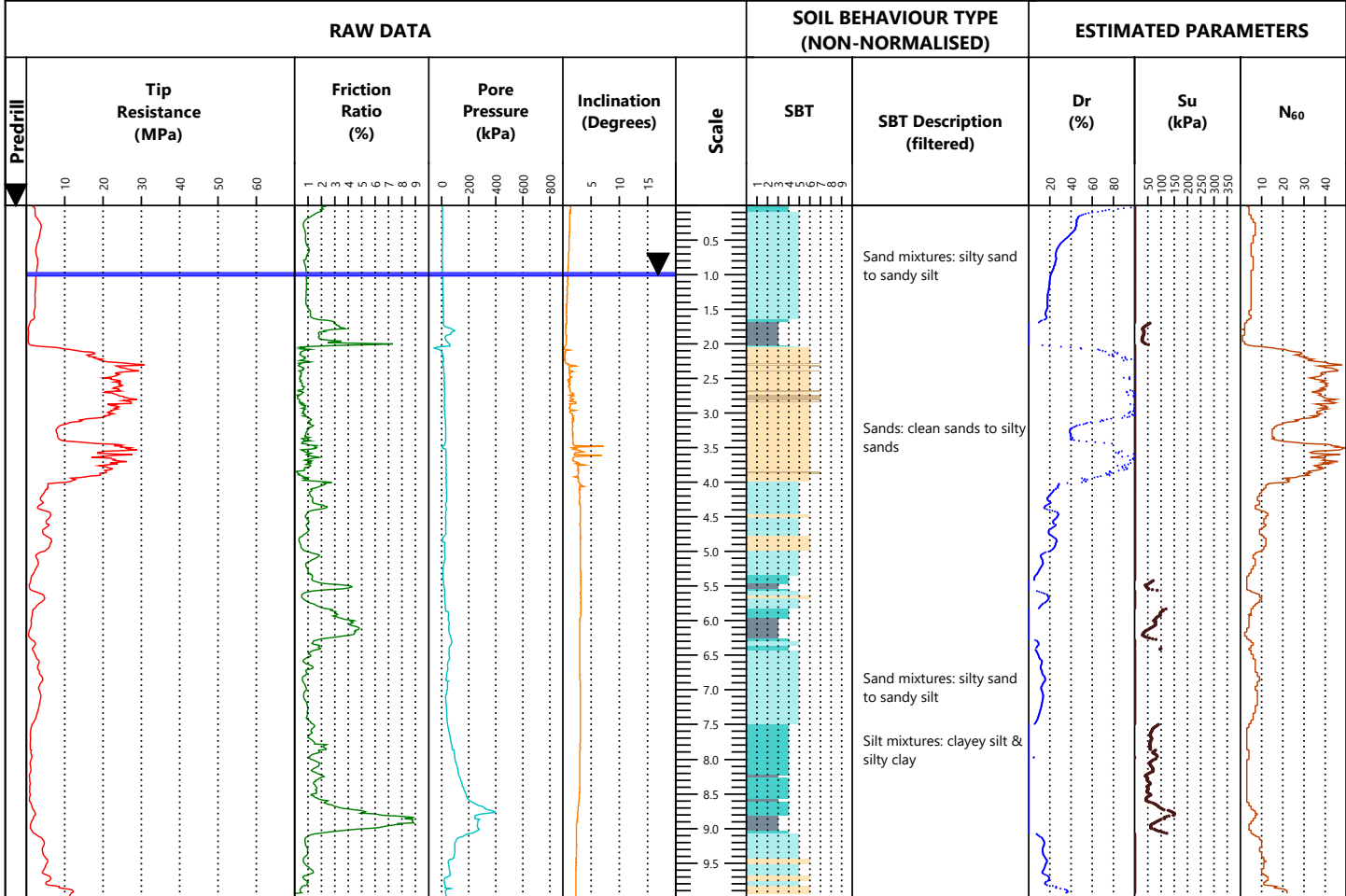
**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 25/9/2020  
**Grid Reference:** 1565043.16m E, 5173036.65m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ329 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012  <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Zero load outputs (MPa)</th> <th>Before test</th> <th>After test</th> </tr> </thead> <tbody> <tr> <td><b>Tip Resistance</b></td> <td>11.9568</td> <td>11.8166</td> </tr> <tr> <td><b>Local Friction</b></td> <td>0.1618</td> <td>0.1622</td> </tr> <tr> <td><b>Pore Pressure</b></td> <td>1.4599</td> <td>1.4582</td> </tr> </tbody> </table>	Zero load outputs (MPa)	Before test	After test	<b>Tip Resistance</b>	11.9568	11.8166	<b>Local Friction</b>	0.1618	0.1622	<b>Pore Pressure</b>	1.4599	1.4582	<b>Predrill:</b> - <b>Water Level:</b> 2.4m <b>Collapse:</b> 2.50m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="0" style="width:100%;"> <tr> <td style="width: 25%;"><b>0</b> Undefined</td> <td style="width: 25%;"><b>5</b> Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td><b>1</b> Sensitive fine-grained</td> <td><b>6</b> Sands: clean sands to silty sands</td> </tr> <tr> <td><b>2</b> Clay - organic soil</td> <td><b>7</b> Dense sand to gravelly sand</td> </tr> <tr> <td><b>3</b> Clays: clay to silty clay</td> <td><b>8</b> Stiff sand to clayey sand</td> </tr> <tr> <td><b>4</b> Silt mixtures: clayey silt &amp; silty clay</td> <td><b>9</b> Stiff fine-grained</td> </tr> </table>	<b>0</b> Undefined	<b>5</b> Sand mixtures: silty sand to sandy silt	<b>1</b> Sensitive fine-grained	<b>6</b> Sands: clean sands to silty sands	<b>2</b> Clay - organic soil	<b>7</b> Dense sand to gravelly sand	<b>3</b> Clays: clay to silty clay	<b>8</b> Stiff sand to clayey sand	<b>4</b> Silt mixtures: clayey silt & silty clay	<b>9</b> Stiff fine-grained
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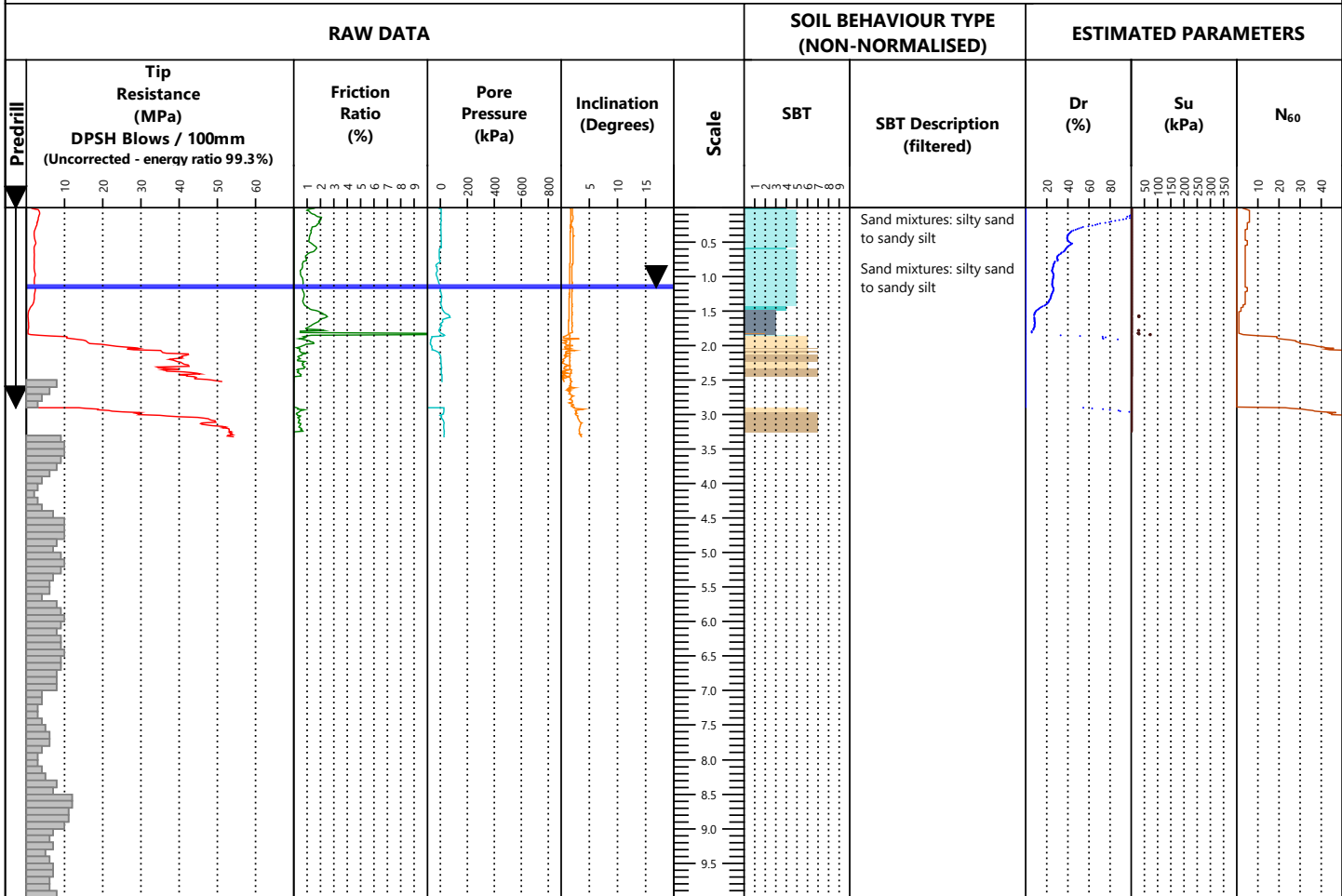
**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 25/9/2020  
**Grid Reference:** 1565055.15m E, 5172937.04m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ329 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012	<b>Predrill:</b> - <b>Water Level:</b> 1m <b>Collapse:</b> 5.1m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="0"> <tr> <td><b>0</b> Undefined</td> <td><b>5</b> Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td><b>1</b> Sensitive fine-grained</td> <td><b>6</b> Sands: clean sands to silty sands</td> </tr> <tr> <td><b>2</b> Clay - organic soil</td> <td><b>7</b> Dense sand to gravelly sand</td> </tr> <tr> <td><b>3</b> Clays: clay to silty clay</td> <td><b>8</b> Stiff sand to clayey sand</td> </tr> <tr> <td><b>4</b> Silt mixtures: clayey silt &amp; silty clay</td> <td><b>9</b> Stiff fine-grained</td> </tr> </table>	<b>0</b> Undefined	<b>5</b> Sand mixtures: silty sand to sandy silt	<b>1</b> Sensitive fine-grained	<b>6</b> Sands: clean sands to silty sands	<b>2</b> Clay - organic soil	<b>7</b> Dense sand to gravelly sand	<b>3</b> Clays: clay to silty clay	<b>8</b> Stiff sand to clayey sand	<b>4</b> Silt mixtures: clayey silt & silty clay	<b>9</b> Stiff fine-grained		
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Zero load outputs (MPa)	Before test	After test													
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<b>Site Location:</b> 2-4 Glovers Road, Christchurch	<b>Date:</b> 29/9/2020
<b>Grid Reference:</b> 1565058.83m E, 5172852.91m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> E. Diaz
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150



EOH: 10m

<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> 2.9m	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ329	<b>Water Level:</b> 1.15m	<b>Target Depth:</b> <input type="checkbox"/>	<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 2.2m	<b>Effective Refusal</b>	<b>6</b> Sands: clean sands to silty sands
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>7</b> Dense sand to gravelly sand
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>8</b> Stiff sand to clayey sand
<b>Tip Resistance</b>	11.8737	Inclinometer: <input type="checkbox"/>	<b>9</b> Stiff fine-grained
<b>Local Friction</b>	0.1612		
<b>Pore Pressure</b>	1.4542		
<b>After test</b>	11.8321		
	0.1611		
	1.4556		

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>
	Sheet 1 of 1

## TEST DETAIL

PointID: CPTu007

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9412	11.8737
Local Friction	0.1606	0.161
Pore Pressure	1.4594	1.262

Date: 24/9/2020

Predrill: -

Water Level: 1.96m

Collapse: 2.0m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu008

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9516	11.8425
Local Friction	0.1609	0.1614
Pore Pressure	1.459	1.4561

Date: 24/9/2020

Predrill: -

Water Level: 1.8m

Collapse: 2.2m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu009

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9464	11.801
Local Friction	0.1604	0.1611
Pore Pressure	1.4592	1.4568

Date: 24/9/2020

Predrill: -

Water Level: 1.68m

Collapse: 1.80m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu010

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9568	11.8166
Local Friction	0.1618	0.1622
Pore Pressure	1.4599	1.4582

Date: 25/9/2020

Predrill: -

Water Level: 2.4m

Collapse: 2.50m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu011

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9464	11.8166
Local Friction	0.1615	0.1621
Pore Pressure	1.4598	1.455

Date: 25/9/2020

Predrill: -

Water Level: 1m

Collapse: 5.1m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

## TEST DETAIL

---

PointID: CPTu012

Sounding: 1

**Operator:** E. Diaz

**Cone Type:** Pagani Piezocone - Compression

**Cone Reference:** MKJ329

**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.9568	11.8062
<b>Local Friction</b>	0.1607	0.1609
<b>Pore Pressure</b>	1.4567	1.4562

**Date:** 29/9/2020

**Predrill:** -

**Water Level:** -

**Collapse:** -

**Termination**

**Target Depth:**

**Effective Refusal**

Tip:

Gauge:

Inclinometer:

Sounding: 2

**Operator:** E. Diaz

**Cone Type:** Pagani Piezocone - Compression

**Cone Reference:** MKJ329

**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.8737	11.8321
<b>Local Friction</b>	0.1612	0.1611
<b>Pore Pressure</b>	1.4542	1.4556

**Date:** 29/9/2020

**Predrill:** 2.9m

**Water Level:** 1.15m

**Collapse:** 2.2m

**Termination**

**Target Depth:**

**Effective Refusal**

Tip:

Gauge:

Inclinometer:



# CPT CALIBRATION AND TECHNICAL NOTES

These notes describe the technical specifications and associated calibration references pertaining to the Pagani piezocone types measuring cone resistance, sleeve friction, inclination and pore pressure (piezocone, 10cm<sup>2</sup>)

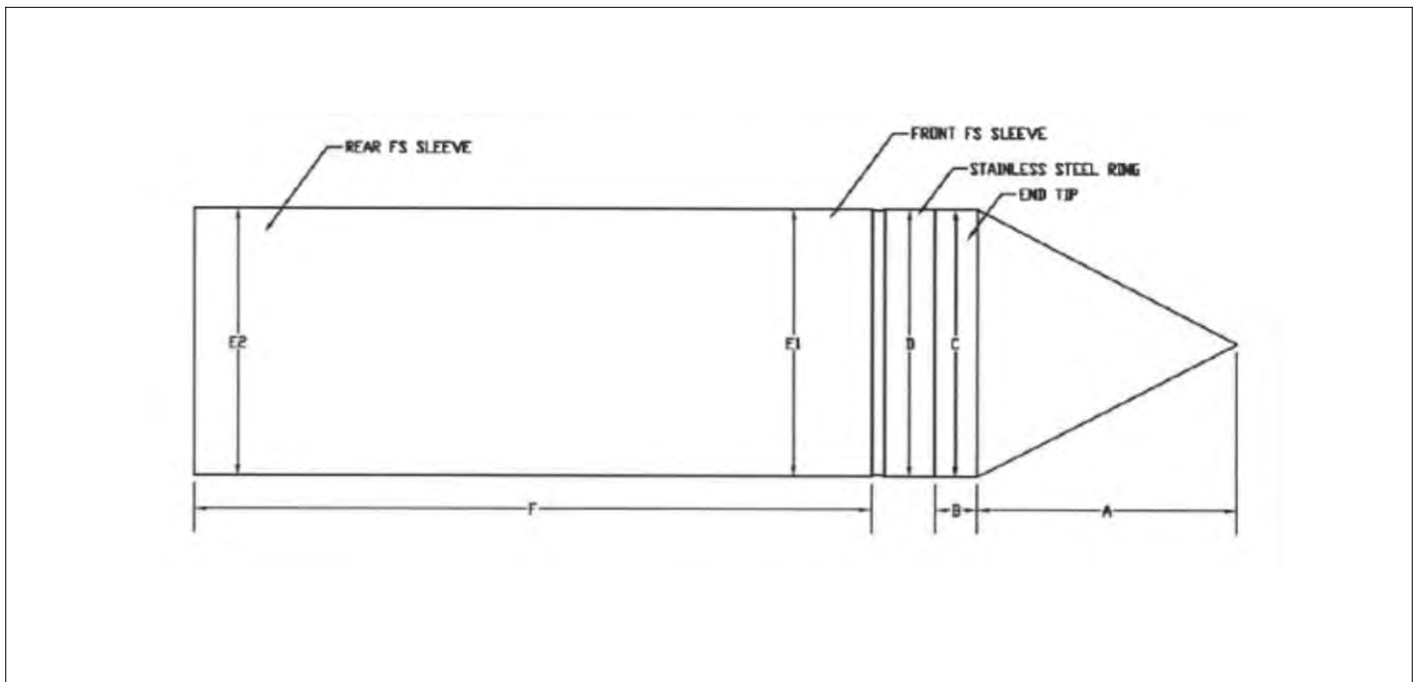
## Dimensions

Dimensional specifications are detailed below. All tolerances are routinely checked prior to testing and measurements taken are electronically recorded. All records are kept on file and available on request.

## Technical specifications

	Tip	Friction	Pore Pressure	Inclination
<b>Maximum Measuring Range:</b>	50 - 100 MPa	1.60 MPa	2.50 MPa	0° - 20°
<b>Resolution:</b>	24 bit	24 bit	24 bit	12 bit
<b>Accuracy:</b>	0.005 MPa	0.04 MPa	0.04 MPa	0.5°

<b>Length:</b>	320 mm	<b>Weight:</b>	1.8 kg
<b>Diameter:</b>	35.8 mm	<b>Opening angle of bit:</b>	60°
<b>Cone base area:</b>	10 cm <sup>2</sup>	<b>Side sleeve surfaces:</b>	150 cm <sup>2</sup>
<b>Cone area ratio:</b>	0.80	<b>Tip and Local Friction sensor displacement:</b>	80 mm





**CONE CALIBRATION CERTIFICATE**  
N° Z023/20

Calibrated system (Sistema tarato):  
 Serial number **Mkj329**  
 Sensor **TIP RESISTANCE**  
 Max. Capacity [MPa]: **100**  
 Scaling Factor: **192610**  
 Tip net area ratio (a<sub>t</sub>): **0,79**  
 Sleeve net ratio (b<sub>s</sub>): **0,00**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 200 KN  
 Serial Number 138913  
 Power press: Easydur Italiana  
 Model Aura 20T  
 Serial Number 29084  
 The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 Certificate N. LAT 091 2020-015  
 Temperature of calibration 22°C  
 Humidity 45%  
 Factory calibration in accordance with ASTM D5778-12



**CONE CALIBRATION CERTIFICATE**  
N° Z023/20

Calibrated system (Sistema tarato):  
 Serial number **Mkj329**  
 Sensor **SLEEVE FRICTION**  
 Max. Capacity [kPa]: **1600**  
 Scaling Factor: **30794**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 50 kN  
 Serial Number 65495  
 Power press: Easydur Italiana  
 Model Aura 10T  
 Serial Number 29002  
 The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 The adopted calibration procedure has been developed according to the suggestions given by Prof. Paul W. Mayne (Georgia Institute of Technology) and Prof. Diego Lo Presti (University of Pisa)

*PLS*



**CONE CALIBRATION CERTIFICATE**  
N° Z023/20

Calibrated system (Sistema tarato):  
 Serial number **Mkj329**  
 Sensor **PORE PRESSURE**  
 Max. Capacity [kPa]: **2500**  
 Scaling Factor: **10657**  
 Sensor **TILT ANGLE**  
 Max. Inclination [°]: **20**  
 Scaling Factor: **151152**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Pressure Generator:  
 Manufacturer MENSOR  
 Model CPC 4000  
 Serial Number 41000V56  
 Sensor Descr Silicon Pressure Transducer  
 Sensor Serial Number 41000SYF  
 The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 28/02/2019

Date of issue 05/02/2020

## D. Southern Geophysical MASW and GPR Report



October 2020

# Geophysical Site Investigation:

2-4 Glovers Road, Christchurch

Report prepared for Miyamoto International NZ Ltd

# GEOPHYSICAL REPORT



**Southern**  
**Geophysical**

3/28 Tanya St, Bromley, Christchurch 8062

Ph: 03 384 4302

Web: [www.southerngeophysical.com](http://www.southerngeophysical.com)

Data collected and report prepared for Southern Geophysical Ltd by:

Christian Ruegg, MSc, Geophysicist

Nick McConachie, BSc, Geologist

Report internally reviewed for Southern Geophysical by:

Mike Finnemore, PhD, Senior Geophysicist

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Methodology: .....	2
Results: .....	3
Conclusions:.....	3
Disclaimer: .....	5

SGL Reference: 2050

Report Version 1



## **Summary:**

Southern Geophysical Ltd was contracted to undertake a geophysical survey using Multi-channel Analysis of Surface Waves (MASW) at 2-4 Glovers Road, Christchurch. The geophysical survey was conducted on September 24<sup>th</sup>, 2020 and includes three MASW lines (Figure 1). The aim of the survey was to assess the shear-wave velocities and structure of the subsurface to a depth of over 20 m. The MASW results show low shear-wave velocities to a depth of 10 m in the northern part of the site (100 m/s to 150 m/s), with higher velocities to the south (100 m/s to 300 m/s). The boundary between these two zones is a feature characteristic of the edge of a paleochannel, buried valley, or dipping volcanic strata, crossing the site east to west and dipping to the north. It is possible that high velocities imaged by the MASW survey to the south (>500 m/s from approximately 20 m depth) are associated with volcanic rock, but there are no boreholes available for ground truthing to that depth.

## **Methodology:**

MASW is a geophysical technique that uses the dispersive nature of surface waves to model shear-wave velocity versus depth.

A MASW survey is undertaken as a series of lines or points across the surface of the site. The MASW points in this survey were collected using a 24-channel towed seismic array, with 4.5 Hz geophones. The geophone spacing was 1 m and the source offset was 10 m. The seismic source was a 16 lb sledgehammer impacting an aluminium plate. Recording parameters for the MASW survey were set with a 0.125 ms sample interval, 1.5 s record length, 24 dB gains, and a geophone trigger system.

The field records were processed using the Kansas Geological Survey software package SurfSeis6++ ©. The geometry for each point was set according to the survey parameters and the dispersion curves were generated and edited. The inversions were run using a 10 layer variable depth model. The velocity data was interpolated into 2D profiles showing  $V_s$  variations with depth (Figures 2 to 3). The output shear-wave velocity data is included as data files (CSV format), supplementary to this report.

Supplementary to the MASW profiles, a series of Ground Penetrating Radar lines were acquired with a GSSI 200 MHz antenna (Figure 1). The radargrams are included in (Figures 4 and 5).

Survey positions were recorded using a Geo 7X Trimble GNSS system with a Tornado antenna. The GNSS positions were differentially corrected using a local GeoNet base station. The GNSS points were output in NZTM2000, with heights in Mean Sea Level (MSL). The accuracy of the survey positions is +/- 0.1 m. The site had no significant topographic changes, and the lines have not been corrected for elevation.

### **Results:**

A total of three MASW lines were acquired at the site with a total MASW survey length of approximately 1 km (Figure 1). The ground surface was well compacted farm tracks and farm yards. A series of GPR lines were acquired along each MASW line to provide a high resolution image of the substrate (Figures 4 and 5).

In homogenous soils, with gradually increasing shear-wave velocities and no sharp lateral discontinuities, the accuracy of the shear-wave velocities derived from the MASW processing is considered to be +/- 10%.<sup>1</sup> The quality of the seismic data and the dispersion curves used in this report is very good, with a good signal-to-noise ratio. If there is a velocity inversion present in the shear-wave profile (decreasing velocity with depth), the shear-wave velocity of the reduced velocity zone and the thickness of that zone can often be underestimated by the inversion process.

### **Conclusions:**

The MASW survey was considered to be of good quality, with modelled shear-wave velocities accurate to +/- 10%. The velocities in the top 5 m are likely to be more accurate than the deeper velocities, due to the presence of multiple velocity inversions. The MASW survey indicates a horizontal layer defined by a sharp increase in shear-wave velocity (180 m/s to 220 m/s) at around 5 m depth in the southern part of the site, consistent with the surface of dense gravels or sands. In the northern part of the site a similar 180 m/s to 220 m/s surface was observed at 20 m depth. There is a well-defined dipping surface dividing the south and the north, possibly associated with a buried valley edge, paleochannel, or

---

<sup>1</sup> Stephenson, W.J., Louie, J.N., Pullammanappallil, S., Williams, R.A., and Odum, J.K. 2005. Blind Shear-wave Velocity Comparison of ReMi and MASW Results with Boreholes to 200 m in Santa Clara Valley: Implications for Earthquake Ground-Motion Assessment. *Bulletin of the Seismological Society of America*, Vol. 95, pp. 2506-2516.

bedrock interface. This edge feature is apparent in both MASW 1 and MASW 3, as well as GPR 4 and GPR 10.

While the limitations of the MASW method should be considered when evaluating these results, the quality of the data collected at the site and the confidence in the shear-wave velocities derived from the MASW data is good.



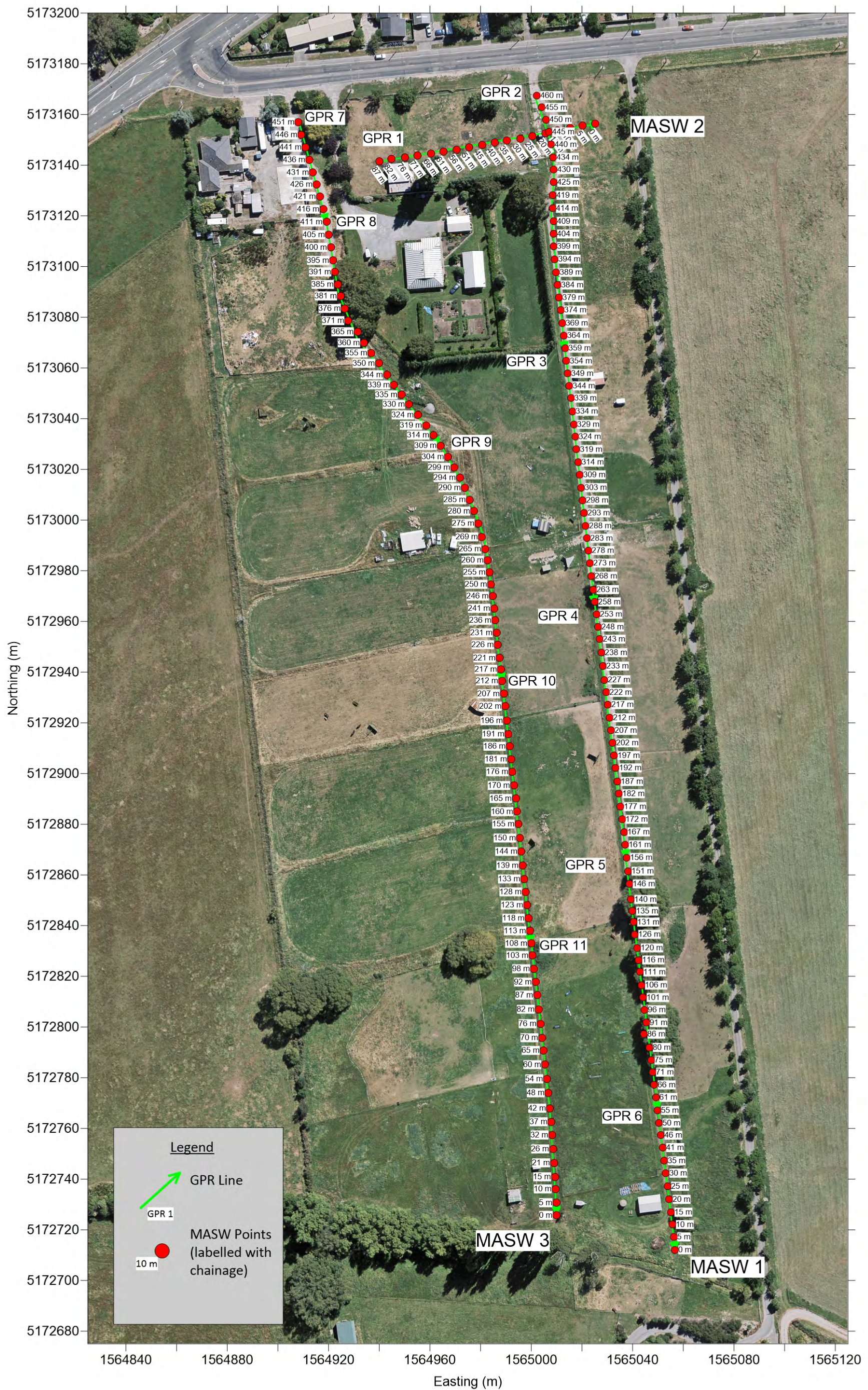
**Disclaimer:**

This document has been provided by Southern Geophysical Ltd subject to the following:

Non-invasive geophysical testing has limitations and is not a complete source of testing. Often there is a need to couple non-invasive methods with invasive testing methods, such as drilling, especially in cases where the non-invasive testing indicates anomalies.

This document has been prepared for the particular purpose outlined in the project proposal and no responsibility is accepted for the use of this document, in whole or in part, in other contexts or for any other purpose. Southern Geophysical Ltd did not perform a complete assessment of all possible conditions or circumstances that may exist at the site. Conditions may exist which were undetectable given the limited nature of the enquiry Southern Geophysical Ltd was retained to undertake with respect to the site. Variations in conditions often occur between investigatory locations, and there may be special conditions pertaining to the site which have not been revealed by the investigation and which have not therefore been taken into account. Accordingly, additional studies and actions may be required by the client.

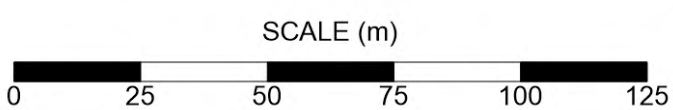
We collected our data and based our report on information which was collected at a specific point in time. The passage of time affects the information and assessment provided by Southern Geophysical Ltd. It is understood that the services provided allowed Southern Geophysical Ltd to form no more than an opinion of the actual conditions of the site at the time the site was visited and cannot be used to assess the effect of any subsequent changes for whatever reason. Where data is supplied by the client or other sources, including where previous site investigation data have been used, it has been assumed that the information is correct. No responsibility is accepted by Southern Geophysical Ltd for incomplete or inaccurate data supplied by others. This document is provided for sole use by the client and is confidential to that client and its professional advisers. No responsibility whatsoever for the contents of this document will be accepted to any person other than the client. Any use which a third party makes of this document, or any reliance on or decisions to be made based on it, is the responsibility of such third parties. Southern Geophysical Ltd accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this document.



**Figure 1: Site Map**

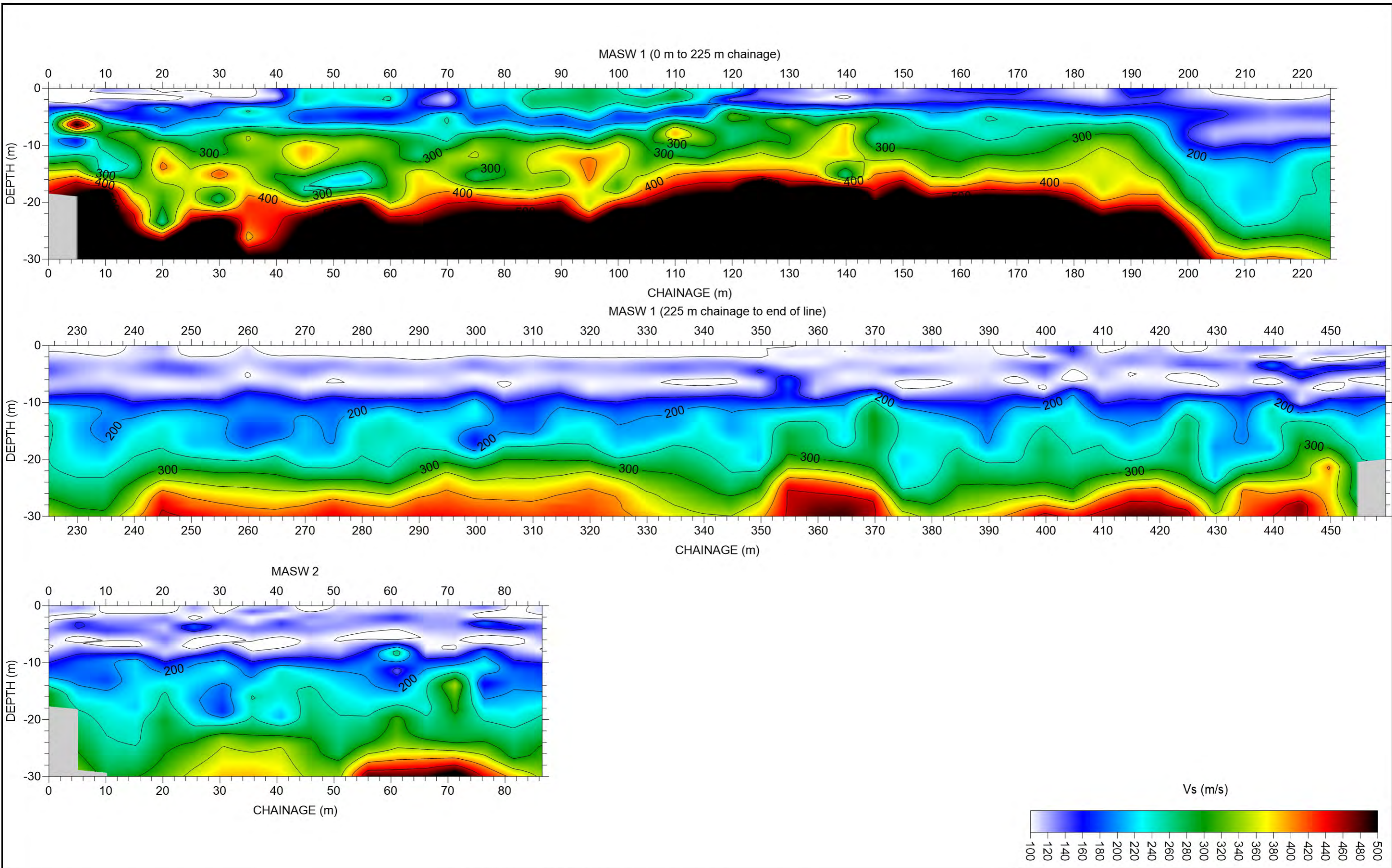
**2-4 Glovers Road, Christchurch**

Coordinates NZ2000 TM Grid.  
 NOTES- Aerial photograph sourced from LINZ, Crown Copyright ©



A3

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[www.southerngeophysical.com](http://www.southerngeophysical.com)



DRAWING- **Figure 2: MASW 1 and 2**

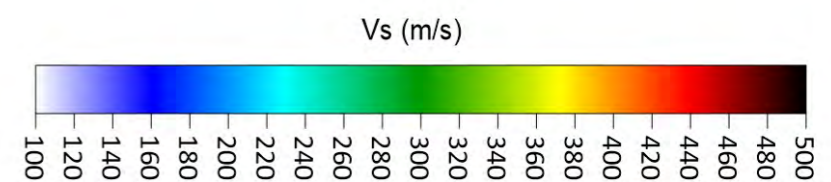
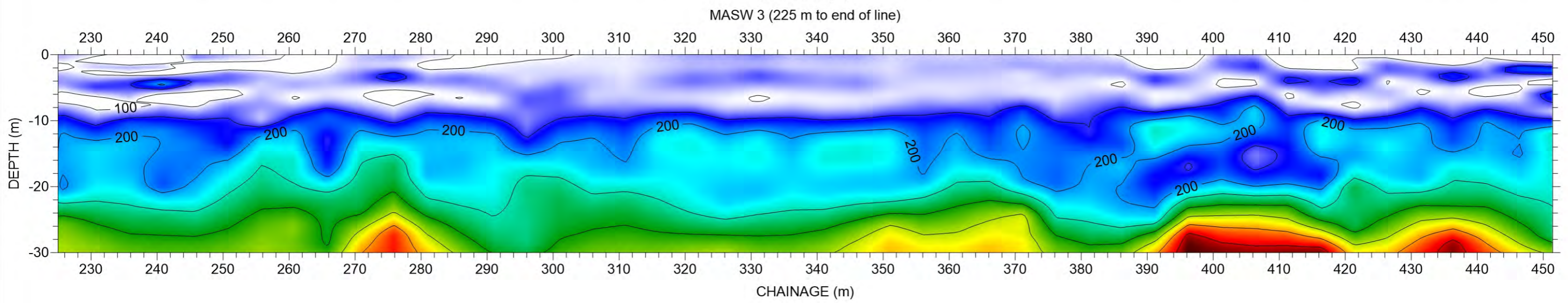
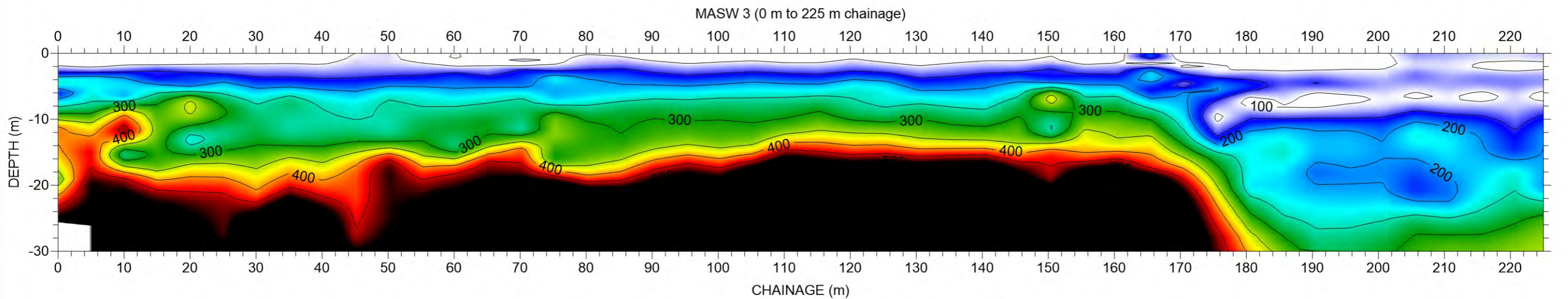
LOCATION- **2-4 Glovers Road, Christchurch**

NOTES MASW Vs profile has contour intervals of 50 m/s (Vs).

See site map for location of points.

A3

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www.southerngeophysical.com



DRAWING- **Figure 3: MASW 3**

LOCATION- **2-4 Glover Street, Christchurch**

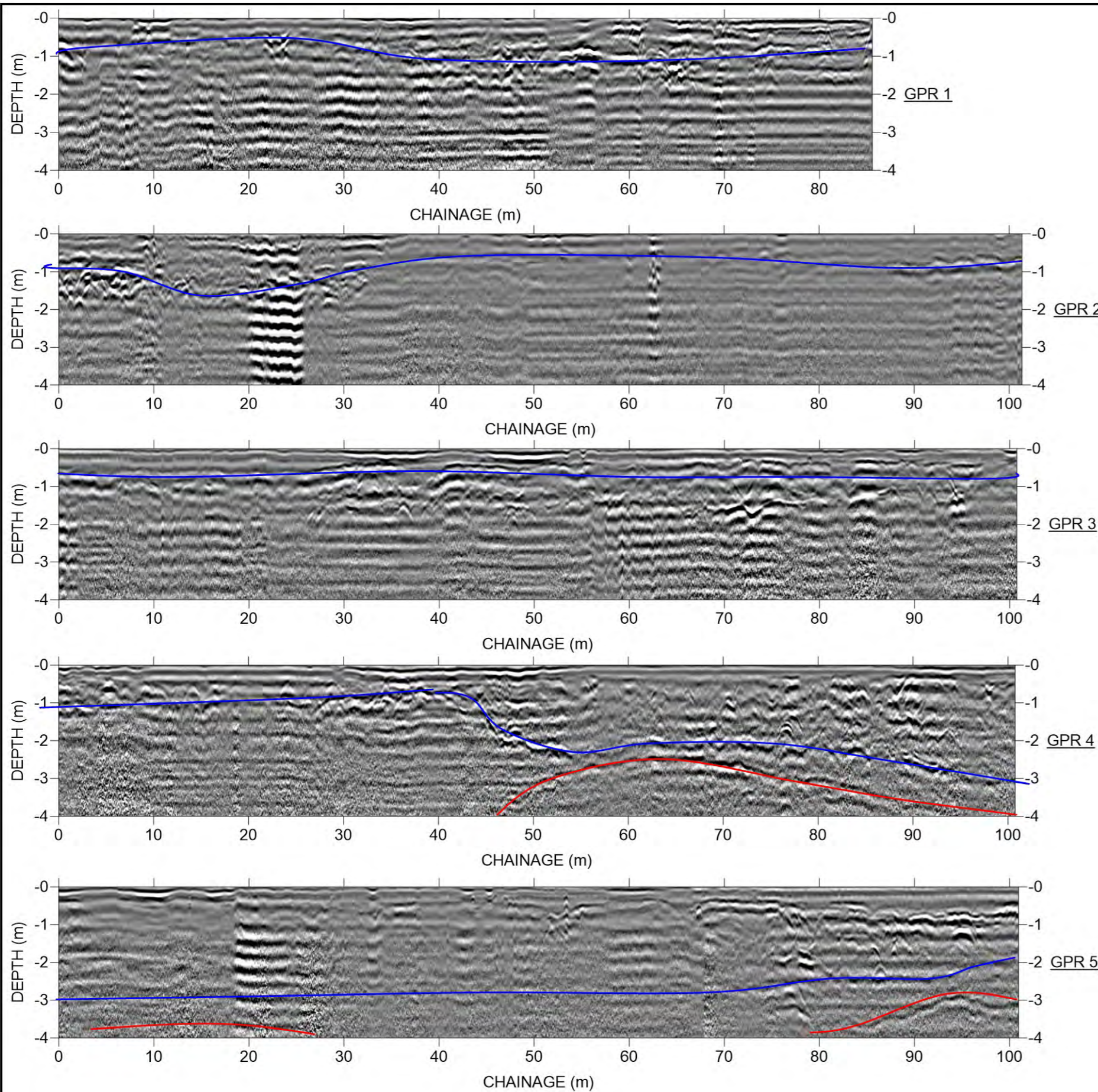
NOTES MASW Vs profile has contour intervals of 50 m/s (Vs).

See site map for location of points.

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A3

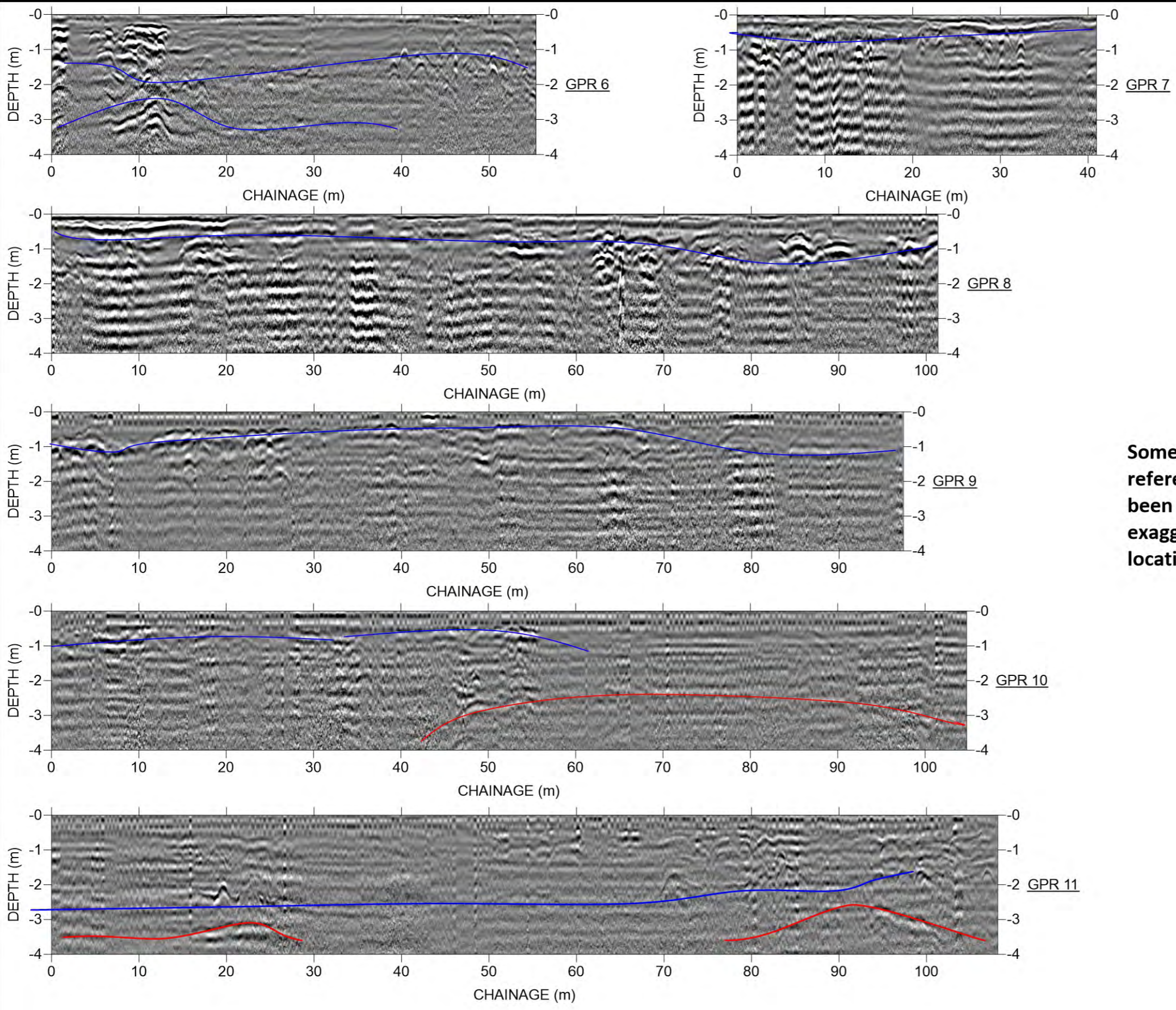


Some reflectors are annotated for reference. Note the profiles have been plotted with a 4:1 vertical exaggeration. See site map for line locations.

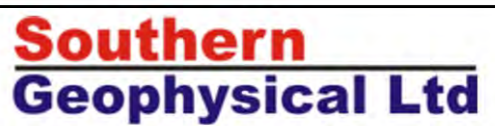
DRAWING- **Figure 4: GPR Radargrams 1 to 5**

LOCATION- **2-4 Glover Street, Christchurch**

NOTES



Some reflectors are annotated for reference. Note the profiles have been plotted with a 4:1 vertical exaggeration. See site map for line locations.

DRAWING- <b>Figure 5: GPR Radargrams 6 to 11</b>	NOTES	 <a href="http://www.southerngeophysical.com">www.southerngeophysical.com</a>
LOCATION- <b>2-4 Glover Street, Christchurch</b>		

## E. Geotechnical Cross Sections





236 Hereford Street,  
PO BOX 137 Cashel Street  
Christchurch 8011

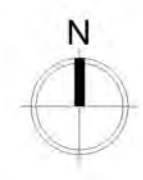
T: 64 03 377 4095  
miyamoto.nz  
projects@miyamoto.nz

**PROJECT No: 200357**  
**GEOTECHNICAL CROSS SECTIONS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**

SHEET LIST		
SHEET N°	SHEET NAME	REV.
S1	LOCATION PLAN	1
S2.1	GEOTECHNICAL CROSS-SECTION 1	1
S2.2	GEOTECHNICAL CROSS-SECTION 2	1
S2.3	GEOTECHNICAL CROSS-SECTION 3	1

ISSUE DATE: 19/10/20 REV: 1





100 m

**miyamoto.**

236 Hereford Street,  
PO BOX 137 Cashel Street  
Christchurch 8011

T: 64 03 377 4095  
miyamoto.nz  
projects@miyamoto.nz

**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**

REVISION HISTORY		
REV	DATE	DESCRIPTION
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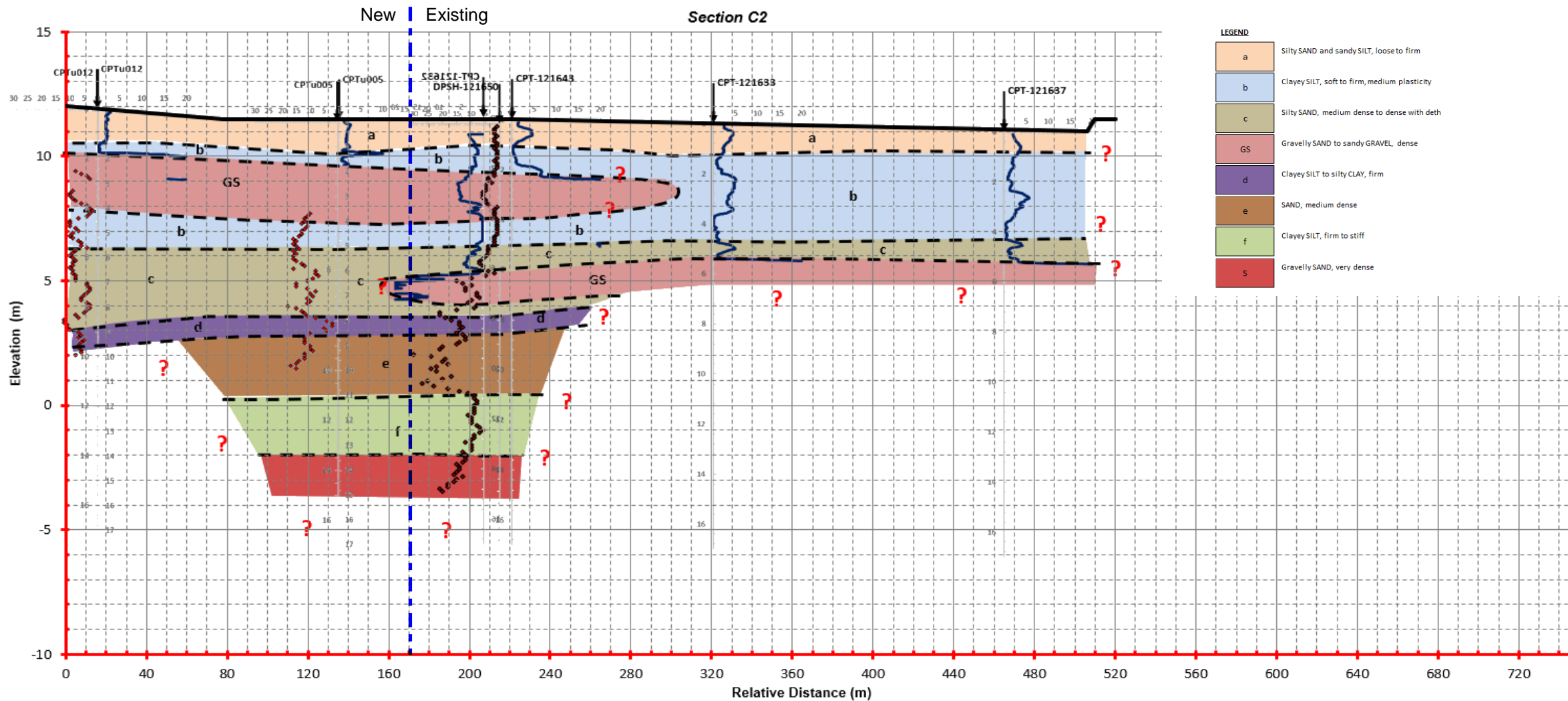
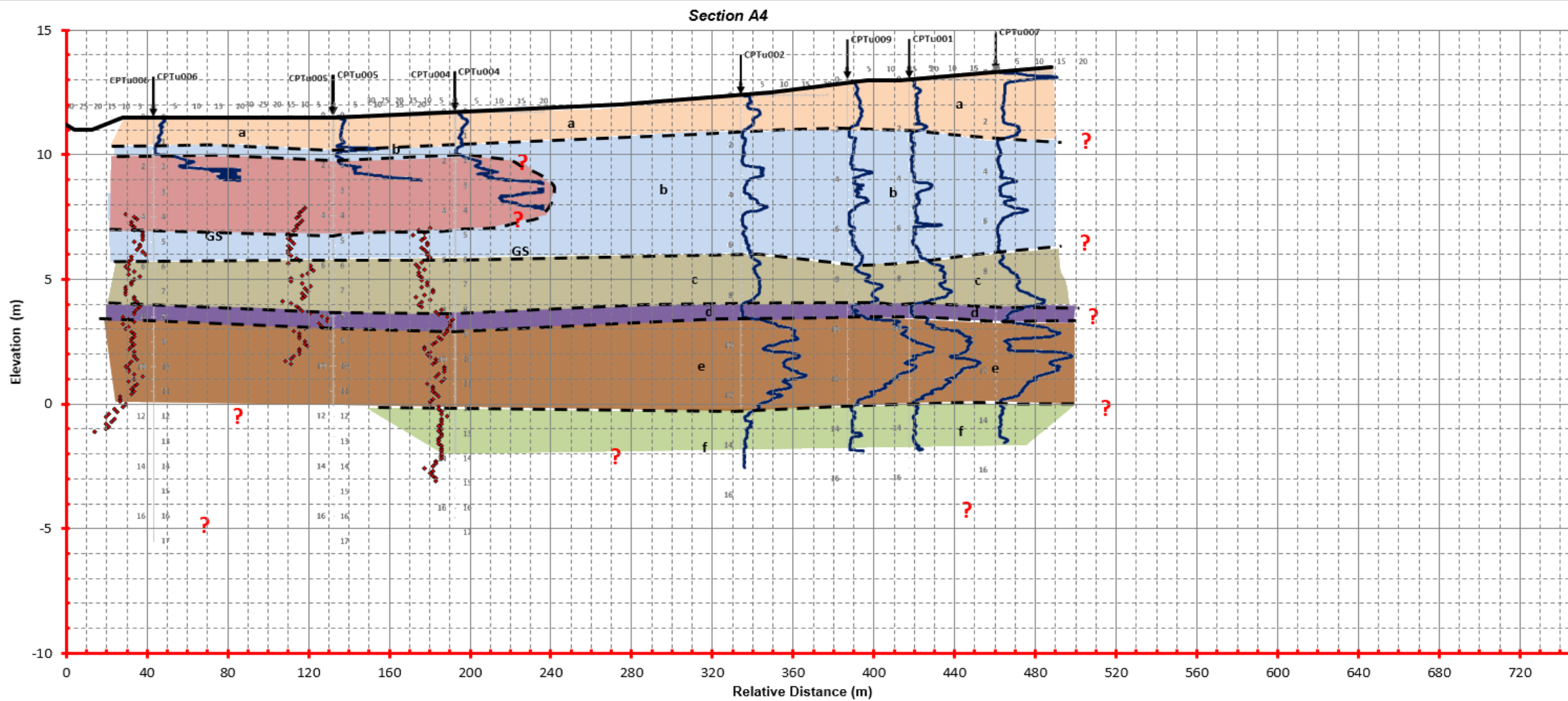
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PROJECT No.:	200357
VERSION DATE:	16/10/2020
DRAWN:	CG
ENGINEER:	CG
APPROVED:	AG

SIZE: A3

LOCATION PLAN

SHEET No.: S1 REV. 1

INFORMATION AND DRAWINGS APPEARING HEREIN CONSTITUTE THE ORIGINAL WORK OF THE ENGINEER AND MAY NOT BE DUPLICATED, USED, OR DISCLOSED WITHOUT THE WRITTEN CONSENT OF THE ENGINEER. DO NOT SCALE OFF THIS DRAWING - CONTRACTOR TO VERIFY ALL DIMENSIONS PRIOR TO CONSTRUCTION. ANY DISCREPANCIES MUST BE REPORTED TO THE ENGINEER.



**LEGEND**

a	Silty SAND and sandy SILT, loose to firm
b	Clayey SILT, soft to firm, medium plasticity
c	Silty SAND, medium dense to dense with deth
GS	Gravelly SAND to sandy GRAVEL, dense
d	Clayey SILT to silty CLAY, firm
e	SAND, medium dense
f	Clayey SILT, firm to stiff
s	Gravelly SAND, very dense

# miyamoto.

T: 64 03 377 4095  
miyamoto.nz  
projects@miyamoto.nz

236 Hereford Street,  
PO BOX 137 Cashel Street  
Christchurch 8011

**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**

**REVISION HISTORY**

REV	DATE	DESCRIPTION
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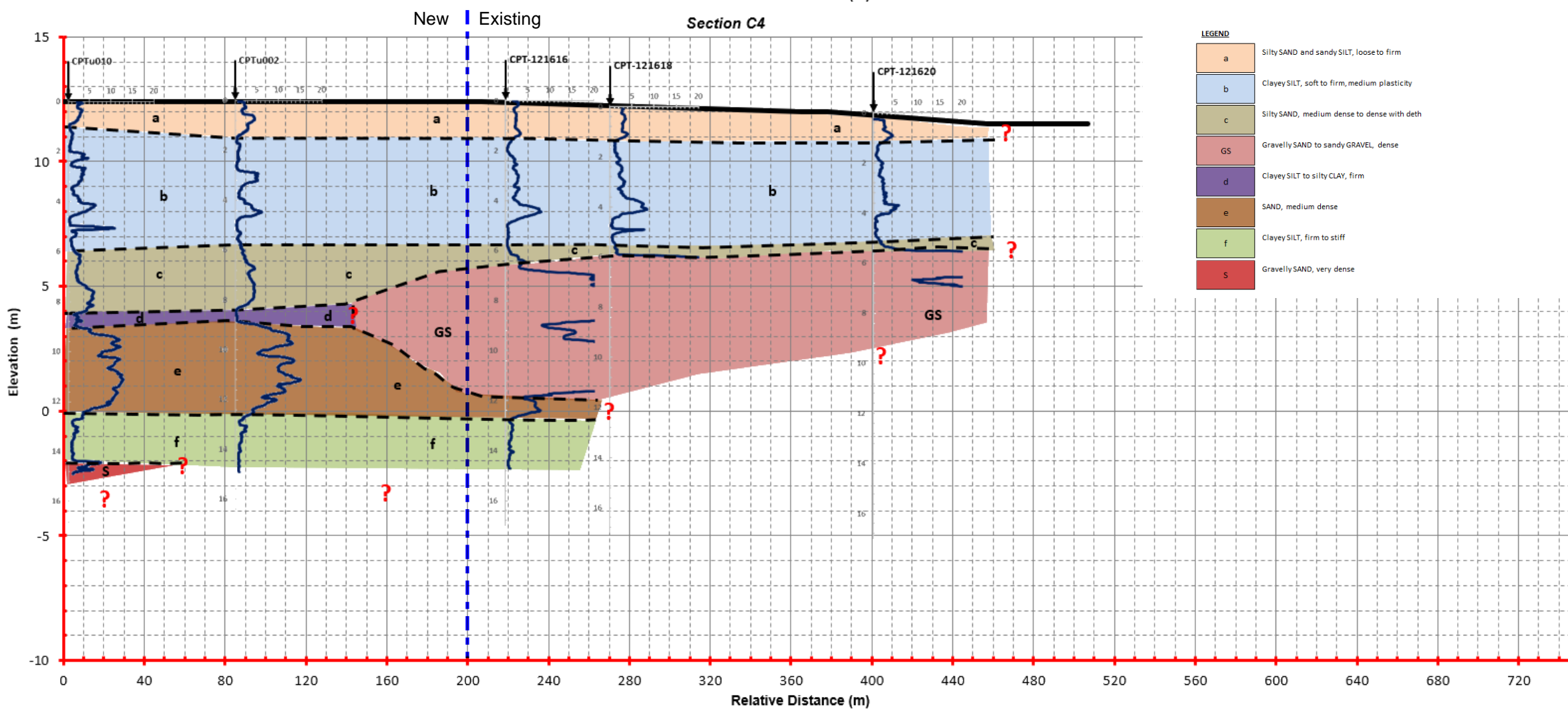
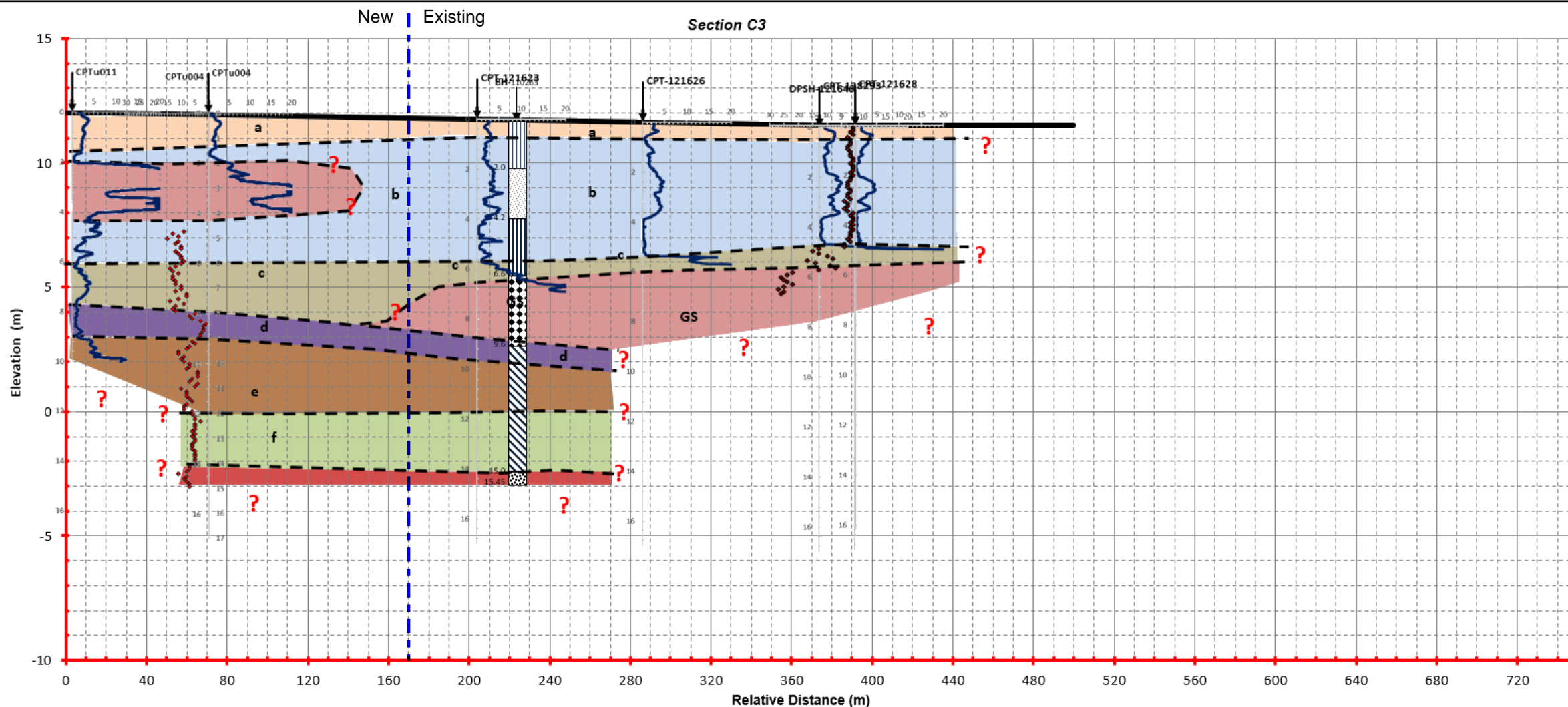
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PROJECT No.: 200357  
VERSION DATE: 16/10/2020  
DRAWN: CG  
ENGINEER: CG  
APPROVED: AG

SIZE: A3

**GROUND MODEL**  
**SHEET 1**

SHEET No.: S2.1 REV. 1

**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**



**LEGEND**

a	Silty SAND and sandy SILT, loose to firm
b	Clayey SILT, soft to firm, medium plasticity
c	Silty SAND, medium dense to dense with deth
GS	Gravelly SAND to sandy GRAVEL, dense
d	Clayey SILT to silty CLAY, firm
e	SAND, medium dense
f	Clayey SILT, firm to stiff
s	Gravelly SAND, very dense

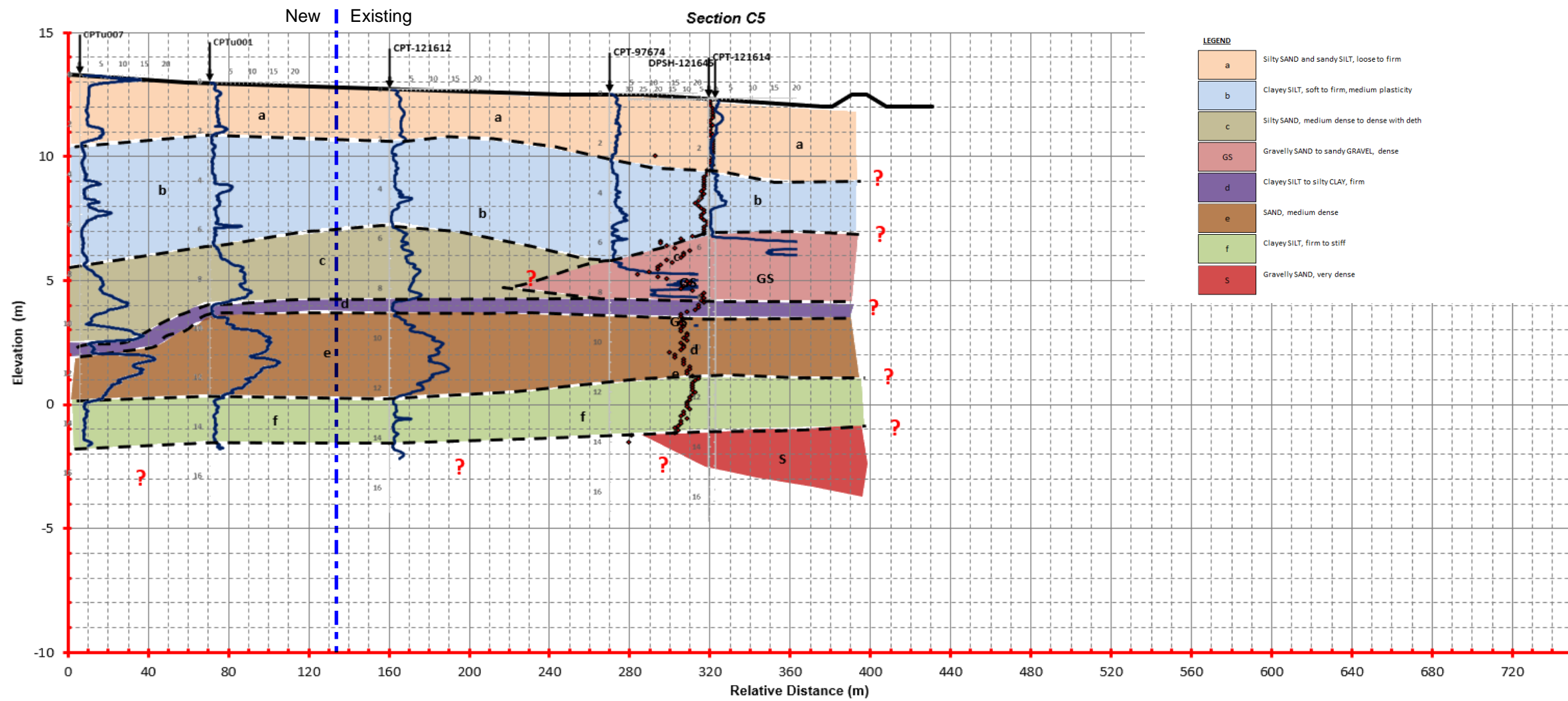
**REVISION HISTORY**

REV	DATE	DESCRIPTION
1	19/10/20	FINAL

CLIENT: YOURSECTION LTD  
PROJECT No.: 200357  
VERSION DATE: 16/10/2020  
DRAWN: CG  
ENGINEER: CG  
APPROVED: AG

SIZE: A3  
**GROUND MODEL SHEET 2**

SHEET No.: S2.2 REV. 1



# miyamoto.

236 Hereford Street,  
PO BOX 137 Cashel Street  
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miyamoto.nz  
projects@miyamoto.nz

**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**

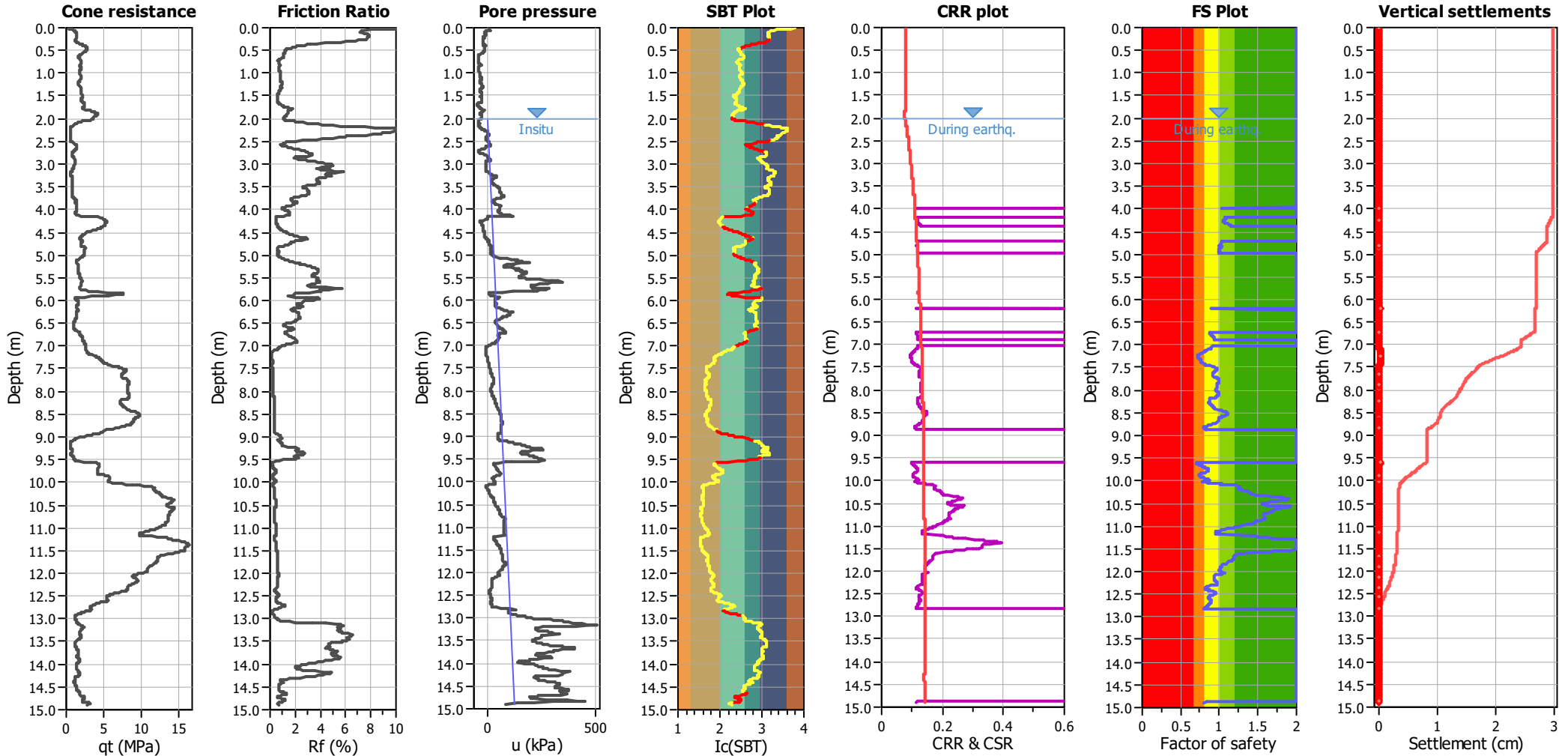
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REV	DATE	DESCRIPTION
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PROJECT No.:	200357
VERSION DATE:	16/10/2020
DRAWN:	CG
ENGINEER:	CG
APPROVED:	AG

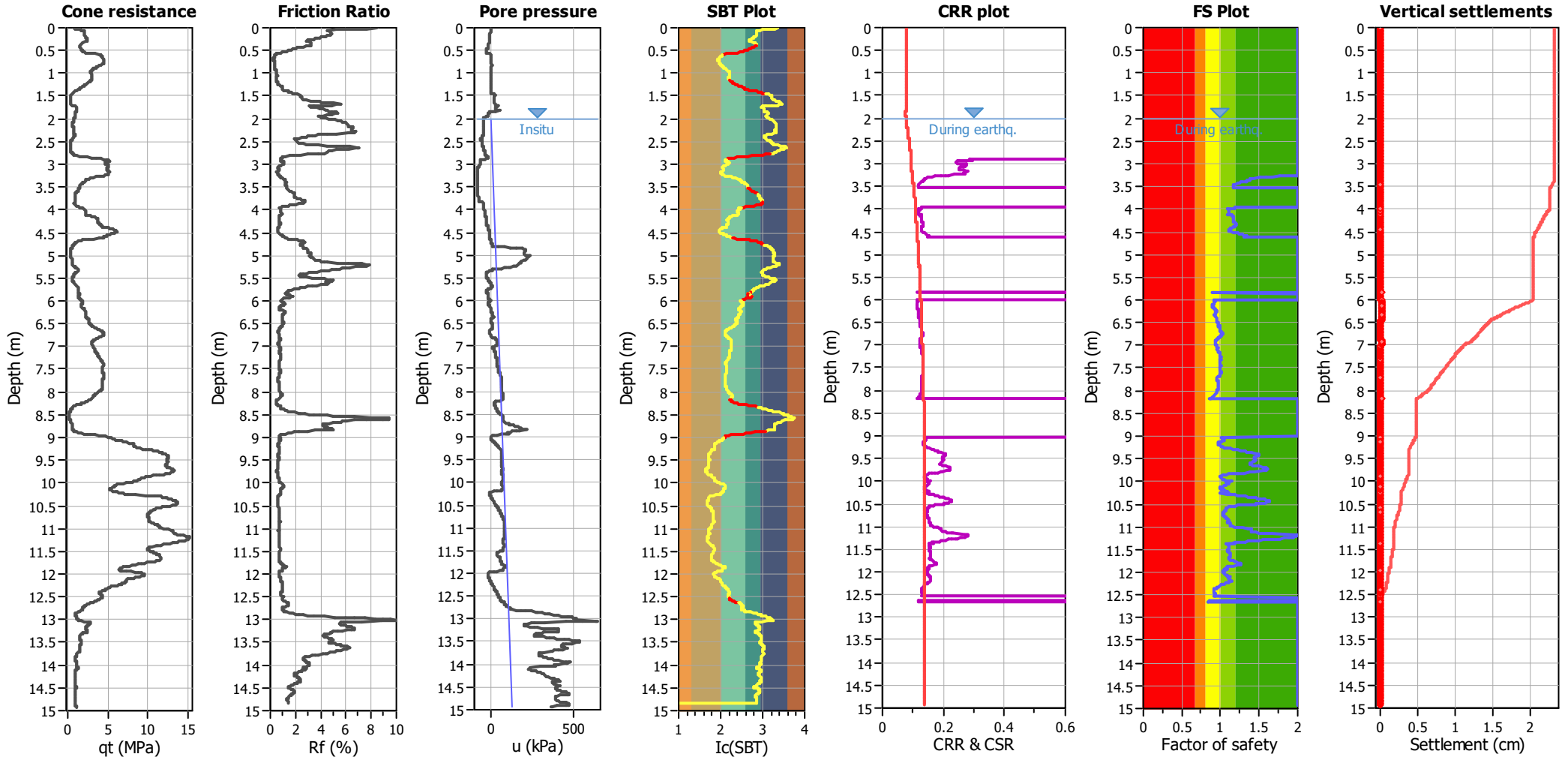
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**GROUND MODEL**  
**SHEET 3**  
SHEET No.: **S2.3** REV. 1

## F. Liquefaction Analyses

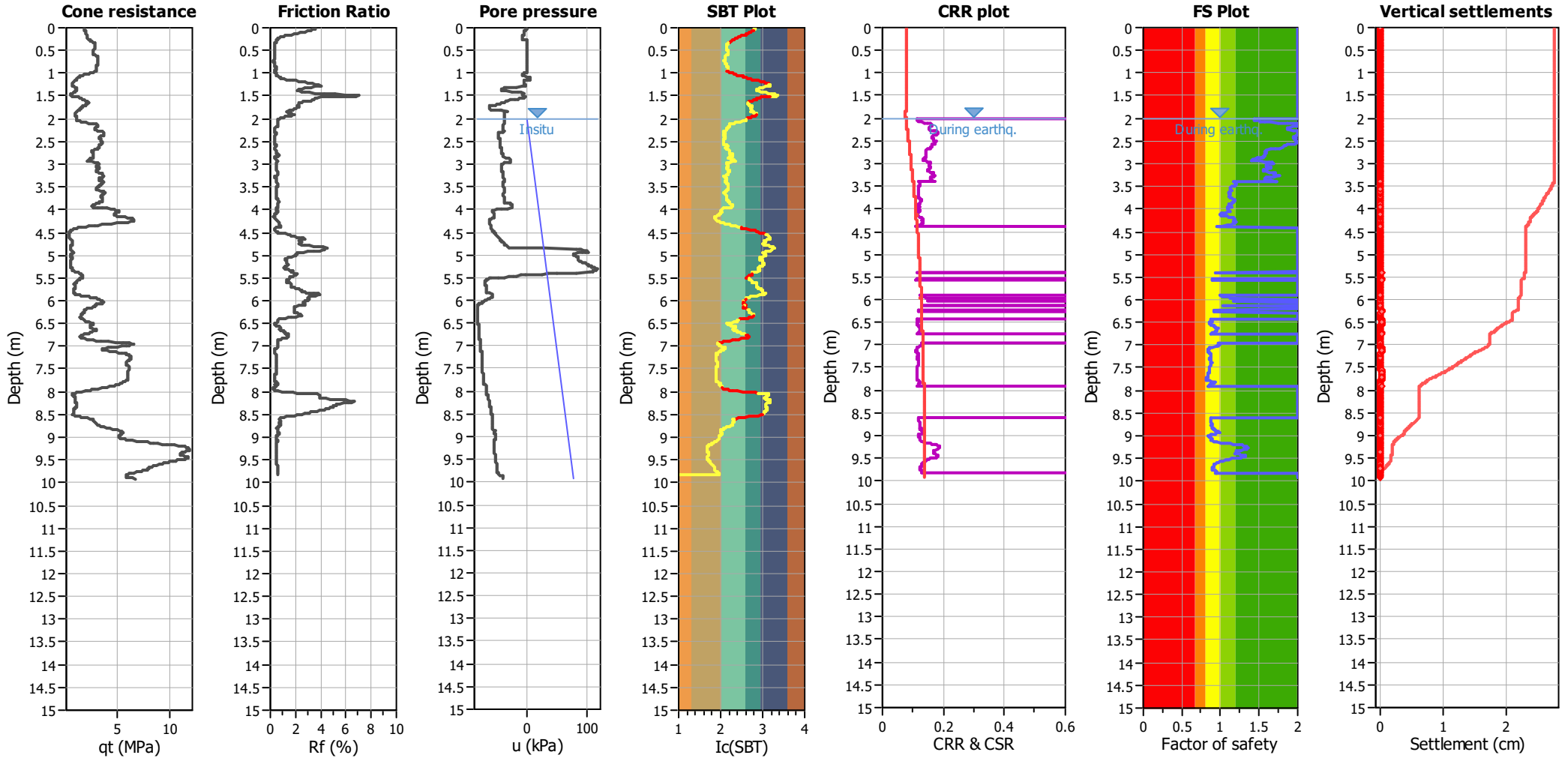




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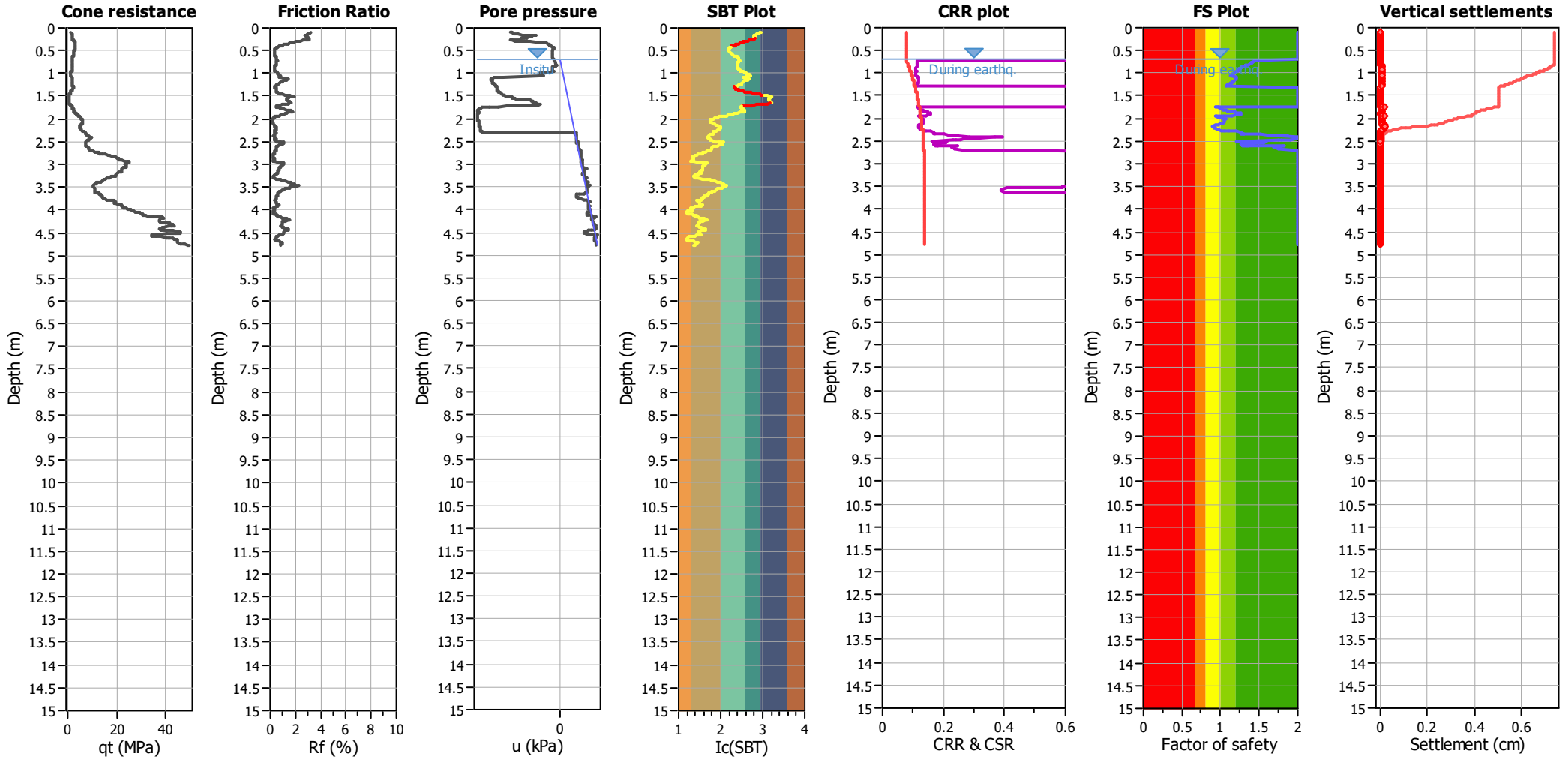


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Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

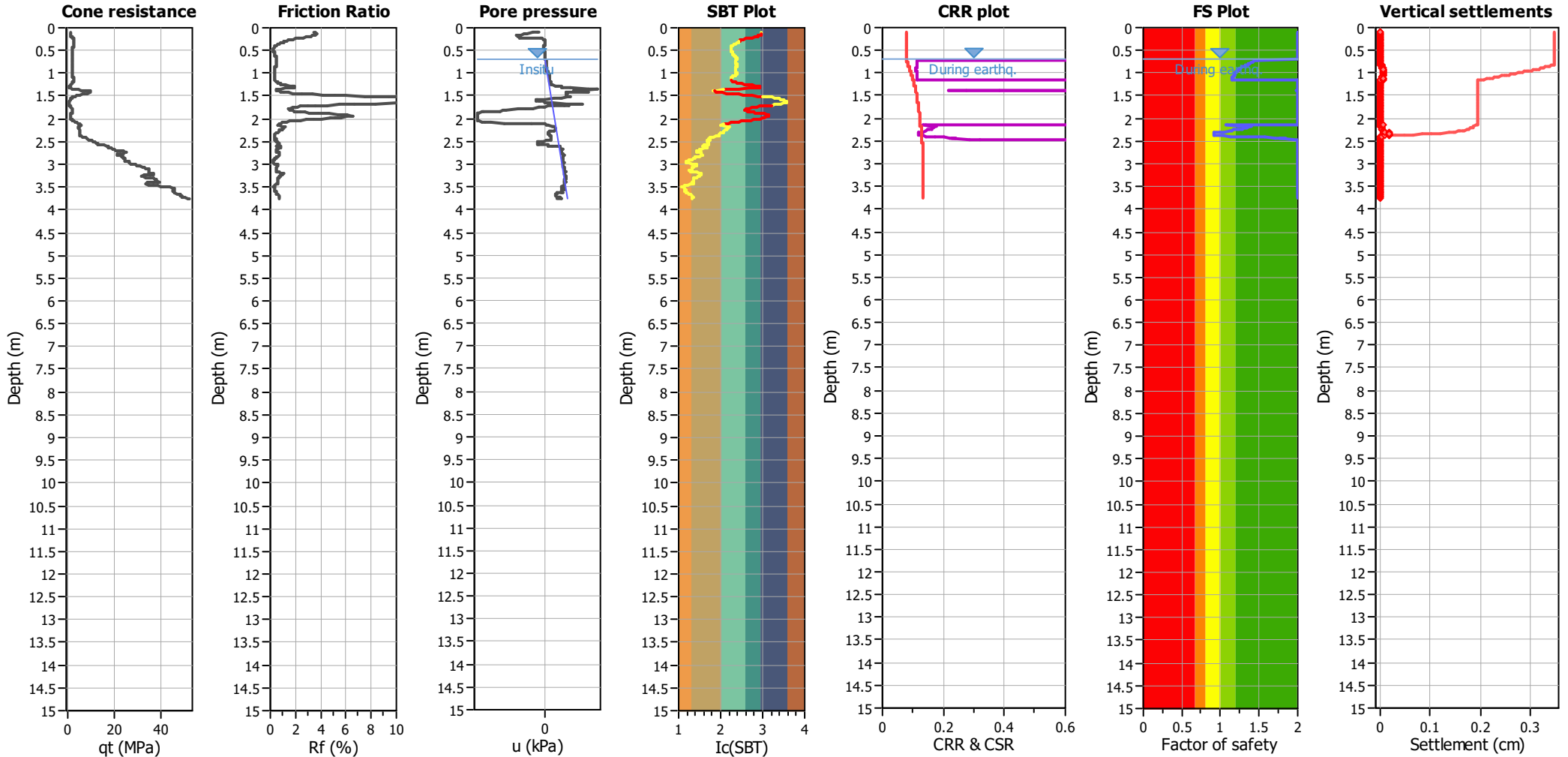


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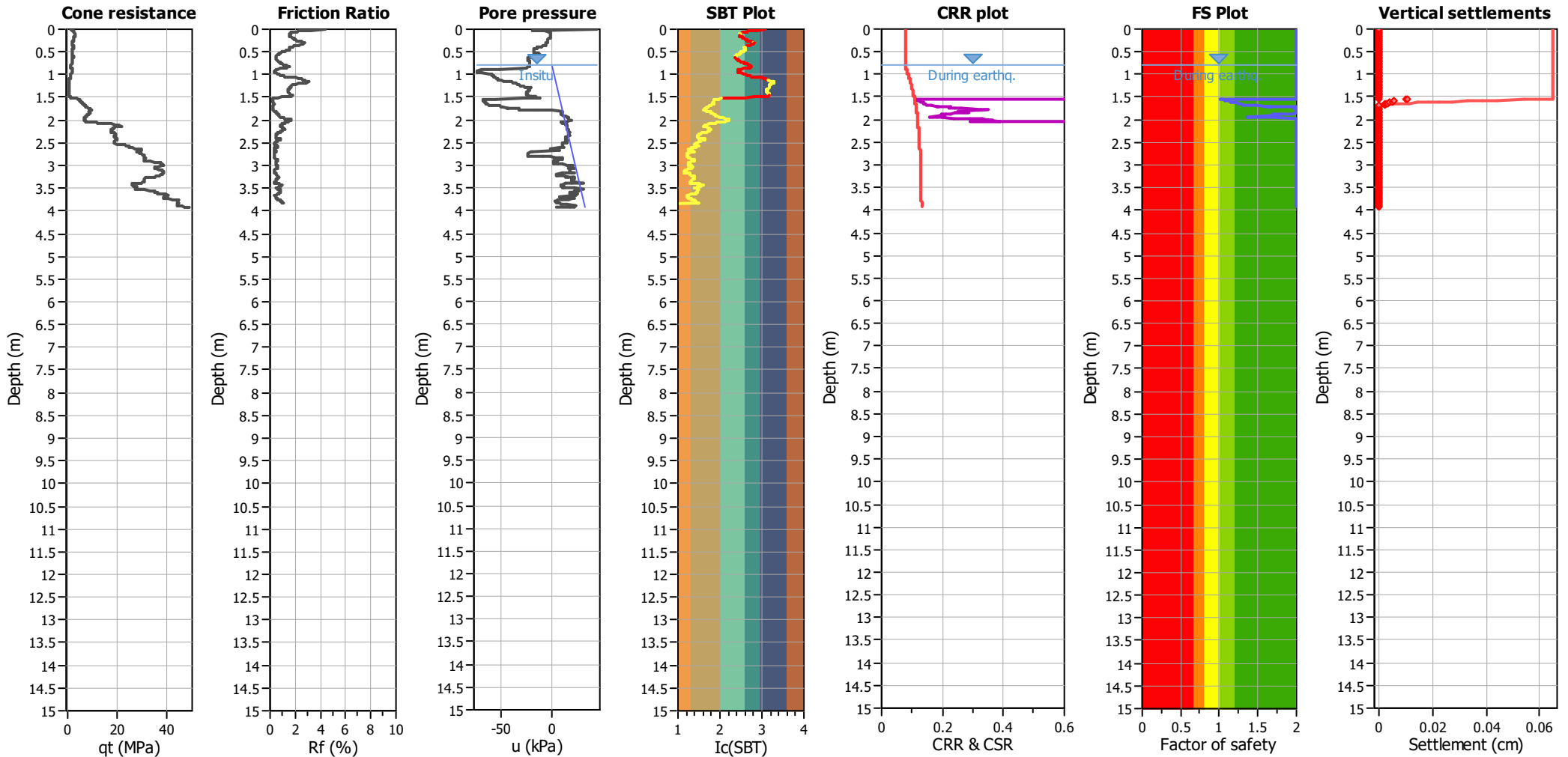




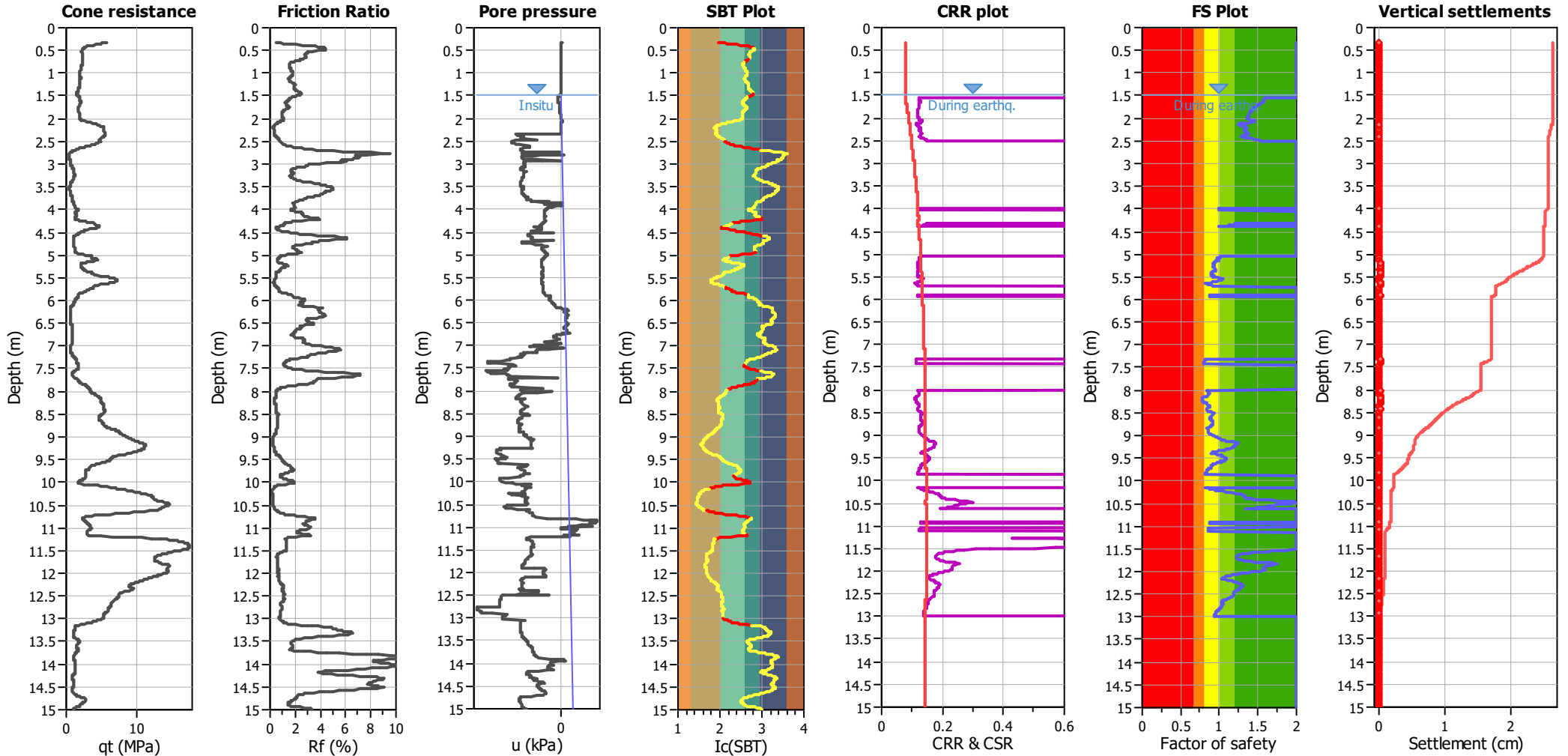
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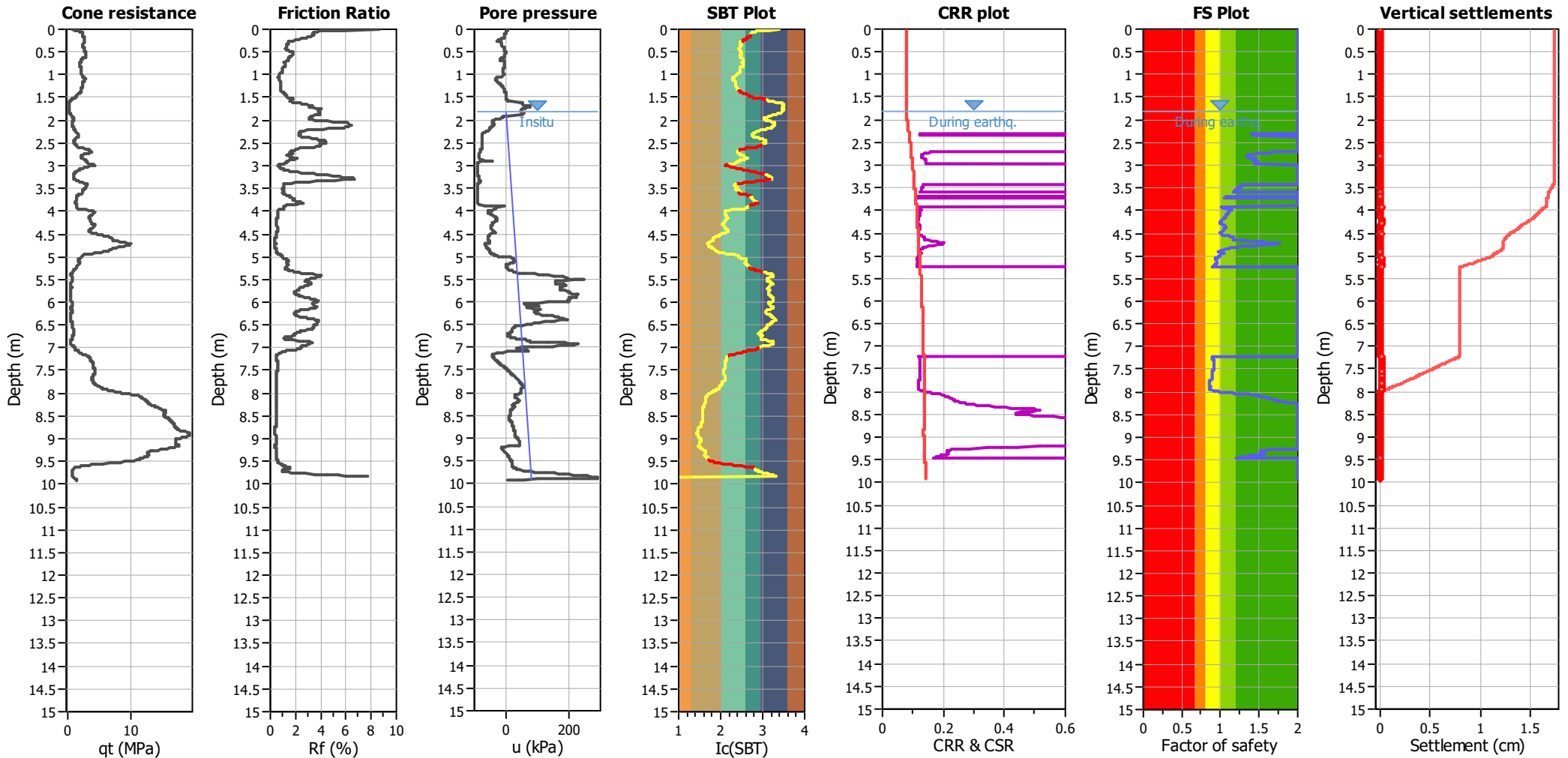
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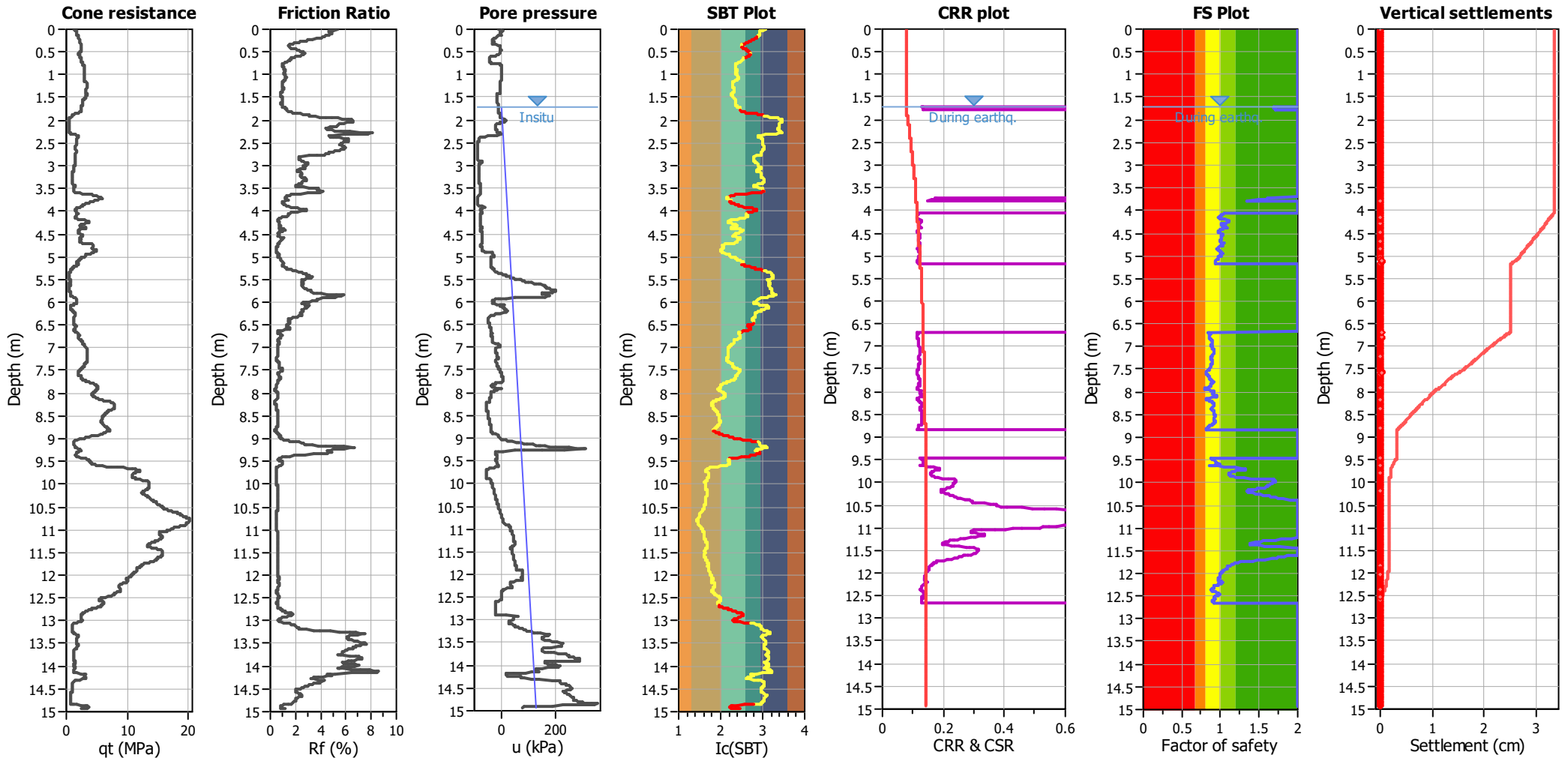
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Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
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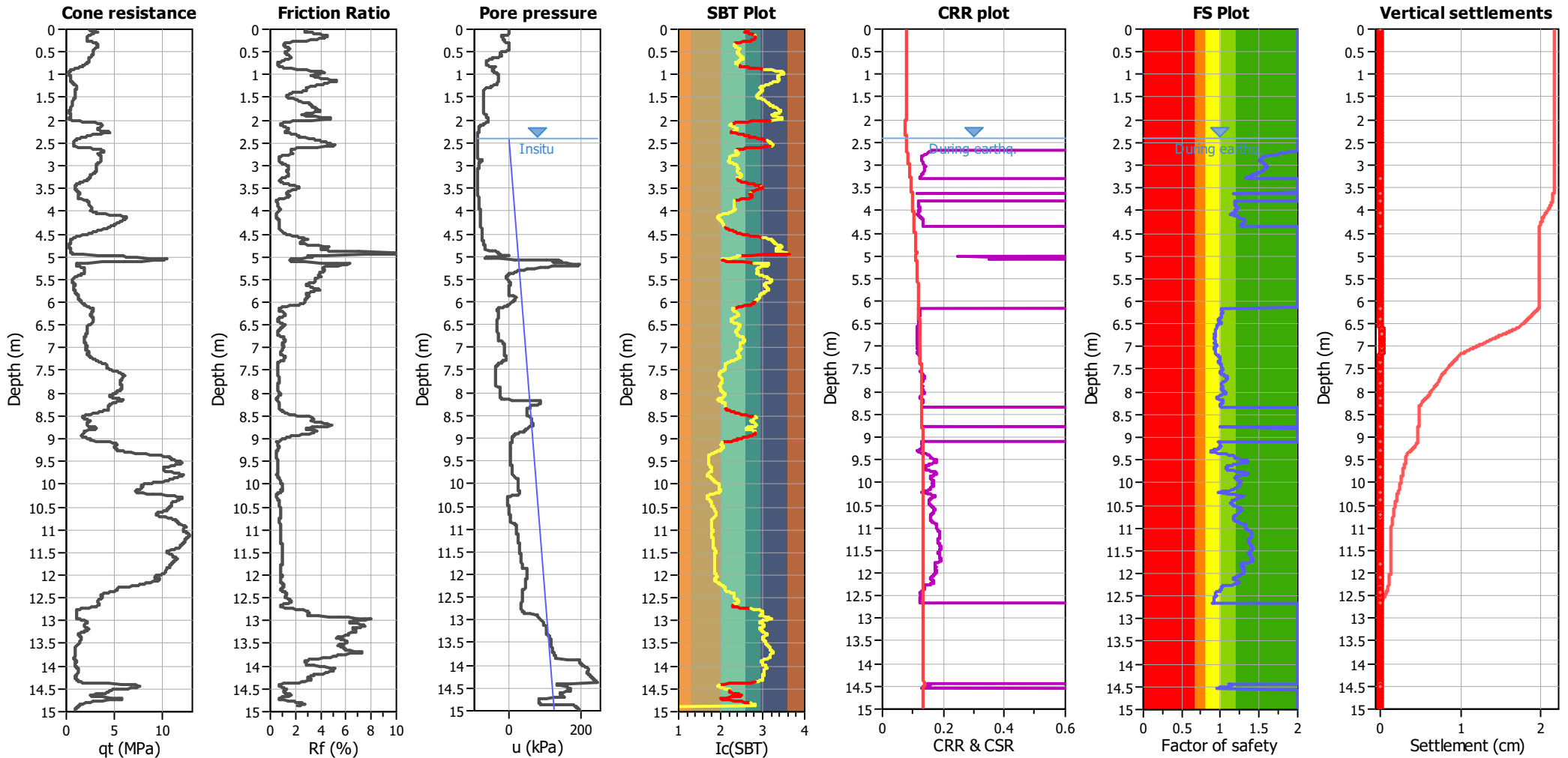
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



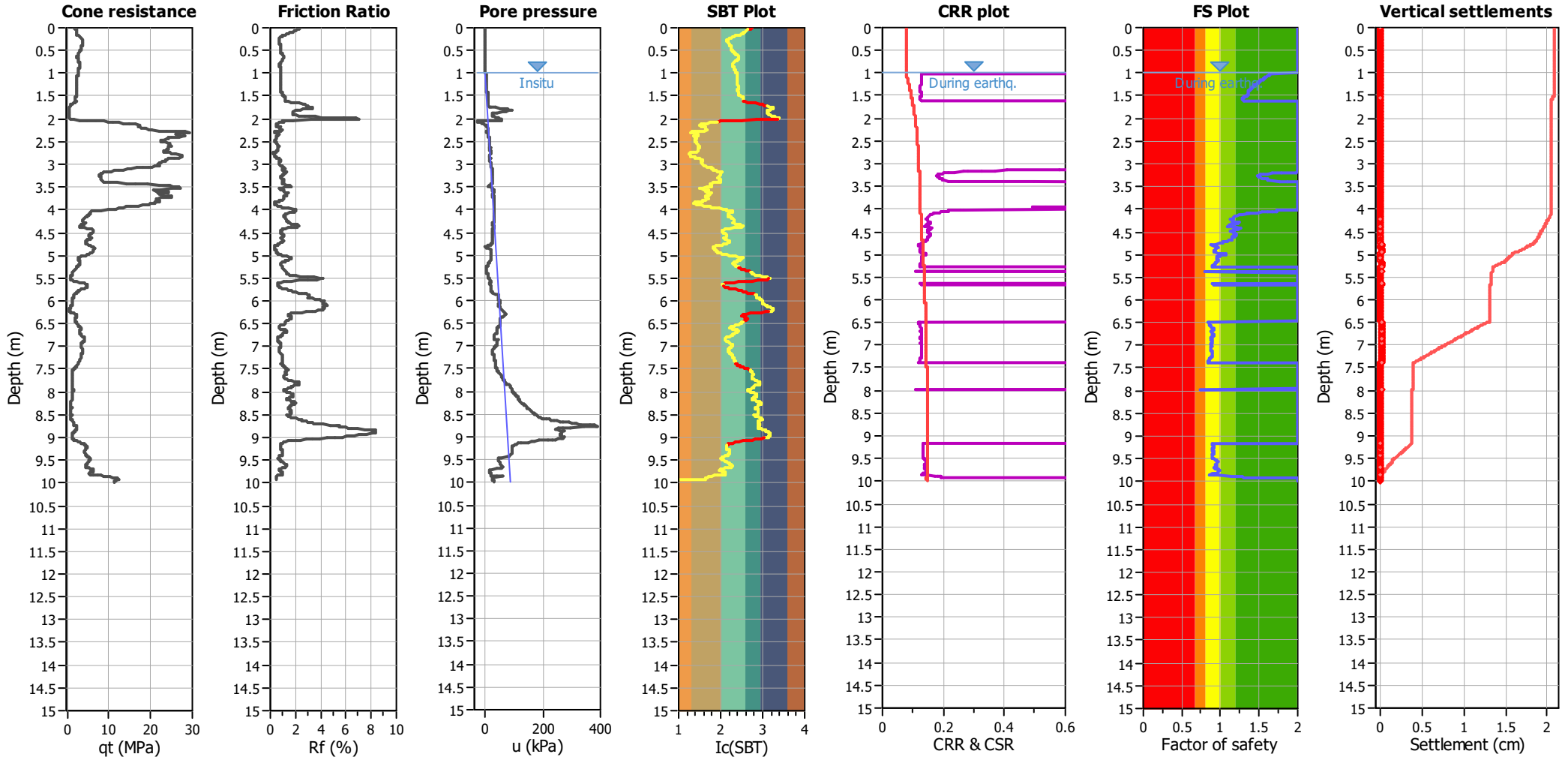
Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.80 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_\sigma$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_\sigma$ applied:	Yes	MSF method:	Method based

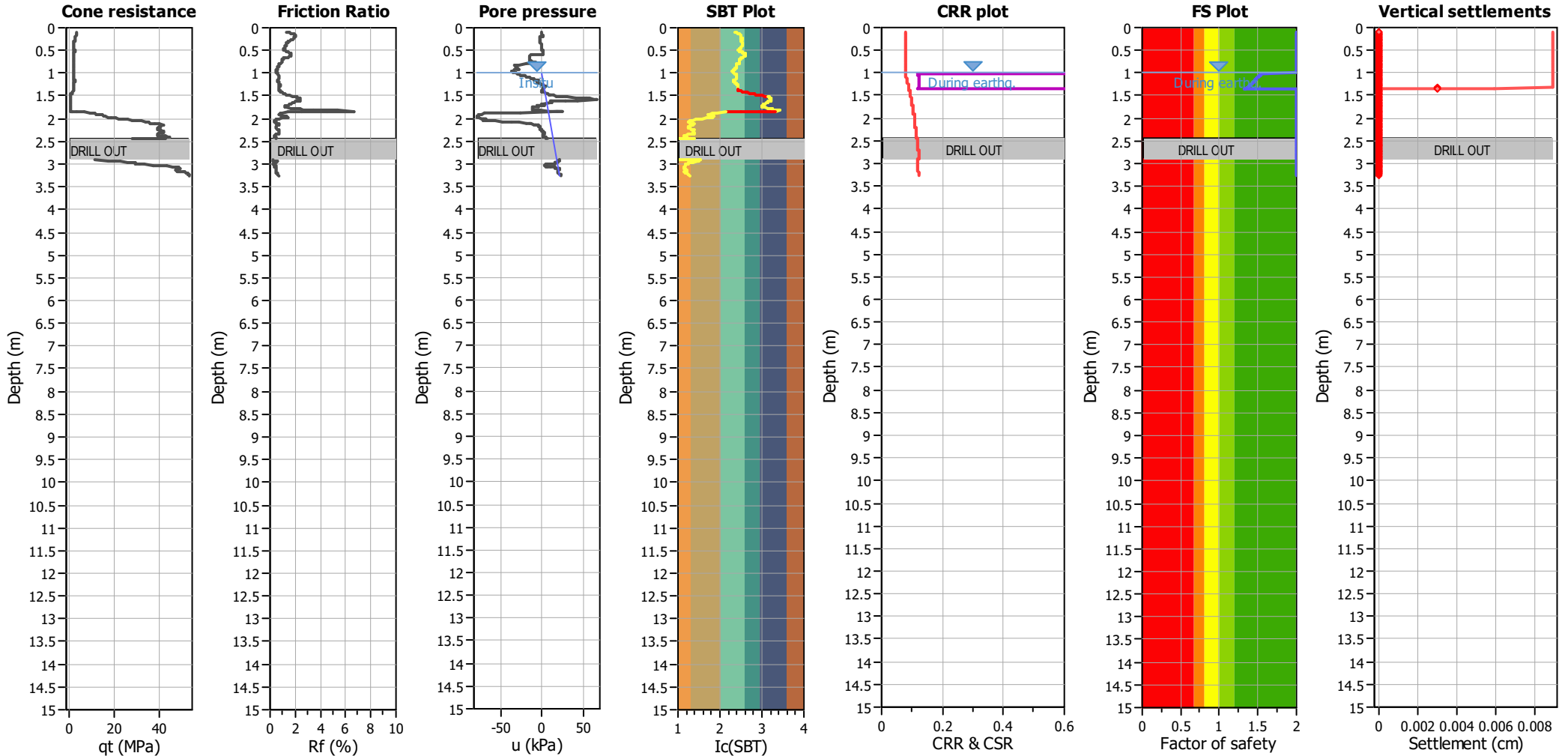


Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.40 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.40 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

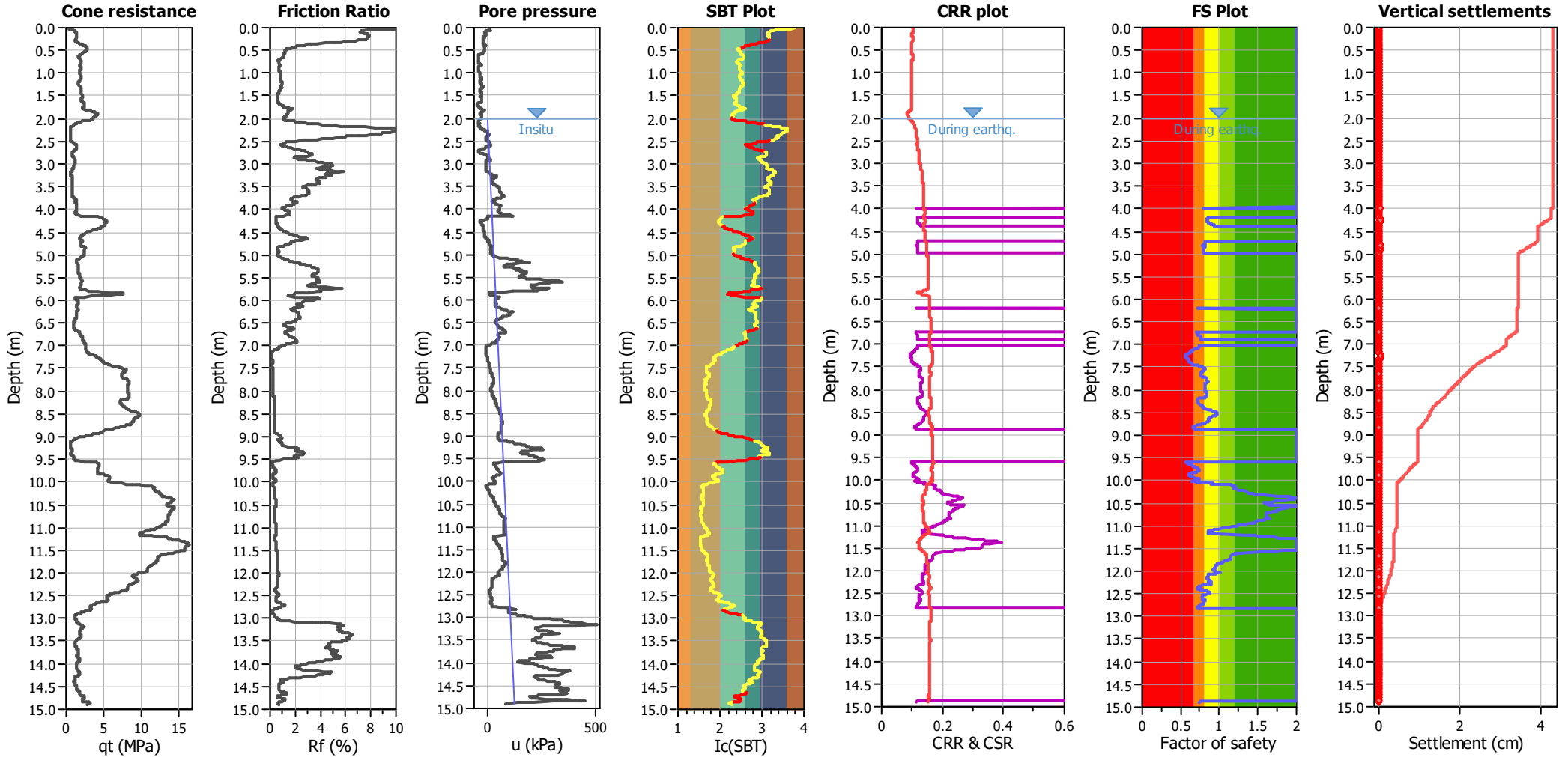


Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

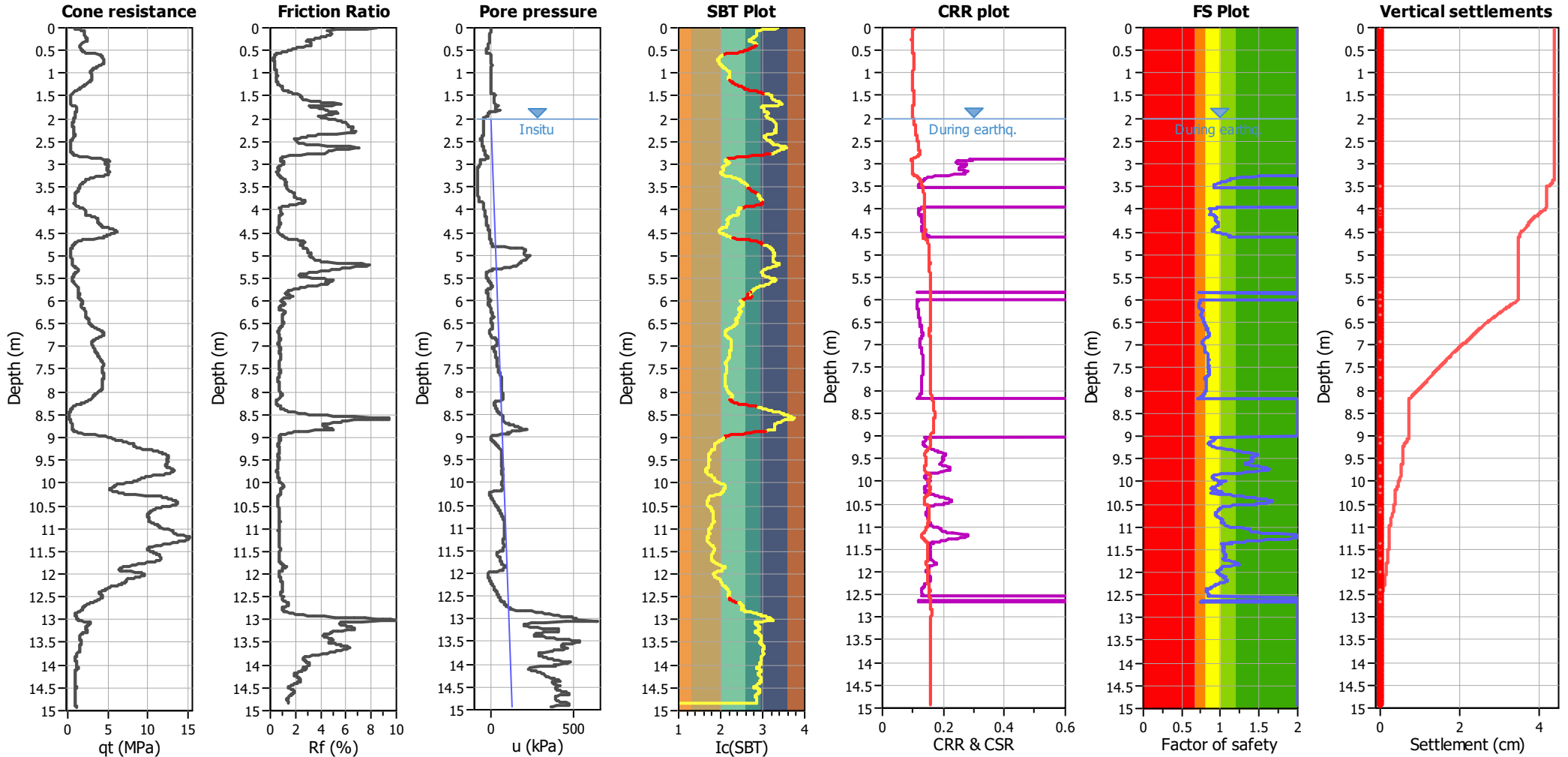




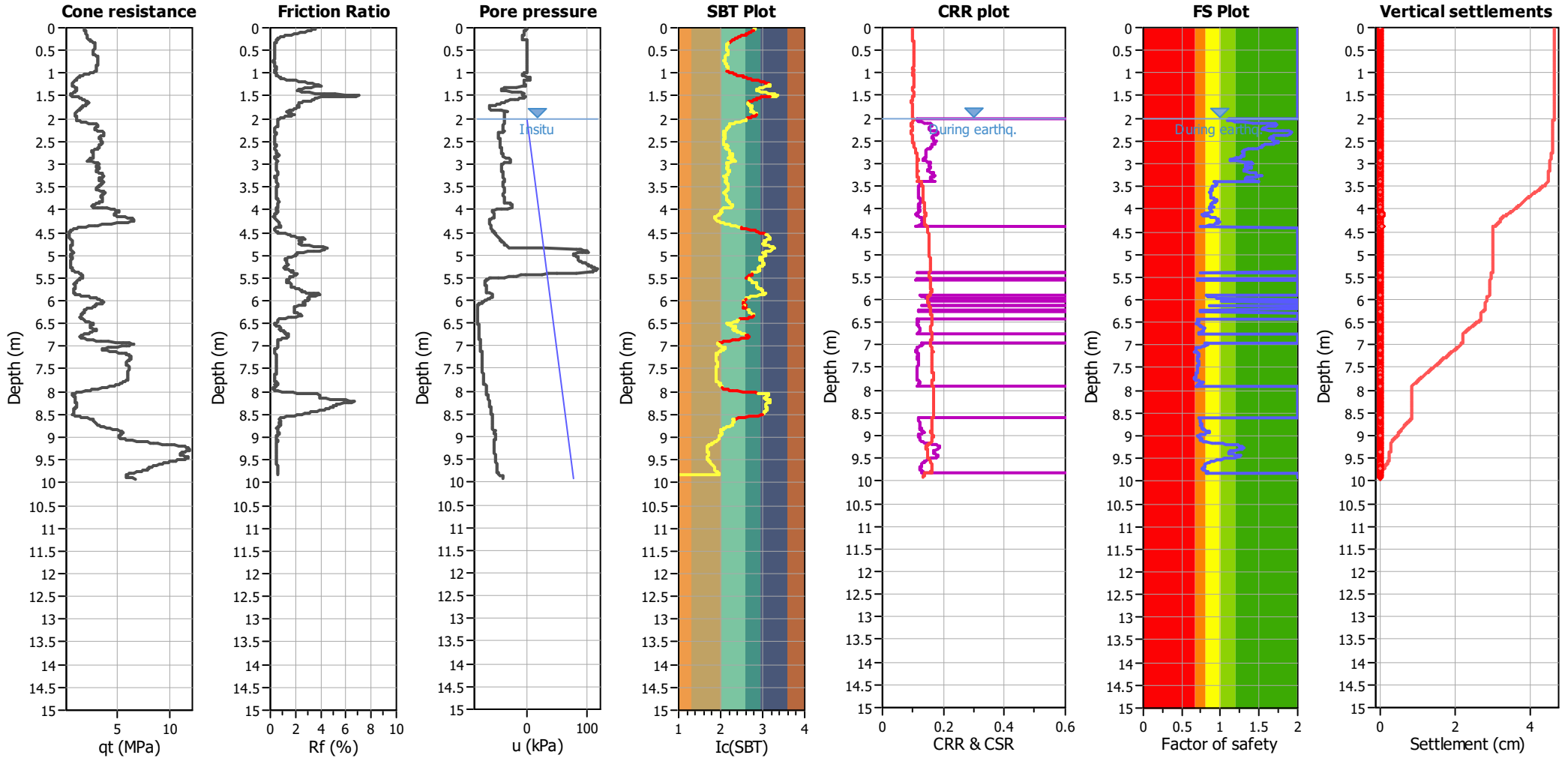
Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



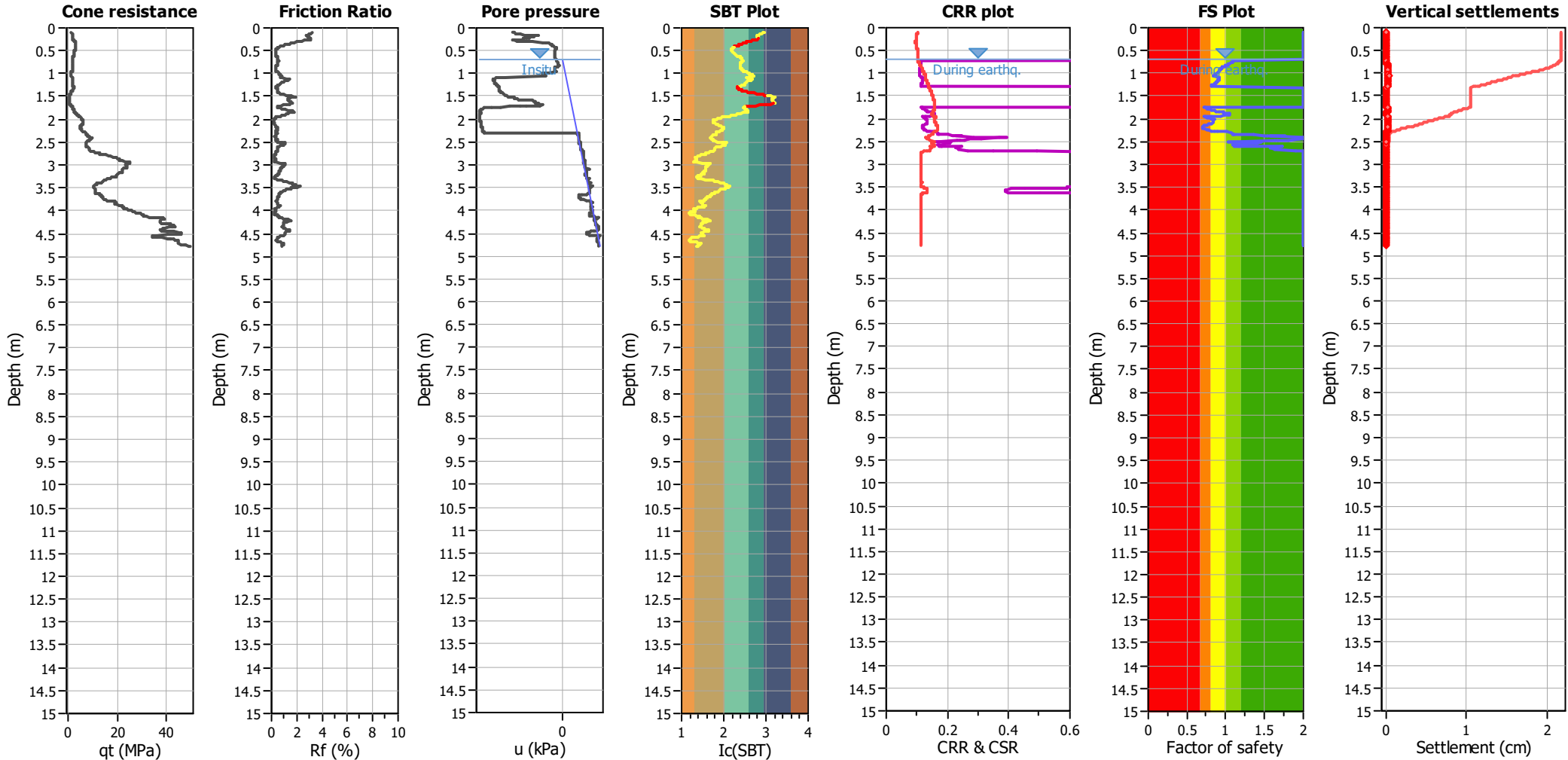
Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



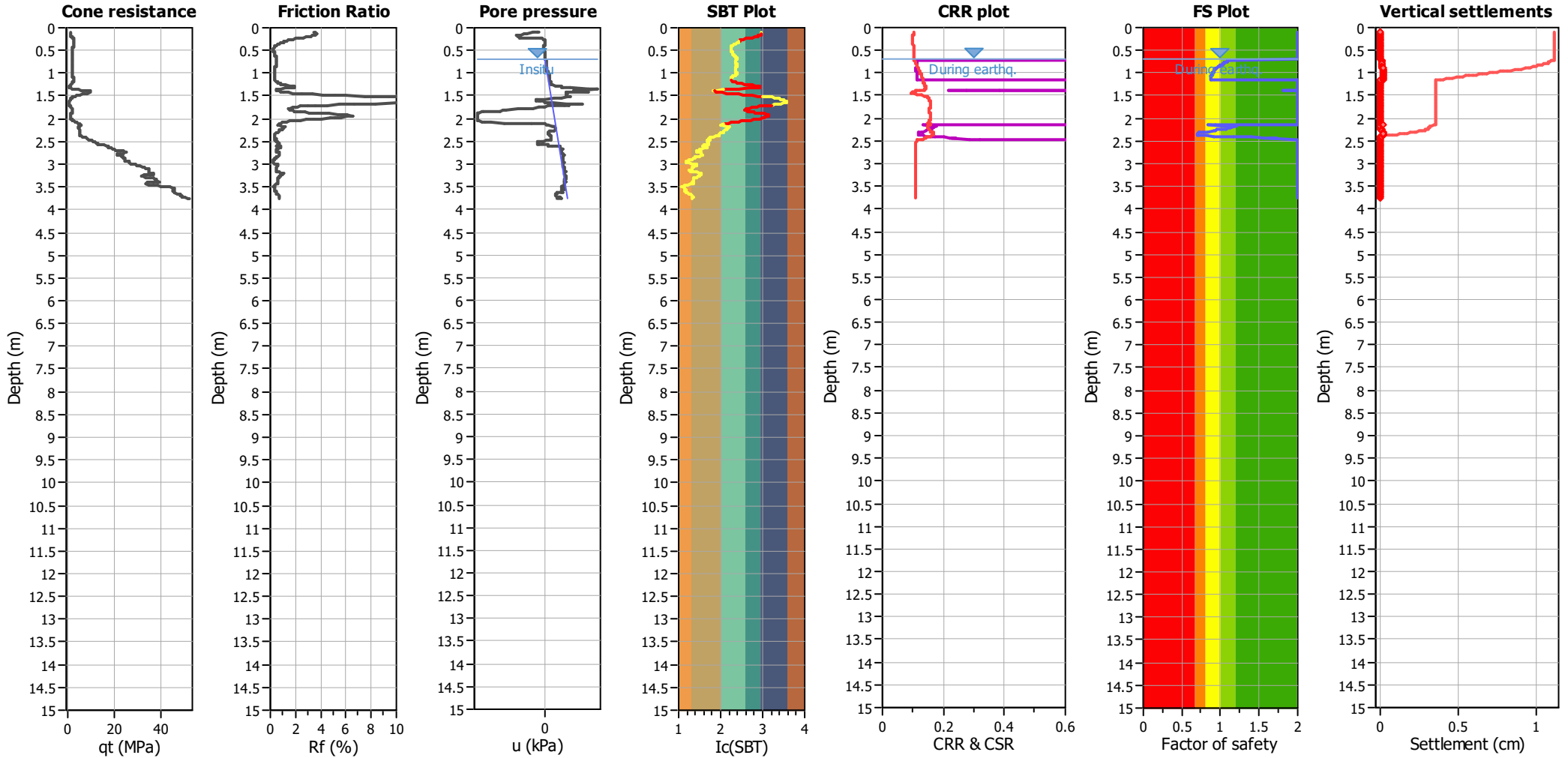
Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



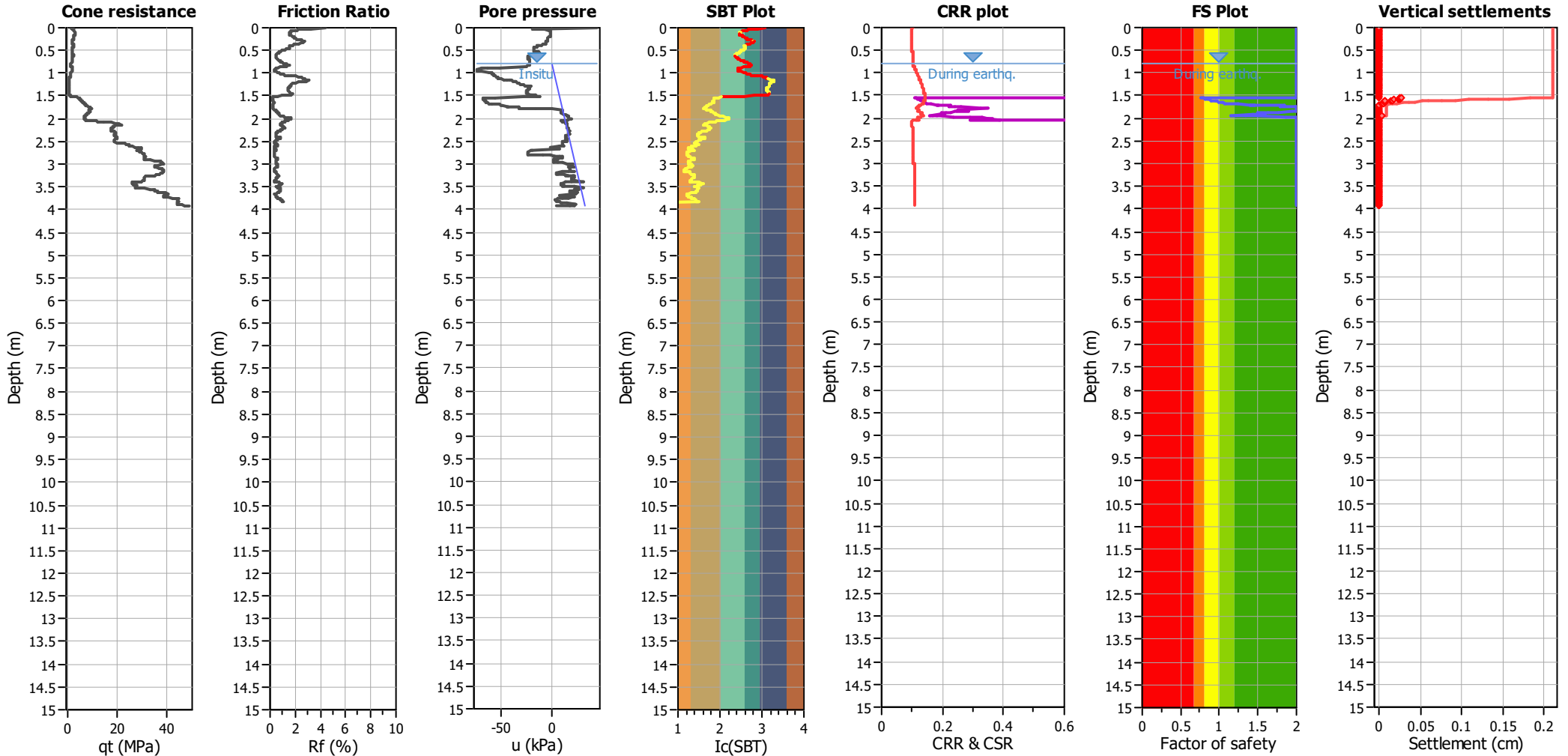
Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



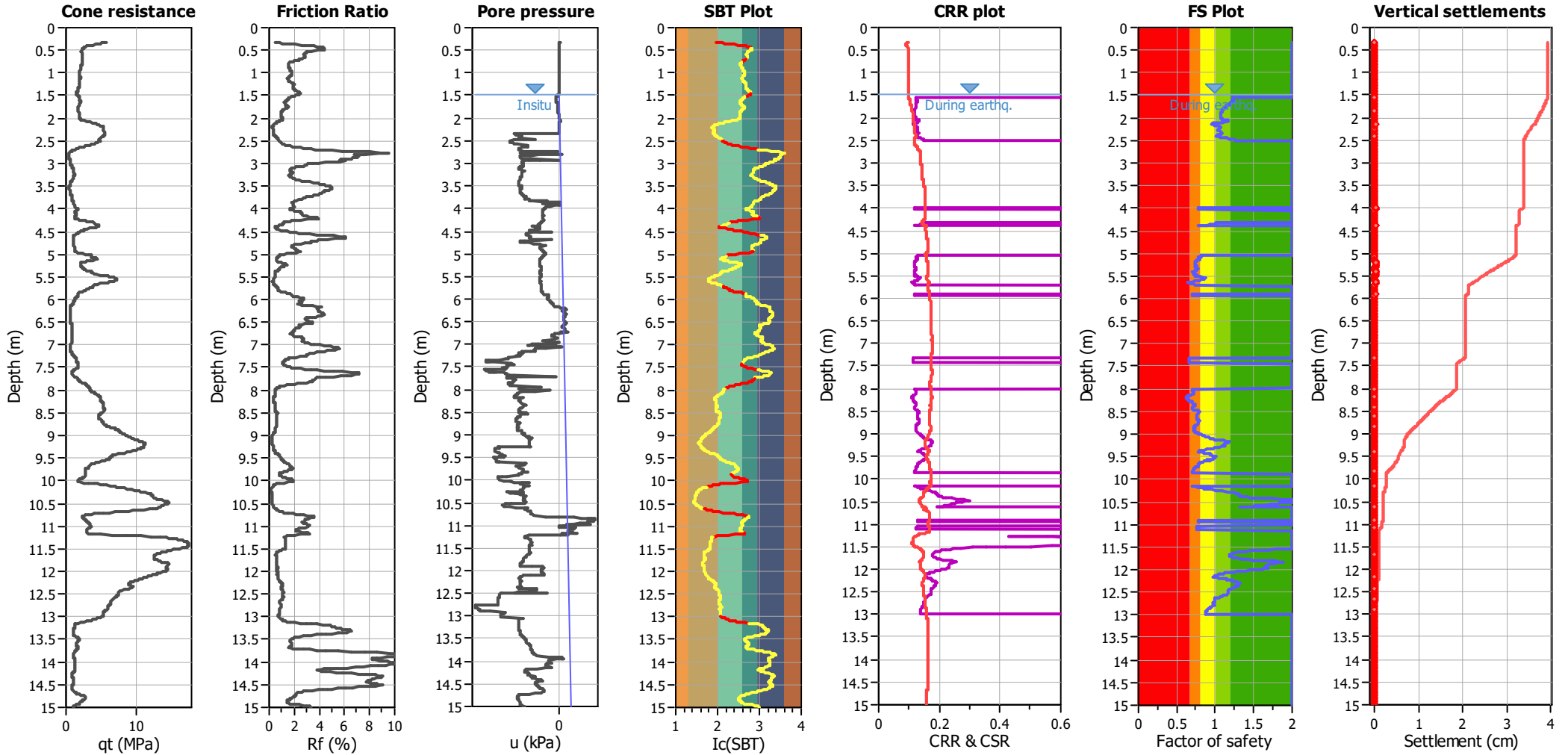
Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

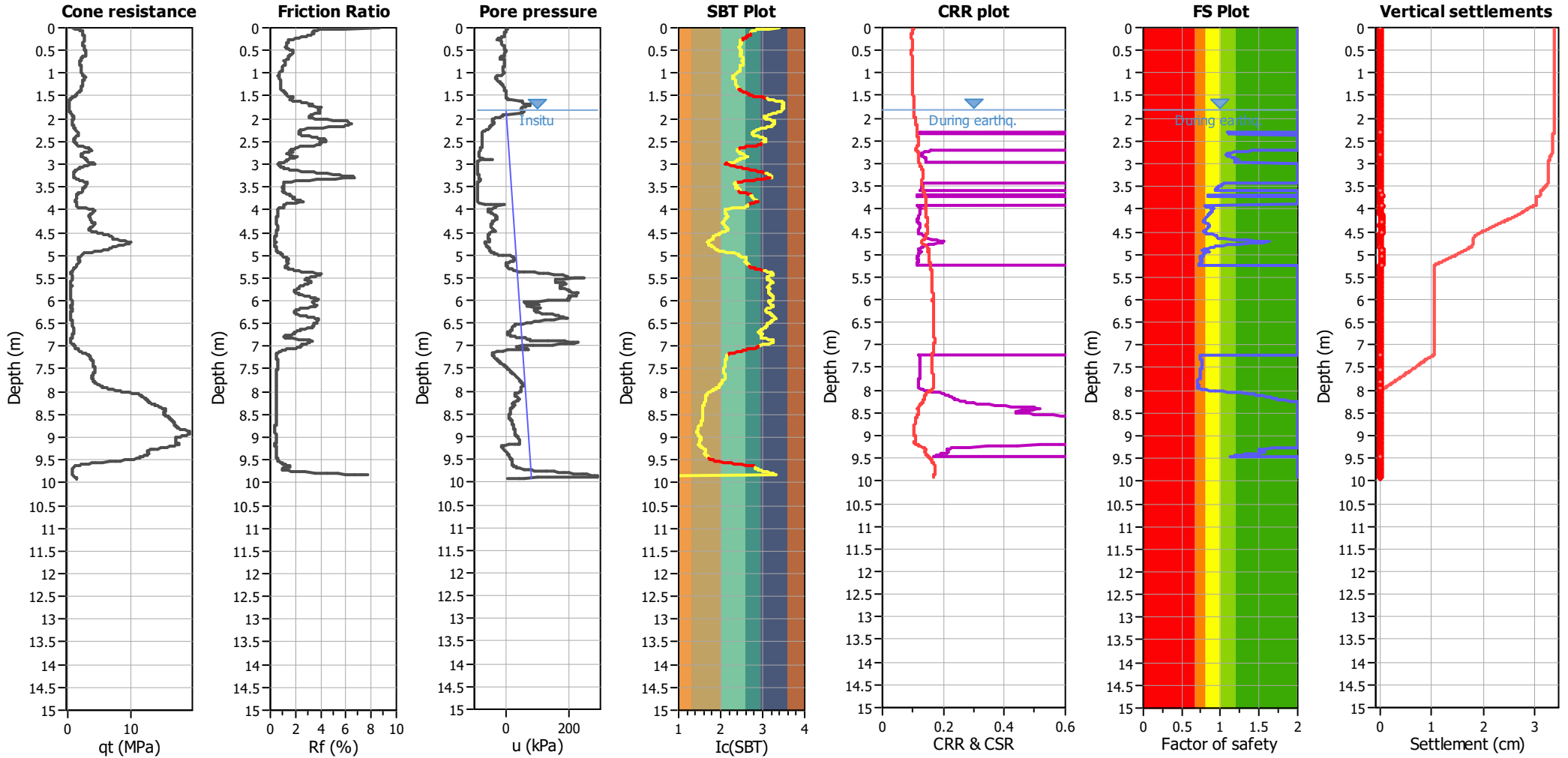


Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.80 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

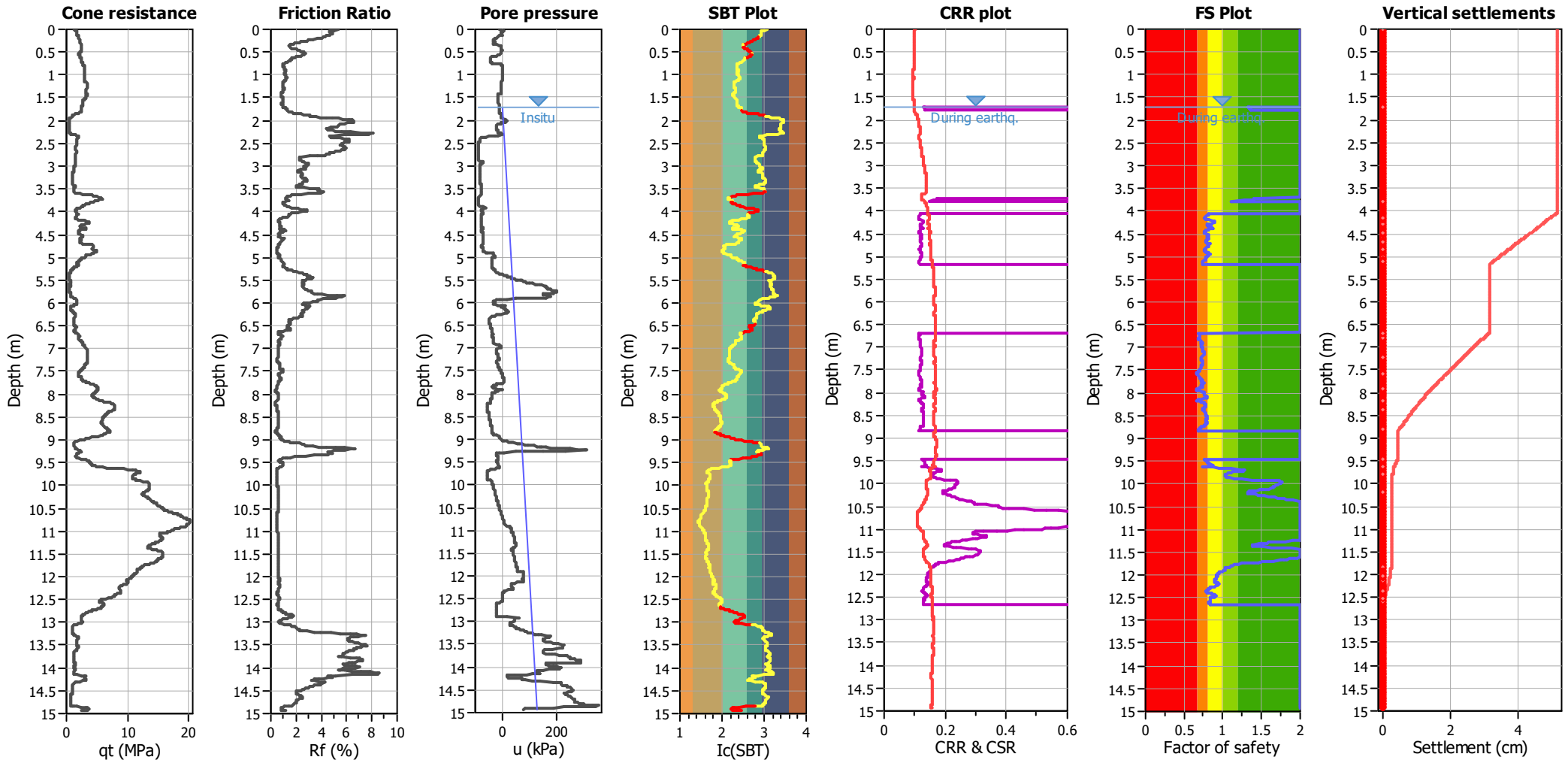


Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.50 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.50 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

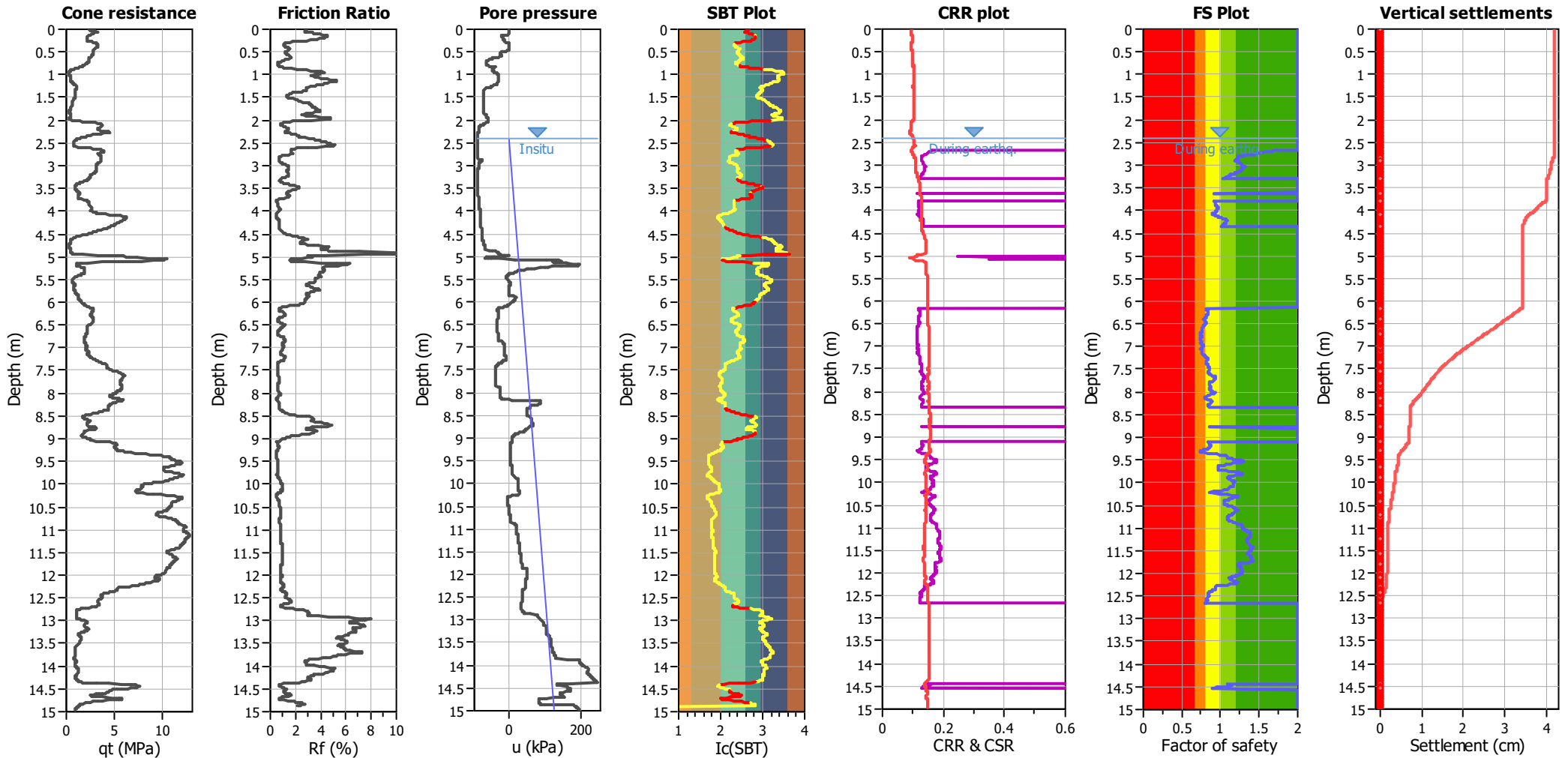




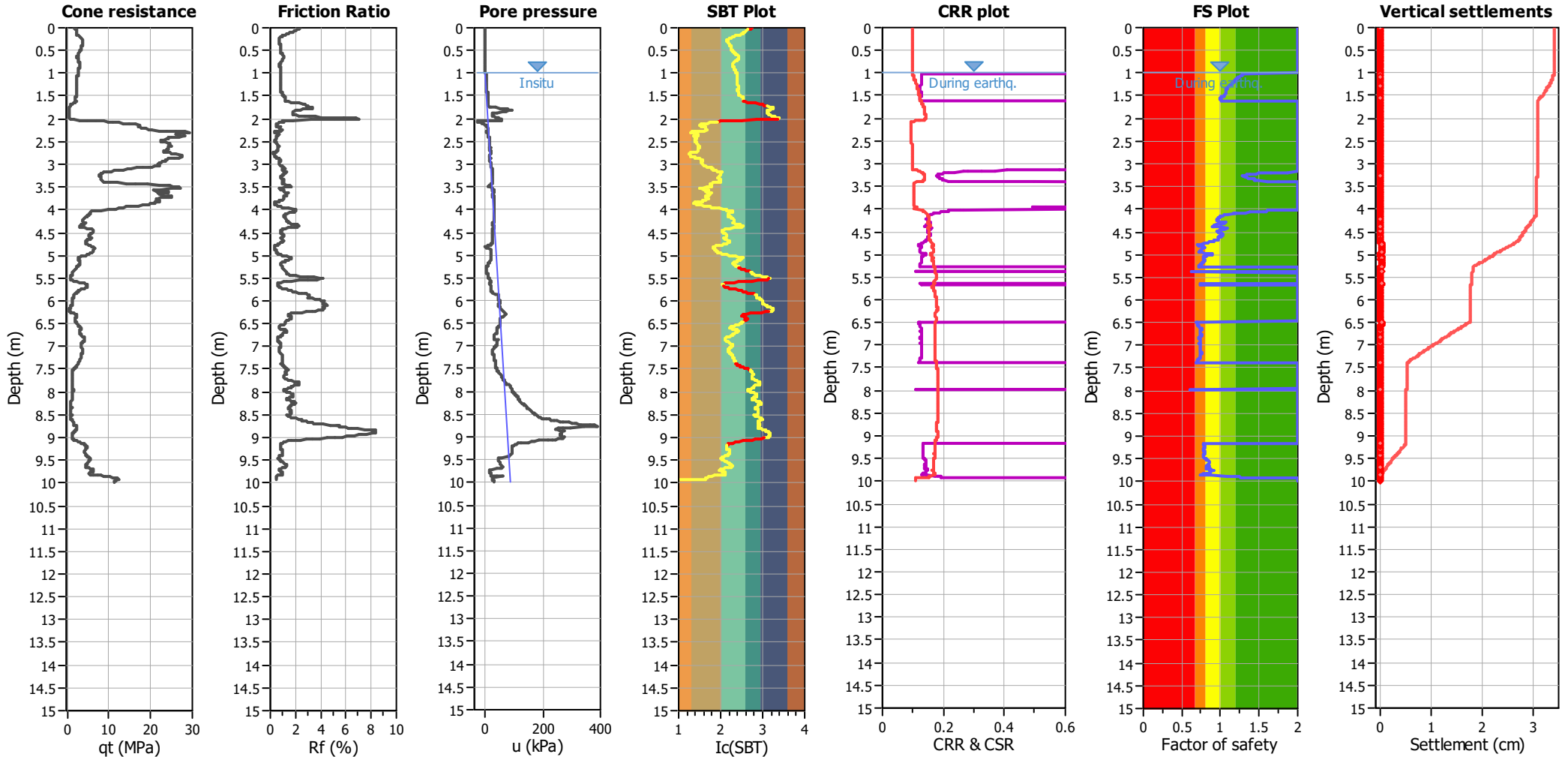
Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.80 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



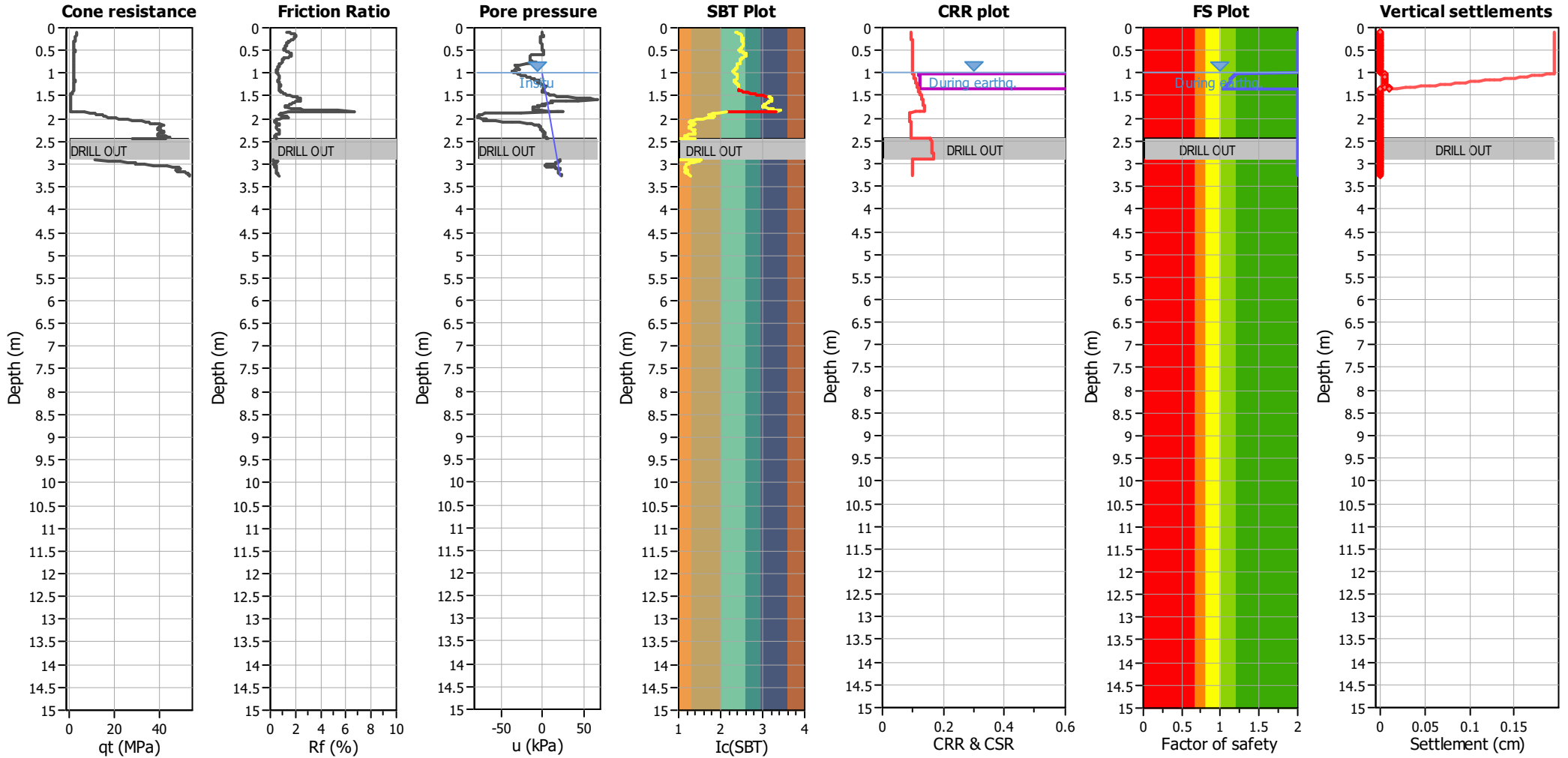
Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



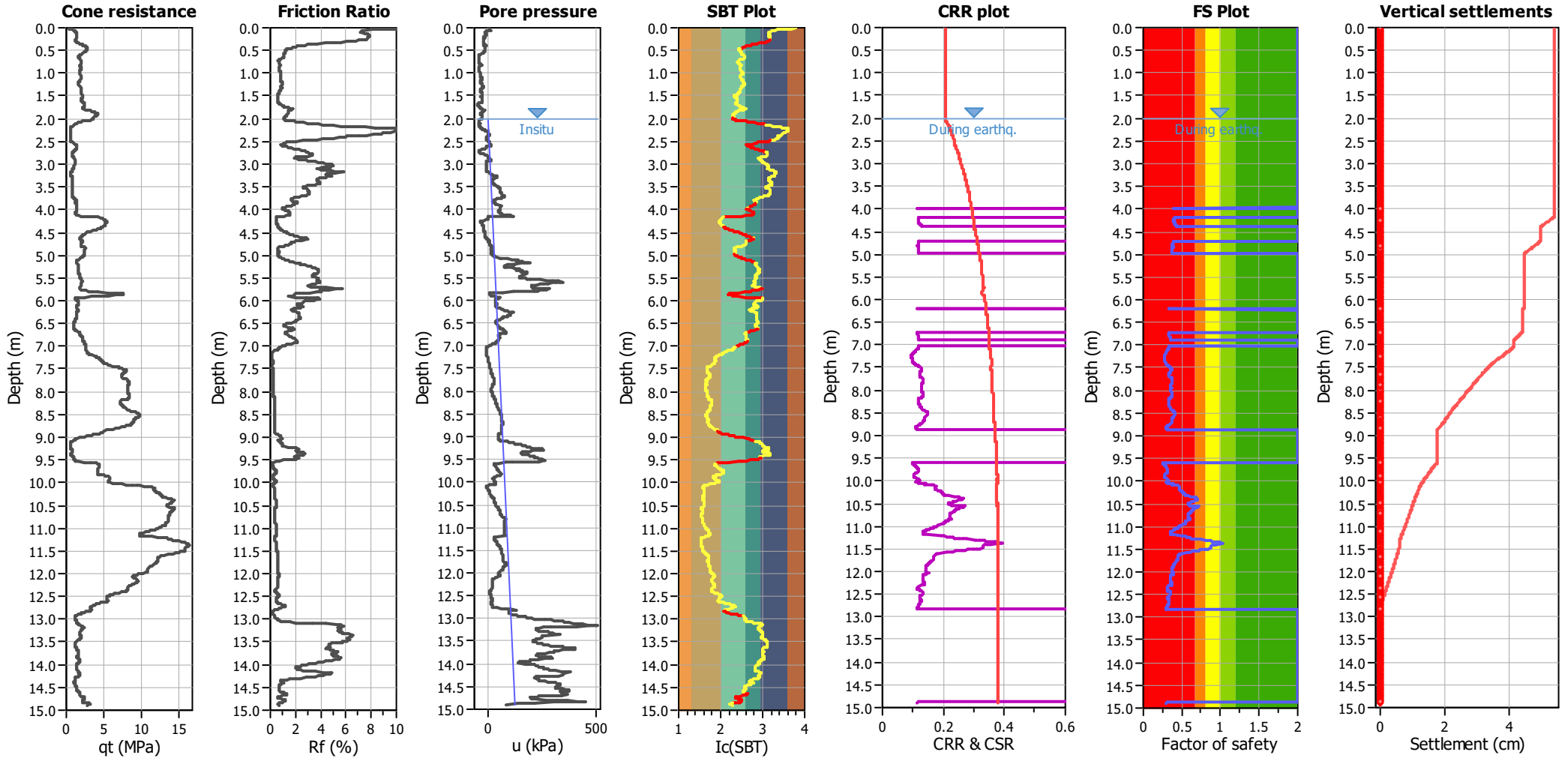
Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.40 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.40 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



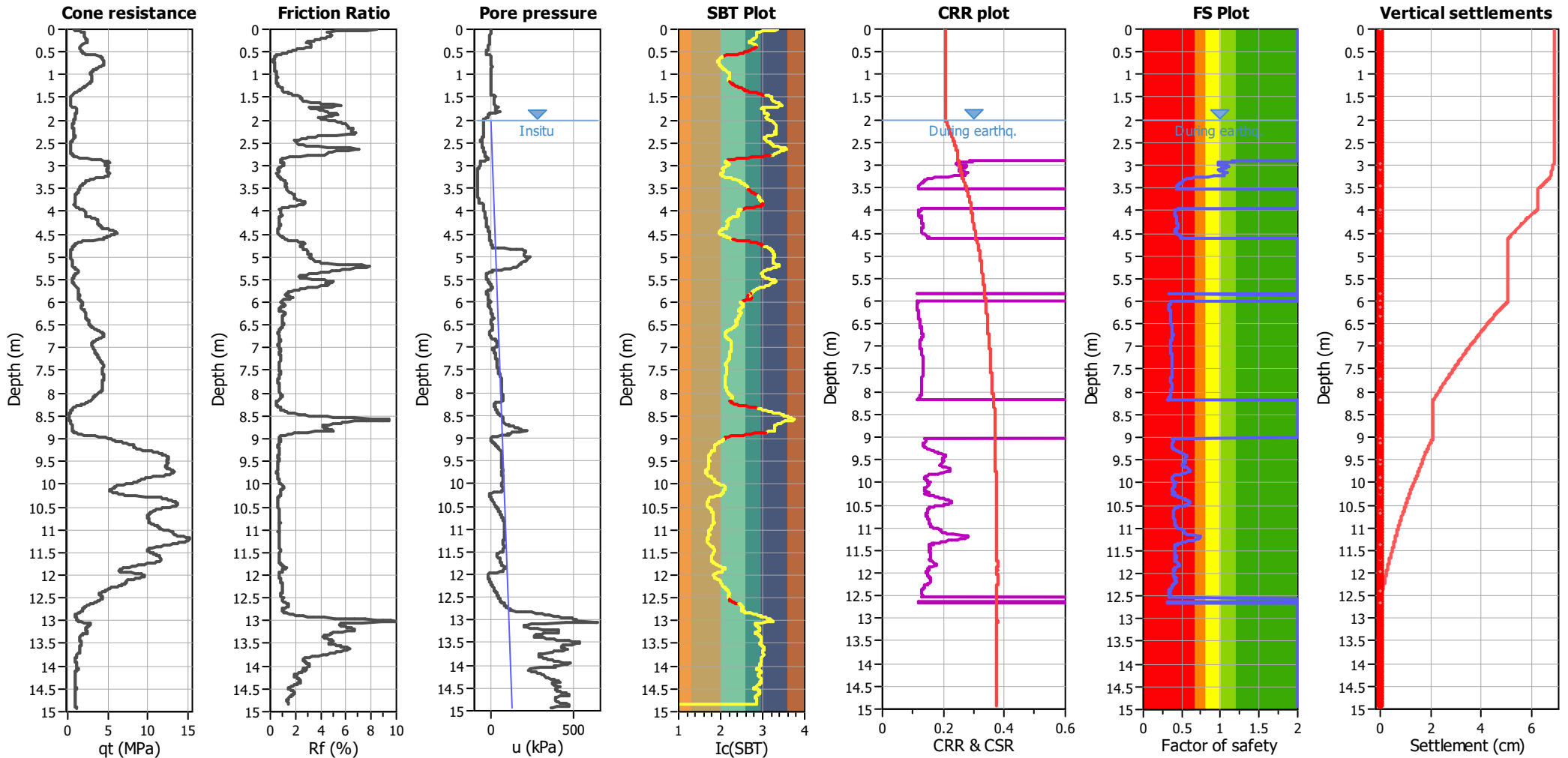
Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



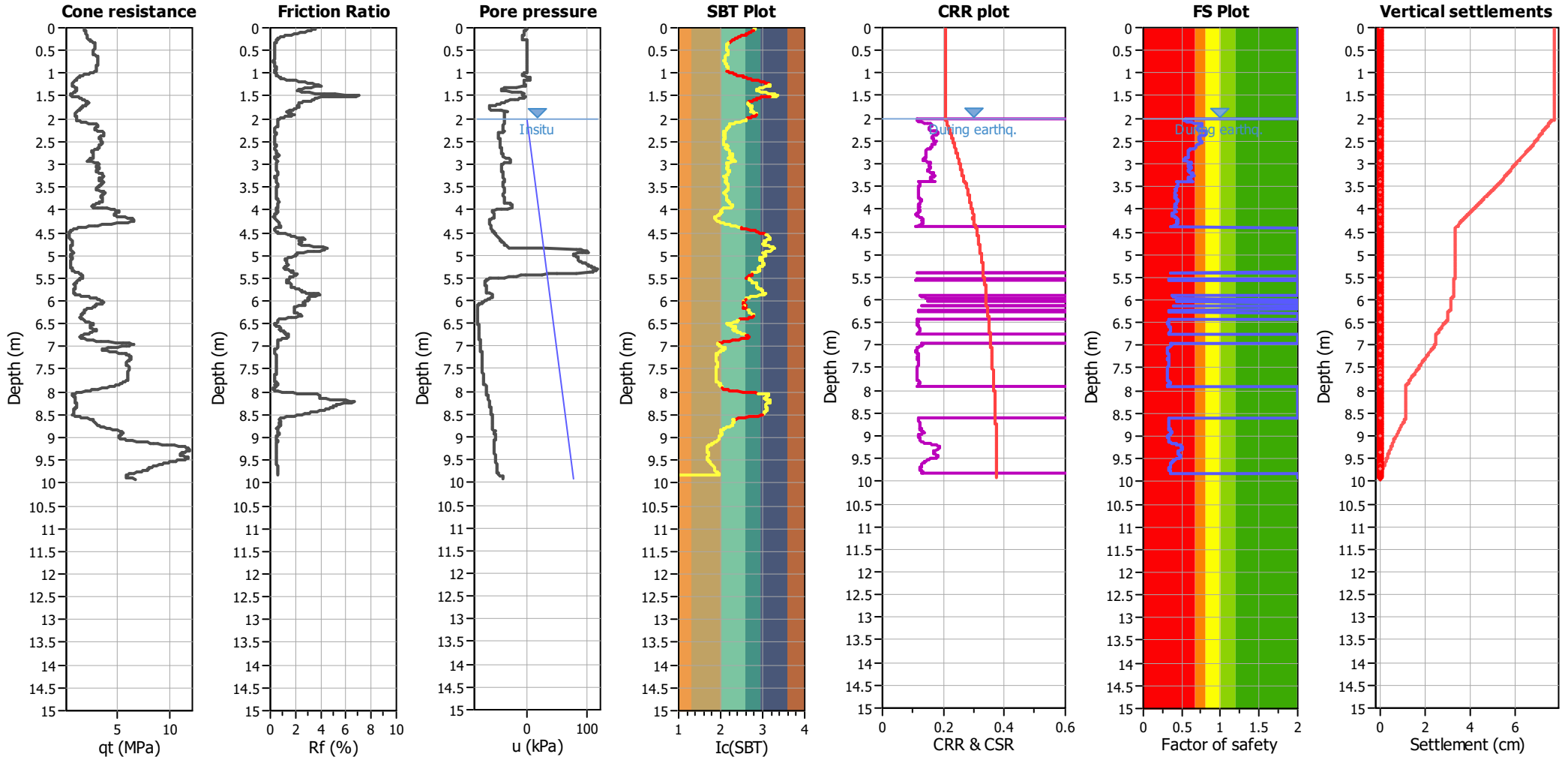
Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

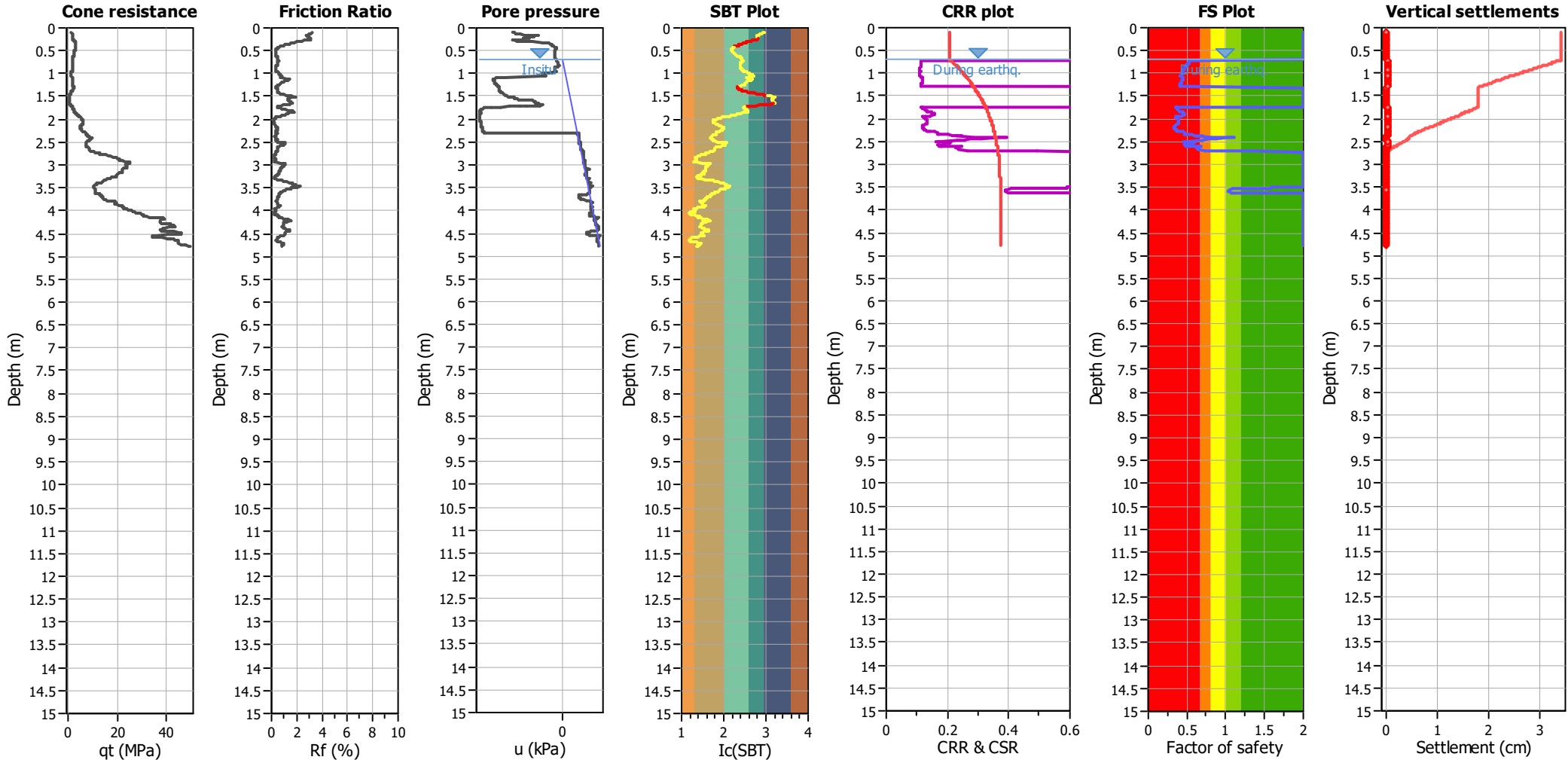


Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

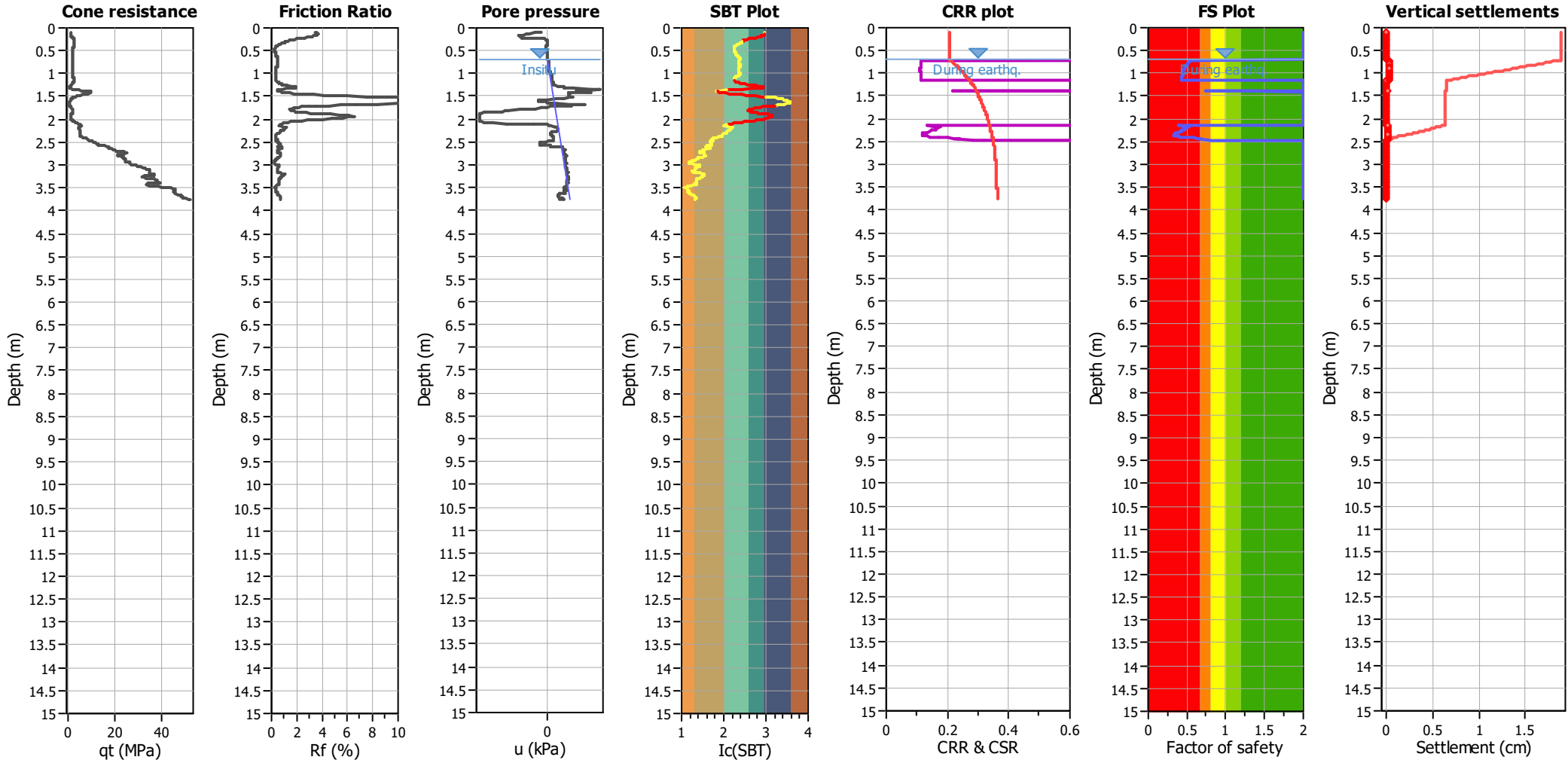


Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

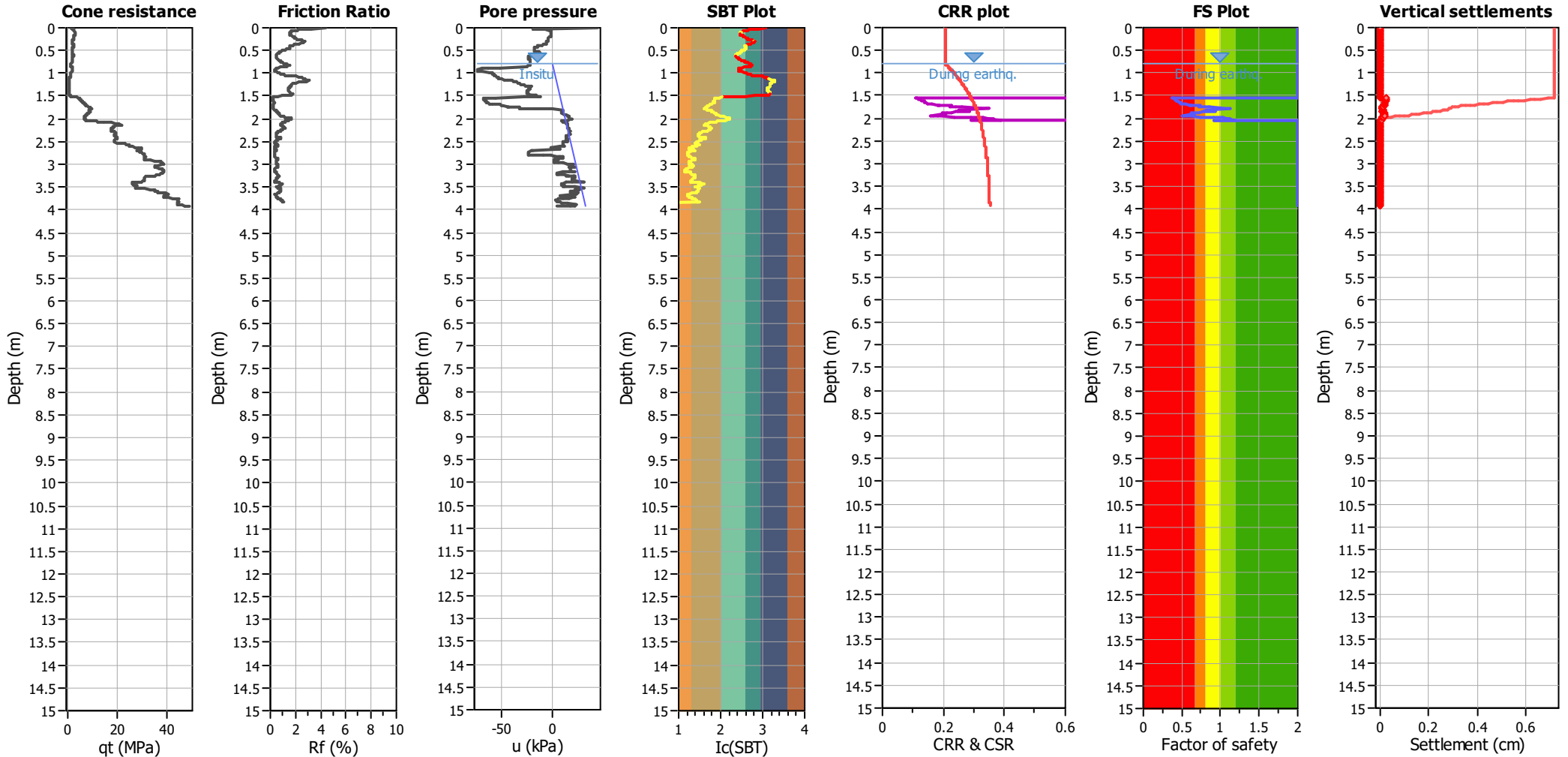




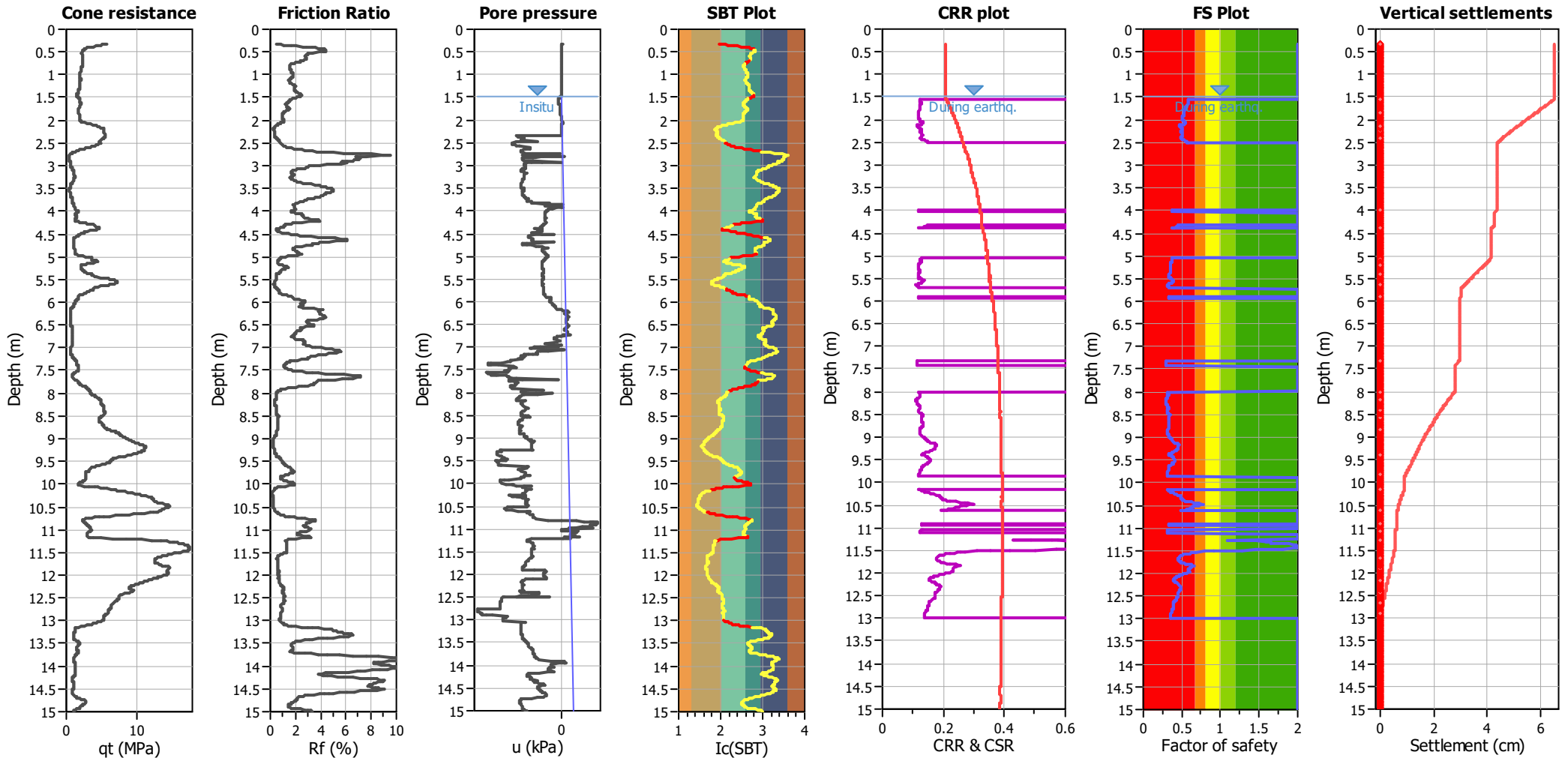
Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



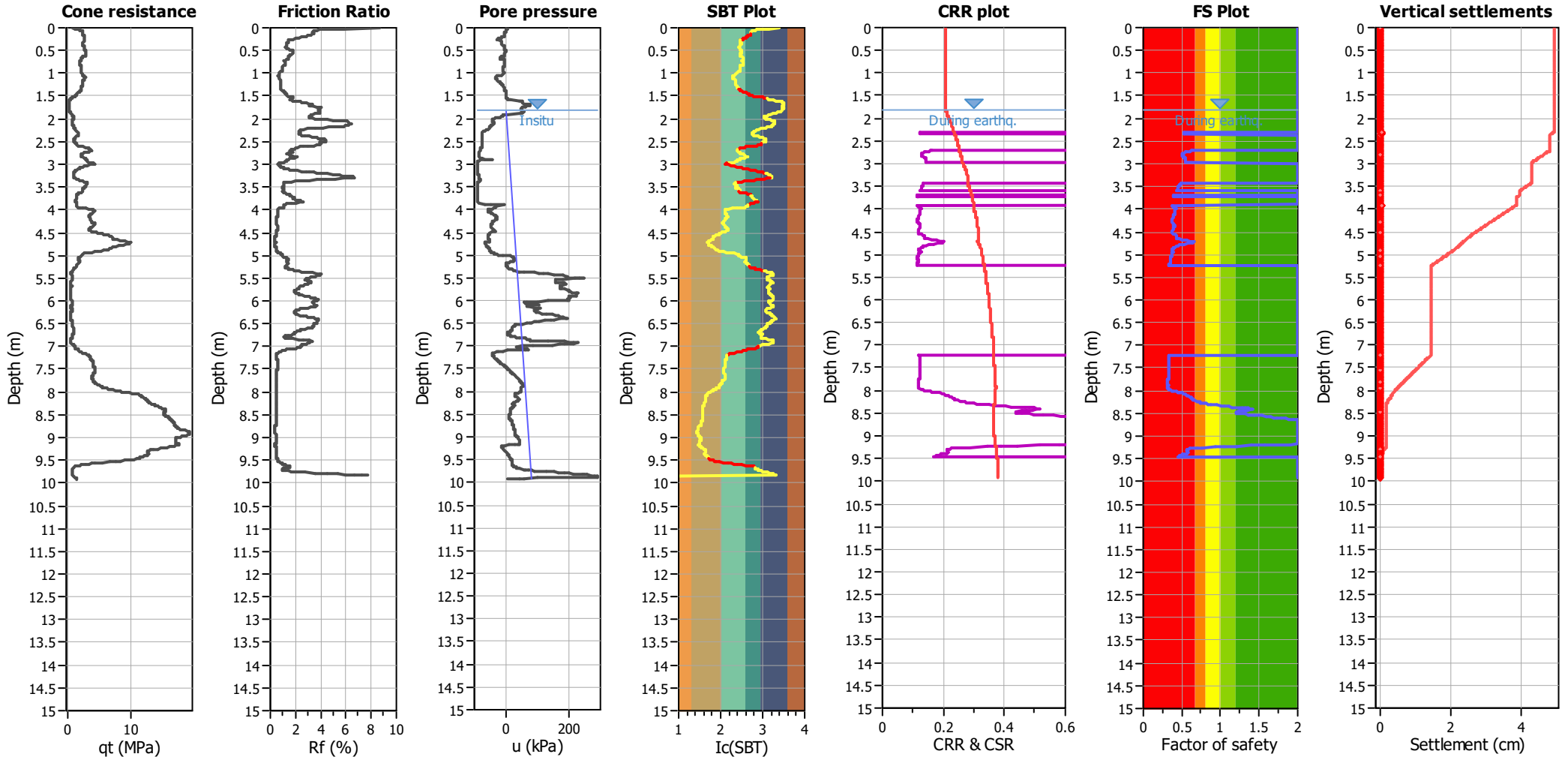
Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



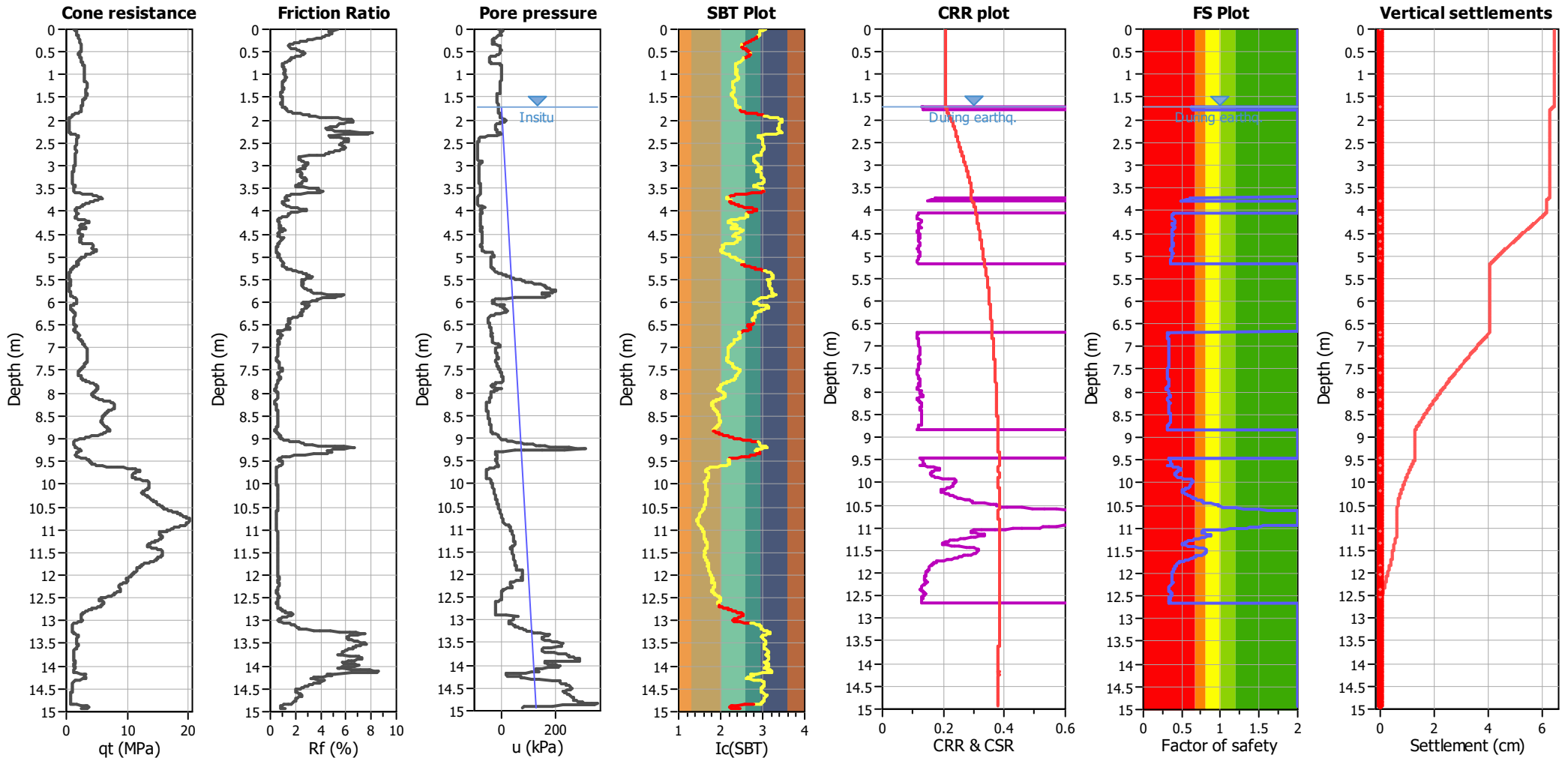
Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.80 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



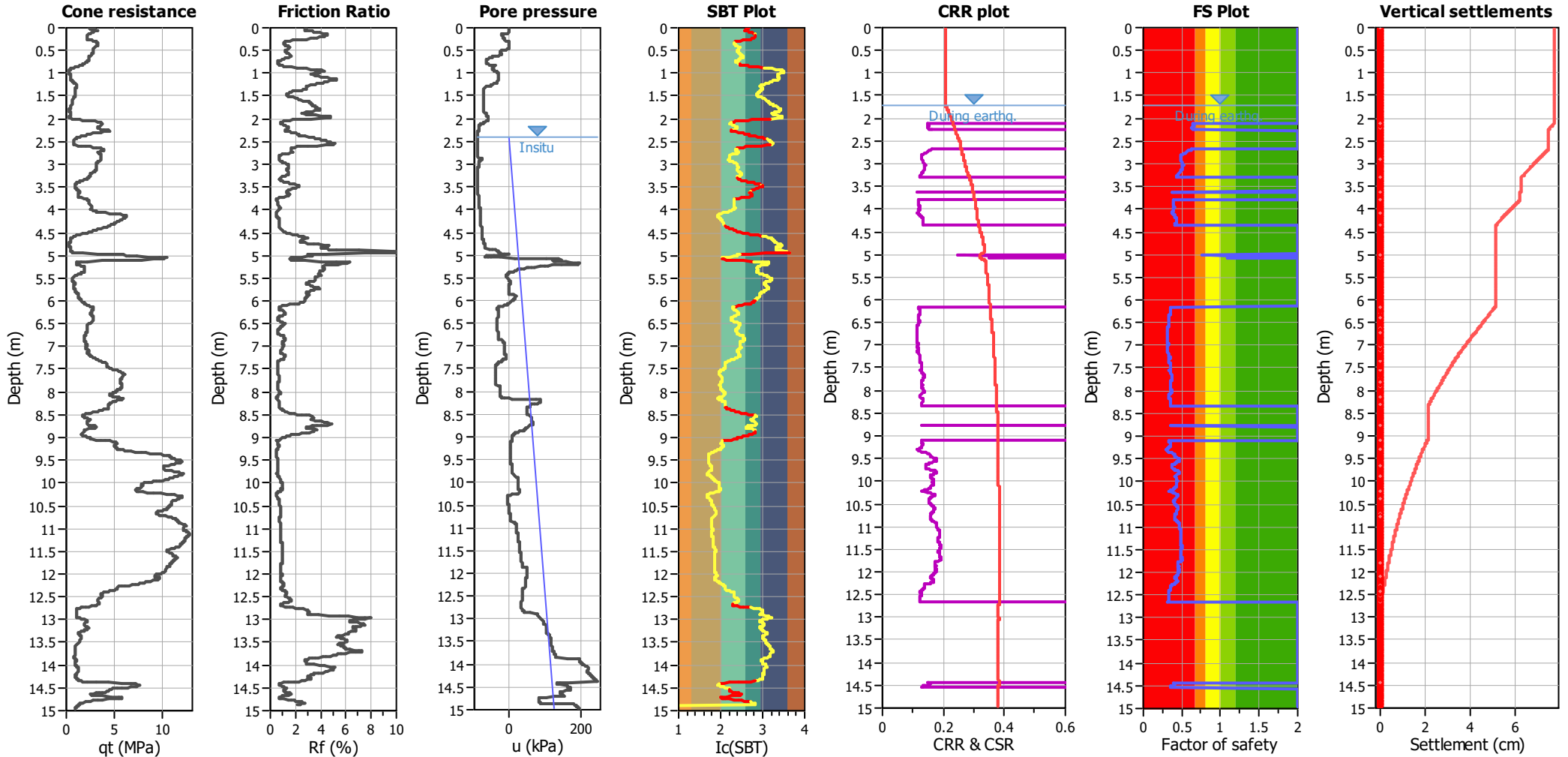
Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.50 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.50 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



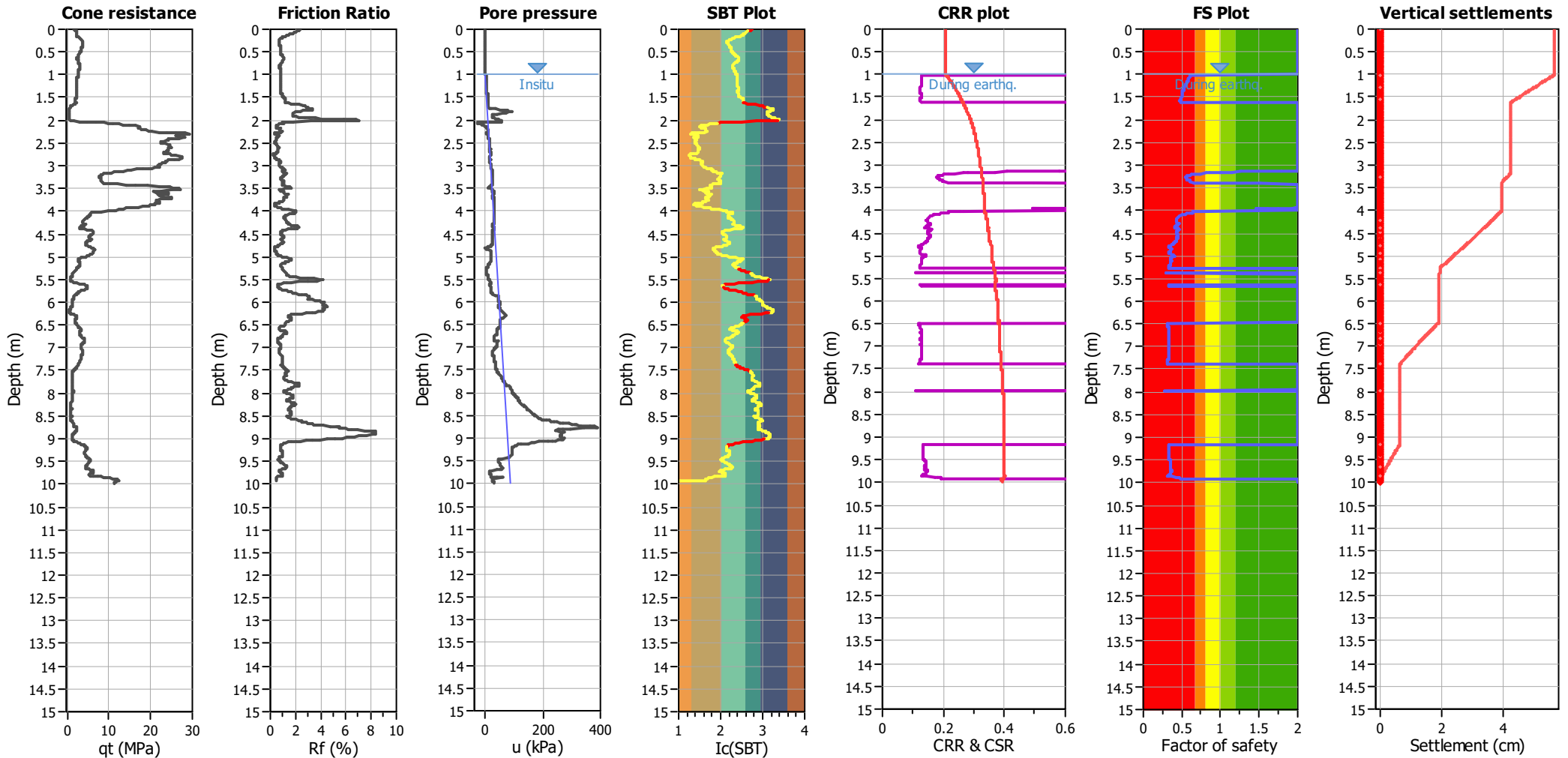
Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.80 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

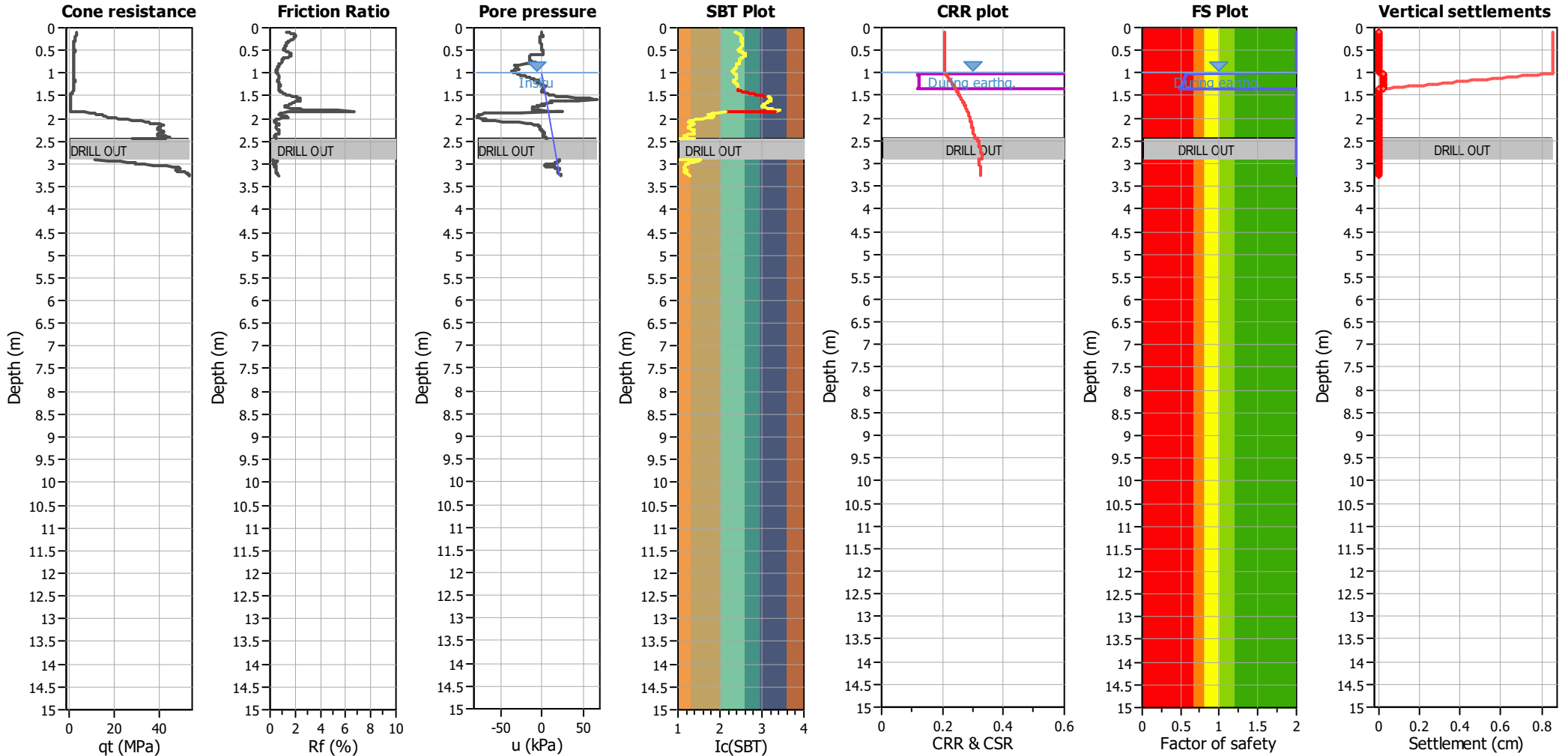


Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.40 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

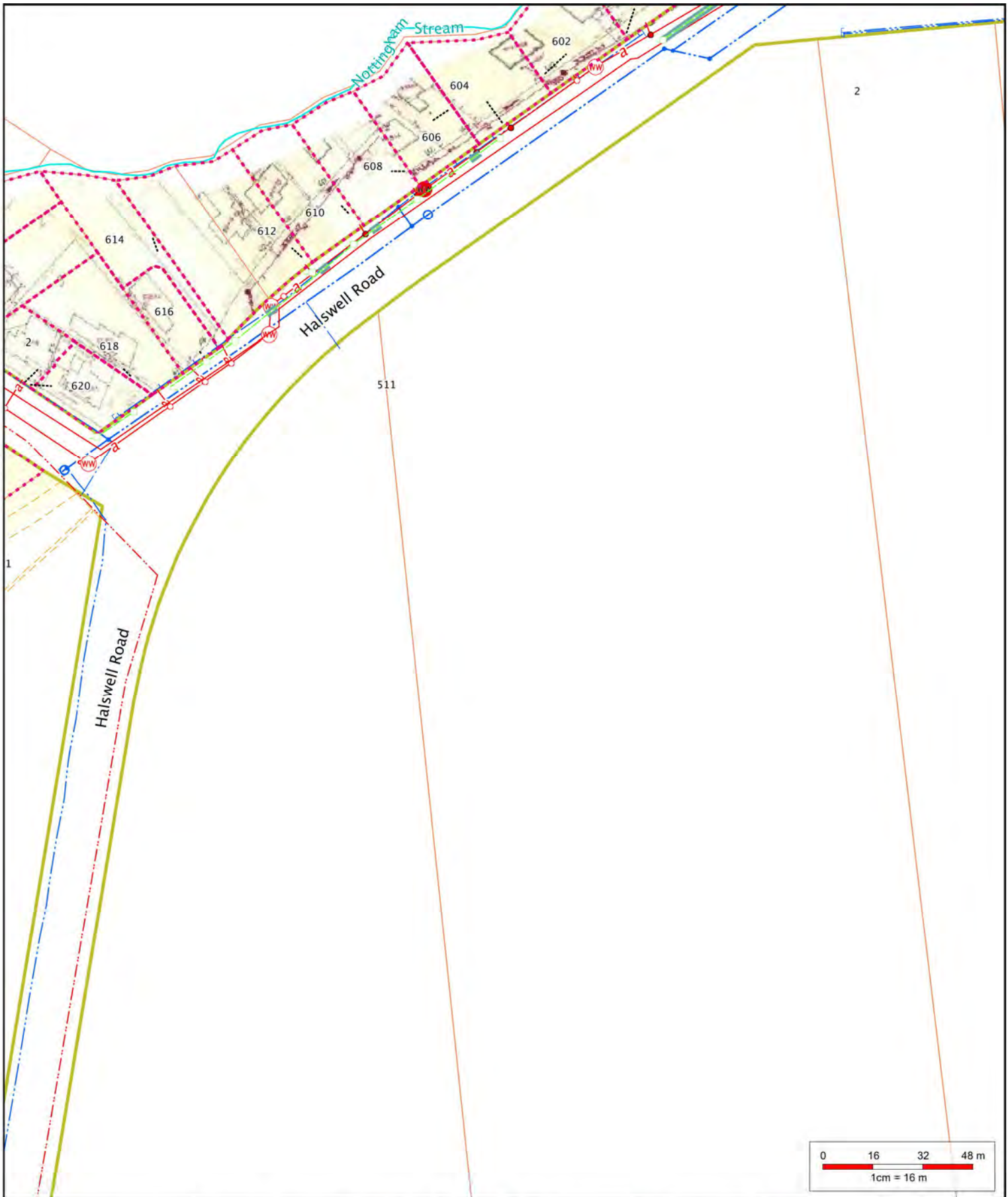


Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



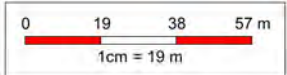


Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based




**1 : 1,600 on A4**  
 18/06/2021 7:42:24 AM  
  
 ph: 941-8300 fax: 941-8385  
 Accuracy not guaranteed. Onsite verification required. Display of data scale dependent, full detail available at 1:500.  
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Private Drainage	Water Intake/Supply	Wastewater	Wastewater	Stormwater	Stormwater
<b>Standard Infrastructure</b>  Bio Gas  Condensate Trap  End Cap  Inlet  Outlet  Valve  Main  Cable	 Inlet  Meter  Outlet  Pump  Restrictor  Valve  Air Release  Butterfly  Flow restriction  Gate  Pressure Activated  Sluice  Valve  Reservoir  Structure  Lateral  Main  Sub Main	 End Cap  Valve  Air Gap Separator  Vent  Eye  Eye (Vertical)  Outfall  Pump  Junction  Access  Flush Manhole  Inspection Point  Standard Manhole  Trap  Vented Manhole  Lateral  Main  Pressure Main	 Lateral Fitting <b>Local Pressure</b>  Control Panel  Boundary Kit  Tank System  Site  Vacuum Chamber  Vacuum Breather <b>Stormwater</b>  Bend  Change  Eye  Flow Restriction  Inlet  Dome Sump  Double Sump  Gross Debris Trap	 Inlet  Inlet Headwall  Pipe End  Silt Trap  Single Sump  Soak Pit  Triple Sump  Junction  Standard Manhole  Outlet  Pump  Structure  Basin  Lateral  Main  Lateral Fitting  Double Sump	<b>All services</b>  Pipe Protection  Abandoned  Proposed  Out of service <b>Landbase</b>  Easement



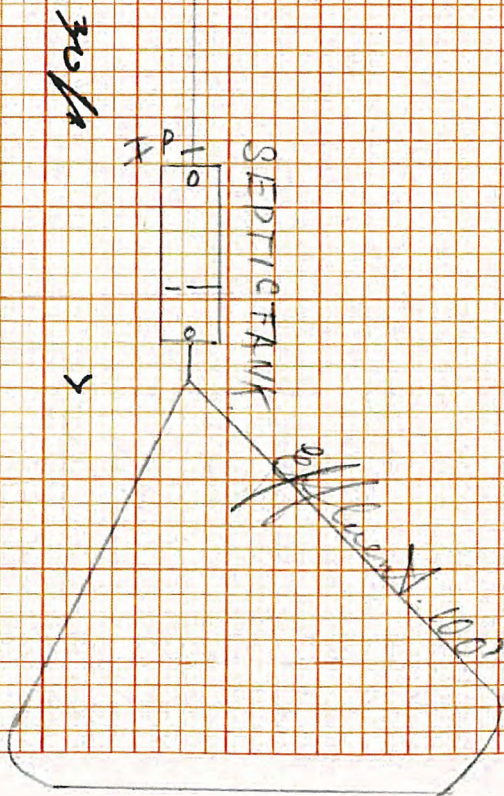
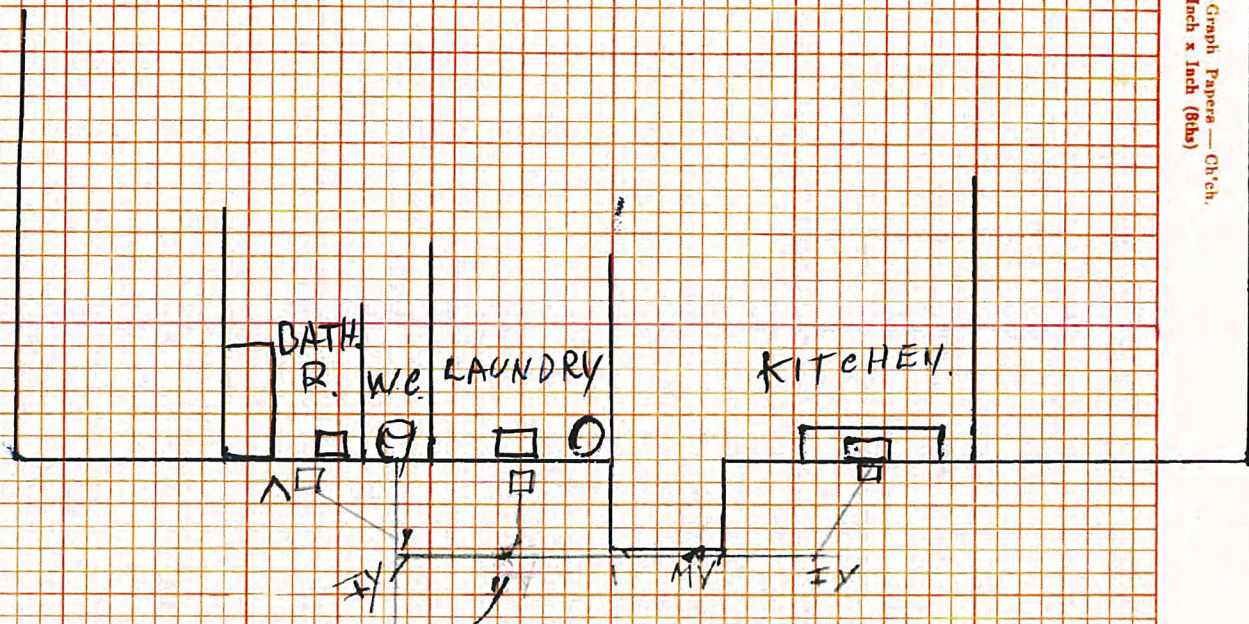

**1 : 1,900 on A4**  
 18/06/2021 7:44:30 AM  
  
 ph: 941-8300 fax: 941-8385  
 Accuracy not guaranteed. Onsite verification required. Display of data scale dependent, full detail available at 1:500.  
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Private Drainage	Water Intake/Supply	Wastewater	Wastewater	Stormwater	Stormwater
<b>Standard Infrastructure</b> Bio Gas Condensate Trap End Cap Inlet Outlet Valve Main Cable	Inlet Meter Outlet Pump Restrictor Valve Air Release Butterfly Flow restriction Gate Pressure Activated Sluice Valve Reservoir Structure Lateral Main Sub Main	End Cap Valve Air Gap Separator Vent Eye Eye (Vertical) Outfall Pump Junction Access Flush Manhole Inspection Point Standard Manhole Trap Vented Manhole Lateral Main Pressure Main	Lateral Fitting Local Pressure Control Panel Boundary Kit Tank System Site Vacuum Chamber Vacuum Breather <b>Stormwater</b> Bend Change Eye Flow Restriction Inlet Dome Sump Double Sump Gross Debris Trap	Inlet Inlet Headwall Pipe End Silt Trap Single Sump Soak Pit Triple Sump Junction Standard Manhole Outlet Pump Structure Basin Lateral Main Lateral Fitting Double Sump	Lateral Fitting Single Sump Soak Pit Inspection point Manhole <b>All services</b> Pipe Protection Abandoned Proposed Out of service <b>Landbase</b> Easement

Mr. J. Legg

Halswell.

Gormack Graph Papers — Ch'ch.  
No. 10 : Inch x Inch (8hs)



# Your guide to the pressure wastewater system



**For alarms call**

**Christchurch  
City Council**



**(03) 941 8999**

# If the alarm sounds

1. The alarm noise can be turned off by pressing the button underneath the alarm panel. The alarm light on the panel will remain on.

If your pressure wastewater system has had a short term build up of wastewater then the system will automatically clean itself and the alarm light will go out.

2. If the alarm light is still on after one hour (1 hr) then call the Christchurch City Council on (03) 941 8999. The Council number is also on the alarm panel.
3. The Council call centre operator will ask you a series of questions to help determine the urgency and nature of any repairs that may be required.
4. The Council call centre operator will ask for your name and contact number so that the maintenance contractor can call you regarding any repairs.
5. The system has a 24hr emergency storage capacity. However, while waiting for any repairs you should try to minimise the amount of wastewater going through the system.
6. If the alarm sounded because of a short term build up of wastewater and then cleared you should consider what might have made this happen (for example flushing inappropriate items) and avoid this happening again.
7. If you notice any irregularity with the system (for example the alarm sounding often), contact the Christchurch City Council on (03) 941 8999.



Press the button located under the alarm panel. This will turn off the sound but the light will remain on.

Wait an hour and then check to see if the light on the alarm panel is still on.

If the light on the alarm panel is no longer lit then no further action is required.

If the light on the alarm panel is still on then call the Christchurch City Council on (03) 941 8999.

The call centre operator will ask for your address, name and contact number.

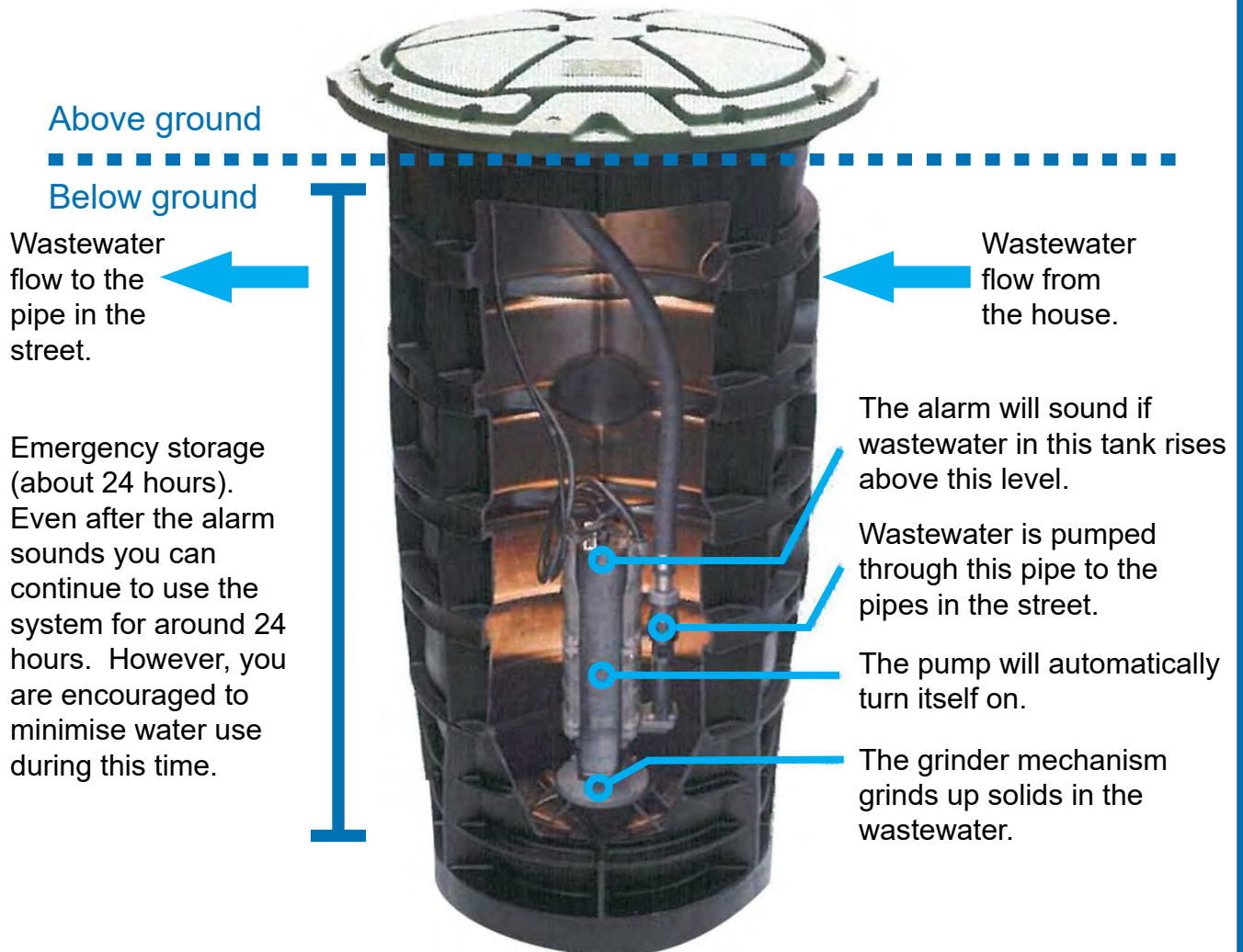
# The pressure wastewater system

**The wastewater system for this property is a pressure wastewater system.**

A pressure wastewater system includes an individual pump and tank. The pump is located within the tank. The tank is located underground and you will only see the lid at the surface. Wastewater from your house flows through a pipe (a private lateral) to the tank. The tank then pumps the wastewater to the pipes in the street. From the street the wastewater goes to the wastewater treatment plant.

The pressure wastewater system is very reliable and robust. There is very little you need to do and very little that can go wrong.

## The pressure wastewater system



# Using the system

There are a few things you need to know to ensure that the pressure wastewater system runs smoothly. The system operates like a normal wastewater system. It takes wastewater from your toilet, sink, shower, bath, dishwasher, and washing machine and transfers it to the wastewater pipes in the street, and onto the wastewater treatment plant.

To avoid blockages and damage to the pressure wastewater system there are a number of items that should not be disposed of via the system.

**The following items should not be flushed down the toilet or sink:**

- **glass**
- **metal**
- **gravel or sand, including stone from fish tanks**
- **seafood shells**
- **socks, rags, clothes**
- **plastic**
- **nappies, sanitary napkins, tampons, 'wet' wipes**
- **kitty litter**
- **explosives**
- **flammable materials**
- **lubricating oil and grease**
- **strong chemicals**
- **petrol, diesel**
- **stormwater runoff**

## Before you go on holiday

Before you go on holiday, even if it is just for a few days, you should flush the pressure wastewater system before you go. This is to avoid the possibility of the system becoming smelly while you are away. **To flush the system simply run a tap in the kitchen or bathroom sink for about five minutes before you go.**



# Taking care of the system

- **Do not flush any inappropriate items through the system.**
- **Do not put heavy weights on the lid of the tank. The lid can be walked on, but this should be avoided.**
- **Do not touch the valves in the boundary kit.**
- **Do not turn off the power to the pump unless evacuating in an emergency or if there is a broken wastewater pipe.**
- **Do not cover the unit in any way. This includes covering it with dirt, garden mulch, or concrete.**
- **Ensure access to the unit is available at all times.**
- **If you are going on holiday, even for just a few days, you should flush the system before you go. Simply run clean water down your kitchen or bathroom sink for five minutes (5 mins).**
- **If you do accidentally break a pipe under the ground contact the Christchurch City Council on (03) 941 8999 immediately and tell them what happened. While waiting for the pipe to be repaired minimise the amount of wastewater going through the system.**
- **Contact the Christchurch City Council on (03) 941 8999 if you install a swimming or spa pool.**
- **Contact the Christchurch City Council on (03) 941 8999 if you are making any modifications to your home which may affect the system (for example a house addition).**
- **Do not attempt to repair the system yourself. Always call the Christchurch City Council on (03) 941 8999.**

# Trouble shooting

## What happens if...

### 1. The system is damaged and needs repair?

The alarm will go off. Follow the alarm procedure on page 2.

### 2. You notice a bad smell around the tank

When operating normally there should be no noticeable odours coming from the unit. If it is smelly, the unit may just need flushing. Just run clean water down your kitchen or bathroom sink for about five minutes. If the unit remains smelly contact the Christchurch City Council on (03) 941 8999.

### 3. You notice wet spots around the unit or wastewater pipes

The pumping unit and pipes are sealed. If you notice wet spots and there hasn't been any recent heavy rain contact the Christchurch City Council on (03) 941 8999.

### 4. The alarm keeps going off when it rains

This means that rainwater may be getting into the system and overloading it. Contact the Christchurch City Council on (03) 941 8999.

### 5. The neighbours alarm goes and they are away

Do not investigate yourself. Contact the Christchurch City Council on (03) 941 8999.

### 6. There is a power failure

If there is a power failure the pump will not run. The tank has 24 hours of emergency storage so minimise the amount of wastewater going through the system. When the power comes on again the system will reset itself.

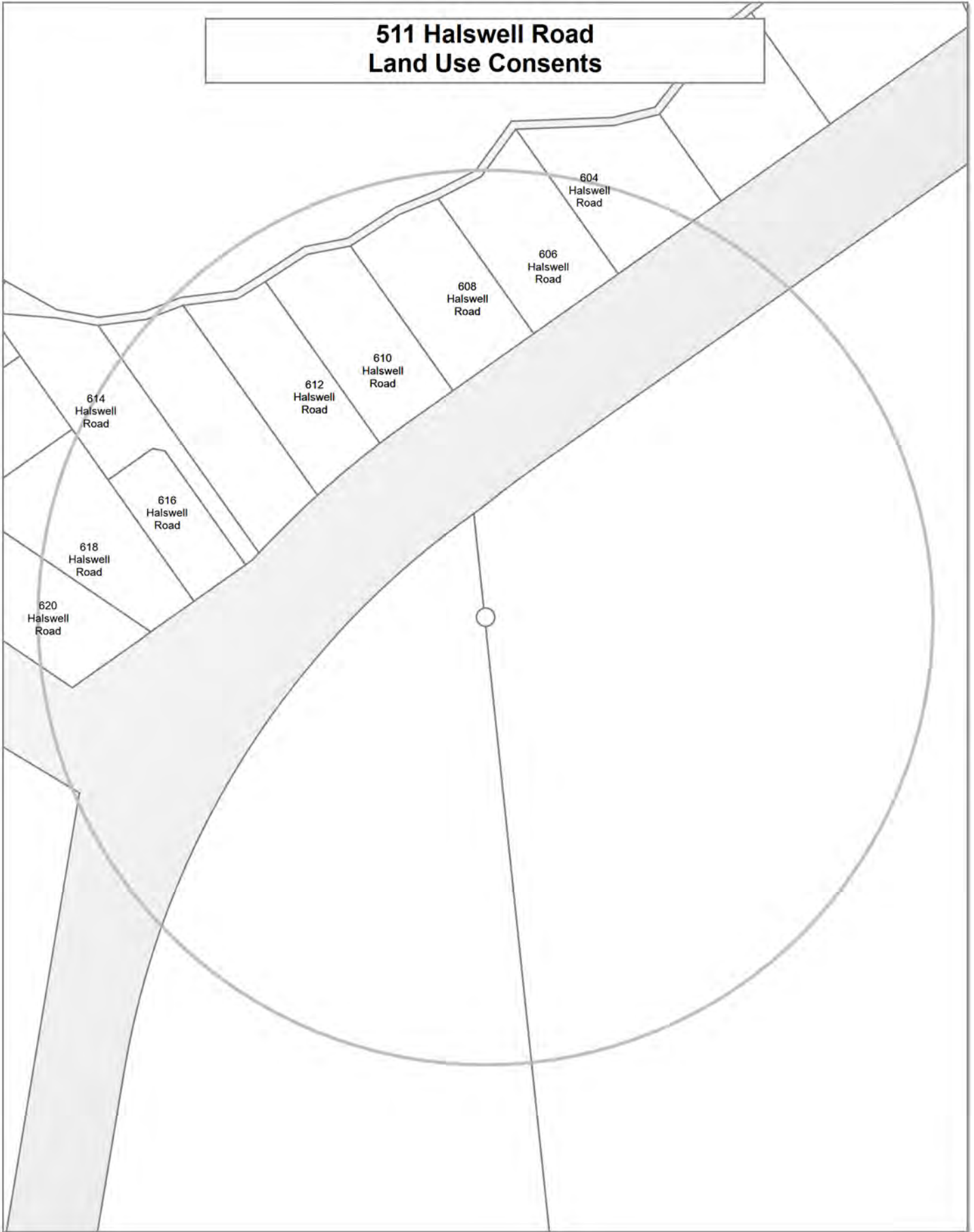
### 7. There is a flood

If you can safely stay in your home in a flood then simply minimise the amount of wastewater going through the system.

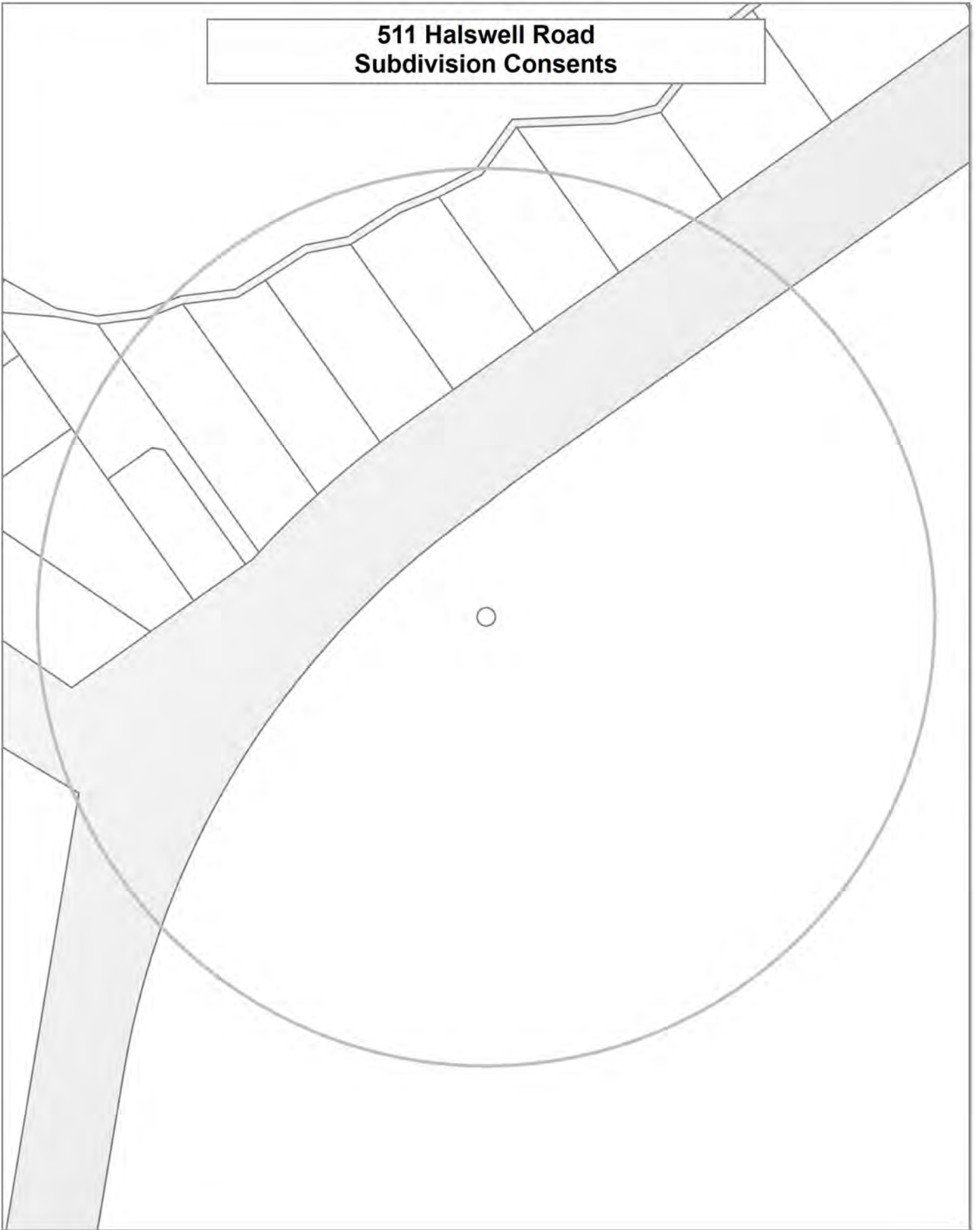
### 8. You need to evacuate due to an emergency (such as an earthquake)

If you can, flush out the system by running water down your kitchen or bathroom sink for about five minutes. Turn off the power to the pump. The on/off switch is located by the alarm panel.

## 511 Halswell Road Land Use Consents



**511 Halswell Road  
Subdivision Consents**



## Land Use Resource Consents within 100 metres of 511 Halswell Road

Note: This list does not include subdivision Consents and Certificates of Compliance issued under the Resource Management Act.

---

### 604 Halswell Road

RMA/2000/2667

Application for alterations to and the erection of additions to a dwelling to create a family flat and alterations to an existing garage - Historical Reference RMA20003424

Processing complete

Applied 25/10/2000

Decision issued 09/11/2000

Granted 08/11/2000

### 606 Halswell Road

RMA/2003/306

Application to construct living area and garage additions to the existing dwelling. - Historical Reference RMA20012561

Processing complete

Applied 30/01/2003

Decision issued 05/03/2003

Granted 05/03/2003

### 608 Halswell Road

RMA/1993/1222

Consent to operate a car dismantling yard in the ind. 4 zone. - Historical Reference RES954404

Processing complete

Applied 23/07/1993

Decision issued 23/08/1993

Granted 23/08/1993

RMA/1999/3584

Application for the total garage length of wall to exceed 9m while located within 1.8m of the internal boundary in terms of both the Proposed and Transitional - Historical Reference RES992616

Processing complete

Applied 10/09/1999

Decision issued 06/10/1999

Granted 06/10/1999

### 610 Halswell Road

RMA/1979/625

Application for consent to use a property at Halswell Junction Road for a relocated car wreckers yard. - Historical Reference RES954401

Processing complete

Applied 01/11/1979

Decision issued 03/06/1980

Granted 03/06/1980

RMA/1982/774

Application for a car, truck and machinery wrecking yard on a site zoned Industrial 3 (R). - Historical Reference RES954397

Processing complete

Applied 11/02/1982

Decision issued 06/04/1982

Granted 06/04/1982

## 612 Halswell Road

RMA/1985/401

Extension is 1.71m from boundary - Historical Reference RES9207117

Processing complete

Applied 24/10/1985

Decision issued 01/01/1999

Declined 01/01/1999

RMA/1986/368

Exceed recession plane on the southwestern boundary (Lot 5) with proposed new dwelling - Historical Reference RES9207118

Processing complete

Applied 08/02/1986

Decision issued 01/01/1999

Declined 01/01/1999

## 614 Halswell Road

RMA/2007/1175

Application to erect a new dwelling with attached garage on the proposed Lot 2 - Historical Reference RMA92008428

Processing complete

Applied 22/05/2007

Decision issued 08/06/2007

Granted 08/06/2007

## 616 Halswell Road

RMA/2006/1492

Application to erect a garage within the street scene setback - Historical Reference RMA92005550

Processing complete

Applied 29/06/2006

Granted 04/08/2006

Decision issued 04/08/2006

## 618 Halswell Road

RMA/2015/189

Replacement single-storey dwelling - Historical Reference RMA92028356

Processing complete

Applied 27/01/2015

Decision issued 26/02/2015

Granted 25/02/2015

## 620 Halswell Road

RMA/1990/346

distance between new dwelling and rear boundary to be reduced from 1.8m to 1.6m - Historical Reference RES9207124

Processing complete

Applied 01/10/1990

Decision issued 24/10/1990

Granted 24/10/1990

## Data Quality Statement

### Land Use Consents

All resource consents are shown for sites that have been labelled with an address. For sites that have been labelled with a cross (+) no resource consents have been found. Sites that have no label have not been checked for resource consents. This will be particularly noticeable on the margins of the search radius. If there are such sites and you would like them included in the check, please ask for the LIM spatial query to be rerun accordingly. This will be done free of charge although there may be a short delay. Resource consents which are on land occupied by roads, railways or rivers are not, and currently cannot be displayed, either on the map or in the list. Resource consents that relate to land that has since been subdivided, will be shown in the list, but not on the map. They will be under the address of the land as it was at the time the resource consent was applied for. Resource consents that are listed as Non-notified and are current, may in fact be notified resource consents that have not yet been through the notification process. If in doubt. Please phone (03)941 8999.

The term "resource consents" in this context means land use consents. Subdivision consents and certificates of compliance are excluded.

### Subdivision Consents

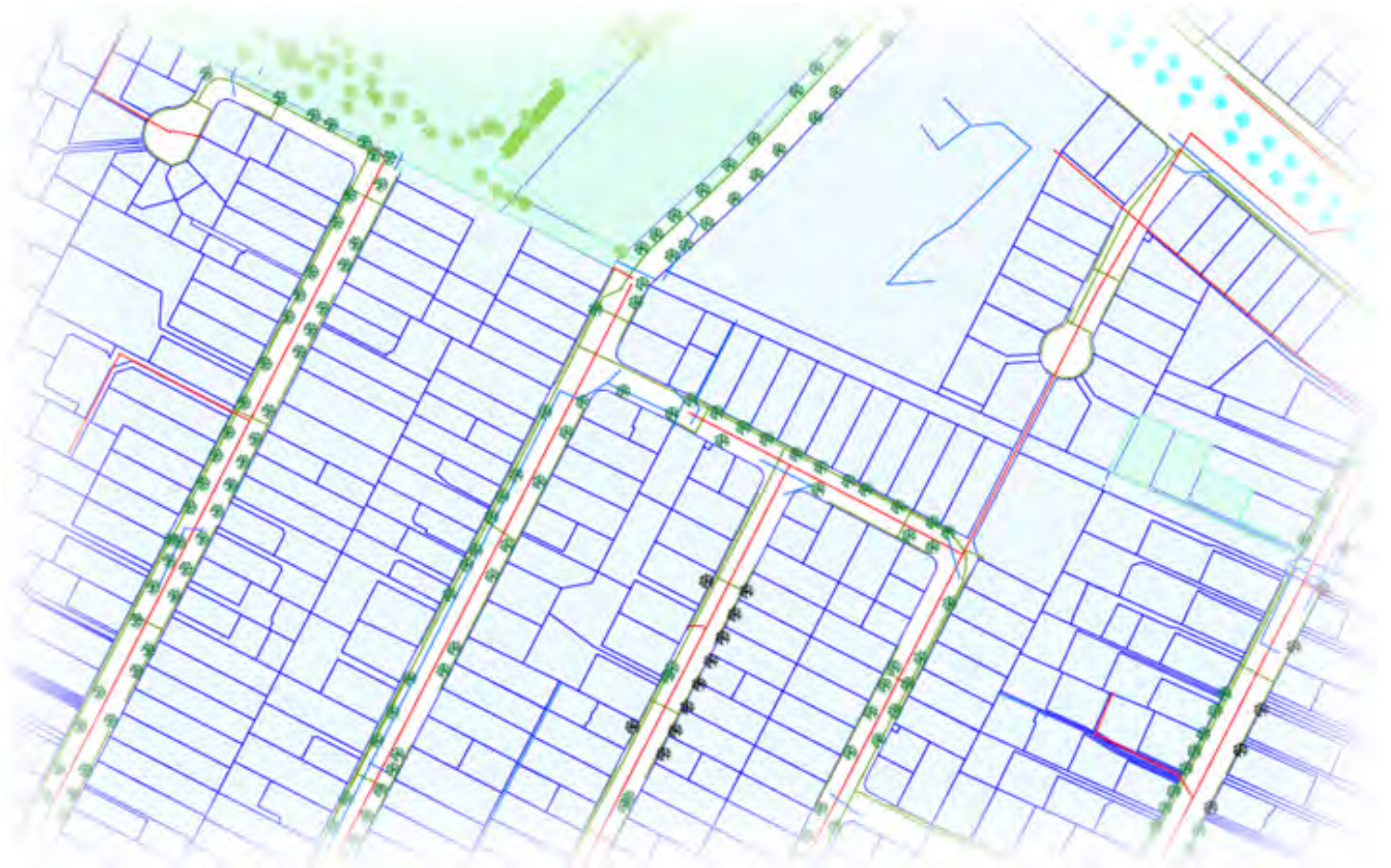
All subdivision consents are shown for the sites that have been labelled with consent details. For Sites that have been labelled with a cross (+) no records have been found. Sites that have no label have not been checked for subdivision consents. This will be particularly noticeable on the margins of the search radius. If there are such sites and you would like them included in the check, please ask for the LIM spatial query to be rerun accordingly. This will be done free of charge although there may be a short delay.

The term "subdivision consents" in this context means a resource consent application to subdivide land. Non subdivision land use resource consents and certificates of compliance are excluded.

This report will only record those subdivision applications which have not been completed i.e once a subdivision has been given effect to and the new lots/properties have been established the application which created those lots will not be shown

All subdivision consent information is contained on the map and no separate list is supplied

# Land Information Memorandum



Property address:  
2 Grovers Road

LIM number: 70247282  
Page 1

Christchurch City Council  
53 Hereford Street, PO Box 73015  
Christchurch 8154, New Zealand  
Tel 64 3 941 8999  
Fax 64 3 941 8984  
[www.ccc.govt.nz](http://www.ccc.govt.nz)



## Application details

Please supply to YOURSECTION RS LTD  
Client reference RIVERSTONE  
Phone number  
Fax number  
Date issued 18 June 2021  
Date received 10 June 2021

## Property details

Property address 2 Glovers Road  
Valuation roll number 23562 09300  
Valuation information Capital Value: \$3050000  
Land Value: \$2400000  
Improvements Value: \$650000  
*Please note: these values are intended for Rating purposes*  
Legal description Lot 1 DP 83635  
Existing owner Yoursection RS Limited  
2 Glovers Road  
Christchurch 8025

## Council references

Debtor number 4188171  
Rate account ID 73054381  
LIM number 70247282  
Property ID 1022692

Property address:  
2 Glovers Road

LIM number: 70247282  
Page 2

Christchurch City Council  
53 Hereford Street, PO Box 73015  
Christchurch 8154, New Zealand  
Tel 64 3 941 8999  
Fax 64 3 941 8984  
[www.ccc.govt.nz](http://www.ccc.govt.nz)

## Document information

This Land Information Memorandum (LIM) has been prepared for the purpose of section 44A of the Local Government Official Information and Meetings Act 1987 (LGOIMA). It is a summary of the information that we hold on the property. Each heading or "clause" in this LIM corresponds to a part of section 44A.

Sections 1 to 10 contain all of the information known to the Christchurch City Council that must be included under section 44A(2) LGOIMA. Any other information concerning the land as the Council considers, at its discretion, to be relevant is included at section 11 of this LIM (section 44A(3) LGOIMA). If there are no comments or information provided in these sections this means that the Council does not hold information on the property that corresponds to that part of section 44A.

The information included in this LIM is based on a search of Council records only and there may be other information relating to the land which is unknown to the Council. Please note that other agencies may also hold information relevant to the property, or administer legislation relevant to the use of the land, for example, the Regional Council (Ecan), Heritage New Zealand Pouhere Taonga, and Land Information New Zealand.

Council records may not show illegal or unauthorised building or works on the property. The applicant is solely responsible for ensuring that the land is suitable for a particular purpose.

A LIM is only valid at the date of issue as information is based only upon information the Council held at the time of that LIM request being made.

## Property file service

This Land Information Memorandum does not contain all information held on a property file. Customers may request property files by phoning the Council's Customer Call Centre on (03) 941 8999, or visiting any of the Council Service Centres. For further information please visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

To enable the Council to measure the accuracy of this LIM document based on our current records, we would appreciate your response should you find any information contained therein which may be considered to be incorrect or omitted. Please telephone the Customer Call Centre on (03) 941 8999.

A search of records held by the Council has revealed the following information:

## 1. Special features and characteristics of the land

*Section 44A(2)(a) LGOIMA. This is information known to the Council but not apparent from the district scheme under the Town and Country Planning Act 1977 or a district plan under the Resource Management Act 1991. It identifies each (if any) special feature or characteristic of the land concerned, including but not limited to potential erosion, avulsion, falling debris, subsidence, slippage, alluvion, or inundation, or likely presence of hazardous contaminants.*

( For enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### ┆ Consultant Report Available

Land Information New Zealand (LINZ) engaged Tonkin and Taylor to provide a Geotechnical Report on Ground Movements that occurred as a result of the Canterbury Earthquake Sequence. The report indicates this property may have been effected by a degree of earthquake induced subsidence. The report obtained by LINZ can be accessed on their website at <https://www.linz.govt.nz/land/surveying/earthquakes/canterbury-earthquakes/information-for-canterbury-surveyors>

### ┆ Liquefaction Vulnerability

Christchurch City Council holds indicative information on liquefaction hazard for Christchurch. Information on liquefaction, including an interactive web tool, can be found on the Council website at [ccc.govt.nz/liquefaction](http://ccc.govt.nz/liquefaction). Depending on the liquefaction potential of the area that the property is in, the Council may require site-specific investigations before granting future subdivision or building consent for the property.

### ┆ Softground

Council records show that site contains Soft Ground. Predominant Ground Material: N/A Reason for Assessment: Subdivision Should further buildings be proposed on this site, specific foundation design may be required.

## Related information

- ┆ There is attached a sub division soil investigation report covering this property.
- ┆ There are attached hazard/special site characteristics supplementary sheet/s.

## 2. Private and public stormwater and sewerage drains

Section 44A(2)(b) LGOIMA. This is information about private and public stormwater and sewerage drains as shown in the Council's records.

( For stormwater and sewerage enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### 1 Property within Local Pressurised Sewer System Zone

This property is in a local pressure sewer system catchment within the Christchurch wastewater network. If there is a house on the property, there will already be a wastewater pressure pump and tank. If a house is yet to be built, a new wastewater pressure pump and tank will need to be installed. General information about pressure sewer systems can be found on the Council website. More detailed information can be obtained by contacting Council Customer Services on 03 941 8999.

### Related information

- 1 The dwelling/building is shown to be served by a sewer drain.
- 1 The dwelling/building is shown to be served by a stormwater drain to soakpit.
- 1 The drainage works associated with this property have not been plotted on the Council's drainage plan. A copy of the field Inspectors pickup/approved site plan showing the drains and house outline is attached.

### 3. Drinking Water Supply

*Section 44A(2)(ba) and (bb) LGOIMA. This is information notified to the Council about whether the land is supplied with drinking water, whether the supplier is the owner of the land or a networked supplier, any conditions that are applicable, and any information the Council has about the supply.*

Please note the council does not guarantee a particular water quality to its customers. If you require information on current water quality at this property please contact the Three Waters & Waste Unit.

( For water supply queries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

#### Water Supply

Christchurch City Council is the networked supplier of water to this property. This property is connected to the Christchurch City Council Water Supply. The conditions of supply are set out in the Christchurch City Council Water Supply, Wastewater & Stormwater Bylaw (2014), refer to [www.ccc.govt.nz](http://www.ccc.govt.nz).

## 4. Rates

Section 44A(2)(c) LGOIMA. This is information on any rates owing in relation to the land.

( For rates enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (a) Annual rates

Annual rates to 30/06/2021: \$ 18,862.95

	Instalment Amount	Date Due
Instalment 1	\$ 4,715.67	31/08/2020
Instalment 2	\$ 4,715.67	30/11/2020
Instalment 3	\$ 4,715.67	28/02/2021
Instalment 4	\$ 4,715.94	31/05/2021

Rates owing as at 18/06/2021: \$ 0.00

### (b) Excess water charges

\$ 0.00

( For water charge enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (c) Final water meter reading required?

Reading is Required

( To arrange a final water meter reading, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

## 5. Consents, certificates, notices, orders, or requisitions affecting the land and buildings

*Section 44A(2)(d) LGOIMA. This is information concerning any consent, certificate, notice, order, or requisition, affecting the land or any building on the land, previously issued by the Council. The information in this section may also cover building consent and/or code compliance information issued by building certifiers under the Building Act 1991 and building consent authorities that are not the Council under the Building Act 2004.*

You can check the property file to identify whether any consent or certificate was issued by a building certifier under the Building Act 1991.

*Section 44A(2)(da) LGOIMA. The information required to be provided to a territorial authority under section 362T(2) of the Building Act 2004. There is currently no information required to be provided by a building contractor to a territorial authority under section 362T(2) of the Building Act 2004. The Building (Residential Consumer Rights and Remedies) Regulations 2014 only prescribed the information that must be given to the clients of a building contractor.*

( For building enquiries, please phone (03) 941 8999, email [EPADutyBCO@ccc.govt.nz](mailto:EPADutyBCO@ccc.govt.nz) or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (a) Consents

- | BCN/1968/6253 Applied: 24/12/1968 Status: Completed  
2 Glovers Road Halswell  
Permit granted 27/01/1969  
Permit issued 27/01/1969  
DWELLING- Historical Reference PER68011068 - No information/ or plans held on property file.
- | BCN/1984/3401 Applied: 10/05/1984 Status: Completed  
2 Glovers Road Halswell  
Permit granted 14/05/1984  
Permit issued 14/05/1984  
KENT LOG FIRE & WETBACK- Historical Reference PER84030024 - No information/ or plans held on property file.
- | BCN/1985/5186 Applied: 31/07/1985 Status: Completed  
2 Glovers Road Halswell  
Permit granted 16/09/1985  
Permit issued 16/09/1985  
ADDITION OF WORKSHOP TO GARAGE- Historical Reference PER85031623 - No information/ or plans held on property file.
- | BCN/1985/7457 Applied: 18/11/1985 Status: Completed  
2 Glovers Road Halswell  
Permit granted 26/11/1985  
Permit issued 26/11/1985  
BATHROOM ,HAYSHED, GARAGE- Historical Reference PER85031989 - No information/ or plans held on property file.
- | BCN/1986/5070 Applied: 01/08/1986 Status: Completed  
2 Glovers Road Halswell  
Permit granted 07/10/1986  
Permit issued 07/10/1986  
OUTSIDE TOILET- Historical Reference PER86032884 - No information/ or plans held on property file.
- | BCN/1988/8181 Applied: 21/11/1988 Status: Completed  
2 Glovers Road Halswell  
Permit granted 01/12/1988  
Permit issued 01/12/1988  
TUNNEL HOUSE- Historical Reference PER88035596 - No information/ or plans held on property file.

Property address:  
2 Glovers Road

- | BCN/1988/8182 Applied: 21/11/1988 Status: Completed  
2 Glovers Road Halswell  
Permit granted 29/11/1988  
Permit issued 29/11/1988  
PACKING SHED- Historical Reference PER88035597 - No information/ or plans held on property file.
- | BCN/1989/5917 Applied: 17/08/1989 Status: Completed  
2 Glovers Road Halswell  
Permit granted 31/08/1989  
Permit issued 31/08/1989  
DWELLING EXTENSION- Historical Reference PER89036498 - No information/ or plans held on property file.
- | BCN/1990/815 Applied: 12/02/1990 Status: Completed  
2 Glovers Road Halswell  
Permit issued 12/02/1990  
DRAINAGE & PLUMBING: ALTERATIONS- Historical Reference PER90151475
- | BCN/1994/504 Applied: 01/02/1994 Status: Completed  
2 Glovers Road Halswell  
Accepted for processing 01/02/1994  
Building consent granted 15/02/1994  
Building consent issued 18/02/1994  
Code Compliance Certificate Granted 25/03/1994  
Code Compliance Certificate Issued 25/03/1994  
GARAGE- Historical Reference CON94000576
- | BCN/1994/6003 Applied: 21/07/1994 Status: Completed  
2 Glovers Road Halswell  
Accepted for processing 21/07/1994  
Building consent granted 30/08/1994  
Building consent issued 01/09/1994  
Code Compliance Certificate Granted 25/10/1995  
Code Compliance Certificate Issued 25/10/1995  
CATTERY- Historical Reference CON94006454
- | BCN/1998/3338 Applied: 19/05/1998 Status: Completed  
2 Glovers Road Halswell  
Accepted for processing 19/05/1998  
Building consent granted 14/08/1998  
Building consent issued 28/08/1998  
Code Compliance Certificate Granted 14/09/2001  
Code Compliance Certificate Issued 14/09/2001  
FOUNDATIONS & ALTERATIONS TO RELOCATE DETACHED DWELLING DEMOLISH EXISTING COTTAGE-  
Historical Reference CON98003663
- | BCN/1998/4204 Applied: 17/06/1998 Status: Completed  
2 Glovers Road Halswell  
Accepted for processing 17/06/1998  
Building consent granted 09/07/1998  
Building consent issued 09/07/1998  
Code Compliance Certificate Granted 22/07/1999  
Code Compliance Certificate Issued 22/07/1999  
CONSERVATORY- Historical Reference CON98004637

Property address:  
2 Glovers Road



- | BCN/1998/7233 Applied: 05/10/1998 Status: Completed  
2 Glovers Road Halswell  
Accepted for processing 05/10/1998  
Building consent granted 15/10/1998  
Building consent issued 30/10/1998  
Code Compliance Certificate Granted 04/03/1999  
Code Compliance Certificate Issued 04/03/1999  
GARAGE/STOREROOM- Historical Reference CON98007958
- | BCN/1998/9233 Applied: 23/12/1998 Status: Completed  
2 Glovers Road Halswell  
Accepted for processing 23/12/1998  
Building consent granted 19/01/1999  
Building consent issued 25/01/1999  
Code Compliance Certificate Granted 02/08/1999  
Code Compliance Certificate Issued 02/08/1999  
DWELLING ADDITION - STUDY, REMOVE WALL & LOGAIRE ATLANTA LOGBURNER - WETBACK- Historical Reference CON98010198
- | BCN/2001/5701 Applied: 13/08/2001 Status: Completed  
2 Glovers Road Halswell  
Accepted for processing 13/08/2001  
Building consent granted 22/08/2001  
Building consent issued 22/08/2001  
PIM Granted 22/08/2001  
PIM Issued 22/08/2001  
Code Compliance Certificate Granted 21/09/2001  
Code Compliance Certificate Issued 21/09/2001  
HAY SHED- Historical Reference ABA10017967
- | BCN/2020/6981 Applied: 06/03/2015 Status: Completed  
2 Glovers Road Halswell  
Certificate of acceptance refused 13/04/2015  
Building Act Certificate of Acceptance considered for a rented sleepout. One Bedroom with no hot or cold water, no kitchen. - Historic Reference BAA37000913

## **(b) Certificates**

*Note: Code Compliance Certificates were only issued by the Christchurch City Council since January 1993.*

## **(c) Notices**

## **(d) Orders**

## **(e) Requisitions**

## Related information

- | The Council has previously issued other consents, certificates, notices, orders, and/ or requisitions for this property that have been resolved or are no longer current or relate to a building that is no longer on the land. For further information please contact the compliance and investigation team on 941 8999 and reference CSR91884083.

Property address:  
2 Glovers Road

LIM number: 70247282  
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Christchurch City Council  
53 Hereford Street, PO Box 73015  
Christchurch 8154, New Zealand  
Tel 64 3 941 8999  
Fax 64 3 941 8984  
[www.ccc.govt.nz](http://www.ccc.govt.nz)

## 6. Certificates issued by a building certifier

Section 44A(2)(e) LGOIMA. This is information notified to the Council concerning any certificate issued by a building certifier pursuant to the Building Act 1991 or the Building Act 2004.

( For building enquiries, please phone (03) 941 8999, email [EPADutyBCO@ccc.govt.nz](mailto:EPADutyBCO@ccc.govt.nz) or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

Property address:  
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LIM number: 70247282  
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Christchurch City Council  
53 Hereford Street, PO Box 73015  
Christchurch 8154, New Zealand  
Tel 64 3 941 8999  
Fax 64 3 941 8984  
[www.ccc.govt.nz](http://www.ccc.govt.nz)

## 7. Weathertightness

*Section 44A(2)(ea) LGOIMA. This is information notified to the Council under section 124 of the Weathertight Homes Resolution Services Act 2006.*

( For weathertight homes enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

*If there is no information below this means Council is unaware of any formal Weathertight Homes Resolution Services claim lodged against this property.*

## 8. Land use and conditions

Section 44A(2)(f) LGOIMA. This is information relating to the use to which the land may be put and conditions attached to that use. The planning information provided below is not exhaustive and reference to the Christchurch District Plan and any notified proposed changes to that plan is recommended: <https://ccc.govt.nz/the-council/plans-strategies-policies-and-bylaws/plans/christchurch-district-plan/>.

There maybe some provisions of the Christchurch City Plan or Banks Peninsula District Plan that affect this property that are still operative.

( For planning queries, please phone (03) 941 8999, email [DutyPlanner@ccc.govt.nz](mailto:DutyPlanner@ccc.govt.nz) or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### Regional plan or bylaw

There may be objectives, policies or rules in a regional plan or a regional bylaw that regulate land use and activities on this site. Please direct enquiries to Canterbury Regional Council (Environment Canterbury).

### Waterway Provisions for Other Councils

A resource consent or permit may also be required from the Canterbury Regional Council or other territorial authority, particularly with respect to water bodies managed by those authorities. Please refer to the relevant regional plan and any relevant bylaws, and contact the Christchurch City Council if you are uncertain which authority manages the water body in question.

## (a) (i) Christchurch City Plan & Banks Peninsula District Plan

### (ii) Christchurch District Plan

#### High Flood Hazard Management Area

This property or parts of, are within the High Flood Hazard Management Area (HFHMA) in the Christchurch District Plan. A resource consent is likely to be required for new buildings or to subdivide this property. Further information can be found at [www.ccc.govt.nz/hfhma](http://www.ccc.govt.nz/hfhma).

#### Liquefaction Management Area (LMA)

Property or part of property within the Liquefaction Management Area (LMA) Overlay which is operative.

#### Outline Development Plan

Property or part of property is within an Outline Development Plan area which is affected by specific provisions that are operative.

#### Remainder Slope Instability Management Area

Property or part of property within the Christchurch District Plan Remainder of Port Hills and Banks Peninsula Slope Instability Management Area overlay.

#### Waterway Provisions

This property or part of this property is close to at least one waterway. It may be within the setback for an Environmental Asset Waterway. Within that setback, District Plan rules apply to activities including buildings, earthworks, fences and impervious surfacing. Any part of the property within the setback will be affected by those rules.

† **Development Constraint Conditions**

Council records show there is a specific condition on the use of this site: Well on Property

† **Development Constraint Conditions**

Council records show there is a specific condition on the use of this site: Specific Site Level required

† **Flood Management Area**

Property or part of property within the Flood Management Area (FMA) Overlay which is operative.

† **District Plan Zone**

Property or part of property within the Residential New Neighbourhood Zone which is operative.

**(b) Resource consents**

If there are any land use resource consents issued for this property the Council recommends that you check those resource consents on the property file. There may be conditions attached to those resource consents for the property that are still required to be complied with.

† RMA/1974/419 - Resource consents

2 Glovers Road Halswell

To permit a subdivision less than the area permitted under the District planning scheme. - Historical Reference RES955313

Status: Processing complete

Applied 21/10/1974

Decision issued 21/10/1974

Granted 21/10/1974

† RMA/1989/257 - Resource consents

2 Glovers Road Halswell

4.6m side yard instead of the required 10m - Historical Reference RES9206551

Status: Processing complete

Applied 17/08/1989

Decision issued 23/08/1989

Granted 23/08/1989

† RMA/1993/1160 - Resource consents

2 Glovers Road Halswell

The erection of a boarding cattery in the rural 2 zone at Glovers Road. - Historical Reference RES94101932

Status: Processing complete

Applied 12/03/1993

Decision issued 19/05/1993

Granted 19/05/1993

- I RMA/1998/1327 - Resource consents  
2 Glovers Road Halswell  
Application for a temporary additional rural dwelling a proposed dwelling is to be constructed which is to replace an existing cottage on - Historical Reference RES981500  
Status: Processing complete  
Applied 08/06/1998  
Decision issued 17/07/1998  
Granted 17/07/1998
  
- I RMA/1998/1529 - Resource consents  
2 Glovers Road Halswell  
Application for a dwelling addition which intrudes the 10m setback in terms of both the Proposed and Transitional Plans. - Historical Reference RES981736  
Status: Processing complete  
Applied 01/07/1998  
Decision issued 08/07/1998  
Granted 08/07/1998
  
- I RMA/1999/2499 - Resource consents  
2 Glovers Road Halswell  
Application to subdivide a 5261m2 allotment, including an existing dwelling, garage and cattery, from a 12.3192 ha property. - Historical Reference RES991246  
Status: Processing complete  
Applied 30/04/1999  
Decision issued 09/09/1999  
Declined 09/09/1999
  
- I RMA/2020/2557 - Land Use Consent  
2 Glovers Road Halswell  
Remediation of contaminated soils  
Status: Processing complete  
Applied 06/11/2020  
Granted 09/12/2020  
Decision issued 09/12/2020
  
- I RMA/2020/2770 - Land Use Consent  
511 Halswell Road Halswell  
To conduct earthworks and stockpiling on site  
Status: Processing complete  
Applied 27/11/2020  
Granted 27/01/2021  
Decision issued 27/01/2021

Property address:  
2 Glovers Road

- | RMA/2020/3076 - Combined subdivision / land use consent  
511 Halswell Road Halswell  
To subdivide 4 allotments to create 87 residential allotments. Land use consent for earthworks and under the NES for contaminated land.  
Status: On hold - waiting for response from applicant  
Applied 22/12/2020
  
- | RMA/1999/5158 - Subdivision Consent  
Fee Simple SUBDIVISION - Historical Reference RMA4366  
Status: Processing complete  
Applied 30/04/1999
  
- | RMA/2000/1933 - Subdivision Consent  
2 LOT FEE SIMPLE APP 223 recieved 29/9/00 certified 9/10/00 224 REQUESTED 08/03/01 Issued 13/3/01 DP 83635  
- Historical Reference RMA20002667  
Status: Processing complete  
Applied 02/08/2000  
Granted 22/08/2000  
Decision issued 22/08/2000

## Related information

- | Council records show that there is a current/on hold monitoring job in our system. This monitoring is to ensure that the resource consent conditions have been met. For further information you can contact the Compliance & Investigation team A on 941 8999 or email: [rcmon@ccc.govt.nz](mailto:rcmon@ccc.govt.nz) and reference to resource consent RMA/2020/2770 - RMA/2020/2557.

## 9. Other land and building classifications

*Section 44A(2)(g) LGOIMA. This is information notified to the Council by any statutory organisation having the power to classify land or buildings for any purpose.*

( For land and building enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

Please refer to Section 1 for details

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2 Glovers Road

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Christchurch City Council  
53 Hereford Street, PO Box 73015  
Christchurch 8154, New Zealand  
Tel 64 3 941 8999  
Fax 64 3 941 8984  
[www.ccc.govt.nz](http://www.ccc.govt.nz)



## 10. Network utility information

*Section 44A(2)(h) LGOIMA. This is information notified to the Council by any network utility operator pursuant to the Building Act 1991 or the Building Act 2004.*

( For network enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

! **None recorded for this property**

## 11. Other information

Section 44A(3) LGOIMA. This is information concerning the land that the Council has the discretion to include if it considers it to be relevant.

( For any enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (a) Kerbside waste collection

- | Your recycling is collected Fortnightly on the Week 2 collection cycle on a Tuesday. Please leave your recycling at the Kerbside by 6:00 a.m. Your nearest recycling depot is the Parkhouse Road EcoDrop.
- | Your refuse is collected Fortnightly on the Week 2 collection cycle on a Tuesday. Please leave your rubbish at the Kerbside by 6:00 a.m. Your nearest rubbish depot is the Parkhouse Road EcoDrop.
- | Your organics are collected Weekly on Tuesday. Please leave your organics at the Kerbside by 6:00 a.m.

### (b) Other

#### | Floor Levels Information

Christchurch City Council holds a variety of information relevant to building/property development across the city. This includes minimum finished floor levels that need to be set to meet the surface water requirements in clause E1.3.2 of the building code (where this applies), and the requirements of the Christchurch District Plan (where a property is in the Flood Management Area). Where this information has been processed for your site, it can be viewed at <https://ccc.govt.nz/floorlevelmap/>, otherwise site specific advice can be obtained by emailing [floorlevels@ccc.govt.nz](mailto:floorlevels@ccc.govt.nz).

#### | Community Board

Property located in Halswell-Hornby-Riccarton Community Board.

#### | Guest Accommodation

Guest accommodation (including whole unit listings on Airbnb; BookaBach; etc.) generally requires a resource consent in this zone when the owner is not residing on the site. For more information, please refer to: <https://ccc.govt.nz/providing-guest-accommodation/>.

#### | Tsunami Evacuation Zone

This property is not in a tsunami evacuation zone. It is not necessary to evacuate in a long or strong earthquake or during an official Civil Defence tsunami warning. Residents may wish to offer to open their home to family or friends who need to evacuate from a tsunami zone, and should plan with potential guests to do so in advance. More information can be found at <https://ccc.govt.nz/services/civil-defence/hazards/tsunami-evacuation-zones-and-routes/>

#### | Electoral Ward

Property located in Halswell Electoral Ward

#### | Listed Land Use Register

Property address:  
2 Glovers Road


LIM number: 70247282  
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Christchurch City Council  
53 Hereford Street, PO Box 73015  
Christchurch 8154, New Zealand  
Tel 64 3 941 8999  
Fax 64 3 941 8984  
[www.ccc.govt.nz](http://www.ccc.govt.nz)

Hazardous activities and industries involve the use, storage or disposal of hazardous substances. These substances can sometimes contaminate the soil. Environment Canterbury identifies land that is used or has been used for hazardous activities and industries. This information is held on a publically available database called the Listed Land Use Register (LLUR). The Christchurch City Council may not hold information that is held on the LLUR. Therefore, it is recommended that you check Environment Canterbury's online database at [www.llur.ecan.govt.nz](http://www.llur.ecan.govt.nz)

## I **Spatial Query Report**

A copy of the spatial query report is attached at the end of this LIM. The spatial query report lists land use resource consents that have been granted within 100 metres of this property.

 <p><b>CHRISTCHURCH</b> THE GARDEN CITY <i>The city that shines</i></p>	<p><b>Resource Management Act 1991/Building Act 1991</b></p> <p><b>Hazards or Special Site Characteristics</b></p> <p><b>SOCKBURN SERVICE CENTRE</b></p>
--	--

Location ..... Glovers Road ..... Number: ..... 2 .....

Legal Description: Lot ..... 1 ..... D.P. .... 83635 ..... Ward: ..... Wigram .....

Date Recorded ..... 4.9.90 ..... Severity ..... 1 ..... Accuracy ..... A ..... by ..... George Marsh ..... Computer Entry ..... 3.6.93 .....

DETAILS:  
Water Way Setback - Specific Site level  
Soft ground: -

<input checked="" type="checkbox"/>	<b>WATER WAY SETBACK</b>	<u>Glovers Drain</u>
LOCATION OF INFORMATION: <b>Sockburn Service Centre</b>		
The site (or part of) is located within the waterway setback requirement of the City Plan as specified below: (as amended and publicly notified 8 May 1999).		
<input type="checkbox"/>	10 metres for upstream rivers	<input type="checkbox"/>
<input type="checkbox"/>	30 metres for downstream rivers	<input checked="" type="checkbox"/>
<input type="checkbox"/>	10 metres Hill waterway (from centreline of waterway)	<input type="checkbox"/>
		<input type="checkbox"/>
		<input type="checkbox"/>
		<input type="checkbox"/>
Within this setback, filling, excavation or the erection of buildings is a Discretionary activity requiring a Resource Consent.		
<input checked="" type="checkbox"/>	<b>SITE LEVEL</b>	<b>FLOOD PRONE AREA</b> <input type="checkbox"/>
File No. or Source of Information: <b>Water Services Unit</b>		
A minimum site level is recorded against the property. The land may require raising for stormwater purposes. (where there is a proposal for further development)		
<input checked="" type="checkbox"/>	RL _____ metres set to Water Services Unit Datum	
<input checked="" type="checkbox"/>	Can be obtained from the Water Services Unit.	
Note: Minimum floor levels above the site level relates to the type of construction, i.e. 150mm brick etc, 225mm weatherboard/AS 3500 Confirmation of the Reduced Level (RL) is required to be made by a Registered Surveyor.		
<input checked="" type="checkbox"/>	<b>SOFT GROUND</b>	
Structural Engineer's soil response and bore hole tests are required for any structures on this site. Where necessary, provide design foundation drawings and supporting calculations or "Producer Statements"		
<u>Uhof 1 DP 54911 Subd Wig 2000 2667</u>		

- KEY Severity  1 Low  2 Moderate  3 Extreme  4 Unknown
- Accuracy  A Confirmed  B Unconfirmed  C Personal Observation

# Geotechnical Investigation and Assessment Report for Subdivision

Riverstone Subdivision, 2 & 4 Glovers Road, Halswell, Christchurch

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Issue Date: **20 October 2020**

Document Ref: **200357-RP-001[A]**



Prepared for: **Yoursection Ltd**



**Report Tracking - 2 & 4 Glovers Road, Halswell, Christchurch**

Revision	Status	Date	Prepared by	Reviewed by
A	Final	20 October 2020	C. Gibbens	A. Giannakogiorgos

**Authorisation**

<b>Author's Signature</b>		<b>Approver's Signature</b>	
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<b>Title</b>	Engineering Geologist BSc MSc (Hons) MEngNZ	<b>Title</b>	Chartered Professional Engineer (Geotechnical) BSc MSc DIC CMEngNZ CPEng IntPE (NZ)

**Miyamoto International New Zealand Ltd**  
Level 1, 236 Hereford Street | Christchurch 8011

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## Executive Summary

Miyamoto International NZ Ltd (MINZ) has been engaged by Yoursection Ltd to undertake a geotechnical land suitability assessment for the proposed residential subdivision at 2 & 4 Glovers Road, Halswell, Christchurch. The key findings of our evaluation and assessment are outlined below.

<b>GROUND CONDITIONS</b>	<b>Ground profile</b>	The sub-surface conditions comprise mainly topsoil over sand-silt mixtures underlain by soft clayey silts and shallow gravel. The ground conditions are variable in horizontal and vertical spread.	
	<b>Soil classification as per NZS 1170.5:2004</b>	Residential Subdivision Area: Class 'D' (deep or soft soil site)	
	<b>Depth to water table</b>	Perched water tables and shallow saturated soils were encountered within the top 1.0 to 2.0m bgl. Permanent ground water is anticipated below the soft silts within the underlying sands and gravels.	
<b>SEISMIC ASSESSMENT</b>	<b>Design Earthquake Event</b>	<b>SLS/SLS2</b>	<b>ULS</b>
	<b>Estimated "free-field" Index post-liquefaction volumetric settlements</b>	< 50mm	< 80mm
	<b>Liquefaction Severity Number (LSN) Value</b>	< 15 Little to minor expression of liquefaction	< 25 Little to moderate expression of liquefaction
	<b>MBIE Technical Categorization (TC)</b>	<b>Mapped MBIE</b>	Rural & Unmapped
		<b>Site Specific Foundation TC</b>	TC2
<b>GEOTECHNICAL CONSIDERATIONS</b>	<p>Our assessment of the site under RMA Section 106 found that the subsidence hazard is present on-site due to presence of soft/loose soil layers and liquefiable deposits, though these hazards can be mitigated by the options listed in this report.</p> <p>As the site is located within an FMA set out by CCC, a portion of the site will require filling to raise the ground level to a suitable level for the proposed development by around 1.0m close to Green's Stream. Filling of the site will likely cause static some consolidation settlements in the soft compressible soils underlying the site, though this is not expected to be a significant risk to the development, based on the pre-loading trial undertaken by MINZ previously. A period of monitoring of the site filling works during the raising of the site levels and for a period (~6 months) is advised to be safeguard against the anticipated static settlements.</p>		

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- A. Updated Indicative Subdivision Plan (Davie Lovell Smith)
- B. ECan Listed Land Use Register Files
- C. Geotechnical Investigation Results
- D. Southern Geophysical MASW and GPR Report
- E. Geotechnical Cross Sections
- F. Liquefaction Analyses



## 1. Introduction

Miyamoto International NZ Ltd (Miyamoto) has been engaged by Yoursection Ltd to undertake a geotechnical evaluation and assessment as part of a land suitability assessment for the proposed new extension of the residential Riverstone Subdivision at 2 & 4 Glovers Road, Halswell, Christchurch.

Miyamoto have previously completed a geotechnical assessment for resource consenting purposes for the initial stage of the Riverstone Subdivision located at 511 Halswell Road, Christchurch (190666-RP-001[A] – 511 Halswell Road, dated 10 October 2019), as well as undertaking a trial pre-load assessment for the same property (190666-TM-001[A]\_511 Halswell Road\_Pre-load Trial, dated 28 January 2020). Both documents are referenced as part of this assessment, with this report supplementing and expanding on the work already undertaken.

The scope of this geotechnical engineering assessment was to evaluate the geotechnical conditions at the site and to provide preliminary recommendations for development of the sections. This assessment comprised the following:

- Research of the available information from the New Zealand Geotechnical Database (NZGD), Christchurch City Council (CCC) and Environment Canterbury (ECan);
- Site walkover inspection of the land;
- Shallow field investigation comprising hand-augered boreholes (HA) with associated dynamic cone penetrometer (DCP) and shear vane (SV) tests;
- Deep field investigation comprising Cone Penetration Tests (CPT) with accompanying Dynamic Probe Super Heavy (DPSH) testing;
- Multichannel Analysis of Surface Waves (MASW) geophysical survey;
- Ground Penetrating Radar (GPR) geophysical survey;
- Liquefaction analyses using CPT-based liquefaction triggering procedures;
- Reporting of the findings.

The geotechnical investigation and assessment were carried out considering the Ministry of Business, Innovation & Employment (MBIE) Guidance documents “Planning and engineering guidance for potentially liquefaction-prone land” - Version 1, dated September 2017, “Repairing and rebuilding houses affected by the Canterbury earthquakes” - Version 3, dated December 2012, and “Earthquake geotechnical engineering practice - Modules 2 & 3”. This report presents our findings and conclusions which are provided to facilitate the development of the extended subdivision plan for the site.

## 2. Site Description

The site, legally described as Lot 1 (2 Glovers) and Lot 2 (4 Glovers) DP 83635, is in Halswell, Christchurch and is approximately 8.3 hectares (ha) in total area. There is an approximate elevation change of 2.0m over 460m at an average gradient of 0.4%. The site generally slopes from north to south, with the low point at the southern boundary of both sections. The property is bound by Glovers Road along the northern boundaries and is bound by rural

properties on the south and east boundaries, and the 511 Halswell Road section to the west. Green's Stream runs through the southern end of both sections.

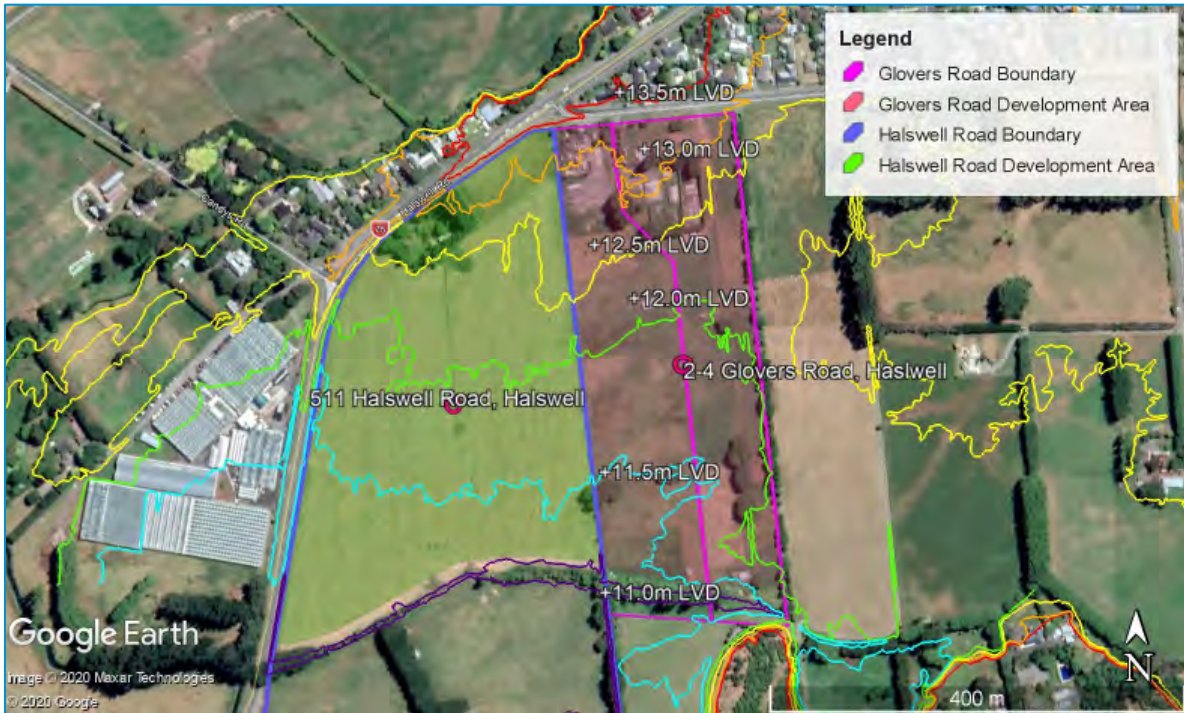


Figure 1: Proposed Site Layout with (Scale as Shown)

The property is located within the “Rural and Unmapped” category listed under the MBIE Technical Categories Map. The site location with reference to the MBIE Technical Categories is shown in Figure 2.

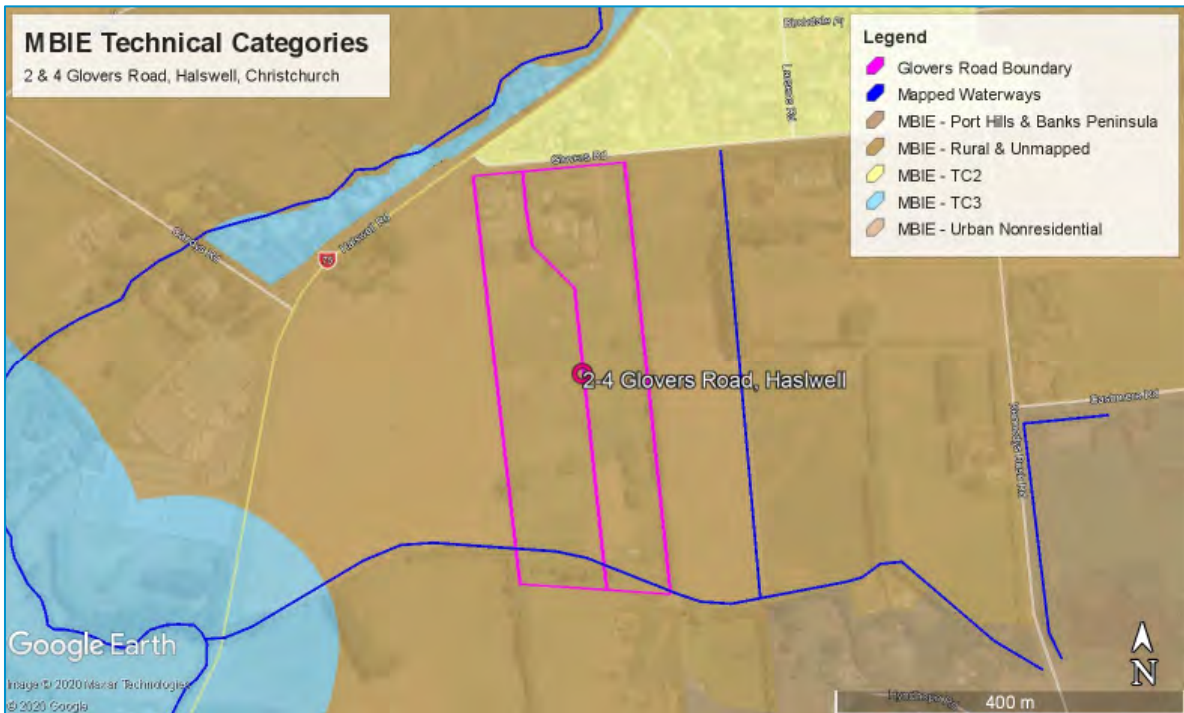


Figure 2: Site Location Plan Showing MBIE Technical Categories and Mapped Waterways (Scale as Shown)

The Riverstone Subdivision is proposed to, currently, be comprised of 239 residential lots with reserves located throughout. A draft plan of the subdivision, including the Glovers Road properties, is presented in Appendix A.

### 3. Desk Study

The following sources of third-party information were considered and are referenced in this report:

- New Zealand Geotechnical Database (NZGD);
- Environment Canterbury (ECan);
- Christchurch City Council (CCC).

#### New Zealand Geotechnical Database

The NZGD website was reviewed to identify any additional information related to the extent of land damage after the CES on the site and in the immediate surrounding areas. The results of this review indicate that no significant land damage was observed across the site. Table 1 provides a summary of the information obtained from our review of the NZGD.

Table 1: Desk Study Information Summary (NZGD)

	September 2010 (M <sub>w</sub> 7.1)	February 2011 (M <sub>w</sub> 6.2)	June 2011 (M <sub>w</sub> 6.0)	December 2011 (M <sub>w</sub> 5.9)
<i>Aerial Photography Review</i>	Outside of photographed area	Areas of likely ejecta identified in the central and northern areas of both properties, though mainly confined to 2 Glovers Road	Outside of photographed area	Outside of photographed area
<i>Land damage observations</i>	Minor ground cracking but no observed ejected liquefied material was recorded on the properties on the opposite side of Glovers Road in the September 2010 CES event and along Halswell Road and sections of Glovers Road during the June 2011 CES event.			
<i>Observed ground cracking</i>	No cracks mapped on the properties, 10mm – 200mm ground cracks mapped ~65m west of the northernmost boundary of the site within the residential area on the opposite side of Halswell Road			
<i>PGA (g) ± SD</i>	0.294 ± 0.390	0.356 ± 0.435	0.145 ± 0.465	0.139 ± 0.250
<i>Scaled PGA<sub>7.5</sub> PGA<sub>16%ile</sub> to PGA<sub>84%ile</sub><sup>(1)</sup> (g)</i>	0.179 to 0.394	0.164 to 0.391	0.061 to 0.156	0.071 to 0.117

(1) Scaled to M7.5 using Idriss and Boulanger recommendations (2008); 68% confidence PGA<sub>7.5</sub> range

## Contaminated Land Considerations

The ECan Listed Land Use Register (LLUR) was reviewed and holds records of potentially Hazardous Activities and Industrial List (HAIL) sites. At this time, a small area that intersects the southern end of both sections is listed as a potential HAIL site. The LLUR lists this small area (in the vicinity of a storage shed) as an A10-classified area, which relates to “persistent pesticide bulk storage or use including sports turfs, market gardens, orchards, glass houses or spray sheds”, though this has not been investigated by ECan. The property reports for both sections are included in Appendix B.

An environmental assessment is outside the scope of this assessment and has been undertaken by others.

## Flood Hazard

Christchurch is a low-lying city and there have always been areas that are prone to flooding during heavy rainfall. The CES has worsened flood risk in many areas of the city through damage to waterways and land. Flood Management Areas (FMAs) have been identified by CCC in the District Plan and take into consideration the impacts of the CES.

At the time of writing this report the site is located within a FMA as indicated by the CCC District Plan.

It is understood that a Finished Floor Level (FFL) of 21.25m above Christchurch Drainage Datum (CDD) is a requirement for development of the site.

## Ground Motion

Using the MBIE and Bradley & Hughes (2012) procedures, we have found that the site was “sufficiently tested” to the Serviceability Limit State (SLS) level of earthquake demand during the September 2010 and February 2011 events of the CES. This indicates that land and building damage in a future SLS event is likely to be similar to these individual events.

Additionally, based on the SLS2 level of shaking ( $M_w$  6.0 and PGA of 0.19g) which was introduced by MBIE following the updated liquefaction triggering CPT-based procedure by Boulanger & Idriss (2014), it is our opinion the site was “sufficiently tested” to the SLS2 level of earthquake demand during the September 2010 and February 2011 events of the CES.

Utilising a derivation of the Bradley and Hughes method, we can suggest that the site was not tested to Ultimate Limit State (ULS) level of shaking during the CES. Based on the probabilistic analysis of the PGAs experienced at the site, the nature of land and building damage is likely to be more severe during a future ULS event than that already experienced during the individual CES events.

## 4. Subsurface Conditions

### Geological Setting

The geological map of the area (GNS 1:250,000 QMap) indicates that most of the site has surface geology consisting of “modern (Quaternary) river floodplain and low-level degradation terraces (<2° slopes) comprised of unweathered, variably sorted gravel/sand/silt/clay”.

## Field Investigations

The NZGD website was reviewed to identify relevant geotechnical investigations completed within the site vicinity, additional to the data identified for use in the original site assessment for the neighbouring section, though nothing for inclusion was identified.

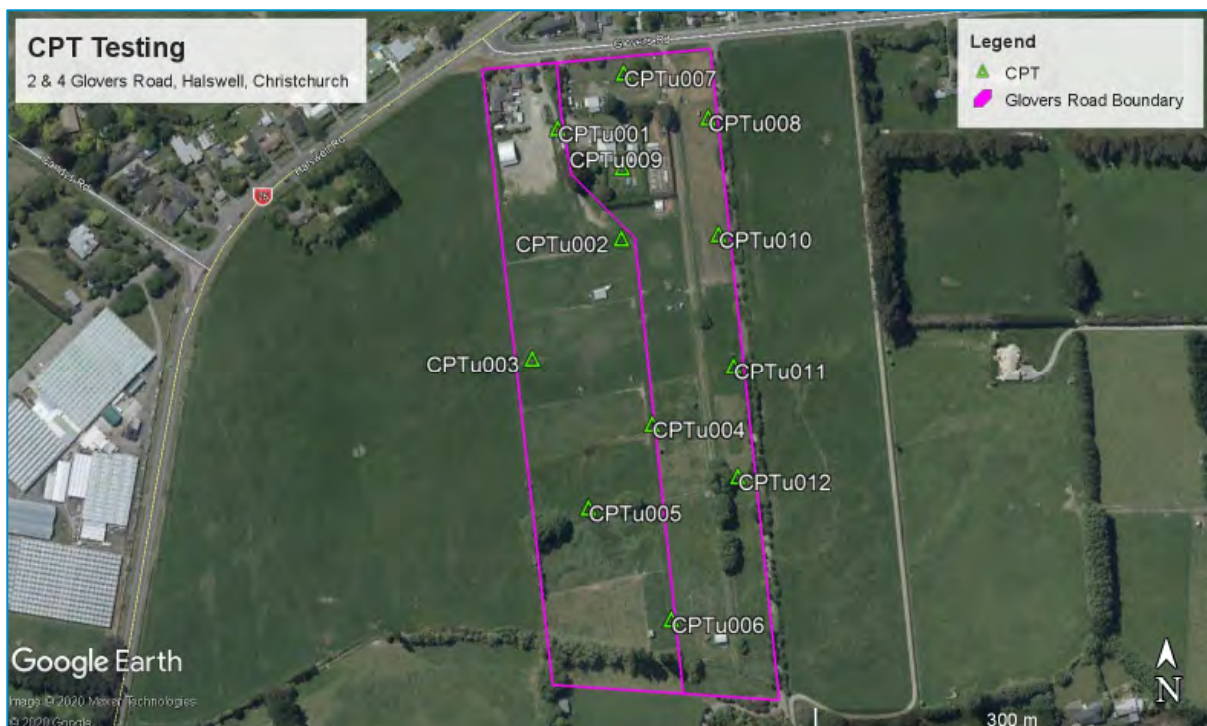
Miyamoto undertook the following site-specific ground investigations and testing:

- Five (5) hand-augered boreholes (referenced HA1 to HA5) with in-situ shear vane testing;
- Five (5) Dynamic Cone Penetrometer (DCP) tests (referenced DCP1 to DCP5);
- Laboratory testing including fines content (FC) and Atterberg Limits;
- Twelve (12) Cone Penetration Tests (CPTu) with porewater pressure measurements;
- Multichannel Analysis of Surface Waves (MASW) geophysical survey;
- Ground Penetrating Radar (GPR) geophysical survey.

The general details of the ground investigations are summarised in Table 2, the test locations are shown in Figure 3 and Figure 4, and the HA/DCP logs and CPT plots are presented in Appendix C and the geophysical survey report is presented in Appendix D.

**Table 2: Summary of Ground Investigations**

Test Ref.	Source	Source Ref.	Test Type	Depth (m bgl)
HA1/DCP1 to HA5/DCP5	MINZ	200357	Hand Auger/ DCP	1.8 to 3.9
CPTu001 to CPTu012	LandTest	19096	CPT	10.0 to 15.0
MASW 1 to MASW 3	Southern Geophysical Ltd	2050	MASW	Up to 40.0
GPR 1 to GPR 11			GPR	Up to 4.0



**Figure 3: CPT Investigation Location Plan (Scale as Shown)**



Figure 4: Other Geotechnical Investigation Location Plan (Scale as Shown)

### Laboratory Test Results

Laboratory testing was undertaken on samples obtained from our shallow ground investigation to assess the soil characteristics across the site. The testing undertaken includes wet sieving to determine the fines content, and Atterberg limits tests to determine the plastic and liquid limits. A summary of the test results is presented in Table 3, with the full results presented in Appendix C.

Table 3: Laboratory Test Results

Sample Ref.	Depth of sample (m)	Soil Description	Plasticity Index	% Passing		
				0.3 mm	0.15 mm	0.063 mm
C20-319	HA1 1.5m – 2.3m	Silty SAND, brownish grey, wet, non-plastic	-	100	90	49
C20-320	HA1 2.3m – 3.8m	Silty SAND, brownish grey, saturated, non-plastic	-	100	91	49
C20-321	HA2 2.7m – 4.0m	Silty CLAY, some sand, dark grey, saturated, low plasticity	9	99	96	85
C20-312	HA3 2.0m – 3.4m	Sandy SILT, dark grey, saturated, non-plastic	NP	100	99	59
C20-323	HA5 1.5m – 1.8m	Silty SAND, brownish grey, wet, non-plastic	-	99	77	42

## Ground Conditions

The ground conditions interpreted from the existing data and investigations undertaken as part of this assessment are presented graphically in the geotechnical cross sections included in Appendix E and the basic soil descriptions are outlined in Table 4.

A near-surface paleo-feature (old river terrace or paleochannel) was identified during the site testing with the CPT's completed at the southern end of the site (CPTu004 to CPTu006 and CPTu012) refusing in dense soils within the upper 5m, before testing was continued with the DPSH. The shallow investigation (HA5/DCP5) also refused at a shallow depth due to dense soils. The testing at the northern end of the site all reached the target depths and were consistent in their findings.

Table 4: Ground Conditions Summary

Layer	Soil Name
a	Silty SAND and Sandy SILT, loose to firm
b	Clayey SILT, soft to firm, medium plasticity
c	Silty SAND, medium dense to dense with increasing depth
GS	Gravelly SAND to Sandy GRAVEL, dense
d	Clayey SILT to silty CLAY, firm
e	Medium dense SAND with silt and gravels
f	Clayey SILT, firm to stiff
S	Silty SAND to Sandy SILT, medium dense to very stiff

## MASW & GPR Geophysical Survey

The shear wave velocity ( $V_s$ ) measurement was assessed with a MASW survey. The results of the survey were used to refine the boundaries and extents between the shallow, softer soils and denser sandy/gravelly layers with the MASW survey reflecting the findings of the intrusive investigations, with 2 clearly defined areas for the north and south of the site. The soils in the northern part of the site had a generally lower shear wave velocity ( $V_s < 180\text{m/s}$ ) to approximately 20.0m depth, though discrete layers of denser, higher  $V_s$  soils were identified above this depth before becoming lower velocity again. For the southern part of the site, the lower  $V_s$  soils are generally terminated shallower (<5m depth) before the  $V_s$  increased in the gravelly dense material.

Additionally, the measured cone tip resistance ( $q_c$ ) and interpreted shear wave velocity from the CPT data generally shows a consistent pattern with the recorded values from the MASW survey as seen in the CPT profiles in Appendix C. It should be noted that due to the high velocity layers towards the south, thin lower velocity layers were not picked up as seen in the DPSH data. This is reflected in the cross sections presented in Appendix E.

The GPR survey was undertaken to further supplement the MASW surveys for the near-surface soils. The primary objective of this survey was to assist in identifying softer or denser layers that may not have been picked up in the MASW survey. The results generally show a consistent correlation with the MASW survey. The softer soils generally had a poor reflection, with denser material showing a clearer reflection. The shallow gravelly soils at the southern end of the site were also clear within the upper 4.0m of the soil profile.

## Groundwater

Our site-specific shallow investigation encountered groundwater levels between 1.0m and 1.8m bgl, however the cohesive soils below the recorded depth were noted to not be saturated, indicating that a perched water table is likely present on-site. The CPT data shows variable piezometric conditions indicating a groundwater table depth between 0.7m and 2.4m bgl, due to the differing depth of cohesive soils in the upper soil profile and different elevations. The shallower groundwater depths were generally confined to the lower elevations of the property.

Based on the above, a groundwater depth range of between 0.7m to 2.4m bgl was adopted for the liquefaction triggering and free-field settlement assessment, depending on the location of the test across the site.

## Site Subsoil Class

Based on the site-specific investigation, geological maps and other available information, the site is classified as a Class D (deep or soft soil) site.

## Shallow Soils

The geotechnical investigations indicate the existence of low velocity ( $V_s \leq 180\text{m/s}$ ), soils between approximately 4.0m and 20.0m depth, with the lower  $V_s$  soils encountered at greater depths towards the north of the sections. There are also locations where denser pockets of material were identified within these lower  $V_s$  layers. Those layers have lower strength and have the potential for long-term consolidation settlements from loads, such as residential dwellings. This is further discussed later in this report.

# 5. Liquefaction Assessment

## Methodology

An assessment of the earthquake-induced free-field post-liquefaction volumetric settlement at the site has been carried out in accordance with the MBIE Guidance and using proprietary liquefaction assessment software, for SLS and ULS earthquake scenarios.

The seismic design requirements adopted for use in the analyses are defined in MBIE/NZGS Earthquake Geotechnical Engineering Practice Module 3 (May 2016), and Part C of the MBIE Guidelines “Repairing and rebuilding houses affected by the Canterbury earthquakes” and its subsequent updates - clarifications. These are:

- Buildings of normal use (Importance Level 2);
- Deep or soft soil sites (Class D) as specified previously;



- Boulanger and Idriss (2014) methodology for liquefaction triggering, as per the MBIE Guidance subsequent updates (Issue 7, October 2014);
- Zhang et al. (2002) post-liquefaction volumetric strain calculation for estimating the free-field settlements;

Calculations were performed for the full depth of the CPTs and the upper 10m of the soil profile (as per the MBIE Guidance “index value” estimations). It should be noted that the settlement estimates only account for the free-field component of the expected settlement. Actual total settlements under SLS or ULS earthquake loading may be greater or less.

The Liquefaction Severity Number (LSN<sup>1</sup>) has been calculated and used in our assessment as it tends to better reflect the more damaging effects of shallow liquefaction, which is more critical for shallow founded structures. The level of ground damage associated with LSN is summarised in Table 5.

**Table 5: Liquefaction Severity Number Ranges and Related Effects**

LSN Value	Observed Performance
<10	Little to no expression of liquefaction, minor effects
10 – 20	Minor expression of liquefaction, some sand boils
20 – 30	Moderate expression of liquefaction, with sand boils and some structural damage
30 – 40	Moderate to severe expression of liquefaction, settlement can cause structural damage
40 – 50	Major expression of liquefaction, undulations and damage to ground surface, sever total and differential settlement of structures
>50	Severe damage, extensive evidence of liquefaction at surface, sever total and differential settlements affecting structures, damage to services

### Liquefaction Assessment Results

Due to the rapid changes at the interface between fine and coarse-grained soils, a layer correction was applied. The cone tip penetration, and subsequently, the ability to resist liquefaction of a sandy material, is reduced by the surrounding silty layers, while the  $I_c^2$  of the silt layers is reduced due to the presence of the surrounding sandy layers and hence the susceptibility of the fine layers is overestimated. For our analysis, an  $I_c$  change of >0.05 per 10mm has been adopted, which eliminates the liquefaction potential for the layer.

The results of our liquefaction triggering analyses utilising the CPT data are presented in Appendix F and summarised in Table 6.

<sup>1</sup> **LSN = Liquefaction Severity Number.** LSN (van Ballegooy et al., 2014) is a vulnerability indicator (damage index) quantifying liquefaction-induced damage developed to reflect more damaging effects of shallow liquefaction on residential land and foundations following the Canterbury Earthquakes (2010-11). LSN considers depth weighted calculated volumetric densification strain within soil layers as a proxy for the severity of liquefaction land damage likely at the ground surface.

<sup>2</sup>  **$I_c$  = Soil Behaviour Classification Index** - Robertson & Wride 1998.

**Table 6: Estimated “Free-Field” Post-Liquefaction Volumetric Ground Surface Settlements**

Earthquake scenario	Moment magnitude ( $M_w$ ) / PGA (g)	MBIE “Index Value” (mm)	MBIE Technical Category	LSN Values
GWD = varying (in-situ) and 0.5m to 1.2m (earthquake); Layer transition applied				
SLS	7.5/0.13	< 35	TC2	1 – 5
SLS2	6.0/0.19	5 – 50	TC2	2 – 16
ULS	7.5/0.35	5 – 80	TC2	5 – 25

In accordance with the MBIE Guidance, the analysis indicates that under SLS and ULS loading conditions the predicted index value settlements fall within the expected future land performance values for a TC2 category site. The higher settlements were located on the land at the northern area of the 2 Glovers Road section, which generally correlates with observed liquefaction ejecta in the aerial photographs.

Based on the LSN estimated for the design events, ‘little to minor’ expression of liquefaction may be expected for a future SLS design event, and ‘little to moderate’ expression of liquefaction may be expected for a future ULS design event. The values of LSN at the upper end of the ranges estimated are generally located in the central portion of the development area (where ejecta has been observed following the CES events).

### Lateral Spreading

Given the generally flat topography of the site, and the assumption that the site will be levelled further during the development of the subdivision, there is unlikely to be significant height differences, apart from the area immediately adjacent to Green’s Stream. As the area needs to be developed with the FMA in mind, and land levels lifted, there is the potential for a more pronounced ‘free-face’ that could create a risk of lateral spreading. Options to address this are discussed later in the report.

## 6. Site Designation Assessment

Based on the findings of our desk study, our site-specific ground investigation and observations, and assessment of the performance of the land, we consider the MBIE TC2 category generally appropriate for the site. Despite the deformation characteristics of TC2, the land does not meet the definition of ‘Good Ground’ as per the New Zealand Standards without modification to standard foundation systems and specific engineering design to account for this due to the soft soils.

## 7. Geotechnical Considerations for Subdivision

### Geotechnical Hazards

The most significant geotechnical hazards at the site comprise the potential for earthquake-induced soil liquefaction and potential static subsidence of the soft compressible soils. These hazards can be partly mitigated by providing strengthened foundations, which reduce the potential for differential settlement of the buildings and are designed to be re-levellable.

However, as part of the land development it is understood that, in order to meet the CCC FFL requirements, the site grade will need to be raised by filling. Site filling works can induce

additional loading of the underlying soft compressible deposits and potentially lead to consolidation settlement of the fill and / or construction above. To assess the likely influence of filling, a pre-load trial was undertaken by Miyamoto. This trial indicates that static settlements are not believed to pose a significant risk to the Halswell Road section of the development. Given the similar soil conditions found, it is our professional opinion that this statement also applies to the Glovers Road properties. It is still recommended that settlement plates are installed during the site filling works and these should be founded at the base of the fill with upstands extending through the top of the fill. It is advised that the settlement plates are monitored during the raising of the site levels and for a period (up to 6 months) to assess any static settlements and ensure performance is in line with the pre-loading trial findings.

The current subdivision plan for the entire site is not currently finalised and until it is further developed, specific detailed recommendations cannot be provided, however, the following sections outline general considerations for future development.

### Development Considerations

Based on the land survey data (provided by others), a maximum level of approximately 22.3m CDD was identified at the northern extent of property. The land drops to approximately 19.6m CDD next to Green's Stream, though the development does not extend to this point. The low point of the development area is at approximately 20.4m CDD. As discussed above, the site will require filling to meet the CCC FFL requirements (FFL = 21.25m CDD based on the Halswell Road site), particularly if the preferred foundation options comprise concrete slab foundations. It is anticipated that maximum filling would be in the proximity of 1.2m.

Currently, there is no indication of cutting or removal of material to the north of the site. All earthworks should be undertaken in accordance with NZS 4431:1989 (code of practice for earth fill for residential development) prior to the construction of any foundations. The monitoring scheme (mentioned earlier) should be fully developed once the final details of the proposed earthworks are known.

The southern extent of the filling (in proximity of Green's Stream) will be the maximum height of fill required and will require detailed design to ensure stability. It is our understanding the development area is to extend to within 15m of Green's Stream. A shallow vegetated slope is considered suitable given the height of filling is not likely to exceed 1.2m, and provided the slope is not at a gradient exceeding 1.0m vertical to 2.0m horizontal.

Based on the above and the previously completed works, the following foundation solutions would be considered suitable for the construction of NZS3604 compliant structures for the subdivision:

- MBIE TC2 (Options 1 to 4) enhanced foundation slab;
- Specifically designed, enhanced NZS 3604 perimeter foundation wall and shallow piles.

Based on development works proposed, a geotechnical ultimate bearing capacity of 200kPa can be assumed at a high level, though this value is indicative only. The available bearing capacity must be confirmed on-site prior to construction works at the time of any building consent application.

The foundation types detailed above are also preliminary and should be further developed and optimised in collaboration with the structural engineer once further details of any proposed structure are finalised.

### Stormwater Management

Stormwater management is outside the scope of our works. However, it is understood the southern section of the Halswell Road site (area south of Green's Stream) will be utilised for stormwater detention and treatment for the Riverstone subdivision as a whole, with shallow basins excavated through this area. As mentioned in the initial assessment undertaken, this material is unlikely to be suitable for filling of the development area.

### Services

Buried services are vulnerable to ground deformations when located within and/or in proximity of potentially liquefiable and compressible soils. Services for the residential development should be designed by a suitably qualified person in collaboration with the geotechnical engineers to accommodate the likelihood of future ground deformations.

### Pavement/Roading Infrastructure

As for the services at the site, pavements will require detailed design by a suitably experienced person in collaboration with the geotechnical engineer, the finished ground levels and compaction characteristics of the filling material.

It is currently understood that the new areas of development will link into the Halswell Road property as well as having its own access onto Glovers Road, and it is assumed that filling in this area will be required to raise the grade. The underlying soils in this area are generally typical for the site with the upper 1.0m comprising topsoil over soft silt (loosely corresponding to a CBR of ~2 to 3 below the topsoil).

## 8. Assessment Against RMA Section 106

As per the requirements of Section 106 of the Resource Management Act (RMA) (2017), we have undertaken a high-level assessment of the significant geotechnical hazards that may affect the site, outside of the hazards already discussed in this report (i.e. static and earthquake-induced subsidence, and lateral spreading). These hazards include, but are not limited to:

- Erosion;
- Falling debris;
- Slippage;
- Inundation.

At the time of our site visit, there was no evidence of erosion. Likewise, no evidence was observed to suggest that lateral movement is an issue on the site, given the site is generally

flat. Rock Fall or slope movement are also not considered a risk to this area of the development.

As part of the site is identified as being within a Flood Management Area (FMA) as defined by the CCC, inundation is likely to be a risk, as the site currently stands. If the site is built up to ensure the FFLs set by the CCC are met and suitable stormwater drainage is in place, then inundation is not considered an imminent risk to the development.

Based on our assessment, we consider that the “significant” geotechnical hazards may be mitigated to an acceptable standard, provided that the geotechnical recommendations given in this report are followed, and the appropriate engineering measures implemented, we consider that the development is unlikely to be affected nor worsen, accelerate or result in material damage.

## 9. Limitations

This report is subject to the following limitations:

- This report has been prepared by Miyamoto for the Client for the purpose/s agreed with the Client (Purpose). Miyamoto accepts no responsibility for the validity, appropriateness, sufficiency or consequences of the Client using the report for purposes other than for the Purpose.
- This report is not intended for general publication or circulation. This report is not to be reproduced by the Client except in relation to the Purpose, without Miyamoto’s prior written permission. Miyamoto disclaims all risk and all responsibility to any third party.
- This report is provided based on the various assumptions contained in the report.
- Miyamoto’s professional services are performed using a degree of care and skill reasonably exercised by reputable consultants providing the same or similar services as at the date of this report.
- The Client is responsible for ensuring that the design of any foundations ensures the functionality of the building under SLS level loads.
- The sub surface information has been obtained from investigation carried out at discrete locations, which by their nature only provide information about a relatively small volume of subsoils. While Miyamoto has taken reasonable skill and care in carrying out the investigation to determine the subsoil condition, the subsoil condition could differ substantially from the results of any sampling investigation. Miyamoto is not responsible for and does not accept any liability in respect of any difference between the actual subsoil conditions and the results of our investigation.
- Any susceptibility analysis carried out in respect of liquefaction is based on Miyamoto’s current understanding as an experienced professional engineering consultant of the data, methods etc. Future seismic events may change our understanding of liquefaction and its affects, which may affect the content of this report. Miyamoto is not responsible for and does not accept any liability where the content of this report is changed due to a change in industry knowledge of matters relating to liquefaction.
- This report specifically excludes assessment or advice relating to hazardous materials, such as asbestos.

- Where the Client provides information to Miyamoto, including design calculations and drawings of the as-built structure, or where the report indicates that we have obtained and/or relied upon information provided from a third party, Miyamoto has not made any independent verification of this information except as expressly stated in the report. Miyamoto assumes no responsibility for any inaccuracies in, or omissions to, that information.
- A change in circumstances, facts, information after the report has been provided may affect the adequacy or accuracy of the report. Miyamoto is not responsible for the adequacy or accuracy of the report as a result of any such changes.
- This report is not to be reproduced, either wholly or in part, without our prior written permission.

If you have any queries or you require any further clarification on any aspects of this report, please do not hesitate to contact Miyamoto International (NZ) Ltd.

## 10. References

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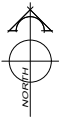
## Appendices





## A. Updated Indicative Subdivision Plan (Davie Lovell Smith)





**DRAFT**

AMENDMENT	DATE	DESCRIPTION



Total Area : 23.1161 ha  
 Comprised in: RT's CB10B/654, CB48C/117 & CB48C/118

**DAVE LOVELL-SMITH**  
 PLANNING SURVEYING ENGINEERING

116 Wrights Road P O Box 679 Christchurch 8140, New Zealand  
 Telephone: 03 379-0793 Website: www.dls.co.nz E-mail: office@dls.co.nz

JOB TITLE: **Halswell Road**

SHEET TITLE: **Proposed Subdivision of  
 Pt RS 1593, RS 772 &  
 Lots 1 & 2 DP 83635**

DRAWING STATUS: **For Discussion Purposes**

SCALE: 1:1000@A1 DATE: October 2020  
 1:2000@A3

CAD FILE: J:\2017\Concept\_R4.dwg REVISION:  
 DRAWING No: **C20017** SHEET No: 1 OF 1 **R6**

- NOTES:
1. Areas and dimensions are approximate only and are subject to final survey and deposit of plans.
  2. Service easements to be created as required.
  3. This plan has been prepared for discussion purposes only. No liability is accepted if the plan is used for any other purposes.
  4. The position of Greens Drain is approximate and subject to survey.

Lot 2  
 DP 490383

Lot 3  
 DP 83635

Pt RS 5786

## B. ECan Listed Land Use Register Files



Dear Sir/Madam

Thank you for submitting your property enquiry in regards to our Listed Land Use Register (LLUR) which holds information about sites that have been used, or are currently used for activities which have the potential to have caused contamination.

The LLUR statement provided indicates the location of the land parcel(s) you enquired about and provides information regarding any LLUR sites within a radius specified in the statement of this land.

Please note that if a property is not currently entered on the LLUR, it does not mean that an activity with the potential to cause contamination has never occurred, or is not currently occurring there. The LLUR is not complete, and new sites are regularly being added as we receive information and conduct our own investigations into current and historic land uses.

The LLUR only contains information held by Environment Canterbury in relation to contaminated or potentially contaminated land; other information relevant to potential contamination may be held in other files (for example consent and enforcement files).

If your enquiry relates to a farm property, please note that many current and past activities undertaken on farms may not be listed on the LLUR. Activities such as the storage, formulation and disposal of pesticides, offal pits, foot rot troughs, animal dips and underground or above ground fuel tanks have the potential to cause contamination.

Please contact and Environment Canterbury Contaminated Sites Officer if you wish to discuss the contents of the LLUR statement, or if you require additional information. For any other information regarding this land please contact Environment Canterbury Customer Services.

Yours sincerely

**Contaminated Sites Team**

# Property Statement from the Listed Land Use Register

Visit [www.ecan.govt.nz/HAIL](http://www.ecan.govt.nz/HAIL) for more information about land uses.

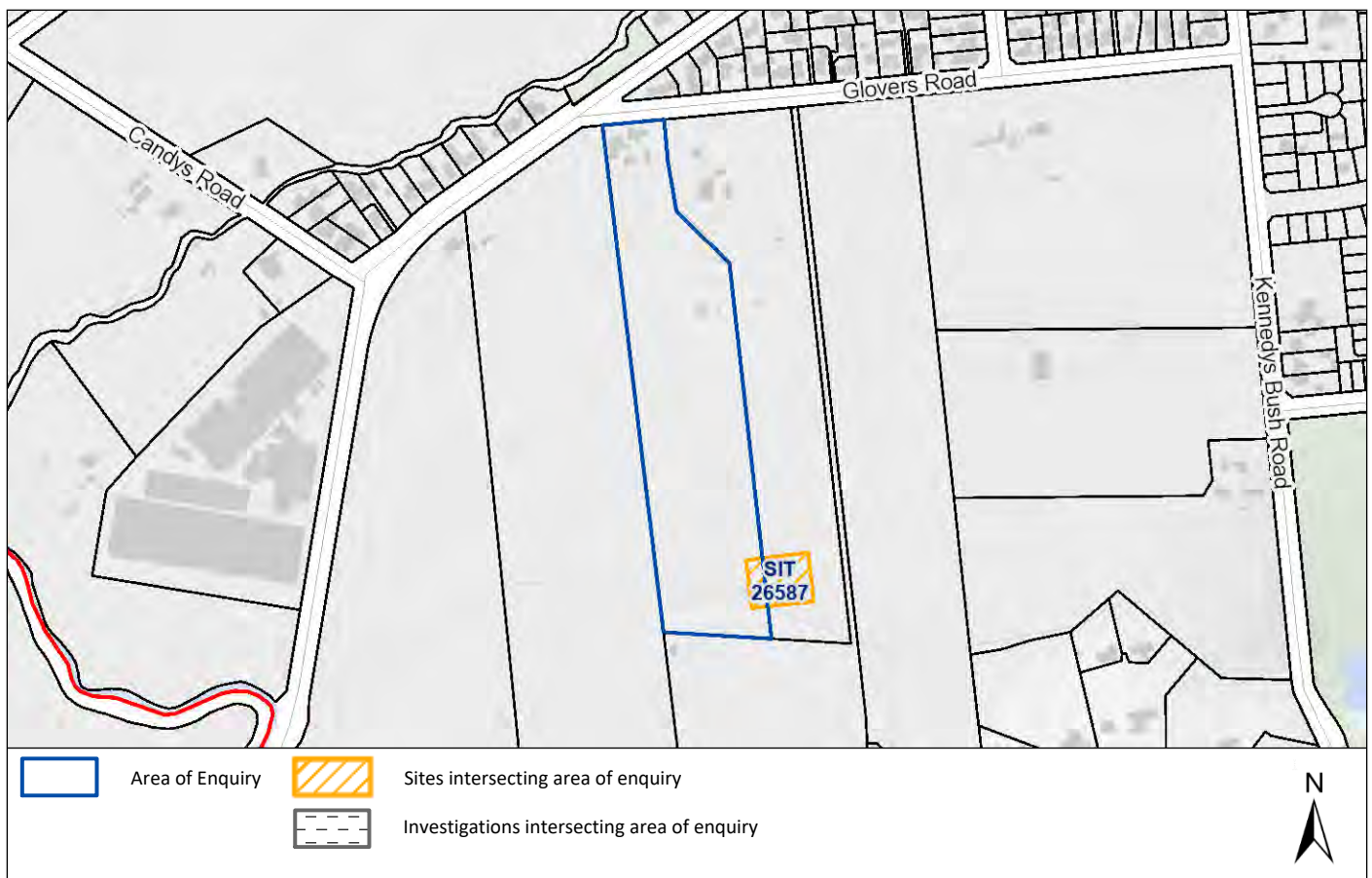
Customer Services  
P. 03 353 9007 or 0800 324 636

PO Box 345  
Christchurch 8140

P. 03 365 3828  
F. 03 365 3194  
E. [ecinfo@ecan.govt.nz](mailto:ecinfo@ecan.govt.nz)

[www.ecan.govt.nz](http://www.ecan.govt.nz)

<b>Date:</b>	13 October 2020	
<b>Land Parcels:</b>	Lot 1 DP 83635	Valuation No(s): 2356209300



*The information presented in this map is specific to the property you have selected. Information on nearby properties may not be shown on this map, even if the property is visible.*

## Summary of sites:

Site ID	Site Name	Location	HAIL Activity(s)	Category
26587	26587	Halswell West	A10 - Persistent pesticide bulk storage or use;	Not Investigated

Please note that the above table represents a summary of sites and HAILS intersecting the area of enquiry only.

## Information held about the sites on the Listed Land Use Register

**Site 26587: 26587** (Intersects enquiry area.)

<b>Site Address:</b>	Halswell West
<b>Legal Description(s):</b>	Lot 1 DP 83635, Lot 2 DP 83635

<b>Site Category:</b>	Not Investigated
<b>Definition:</b>	Verified HAIL has not been investigated.

<b>Land Uses (from HAIL):</b>	<b>Period From</b>	<b>Period To</b>	<b>HAIL land use</b>
	Pre 1994	Pre 2004	Persistent pesticide bulk storage or use including sports turfs, market gardens, orchards, glass houses or spray sheds

**Notes:**

17 Oct 2013                    Area defined from: 1994-2004 ECan Aerial Photographs  
 Note: Multiple glass houses were noted in aerial photographs reviewed.

**Investigations:**

There are no investigations associated with this site.

---

**Information held about other investigations on the Listed Land Use Register**

For further information from Environment Canterbury, contact Customer Services and refer to enquiry number ENQ265562.

**Disclaimer:**        *The enclosed information is derived from Environment Canterbury’s Listed Land Use Register and is made available to you under the Local Government Official Information and Meetings Act 1987 and Environment Canterbury’s Contaminated Land Information Management Strategy (ECan 2009).*

*The information contained in this report reflects the current records held by Environment Canterbury regarding the activities undertaken on the site, its possible contamination and based on that information, the categorisation of the site. Environment Canterbury has not verified the accuracy or completeness of this information. It is released only as a copy of Environment Canterbury's records and is not intended to provide a full, complete or totally accurate assessment of the site. It is provided on the basis that Environment Canterbury makes no warranty or representation regarding the reliability, accuracy or completeness of the information provided or the level of contamination (if any) at the relevant site or that the site is suitable or otherwise for any particular purpose. Environment Canterbury accepts no responsibility for any loss, cost, damage or expense any person may incur as a result of the use, reference to or reliance on the information contained in this report.*

*Any person receiving and using this information is bound by the provisions of the Privacy Act 1993.*

Dear Sir/Madam

Thank you for submitting your property enquiry in regards to our Listed Land Use Register (LLUR) which holds information about sites that have been used, or are currently used for activities which have the potential to have caused contamination.

The LLUR statement provided indicates the location of the land parcel(s) you enquired about and provides information regarding any LLUR sites within a radius specified in the statement of this land.

Please note that if a property is not currently entered on the LLUR, it does not mean that an activity with the potential to cause contamination has never occurred, or is not currently occurring there. The LLUR is not complete, and new sites are regularly being added as we receive information and conduct our own investigations into current and historic land uses.

The LLUR only contains information held by Environment Canterbury in relation to contaminated or potentially contaminated land; other information relevant to potential contamination may be held in other files (for example consent and enforcement files).

If your enquiry relates to a farm property, please note that many current and past activities undertaken on farms may not be listed on the LLUR. Activities such as the storage, formulation and disposal of pesticides, offal pits, foot rot troughs, animal dips and underground or above ground fuel tanks have the potential to cause contamination.

Please contact and Environment Canterbury Contaminated Sites Officer if you wish to discuss the contents of the LLUR statement, or if you require additional information. For any other information regarding this land please contact Environment Canterbury Customer Services.

Yours sincerely

**Contaminated Sites Team**

# Property Statement from the Listed Land Use Register

Visit [www.ecan.govt.nz/HAIL](http://www.ecan.govt.nz/HAIL) for more information about land uses.



Customer Services  
P. 03 353 9007 or 0800 324 636

PO Box 345  
Christchurch 8140

P. 03 365 3828  
F. 03 365 3194  
E. [ecinfo@ecan.govt.nz](mailto:ecinfo@ecan.govt.nz)

[www.ecan.govt.nz](http://www.ecan.govt.nz)

Date:	13 October 2020	
Land Parcels:	Lot 2 DP 83635	Valuation No(s): 2356209301



*The information presented in this map is specific to the property you have selected. Information on nearby properties may not be shown on this map, even if the property is visible.*

## Summary of sites:

Site ID	Site Name	Location	HAIL Activity(s)	Category
26587	26587	Halswell West	A10 - Persistent pesticide bulk storage or use;	Not Investigated

Please note that the above table represents a summary of sites and HAILS intersecting the area of enquiry only.

## Information held about the sites on the Listed Land Use Register

**Site 26587: 26587** (Intersects enquiry area.)

Site Address:	Halswell West
Legal Description(s):	Lot 1 DP 83635, Lot 2 DP 83635



<b>Site Category:</b>	Not Investigated
<b>Definition:</b>	Verified HAIL has not been investigated.

Land Uses (from HAIL):	Period From	Period To	HAIL land use
	Pre 1994	Pre 2004	Persistent pesticide bulk storage or use including sports turfs, market gardens, orchards, glass houses or spray sheds

**Notes:**

17 Oct 2013                    Area defined from: 1994-2004 ECan Aerial Photographs  
 Note: Multiple glass houses were noted in aerial photographs reviewed.

**Investigations:**

There are no investigations associated with this site.

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**Information held about other investigations on the Listed Land Use Register**

For further information from Environment Canterbury, contact Customer Services and refer to enquiry number ENQ265560.

**Disclaimer:**        *The enclosed information is derived from Environment Canterbury’s Listed Land Use Register and is made available to you under the Local Government Official Information and Meetings Act 1987 and Environment Canterbury’s Contaminated Land Information Management Strategy (ECan 2009).*

*The information contained in this report reflects the current records held by Environment Canterbury regarding the activities undertaken on the site, its possible contamination and based on that information, the categorisation of the site. Environment Canterbury has not verified the accuracy or completeness of this information. It is released only as a copy of Environment Canterbury’s records and is not intended to provide a full, complete or totally accurate assessment of the site. It is provided on the basis that Environment Canterbury makes no warranty or representation regarding the reliability, accuracy or completeness of the information provided or the level of contamination (if any) at the relevant site or that the site is suitable or otherwise for any particular purpose. Environment Canterbury accepts no responsibility for any loss, cost, damage or expense any person may incur as a result of the use, reference to or reliance on the information contained in this report.*

*Any person receiving and using this information is bound by the provisions of the Privacy Act 1993.*

## C. Geotechnical Investigation Results

MINZ Shallow Investigation Logs

Laboratory Soil Sample Test Results

LandTest CPT/DPSH Plot



## SHALLOW GROUND INVESTIGATION LOG

HA1/DCP1

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
LOGGED BY: CG	TOTAL DEPTH OF HOLE: 2.9 mbgl
PROCESSED BY: CG	HOLE DIAMETER: 50 mm
LOCATION: REFER TO SITE PLAN	DRILLING METHOD: Hand Auger
	SHEAR VANE NUMBER: 2102
	GROUNDWATER LEVEL: 1.65 mbgl
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded	
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size				
							LL	PL	PI	Gr	Sa	FC		WC (%)
0.0 - 0.5	1, 1, 1, 1, 3, 2			SILT: low plasticity, dark brown, moist, with minor rootlets (TOPSOIL)	[Cross-hatch pattern]									
0.5 - 1.5	1, 2, 1, 2, 2, 2, 2, 2, 2, 1			SILT: low plasticity, brown, moist, with minor fine sand	[X pattern]									
1.5 - 2.5	2, 2, 2, 2, 2, 2, 3, 3, 2, 1, 1, 2, 2, 3, 4, 5	1.65		Silty SAND: fine to medium, brown-grey, wet  at 2.0m: becomes blue-grey, saturated	[Dotted pattern]	DIST. SAMPLE					51%	49%		
2.5 - 3.0						DIST. SAMPLE					51%	49%		

...contd on next page

### LEGEND

**ABBREVIATIONS**

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 ...▽... STANDING GWL

**NOTES**

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA1/DCP1 (contd.)

<b>PROJECT:</b>	2 & 4 Glovers Road, Halswell, Christchurch				
<b>LOGGED BY:</b>	CG	<b>TOTAL DEPTH OF HOLE:</b>	3.9 mbgl	<b>HOLE DIAMETER:</b>	50 mm
<b>PROCESSED BY:</b>	CG	<b>DRILLING METHOD:</b>	Hand Auger	<b>SHEAR VANE NUMBER:</b>	2102
<b>LOCATION:</b>	REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b>	1.65 mbgl	This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size				WC (%)	UW
							LL	PL	PI	Gr	Sa	FC			
3.5	9 9 9 9 7 6 6 7 7	1.65m bgl →		Silty SAND: fine to medium, blue-grey, saturated (contd.)		DIST. SAMPLE					51%	49%			
4.0				SILT: low plasticity, blue-grey, saturated											
4.5				EOH (Target Depth Reached)											
5.0															
5.5															

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
GWL GROUNDWATER LEVEL  
mbgl METERS BELOW GROUND LEVEL  
WC WATER CONTENT

HA HAND AUGER  
UTP UNABLE TO PENETRATE  
EOH END OF HOLE  
UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
PL PLASTIC LIMIT  
PI PLASTICITY INDEX  
NE NOT ENCOUNTERED

Gr GRAVEL  
Sa SAND  
FC FINES CONTENT  
...▽... STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

## HA2/DCP2

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 3.9 mbgl
<b>PROCESSED BY:</b> CG	<b>DRILLING METHOD:</b> Hand Auger
<b>LOCATION:</b> REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b> 1.3 mbgl
<b>HOLE DIAMETER:</b> 50 mm	
<b>SHEAR VANE NUMBER:</b> 2102	
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing							Vane shear strength (kPa) peak/remoulded	
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size			WC (%)		UW
							LL	PL	PI	Gr	Sa	FC			
1	1	▽		SILT: non-plastic, dark brown, moist, with some sand and rootlets (TOPSOIL)										66 / 16	
2	2			SILT: low plasticity, yellow-brown, moist, with some sand											
0.5	2														
	3														
	3				SAND: fine to medium, orange-brown, moist, with trace of silt										
1.0	2														
	2														
	4														
	3														
	2														
	3														
	2														
1.5	2														
	3				Clayey SILT: low to medium plasticity, grey, moist, with some sand										
	4														
	3														
	3			at 1.9m: becomes wet, mottled orange											
2.0	Self Weight														
	1														
	3														
	3			at 2.2m: mottling absent											
	3														
	3			at 2.3m: becomes saturated											
2.5	4														
	4														
	5														
	5														
	7														
	7														
...contd on next page															
						DIST. SAMPLE	29	20	9	-	15%	85%			

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 ▽ STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA2/DCP2 (contd.)

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 3.9 mbgl
<b>PROCESSED BY:</b> CG	<b>DRILLING METHOD:</b> Hand Auger
<b>LOCATION:</b> REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b> 1.3 mbgl
<b>HOLE DIAMETER:</b> 50 mm	
<b>SHEAR VANE NUMBER:</b> 2102	
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size				WC (%)	UW
							LL	PL	PI	Gr	Sa	FC			
7	7	1.3m bgl -->		Clayey SILT: low to medium plasticity, grey, saturated, with some sand (contd.)		DIST. SAMPLE	29	20	9	-	15%	85%			
7	7														
8	8														
7	7														
3.5	7														
6	6														
7	7														
8	8														
7	7		EOH (Target Depth Reached)												
4.0															
4.5															
5.0															
5.5															

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA3/DCP3

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
LOGGED BY: CG	TOTAL DEPTH OF HOLE: 4.1 mbgl
PROCESSED BY: CG	HOLE DIAMETER: 50 mm
LOCATION: REFER TO SITE PLAN	DRILLING METHOD: Hand Auger
	SHEAR VANE NUMBER: 2102
	GROUNDWATER LEVEL: 1.8 mbgl
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size					
							LL	PL	PI	Gr	Sa	FC		WC (%)	UW
0.0 - 0.5	2			SILT: non-plastic, dark brown, dry, with some sand and rootlets (TOPSOIL)											
0.5 - 1.0	2			SILT: low plasticity, light brown, moist											
1.0 - 1.5	2			SAND: fine to medium, orange brown, moist											
1.5 - 2.0	3			Sandy SILT: low plasticity, orange brown, wet											
2.0 - 2.5	3			SILT: medium plasticity, brown, wet											
2.5 - 3.0	5	1.8 mbgl		Sandy SILT: non-plastic, dark grey, saturated		DIST. SAMPLE	Non-Plastic			-	41%	59%			
3.0 - 3.5	2														
3.5 - 4.0	2														
4.0 - 4.5	4														
4.5 - 5.0	4														
5.0 - 5.5	5														
5.5 - 6.0	2														
6.0 - 6.5	4														
6.5 - 7.0	5														

...contd on next page

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 ...▽... STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

## HA3/DCP3 (contd.)

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 4.1 mbgl
<b>PROCESSED BY:</b> CG	<b>DRILLING METHOD:</b> Hand Auger
<b>LOCATION:</b> REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b> 1.8 mbgl
<b>HOLE DIAMETER:</b> 50 mm	
<b>SHEAR VANE NUMBER:</b> 2102	
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size					
							LL	PL	PI	Gr	Sa	FC		WC (%)	UW
5	5	1.8m bgl →		Sandy SILT: non-plastic, dark grey, saturated (contd.)	x x	DIST. SAMPLE	Non-Plastic			-	41%	59%			
7	7														
8	8														
8	8														
3.5	8														
	7														
	8														
	9														
	10														
4.0				EOH (Target Depth Reached)											
4.5															
5.0															
5.5															

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER	HA HAND AUGER	LL LIQUID LIMIT
GWL GROUNDWATER LEVEL	UTP UNABLE TO PENETRATE	PL PLASTIC LIMIT
mbgl METERS BELOW GROUND LEVEL	EOH END OF HOLE	PI PLASTICITY INDEX
WC WATER CONTENT	UW UNIT WEIGHT (kN/m³)	NE NOT ENCOUNTERED

Gr GRAVEL
Sa SAND
FC FINES CONTENT
∇ STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth



## SHALLOW GROUND INVESTIGATION LOG

HA4/DCP4

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 2.9 mbgl
<b>PROCESSED BY:</b> CG	<b>DRILLING METHOD:</b> Hand Auger
<b>LOCATION:</b> REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b> 1.2 mbgl
<b>HOLE DIAMETER:</b> 50 mm	
<b>SHEAR VANE NUMBER:</b> 2102	
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing							Vane shear strength (kPa) peak/remoulded	
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size			WC (%)		UW
							LL	PL	PI	Gr	Sa	FC			
0.0 - 0.2	2			Sandy SILT: non-plastic, brown, moist, with minor rootlets (TOPSOIL)											
0.2 - 0.8	2			SAND: fine to medium, grey, moist, with some silt											
0.8 - 1.2	2			at 0.8m: becomes wet											
1.2 - 1.9	3	1.2		Sandy SILT: low plasticity, brown-grey, wet, sand is fine											
1.9 - 2.0	3			at 1.2m: becomes saturated											
2.0 - 2.2	3			SILT: low to medium plasticity, blue-grey, saturated											
2.2 - 2.4	4			Silty SAND: fine to medium, grey, saturated											
2.4 - 2.5	4														
			EOH (Target Depth Reached)												

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 (kN/m<sup>3</sup>)  
 UW UNIT WEIGHT

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA5/DCP5

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 1.9 mbgl
<b>PROCESSED BY:</b> CG	<b>DRILLING METHOD:</b> Hand Auger
<b>LOCATION:</b> REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b> 1.0 mbgl
<b>HOLE DIAMETER:</b> 50 mm	
<b>SHEAR VANE NUMBER:</b> 2102	
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing							Vane shear strength (kPa) peak/remoulded					
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size			WC (%)		UW				
							LL	PL	PI	Gr	Sa	FC							
0.0 - 0.2	2	▽		SILT: low plasticity, brown, moist, with minor fine sand (TOPSOIL)	[Cross-hatch pattern]														
0.2 - 0.4	1			Sandy SILT: low plasticity, grey, moist, sand is fine	[X pattern]														
0.4 - 0.6	2																		
0.6 - 0.8	2																		
0.8 - 1.0	2																		
1.0 - 1.2	2																		
1.2 - 1.4	2																		
1.4 - 1.6	1				at 1.0m: becomes wet														
1.6 - 1.8	1				at 1.2m: becomes saturated														
1.8 - 2.0	2				Silty SAND: fine to medium, grey, saturated	[Dotted pattern]	DIST. SAMPLE					58%	42%						
2.0 - 2.2	5			at 1.8m: with minor fine to medium gravel	[Small dots pattern]														
2.2 - 2.4	11			EOH (Practical Refusal on Gravel)															

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UN (kN/m<sup>3</sup>) UNIT WEIGHT

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 ▽ STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

**SITE INVESTIGATION PLAN**

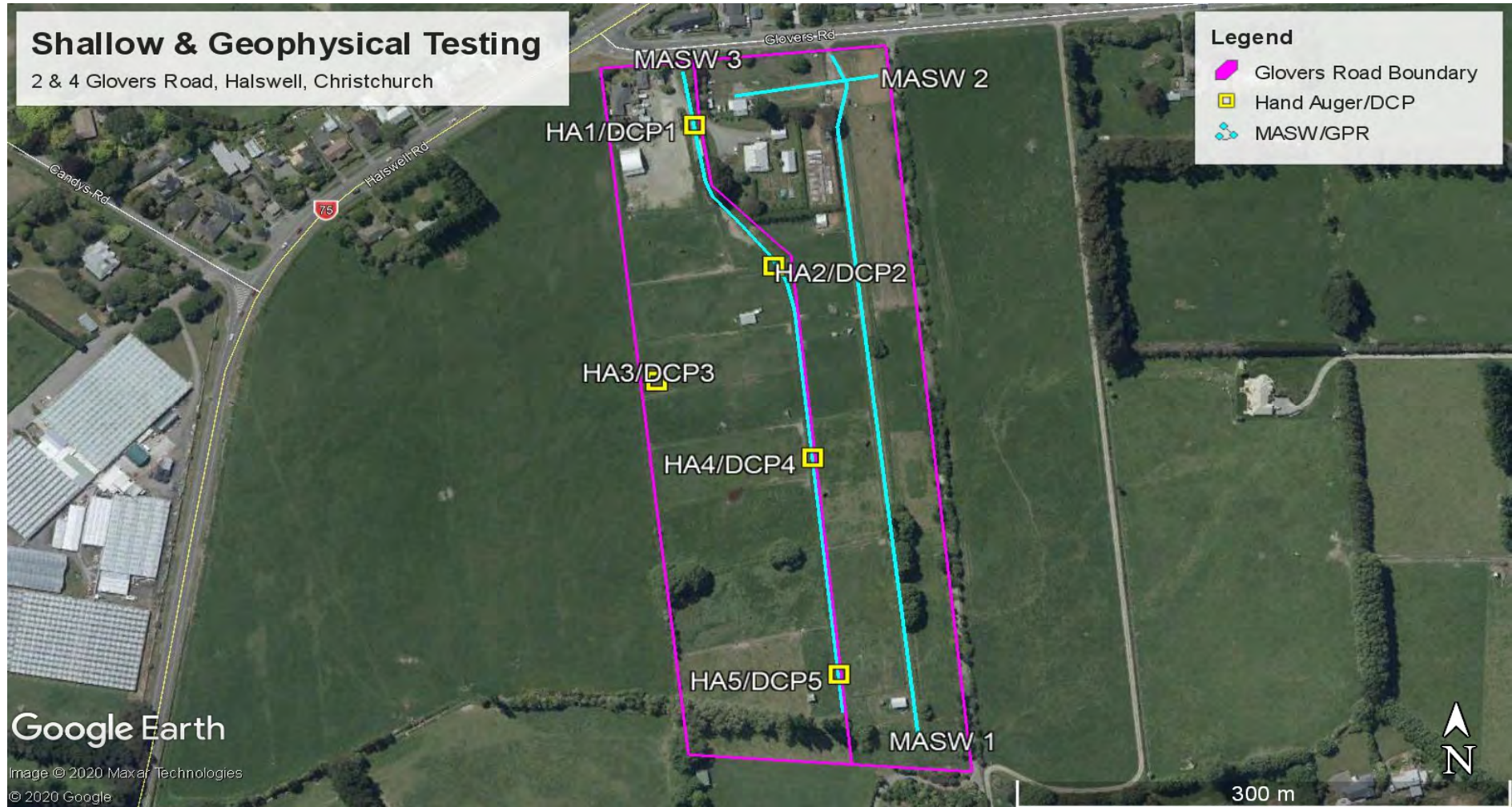
2 & 4 Glovers Road, Halswell, Christchurch

**Shallow & Geophysical Testing**

2 & 4 Glovers Road, Halswell, Christchurch

**Legend**

- Glovers Road Boundary
- Hand Auger/DCP
- MASW/GPR



## TEST REPORT

Lab Job No: 8378-032  
Your ref.: -  
Date of Issue: 14/09/2020  
Date of Re-Issue: -  
Page: 1 of 8

### Test Report

#### C20-450

PROJECT: 2 Glovers Road – Laboratory Testing  
CLIENT: Miyamoto International NZ Ltd,  
518 Colombo Street,  
Christchurch, 8011  
ATTENTION: Clem Gibbens  
INSTRUCTIONS: Determination of Particle-Size Distribution-Wet Sieving method  
Determination of the Liquid & Plastic Limits, Plasticity Index and Water Content  
Determination of the Water Content of Soils  
TEST METHOD: NZS 4402:1986 Test 2.8.1  
NZS 4402:1986 Tests 2.2, 2.3, 2.4  
NZS 4402:1986 Test 2.1  
SAMPLING METHOD: Client - SNA  
TEST RESULTS: As per Laboratory sheets attached



Jeremy Brokenshire  
Laboratory Technician



Nick van Warmerdam  
Approved Signatory



All tests reported herein  
have been performed in  
accordance with the  
laboratory's scope of  
accreditation

-CPT – Aggregates – Soil – Roadings-

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Christchurch Laboratory  
18B Birmingham Drive  
Middleton, Christchurch  
E: info@geocivil.co.nz  
M: 027 6565 317

DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH

NZS 4402: 1986 Test 2.8.1, 2.8.2

Lab Job No: 8378-032  
Client: Miyamoto International NZ Ltd  
Location: 2 Glovers Road  
HA01 (1.5-2.3m)  
Date Received: 8/09/2020  
Report No: C20-450  
REF: -

Sample No: C20-319  
Tested By: D.P  
Date: 9/09/2020  
Checked By: J.B  
Date: 14/09/2020  
Page: 2 of 8

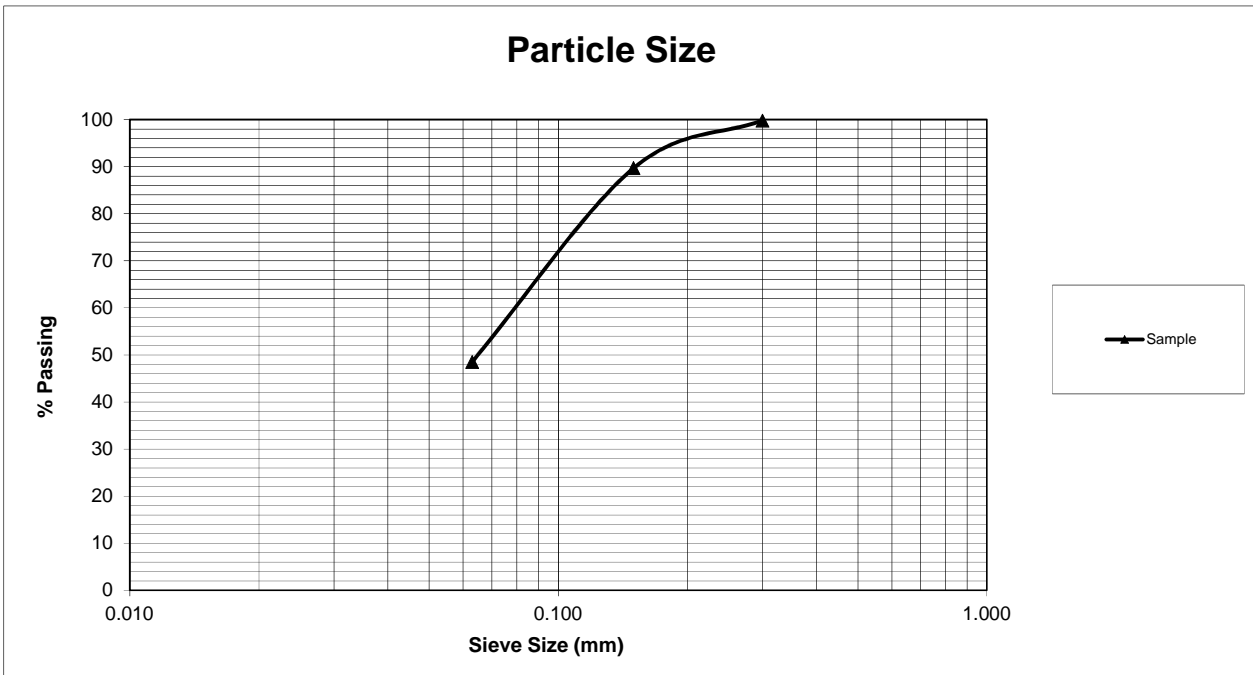
Sampling Method: Sampled by client - SNA  
Date Sampled: 4/09/2020

Sampled By: Client

Test Details: Wet sieving method  
History: Natural

Description of Sample: Silty SAND, brownish grey, wet, no plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	100
0.150	-	-	90
0.063	-	-	49



\*The percentage passing the finest sieve was obtained by difference.

N. van Warmerdam  
Approved Signatory



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18B Birmingham Drive  
Middleton, Christchurch  
E: info@geocivil.co.nz  
M: 027 6565 317

DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH

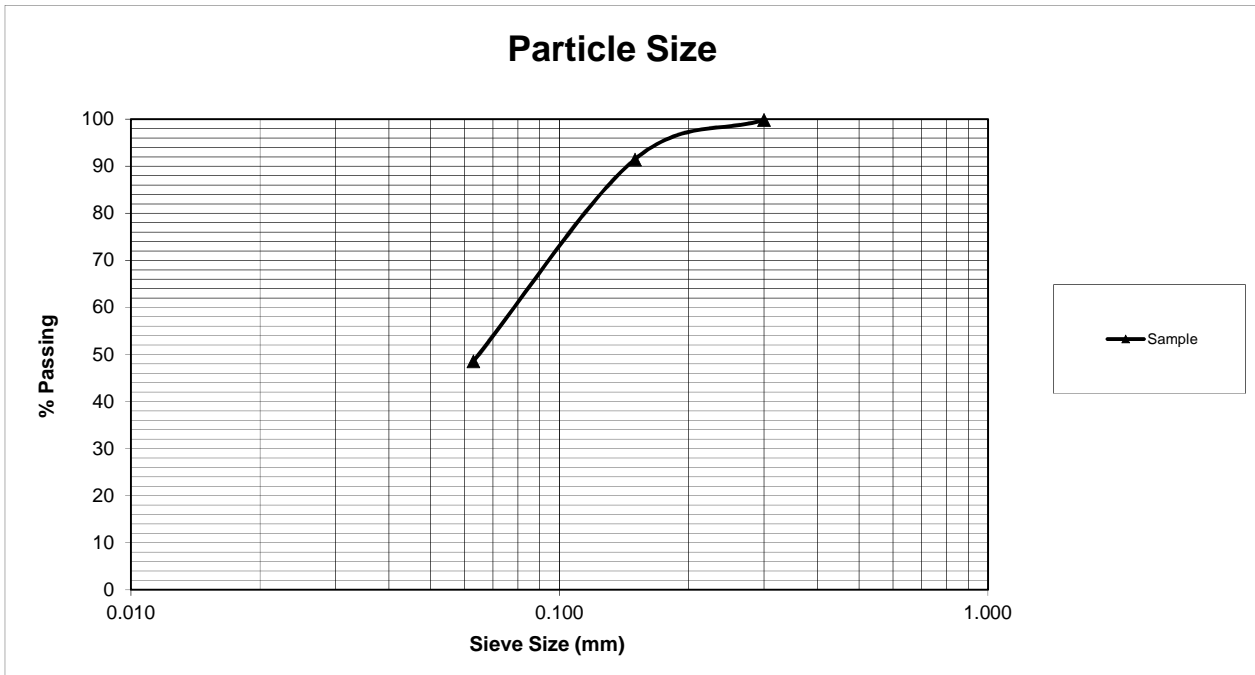
NZS 4402: 1986 Test 2.8.1, 2.8.2

Lab Job No: 8378-032      Sample No: C20-320  
Client: Miyamoto International NZ Ltd      Tested By: D.P  
Location: 2 Glovers Road      Date: 9/09/2020  
          HA01 (2.3-3.8m)      Checked By: J.B  
Date Received: 8/09/2020      Date: 14/09/2020  
Report No: C20-450      Page: 3 of 8  
REF: -  
Sampling Method: Sampled by client - SNA      Sampled By: Client  
Date Sampled: 4/09/2020

Test Details: Wet sieving method  
History: Natural

Description of Sample: Silty SAND, brownish grey, saturated, no plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	100
0.150	-	-	91
0.063	-	-	49



\*The percentage passing the finest sieve was obtained by difference.



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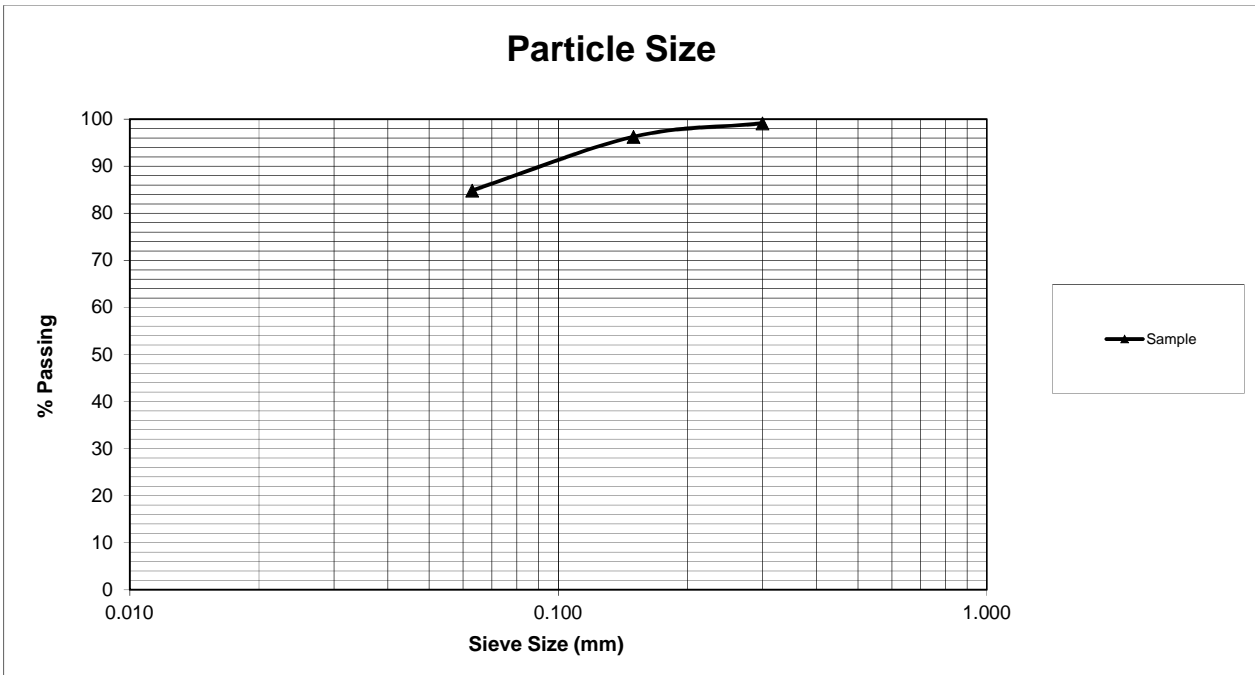
DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH

NZS 4402: 1986 Test 2.8.1, 2.8.2

<b>Lab Job No:</b>	8378-032	<b>Sample No:</b>	C20-321
<b>Client:</b>	Miyamoto International NZ Ltd	<b>Tested By:</b>	D.P
<b>Location:</b>	2 Glovers Road HA02 (2.7-4.0m)	<b>Date:</b>	9/09/2020
<b>Date Received:</b>	8/09/2020	<b>Checked By:</b>	J.B
<b>Report No:</b>	C20-450	<b>Date:</b>	14/09/2020
<b>REF:</b>	-	<b>Page:</b>	4 of 8
<b>Sampling Method:</b>	Sampled by client - SNA	<b>Sampled By:</b>	Client
<b>Date Sampled:</b>	4/09/2020		
<b>Test Details:</b>	Wet sieving method		
<b>History:</b>	Natural		

Description of Sample: Silty CLAY, some sand, dark grey saturated, low plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	99
0.150	-	-	96
0.063	-	-	85



\*The percentage passing the finest sieve was obtained by difference.

N. van Warmerdam  
Approved Signatory

**DETERMINATION OF THE LIQUID & PLASTIC LIMITS,  
PLASTICITY INDEX & WATER CONTENT**

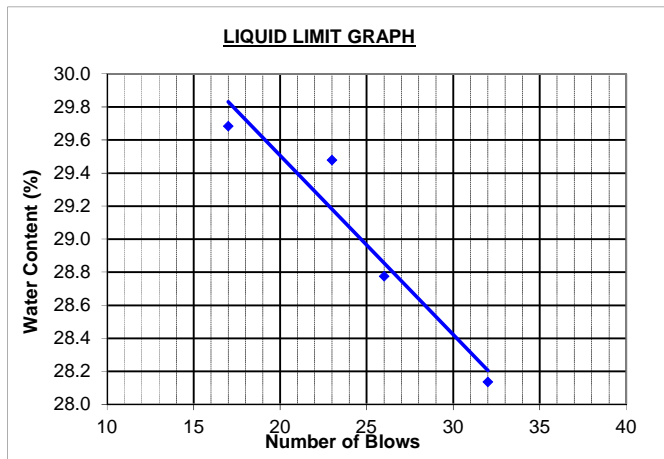
NZS 4402: 1986 Test 2.2, 2.3, 2.4

<b>Lab Job No:</b>	8378-032	<b>Sample No.:</b>	C20-321
<b>Client:</b>	Miyamoto International NZ Ltd	<b>Tested By:</b>	S.P.S
<b>Location:</b>	2 Glovers Road HA02 (2.7-4.0m)	<b>Date Tested:</b>	11/09/2020
<b>Date Received:</b>	8/09/2020	<b>Checked By:</b>	J.B
<b>Report No:</b>	C20-450	<b>Date Checked:</b>	14/09/2020
<b>REF:</b>	-	<b>Page:</b>	5 of 8
<b>Sampling Method:</b>	Sampled by client - SNA	<b>Sampled By:</b>	Client
<b>Date Sampled:</b>	4/09/2020		

**Test Details:**  
 Test performed on: Fraction passing 425mm sieve  
 Sample history: Natural state

**Description of Sample:** Silty CLAY, some sand, dark grey saturated, low plasticity

		Liquid Limit				Plastic Limit		NWC	
No. of blows	17	23	26	32			Liquid Limit	30.5	
Water content (%)	29.7	29.5	28.8	28.1	20.0	19.2	Plastic Limit	20	
							Plasticity Index	9	







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**DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH**

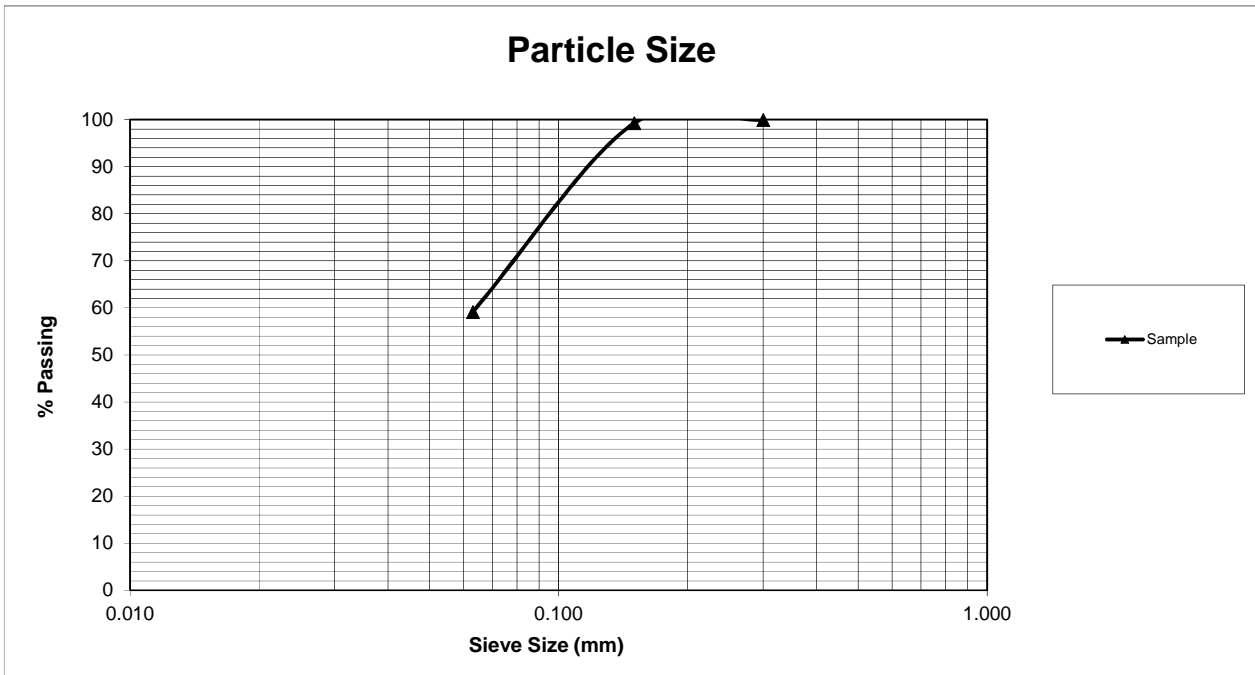
NZS 4402: 1986 Test 2.8.1, 2.8.2

<b>Lab Job No:</b>	8378-032	<b>Sample No:</b>	C20-322
<b>Client:</b>	Miyamoto International NZ Ltd	<b>Tested By:</b>	D.P
<b>Location:</b>	2 Glovers Road HA03 (2.0-3.4m)	<b>Date:</b>	9/09/2020
<b>Date Received:</b>	8/09/2020	<b>Checked By:</b>	J.B
<b>Report No:</b>	C20-450	<b>Date:</b>	14/09/2020
<b>REF:</b>	-	<b>Page:</b>	6 of 8
<b>Sampling Method:</b>	Sampled by client - SNA	<b>Sampled By:</b>	Client
<b>Date Sampled:</b>	4/09/2020		

**Test Details:** Wet sieving method  
**History:** Natural

**Description of Sample:** Sandy SILT, dark grey, saturated, no plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	100
0.150	-	-	99
0.063	-	-	59



\*The percentage passing the finest sieve was obtained by difference.

N. van Warmerdam  
 Approved Signatory

**DETERMINATION OF THE LIQUID & PLASTIC LIMITS,  
PLASTICITY INDEX & WATER CONTENT**

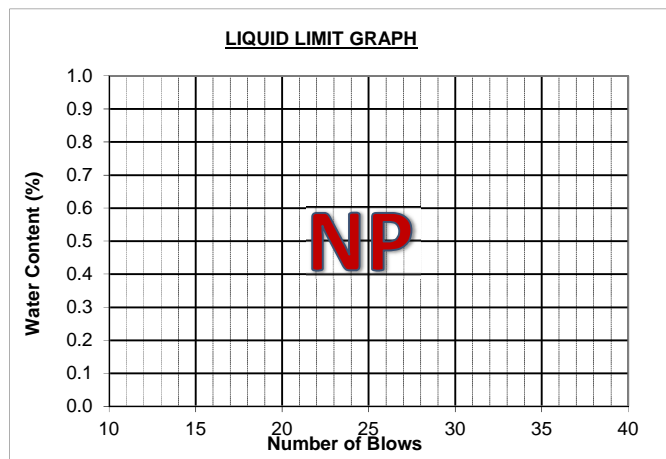
NZS 4402: 1986 Test 2.2, 2.3, 2.4

<b>Lab Job No:</b>	8378-032	<b>Sample No.:</b>	C20-322
<b>Client:</b>	Miyamoto International NZ Ltd	<b>Tested By:</b>	S.P.S
<b>Location:</b>	2 Glovers Road HA03 (2.0-3.4m)	<b>Date Tested:</b>	11/09/2020
<b>Date Received:</b>	8/09/2020	<b>Checked By:</b>	J.B
<b>Report No:</b>	C20-450	<b>Date Checked:</b>	14/09/2020
<b>REF:</b>	-	<b>Page:</b>	7 of 8
<b>Sampling Method:</b>	Sampled by client - SNA	<b>Sampled By:</b>	Client
<b>Date Sampled:</b>	4/09/2020		

**Test Details:**  
 Test performed on: Fraction passing 425mm sieve  
 Sample history: Natural state

**Description of Sample:** Sandy SILT, dark grey, saturated, no plasticity

	<b>Liquid Limit</b>	<b>Plastic Limit</b>	<b>NWC</b>	<b>28.9</b>
<b>No. of blows</b>	<b>NP</b>	<b>NP</b>	<b>Liquid Limit</b>	-
<b>Water content (%)</b>			<b>Plastic Limit</b>	-
			<b>Plasticity Index</b>	-



\*Unable to obtain Liquid Limit or Plastic Limit.



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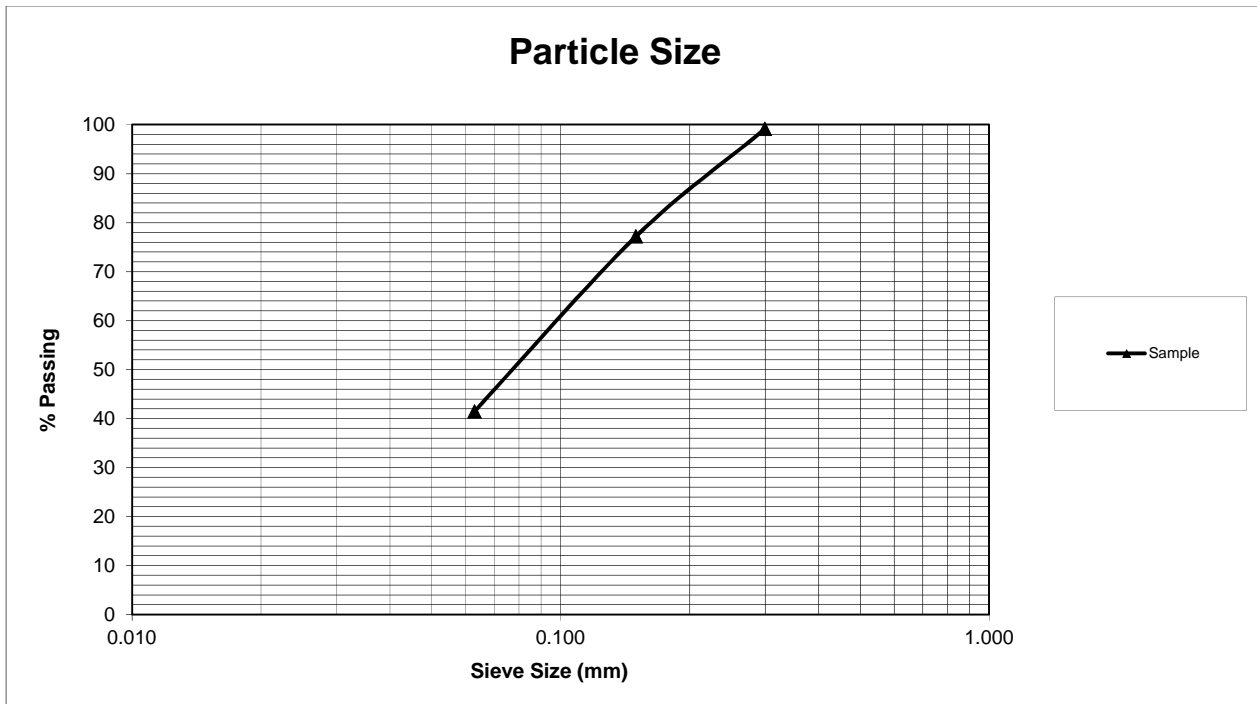
DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH

NZS 4402: 1986 Test 2.8.1, 2.8.2

**Lab Job No:** 8378-032  
**Client:** Miyamoto International NZ Ltd  
**Location:** 2 Glovers Road  
 HA05 (1.5-1.8m)  
**Date Received:** 8/09/2020  
**Report No:** C20-450  
**REF:** -  
**Sampling Method:** Sampled by client - SNA  
**Date Sampled:** 4/09/2020  
**Test Details:** Wet sieving method  
**History:** Natural  
**Description of Sample:** Silty SAND, brownish grey, wet, no plasticity

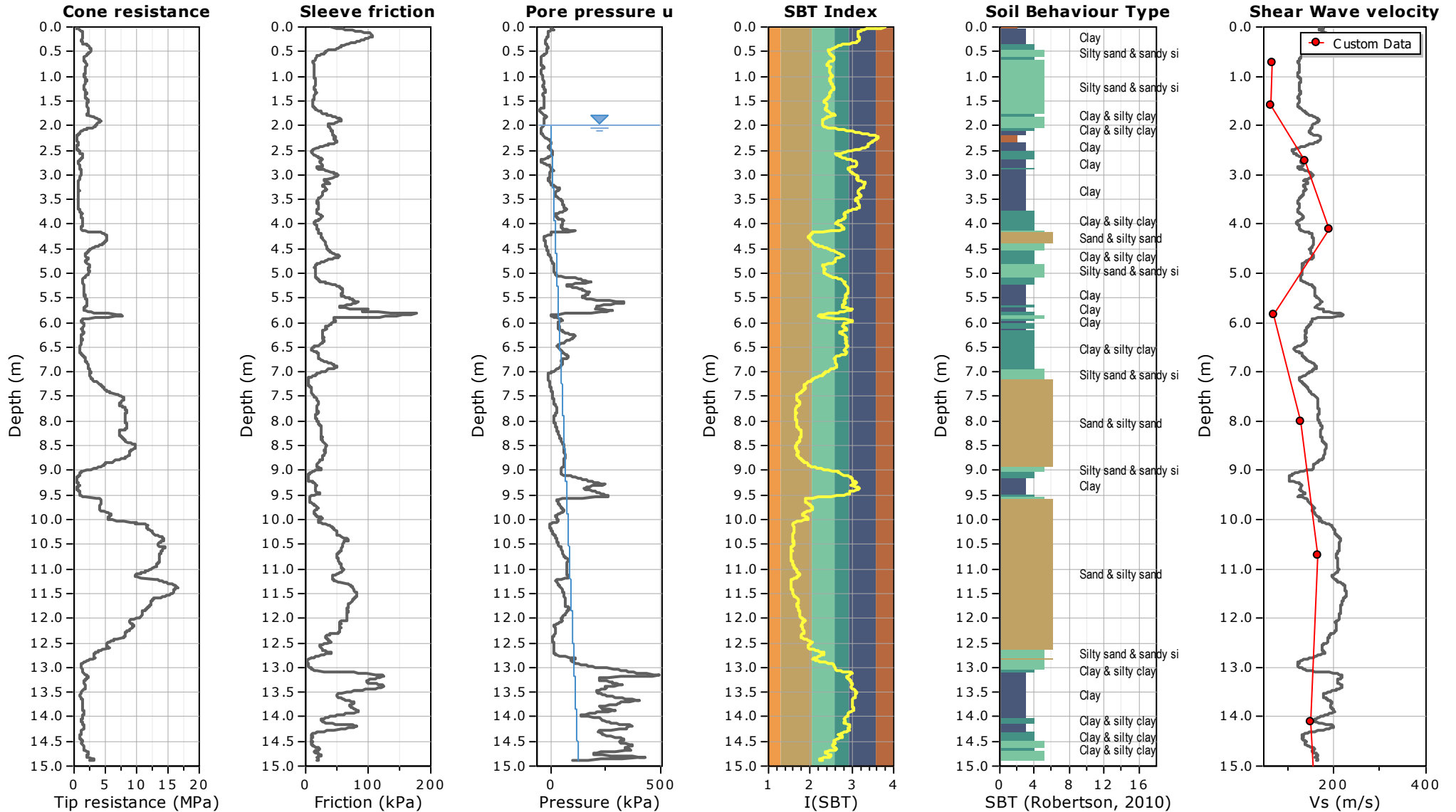
**Sample No:** C20-323  
**Tested By:** D.P  
**Date:** 9/09/2020  
**Checked By:** J.B  
**Date:** 14/09/2020  
**Page:** 8 of 8  
**Sampled By:** Client

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	99
0.150	-	-	77
0.063	-	-	42

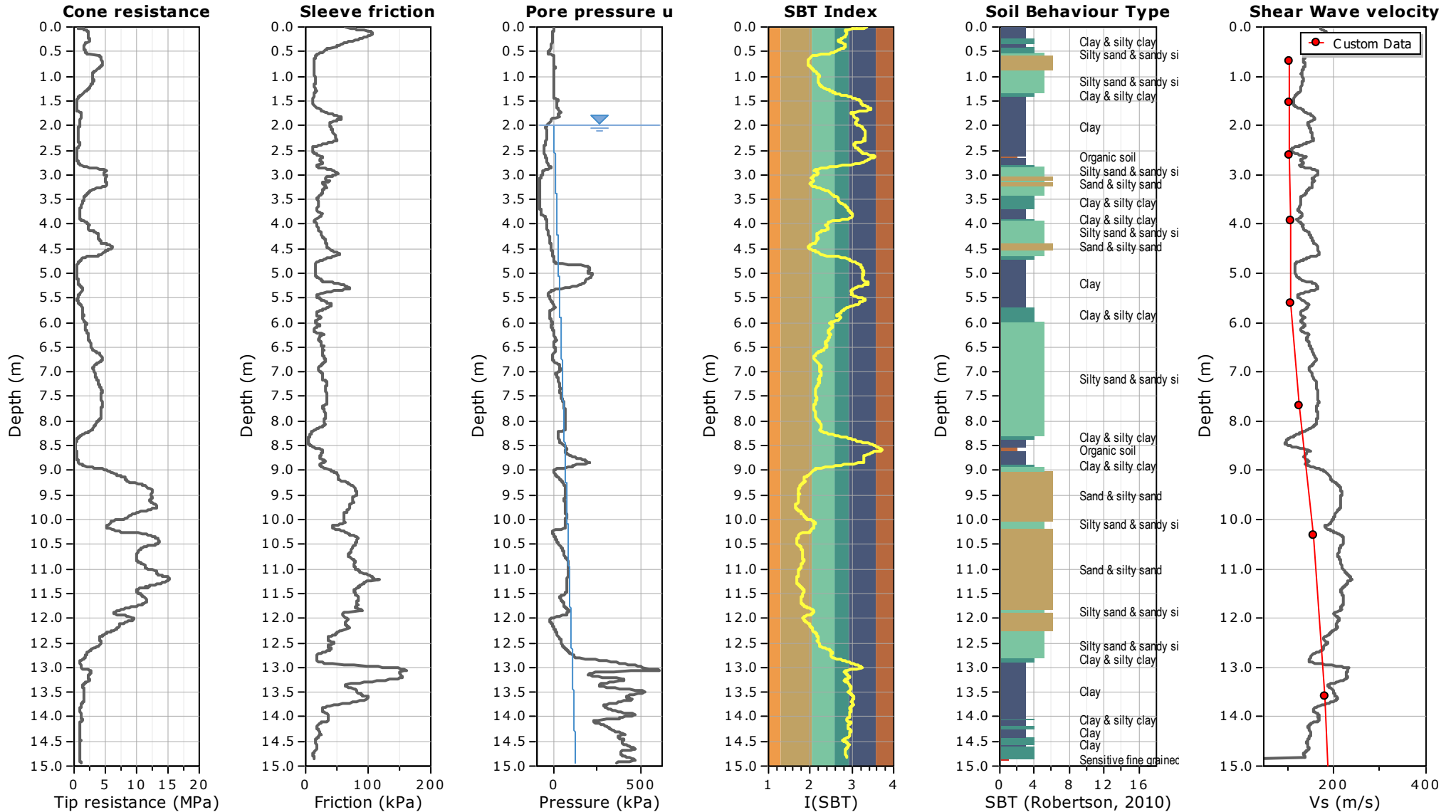


\*The percentage passing the finest sieve was obtained by difference.

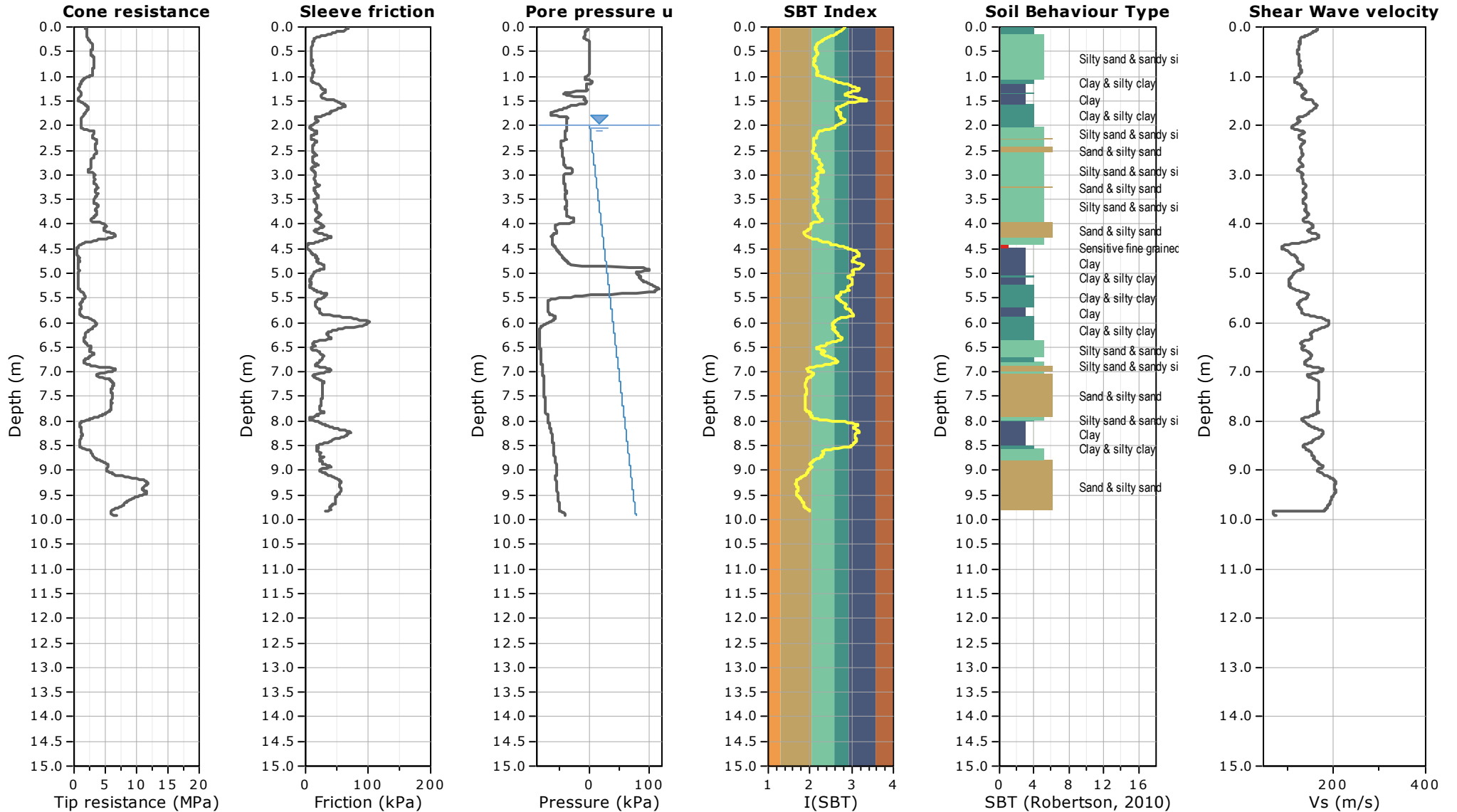
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



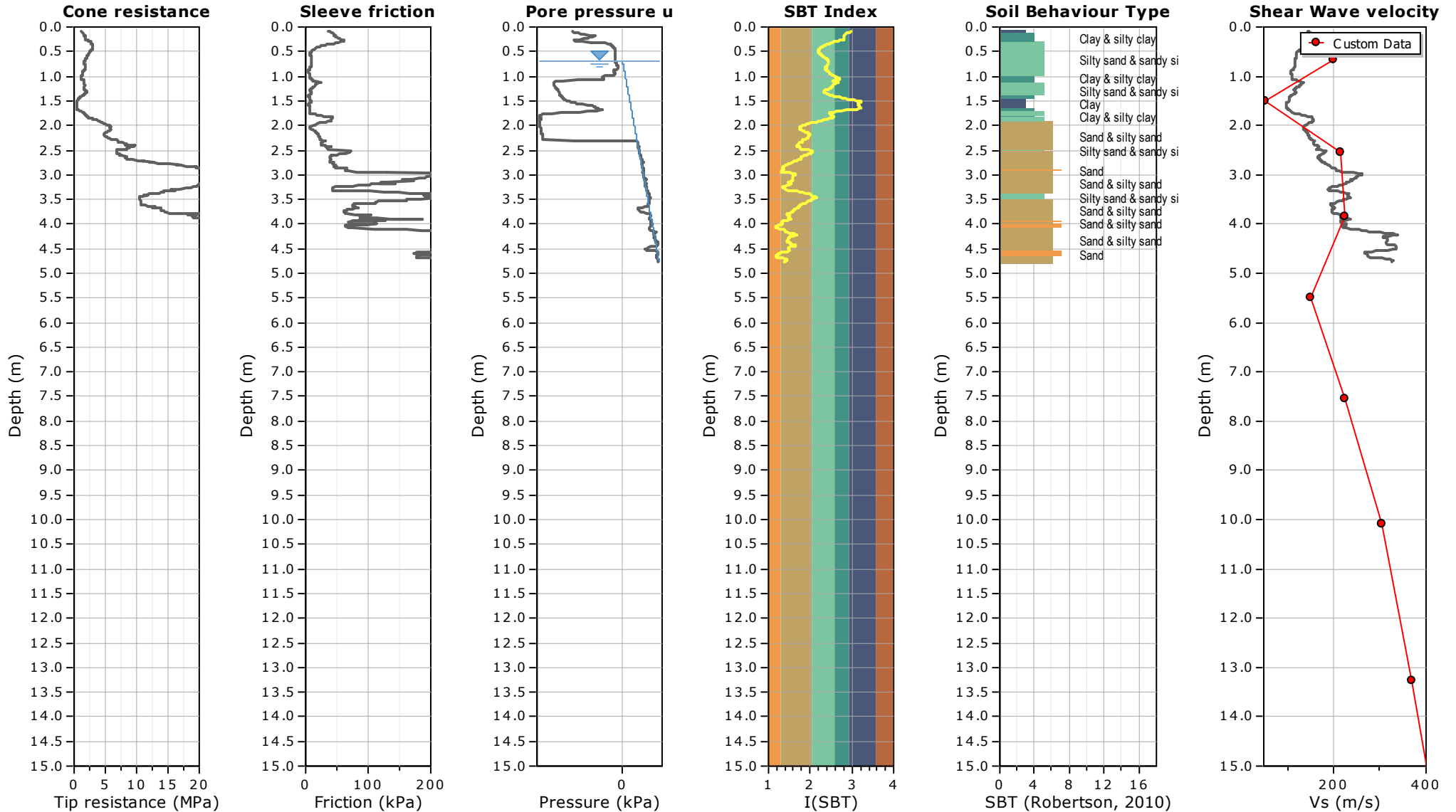
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



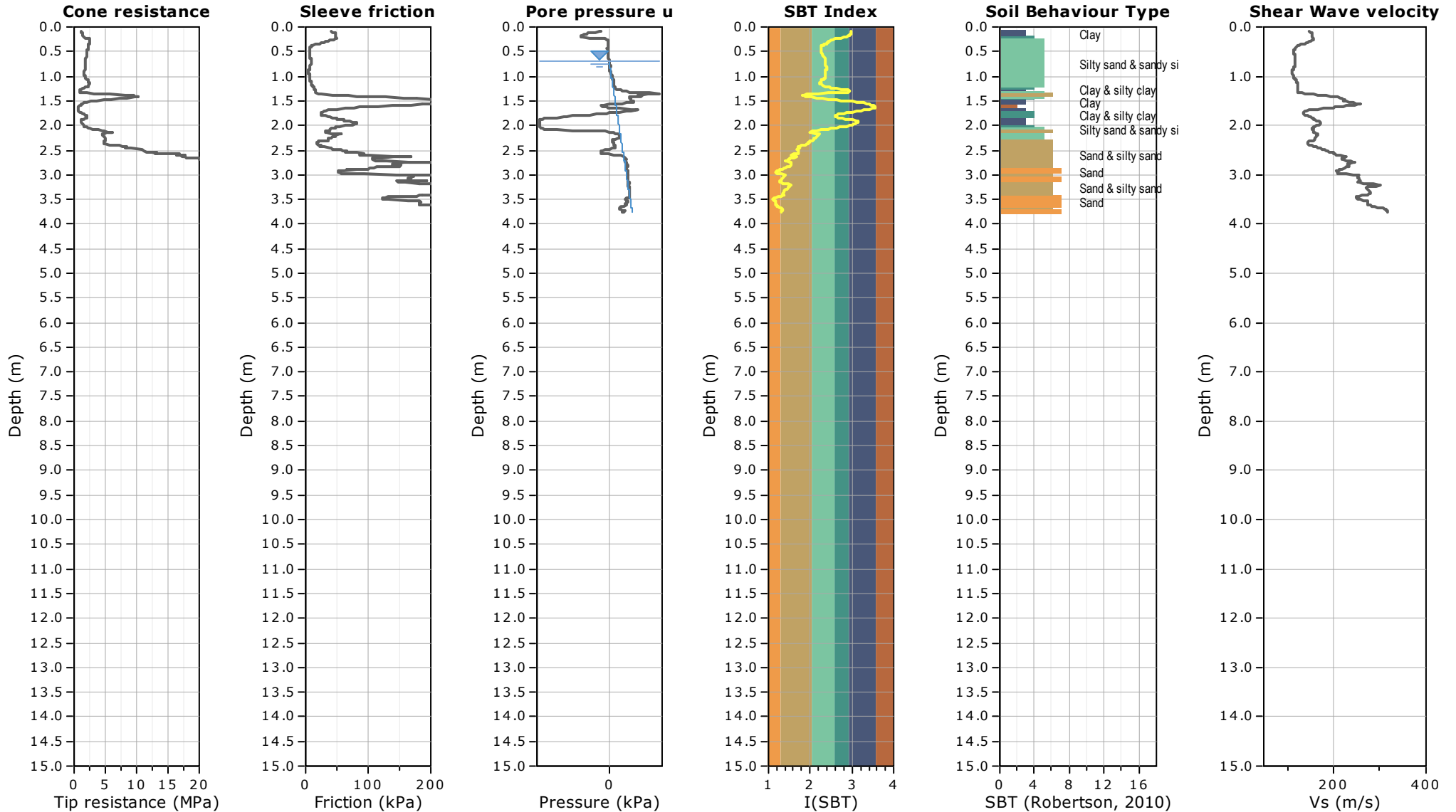
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch

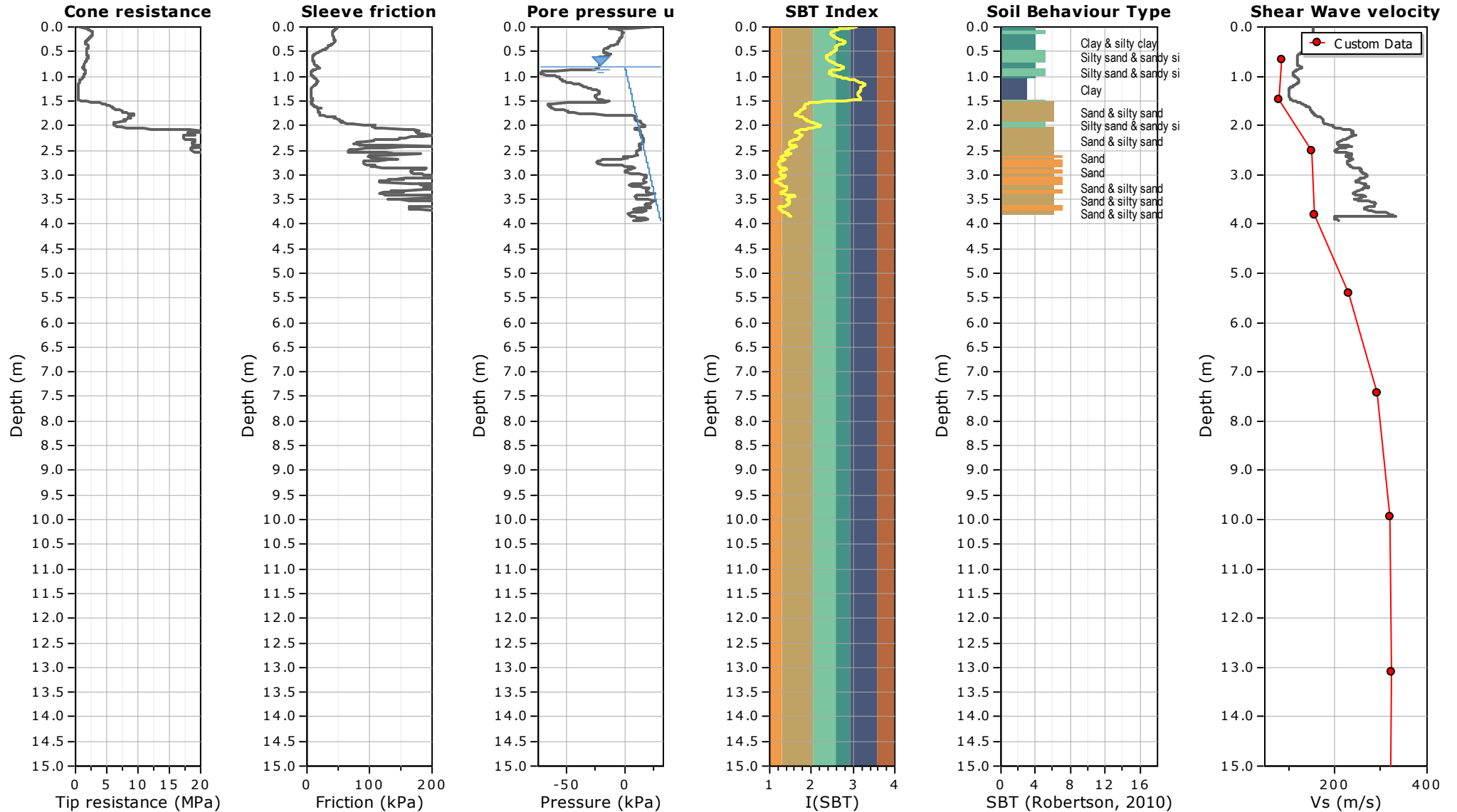


Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch

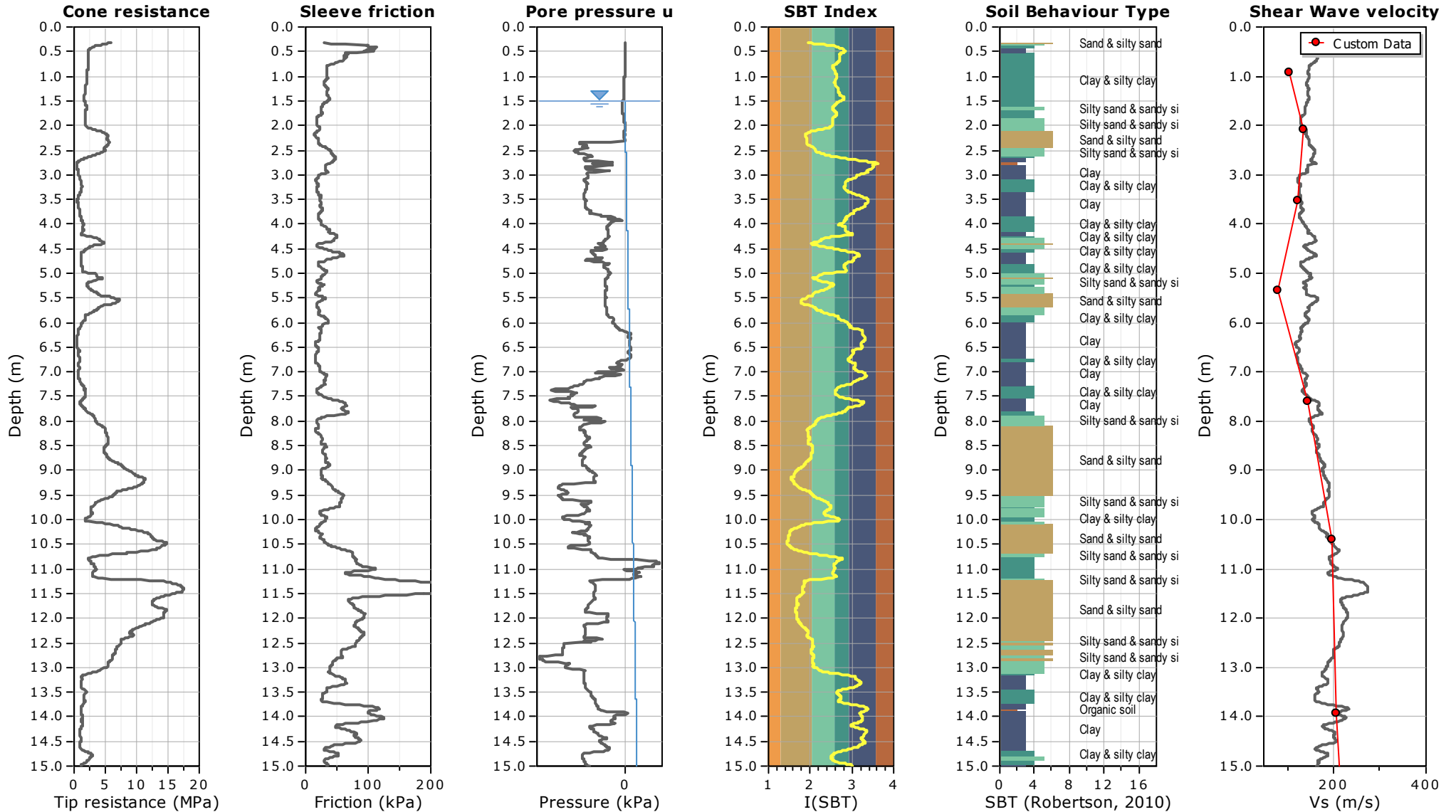




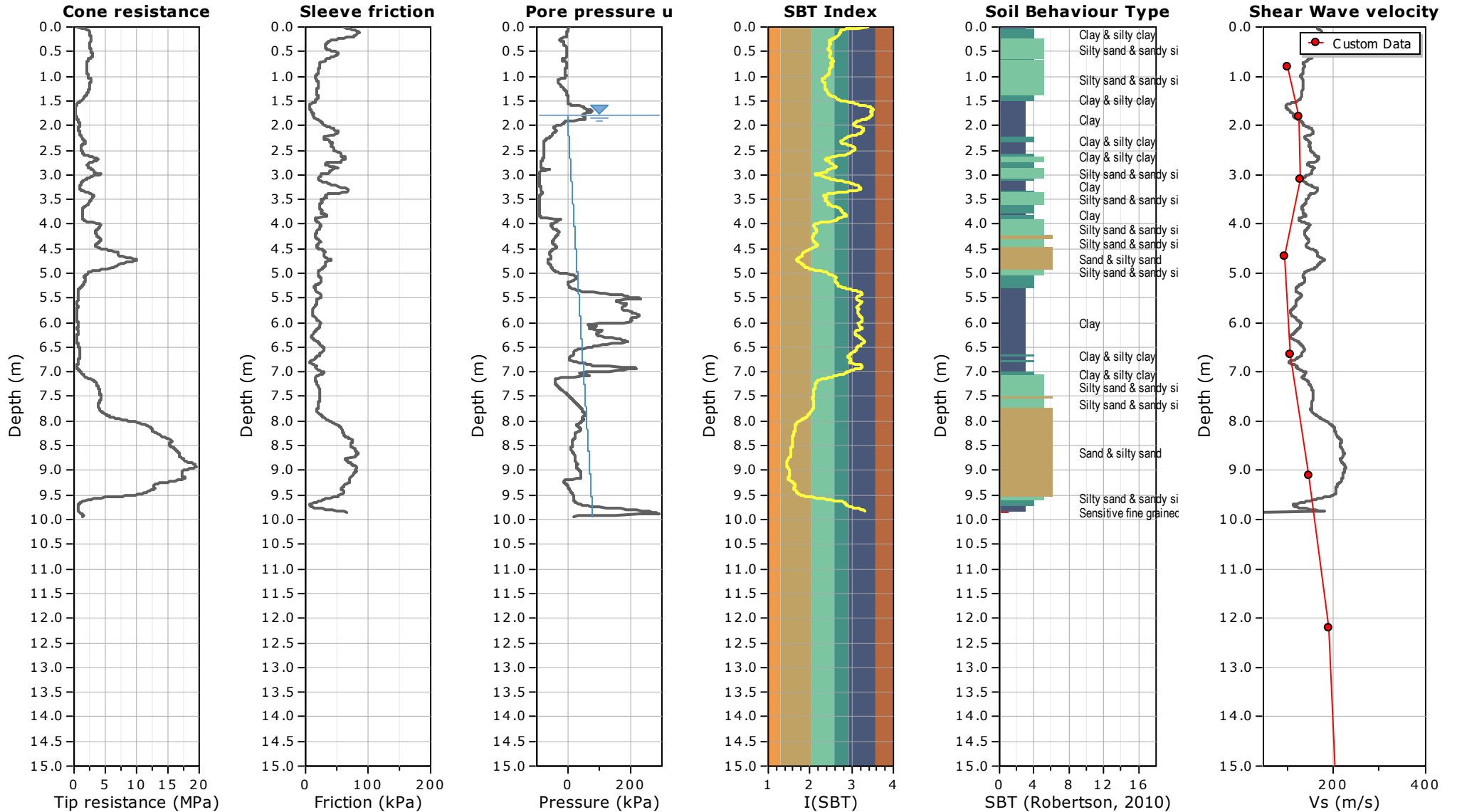
**Project: MINZ200357 - Geotechnical Investigation and Assessment**  
**Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch**



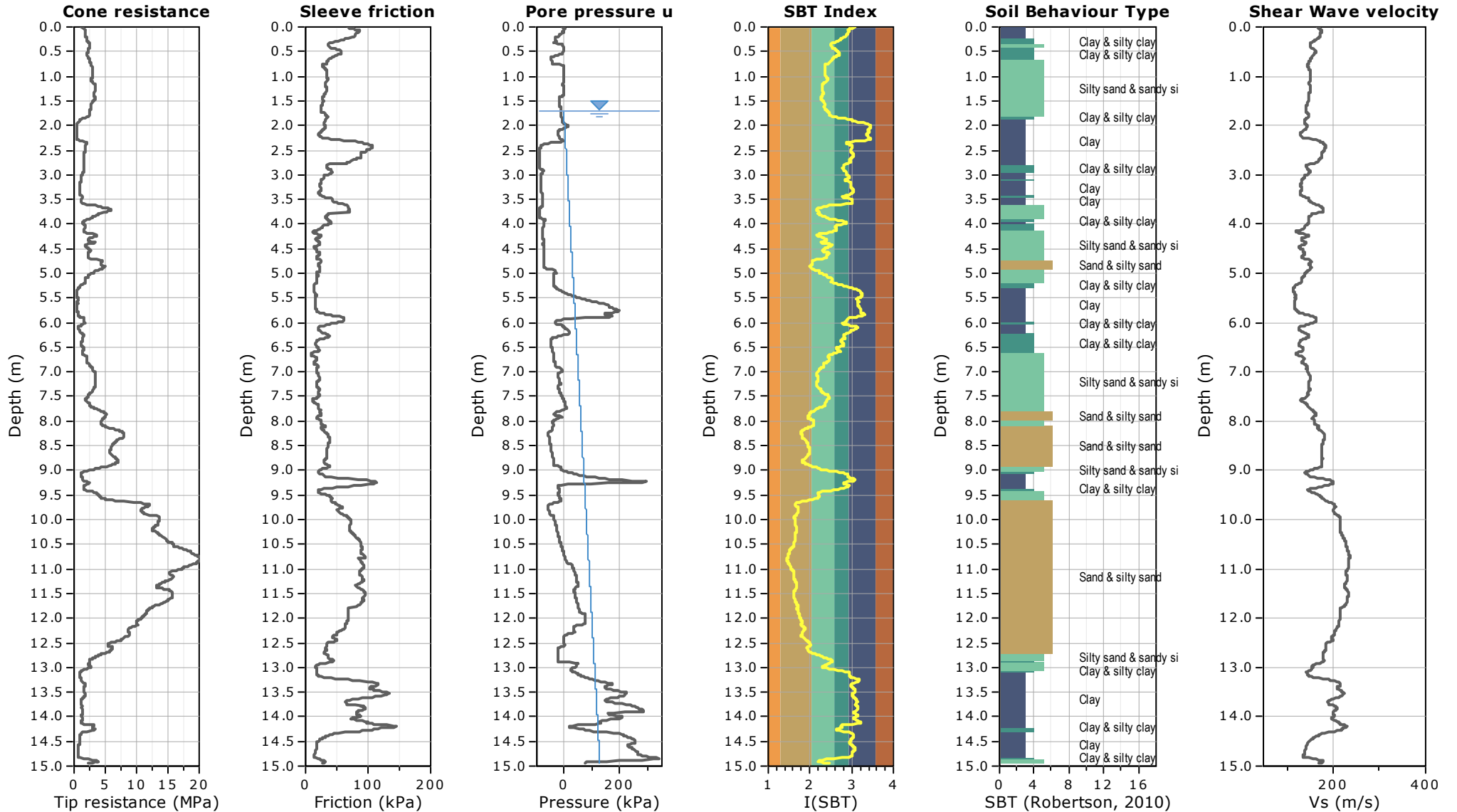
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



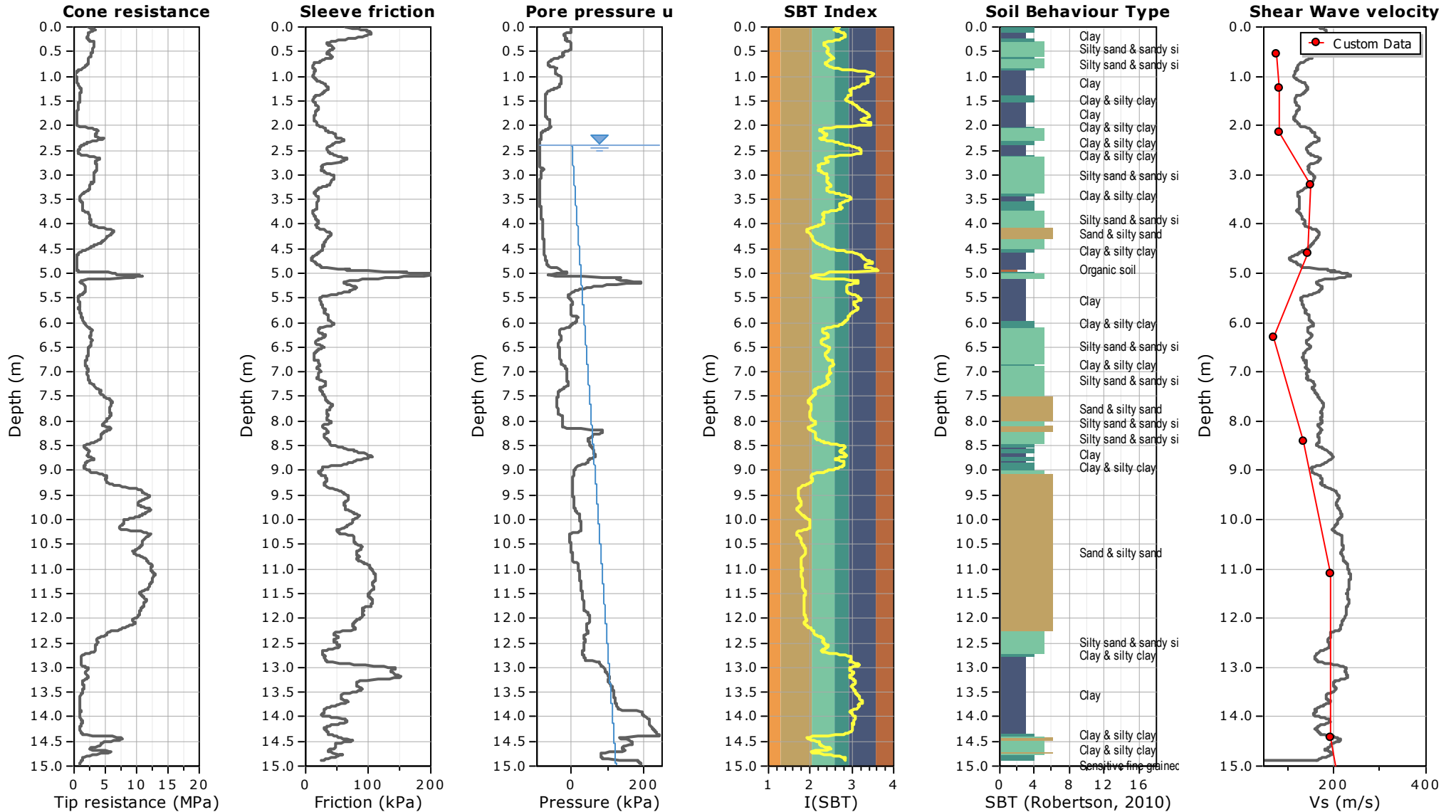
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



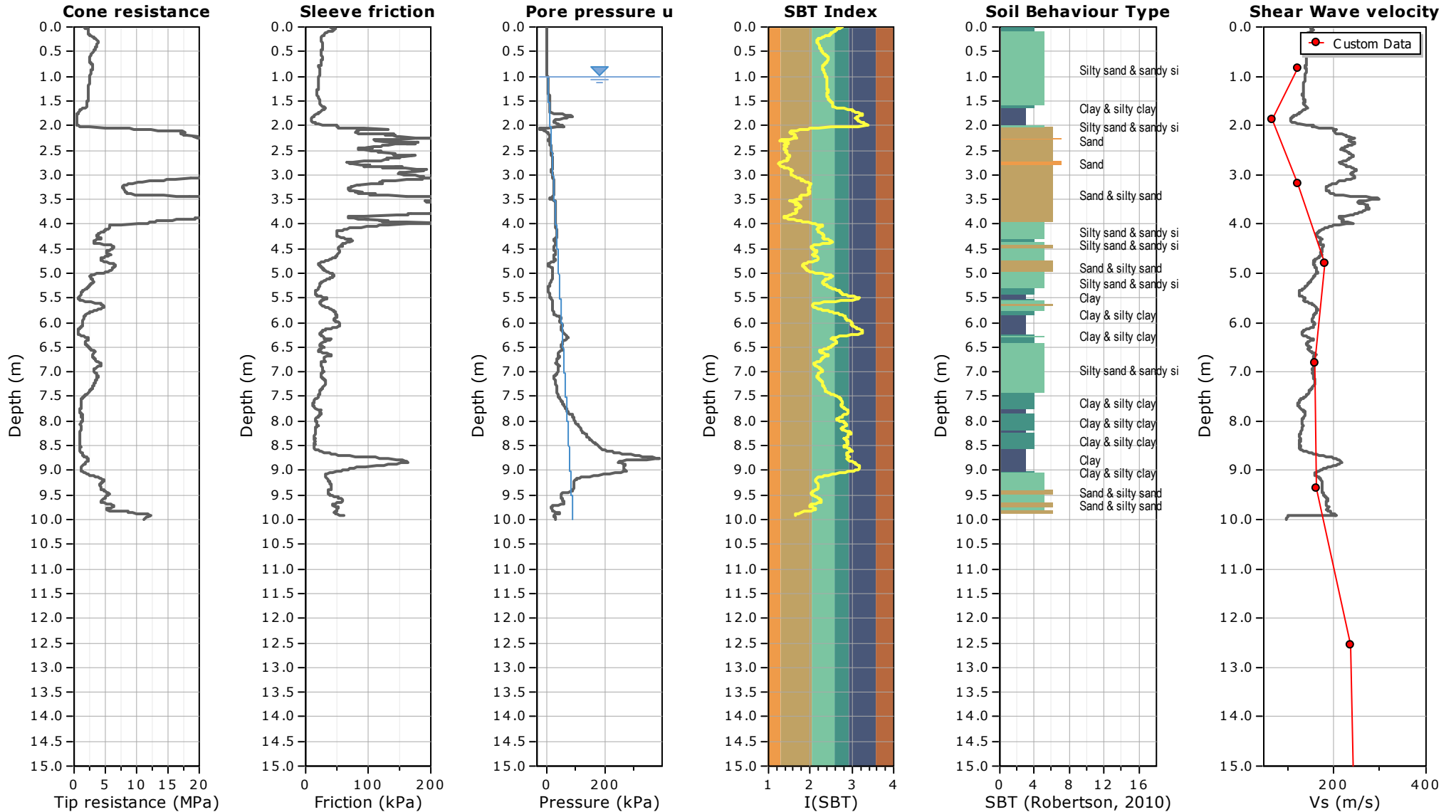
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



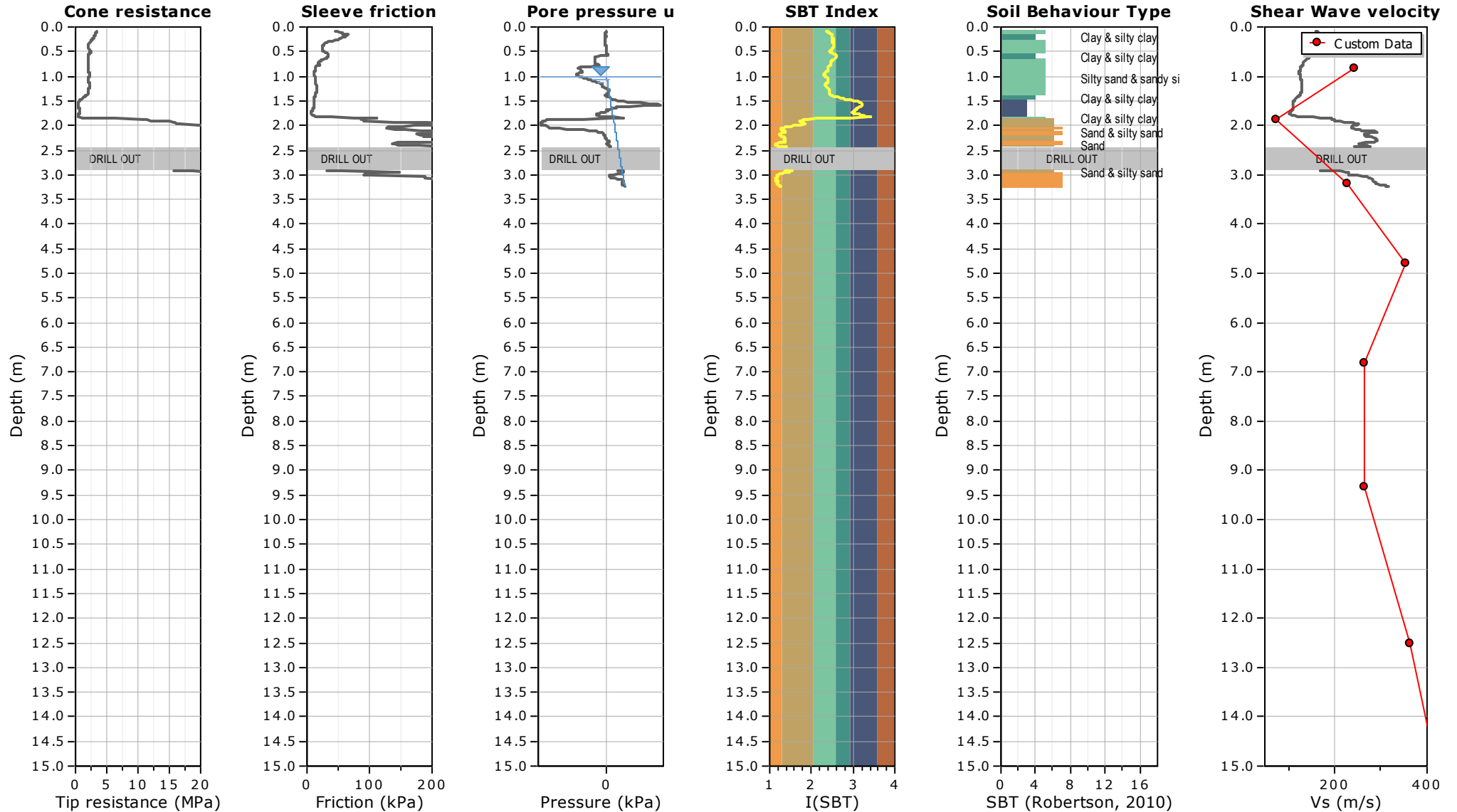
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



# **CONE PENETRATION TEST (CPT) REPORT**



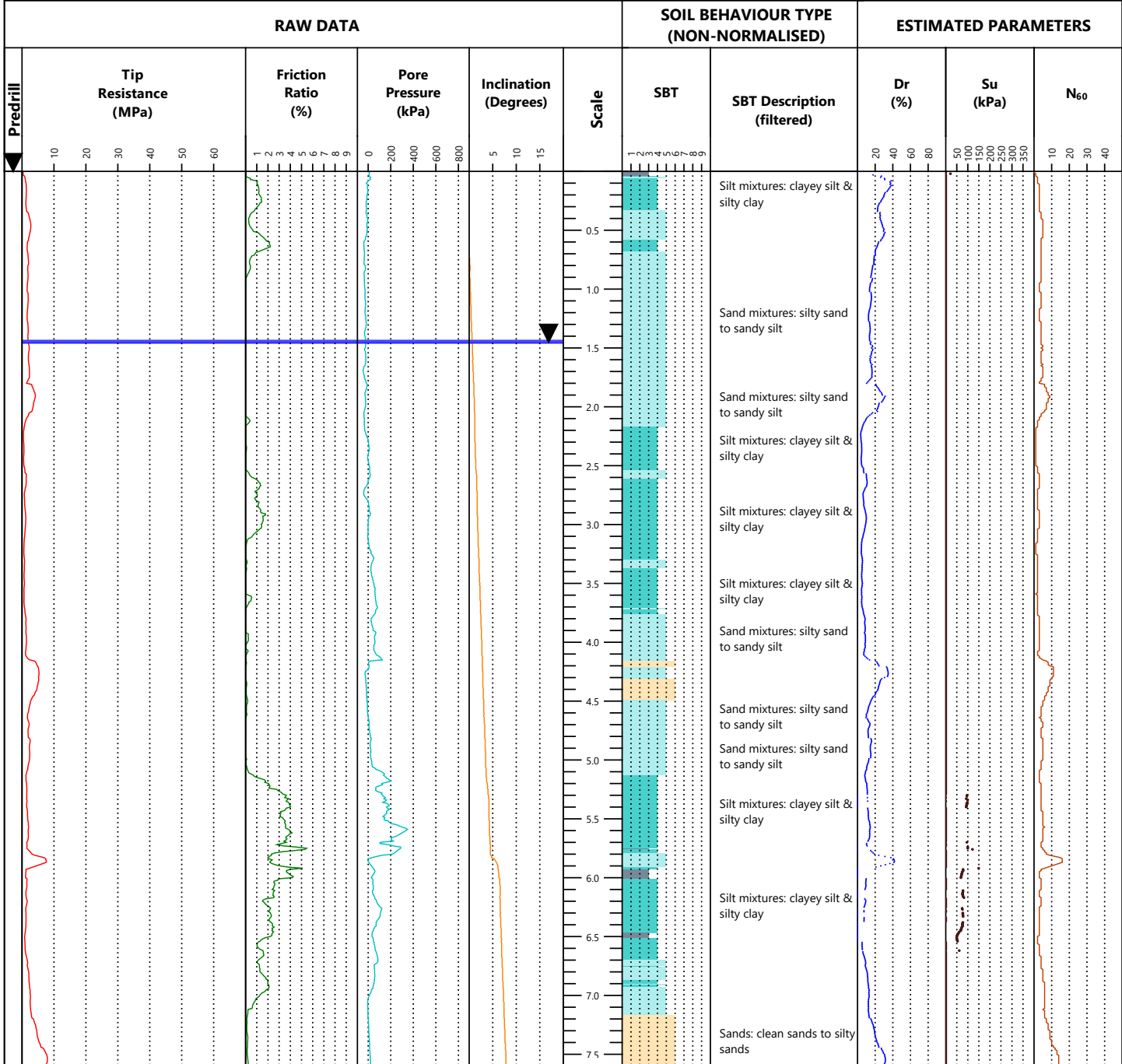
**Client: Miyamoto International NZ**

**Location: 2 Glovers Road, Christchurch**

**Printed: 20/08/2020**



**Site Location:** 2 Glovers Road, Christchurch **Date:** 18/8/2020  
**Grid Reference:** 1564920.46m E, 5173116.23m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150

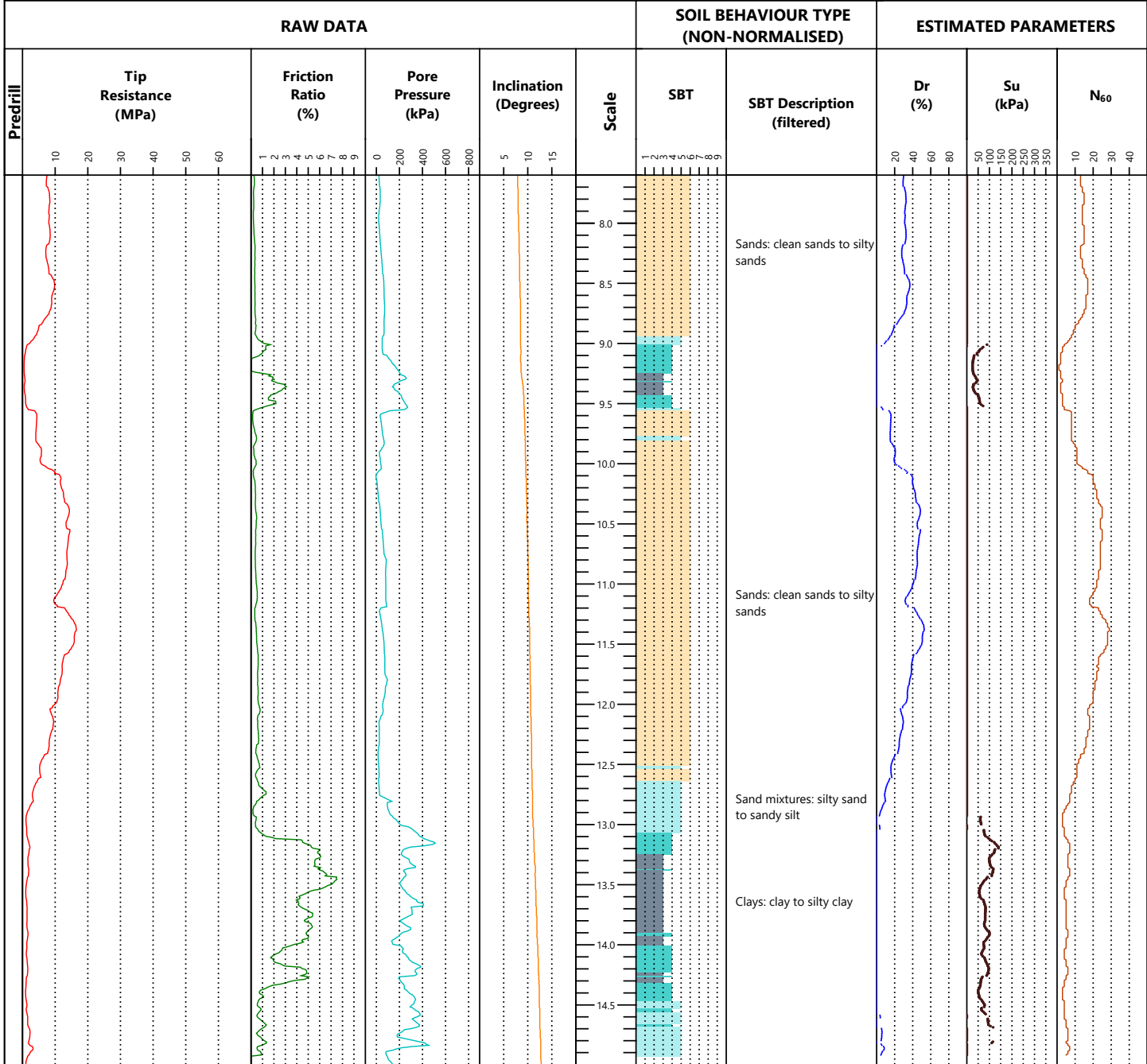


<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKS711	<b>Water Level:</b> 1.45m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 1.60m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	20.4528	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.2535		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	3.0597		<b>6</b> Sands: clean sands to silty sands
			<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

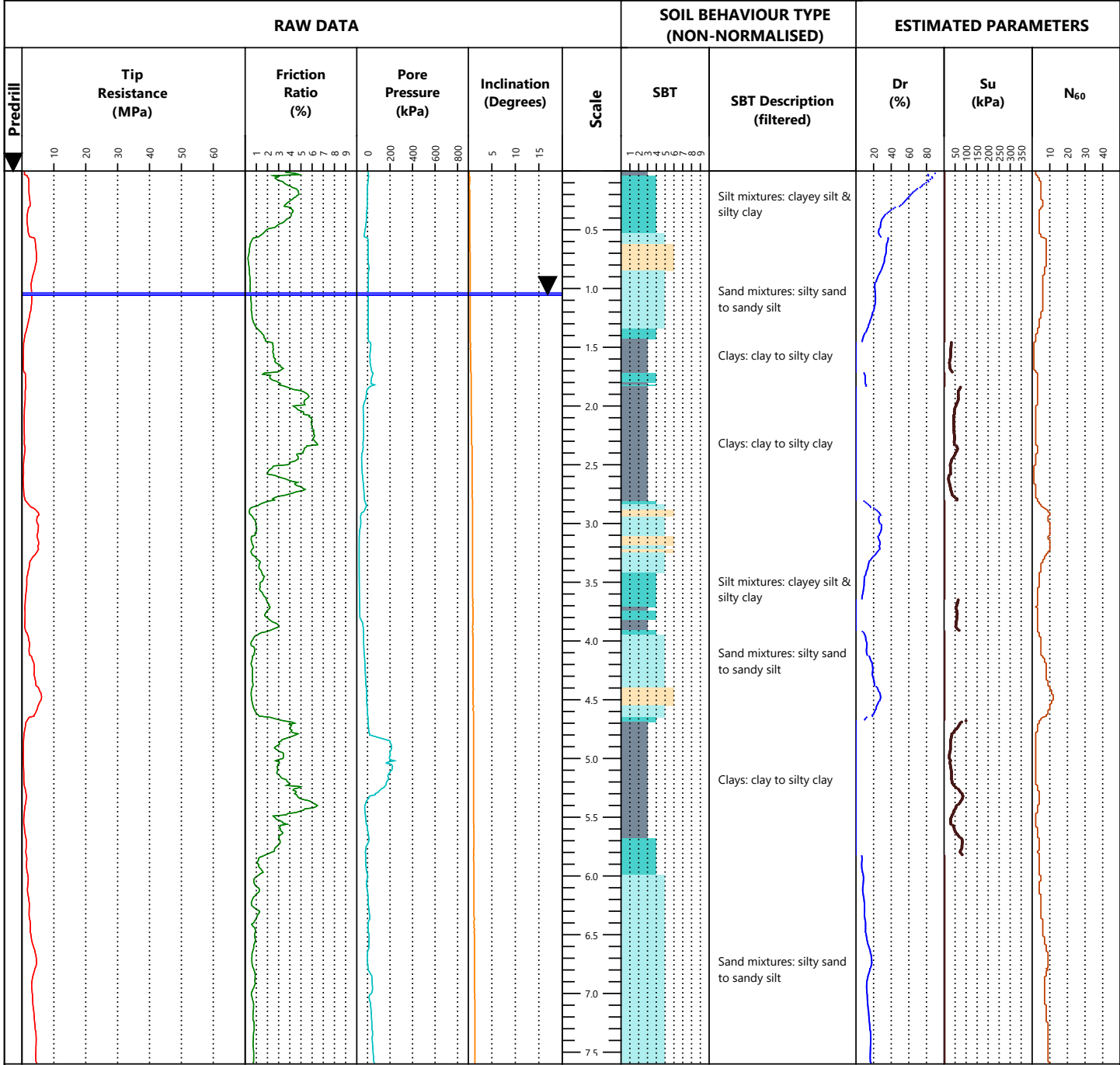
**Site Location:** 2 Glovers Road, Christchurch **Date:** 18/8/2020  
**Grid Reference:** 1564920.46m E, 5173116.23m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKS711 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012  <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>Zero load outputs (MPa)</th> <th>Before test</th> <th>After test</th> </tr> <tr> <td><b>Tip Resistance</b></td> <td>20.4528</td> <td>20.369</td> </tr> <tr> <td><b>Local Friction</b></td> <td>0.2535</td> <td>0.2535</td> </tr> <tr> <td><b>Pore Pressure</b></td> <td>3.0597</td> <td>3.0579</td> </tr> </table>	Zero load outputs (MPa)	Before test	After test	<b>Tip Resistance</b>	20.4528	20.369	<b>Local Friction</b>	0.2535	0.2535	<b>Pore Pressure</b>	3.0597	3.0579	<b>Predrill:</b> - <b>Water Level:</b> 1.45m <b>Collapse:</b> 1.60m  <b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>  <b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td style="background-color: black; color: white;">0</td> <td>Undefined</td> <td style="background-color: #90EE90;">5</td> <td>Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td style="background-color: #FF0000;">1</td> <td>Sensitive fine-grained</td> <td style="background-color: #FFD700;">6</td> <td>Sands: clean sands to silty sands</td> </tr> <tr> <td style="background-color: #FF8C00;">2</td> <td>Clay - organic soil</td> <td style="background-color: #8B4513;">7</td> <td>Dense sand to gravelly sand</td> </tr> <tr> <td style="background-color: #4682B4;">3</td> <td>Clays: clay to silty clay</td> <td style="background-color: #808080;">8</td> <td>Stiff sand to clayey sand</td> </tr> <tr> <td style="background-color: #00CED1;">4</td> <td>Silt mixtures: clayey silt &amp; silty clay</td> <td style="background-color: #404040;">9</td> <td>Stiff fine-grained</td> </tr> </table>	0	Undefined	5	Sand mixtures: silty sand to sandy silt	1	Sensitive fine-grained	6	Sands: clean sands to silty sands	2	Clay - organic soil	7	Dense sand to gravelly sand	3	Clays: clay to silty clay	8	Stiff sand to clayey sand	4	Silt mixtures: clayey silt & silty clay	9	Stiff fine-grained
Zero load outputs (MPa)	Before test	After test																																
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<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>   <div style="text-align: right;">Sheet 2 of 2</div>
--	--

**Site Location:** 2 Glovers Road, Christchurch **Date:** 17/8/2020  
**Grid Reference:** 1564969.32m E, 5173033.19m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150

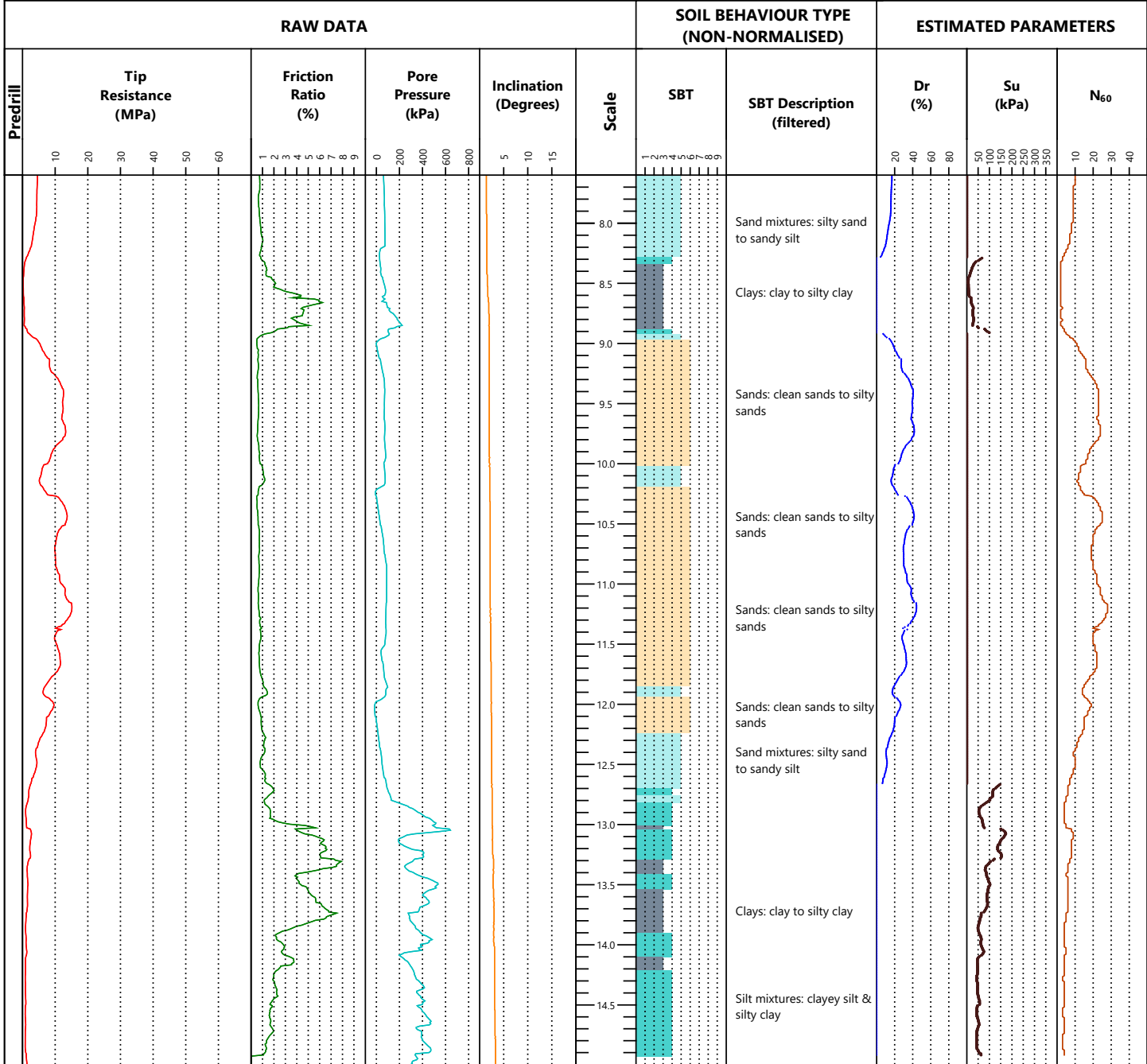


<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKS711	<b>Water Level:</b> 1.05m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 2.45m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	20.4004	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.2537		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	3.0612		<b>6</b> Sands: clean sands to silty sands
	3.0605		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

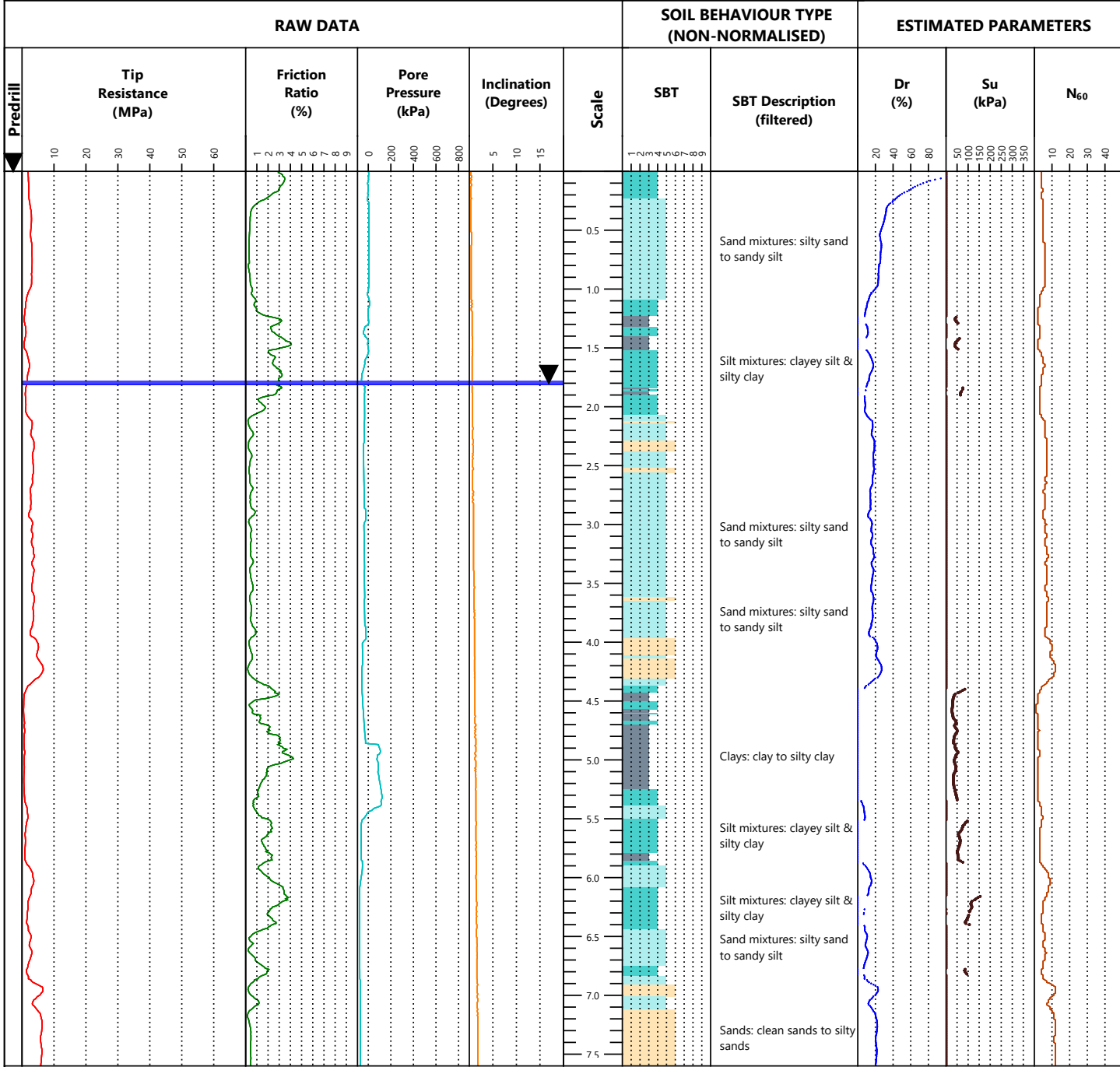
**Site Location:** 2 Glovers Road, Christchurch **Date:** 17/8/2020  
**Grid Reference:** 1564969.32m E, 5173033.19m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKS711 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012  <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th style="text-align: left;">Zero load outputs (MPa)</th> <th style="text-align: left;">Before test</th> <th style="text-align: left;">After test</th> </tr> <tr> <td><b>Tip Resistance</b></td> <td>20.4004</td> <td>20.348</td> </tr> <tr> <td><b>Local Friction</b></td> <td>0.2537</td> <td>0.2536</td> </tr> <tr> <td><b>Pore Pressure</b></td> <td>3.0612</td> <td>3.0605</td> </tr> </table>	Zero load outputs (MPa)	Before test	After test	<b>Tip Resistance</b>	20.4004	20.348	<b>Local Friction</b>	0.2537	0.2536	<b>Pore Pressure</b>	3.0612	3.0605	<b>Predrill:</b> - <b>Water Level:</b> 1.05m <b>Collapse:</b> 2.45m  <b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>  <b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td style="width:30%;">0 Undefined</td> <td style="width:30%;">5 Sand mixtures: silty sand to sandy silt</td> <td style="width:30%;">8 Stiff sand to clayey sand</td> </tr> <tr> <td>1 Sensitive fine-grained</td> <td>6 Sands: clean sands to silty sands</td> <td>9 Stiff fine-grained</td> </tr> <tr> <td>2 Clay - organic soil</td> <td>7 Dense sand to gravelly sand</td> <td></td> </tr> <tr> <td>3 Clays: clay to silty clay</td> <td></td> <td></td> </tr> <tr> <td>4 Silt mixtures: clayey silt &amp; silty clay</td> <td></td> <td></td> </tr> </table>	0 Undefined	5 Sand mixtures: silty sand to sandy silt	8 Stiff sand to clayey sand	1 Sensitive fine-grained	6 Sands: clean sands to silty sands	9 Stiff fine-grained	2 Clay - organic soil	7 Dense sand to gravelly sand		3 Clays: clay to silty clay			4 Silt mixtures: clayey silt & silty clay		
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<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>   <div style="text-align: right;">Sheet 2 of 2</div>
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**Site Location:** 2 Glovers Road, Christchurch **Date:** 13/8/2020  
**Grid Reference:** 1564902m E, 5172941.77m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ328 <b>Cone Area Ratio:</b> 0.80 <b>Standards:</b> ISO 22476-1:2012		<b>Predrill:</b> - <b>Water Level:</b> 1.8m <b>Collapse:</b> 2.70m		<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>		<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>		
<b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>		<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>		<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>		<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>		
<b>Zero load outputs (MPa)</b> <b>Tip Resistance</b> <b>Local Friction</b> <b>Pore Pressure</b>	<b>Before test</b> 11.3554 0.1187 0.9596	<b>After test</b> 11.3094 0.1186 0.9557	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>		<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>		<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>	

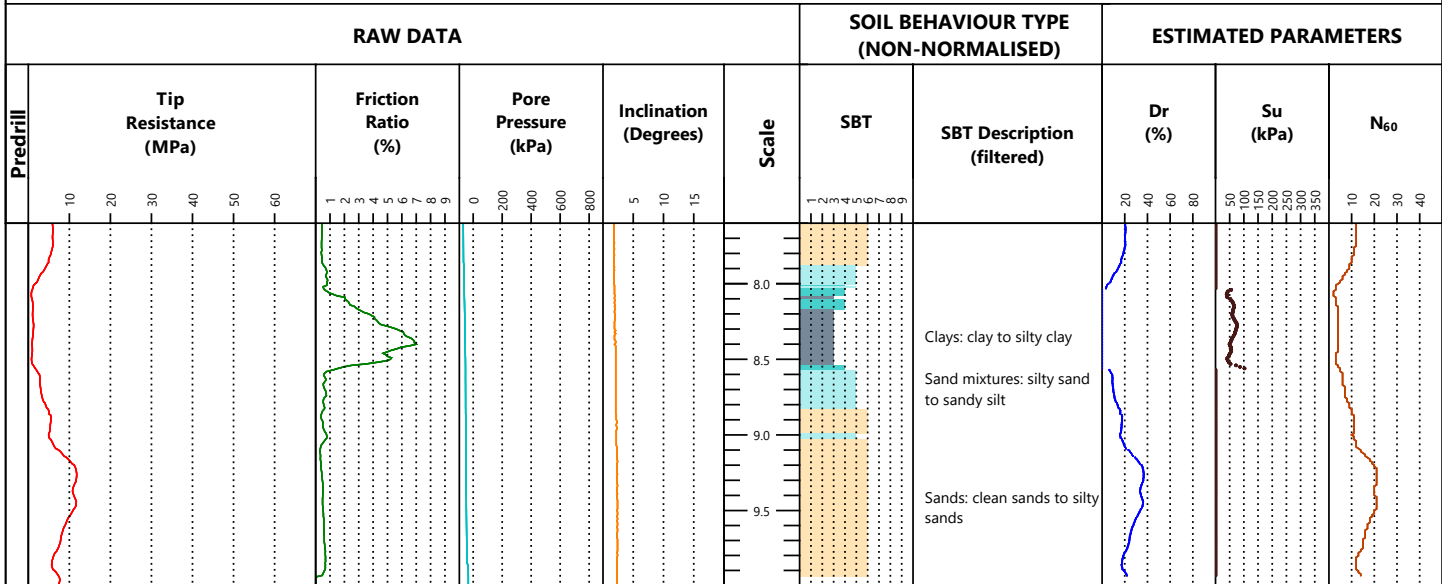
**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

Sheet 1 of 2

<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu003</b>
<b>Project:</b>	2 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

<b>Site Location:</b> 2 Glovers Road, Christchurch	<b>Date:</b> 13/8/2020
<b>Grid Reference:</b> 1564902m E, 5172941.77m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> B. Wilson
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150

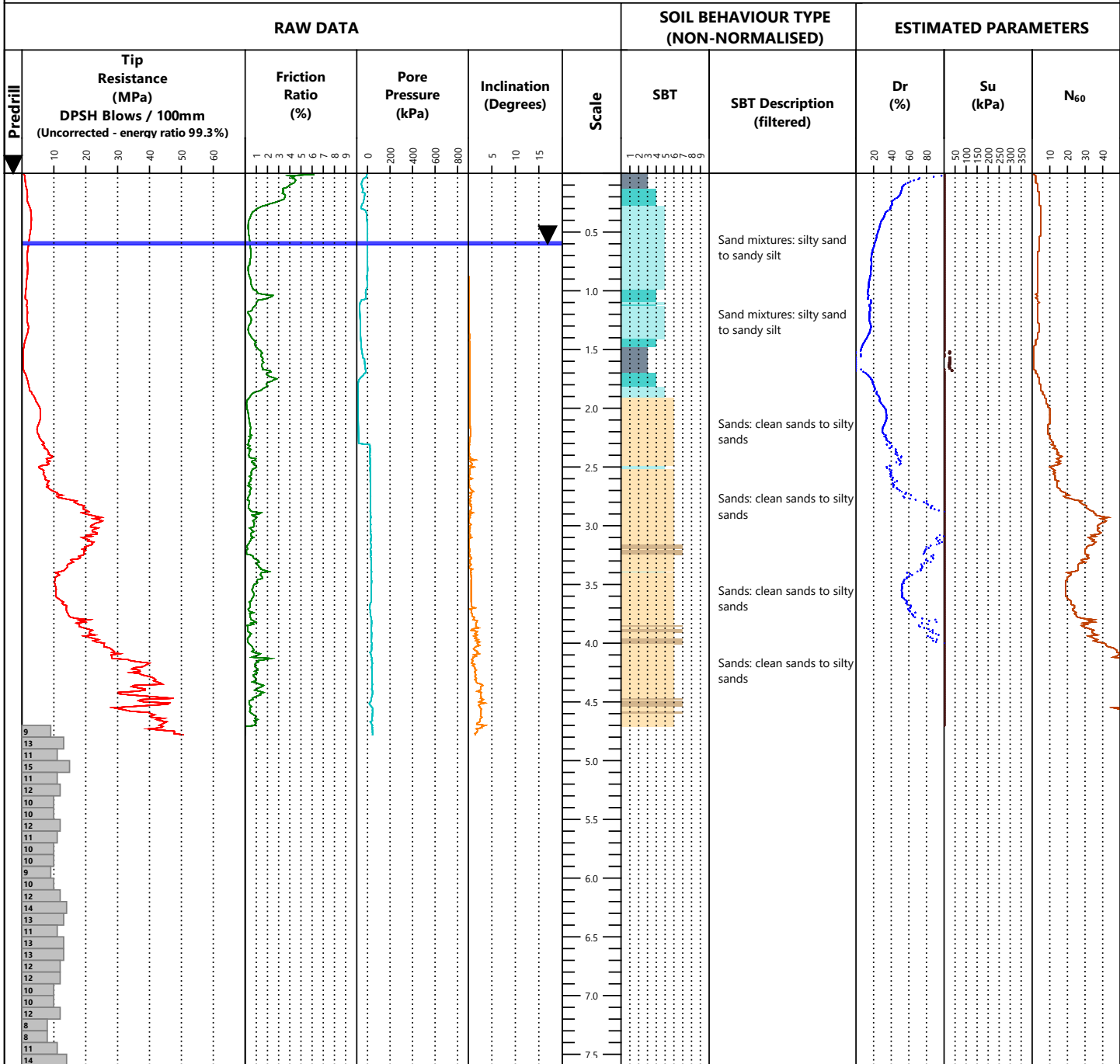


EOH: 10m

<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ328 <b>Cone Area Ratio:</b> 0.80 <b>Standards:</b> ISO 22476-1:2012	<b>Predrill:</b> - <b>Water Level:</b> 1.8m <b>Collapse:</b> 2.70m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="0"> <tr> <td>0 Undefined</td> <td>5 Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td>1 Sensitive fine-grained</td> <td>6 Sands: clean sands to silty sands</td> </tr> <tr> <td>2 Clay - organic soil</td> <td>7 Dense sand to gravelly sand</td> </tr> <tr> <td>3 Clays: clay to silty clay</td> <td>8 Stiff sand to clayey sand</td> </tr> <tr> <td>4 Silt mixtures: clayey silt &amp; silty clay</td> <td>9 Stiff fine-grained</td> </tr> </table>	0 Undefined	5 Sand mixtures: silty sand to sandy silt	1 Sensitive fine-grained	6 Sands: clean sands to silty sands	2 Clay - organic soil	7 Dense sand to gravelly sand	3 Clays: clay to silty clay	8 Stiff sand to clayey sand	4 Silt mixtures: clayey silt & silty clay	9 Stiff fine-grained
0 Undefined	5 Sand mixtures: silty sand to sandy silt												
1 Sensitive fine-grained	6 Sands: clean sands to silty sands												
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4 Silt mixtures: clayey silt & silty clay	9 Stiff fine-grained												
<b>Zero load outputs (MPa)</b> <b>Tip Resistance</b> 11.3554    11.3094 <b>Local Friction</b> 0.1187    0.1186 <b>Pore Pressure</b> 0.9596    0.9557	<b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>												

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>  Sheet 2 of 2
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**Site Location:** 2 Glovers Road, Christchurch **Date:** 19/8/2020  
**Grid Reference:** 1564993.47m E, 5172892.27m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.6m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.95m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3452	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1186		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9595		<b>6</b> Sands: clean sands to silty sands
			<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu004</b>
<b>Project:</b>	2 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

**Site Location:** 2 Glovers Road, Christchurch **Date:** 19/8/2020  
**Grid Reference:** 1564993.47m E, 5172892.27m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150

Predrill	RAW DATA				SOIL BEHAVIOUR TYPE (NON-NORMALISED)		ESTIMATED PARAMETERS			
	Tip Resistance (MPa) DPSH Blows / 100mm (Uncorrected - energy ratio 99.3%)	Friction Ratio (%)	Pore Pressure (kPa)	Inclination (Degrees)	Scale	SBT	SBT Description (filtered)	Dr (%)	Su (kPa)	N <sub>60</sub>
	10 20 30 40 50 60	1 2 3 4 5 6 7 8 9	0 200 400 600 800	5 10 15		0 1 2 3 4 5 6 7 8 9		20 40 60 80	50 100 150 200 250 300 350	10 20 30 40
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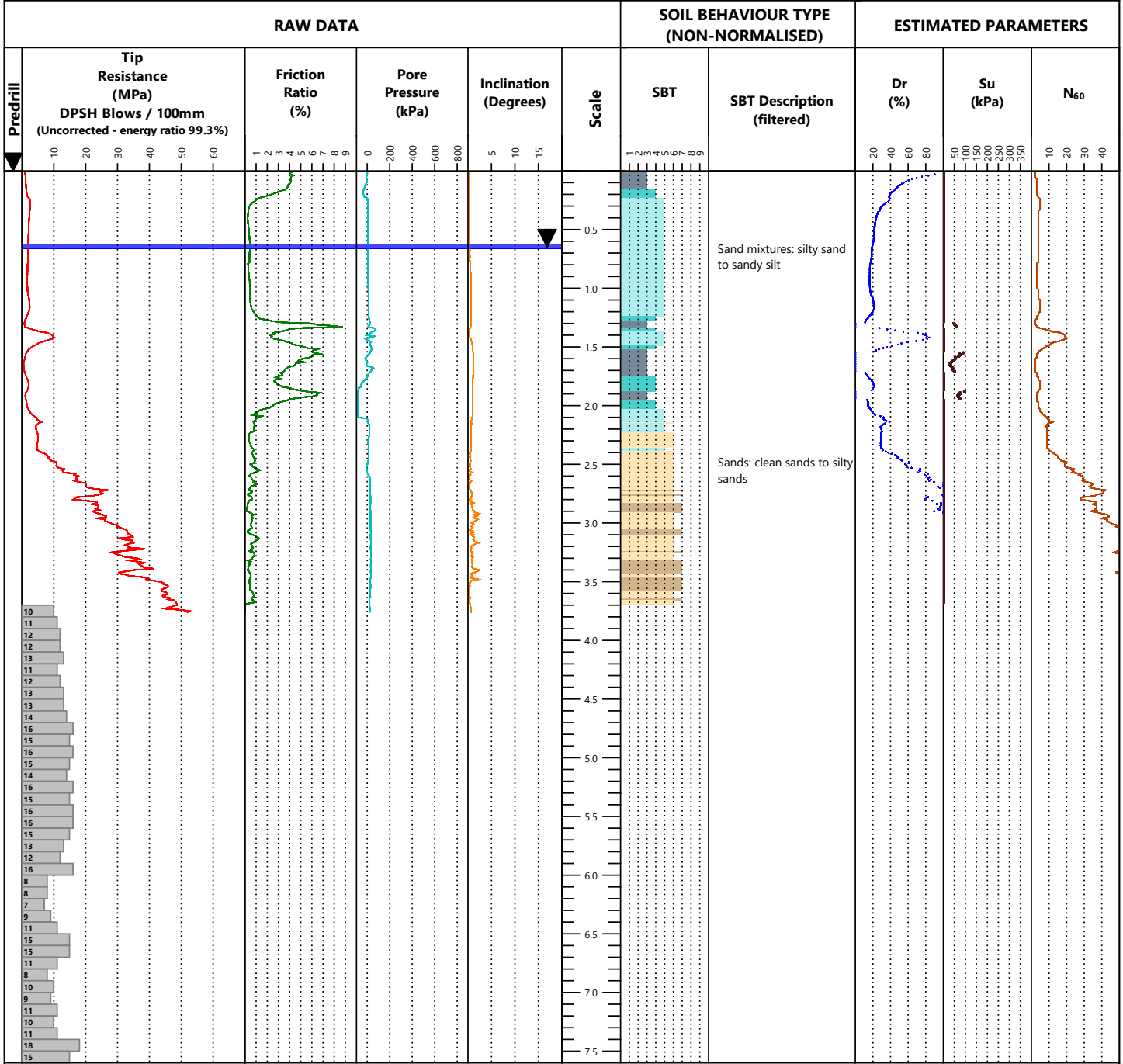
EOH: 15m

<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.6m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.95m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3452	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1186		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9595		<b>6</b> Sands: clean sands to silty sands
	0.9554		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>
	Sheet 2 of 2



**Site Location:** 2 Glovers Road, Christchurch **Date:** 19/8/2020  
**Grid Reference:** 1564945.37m E, 5172828.71m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



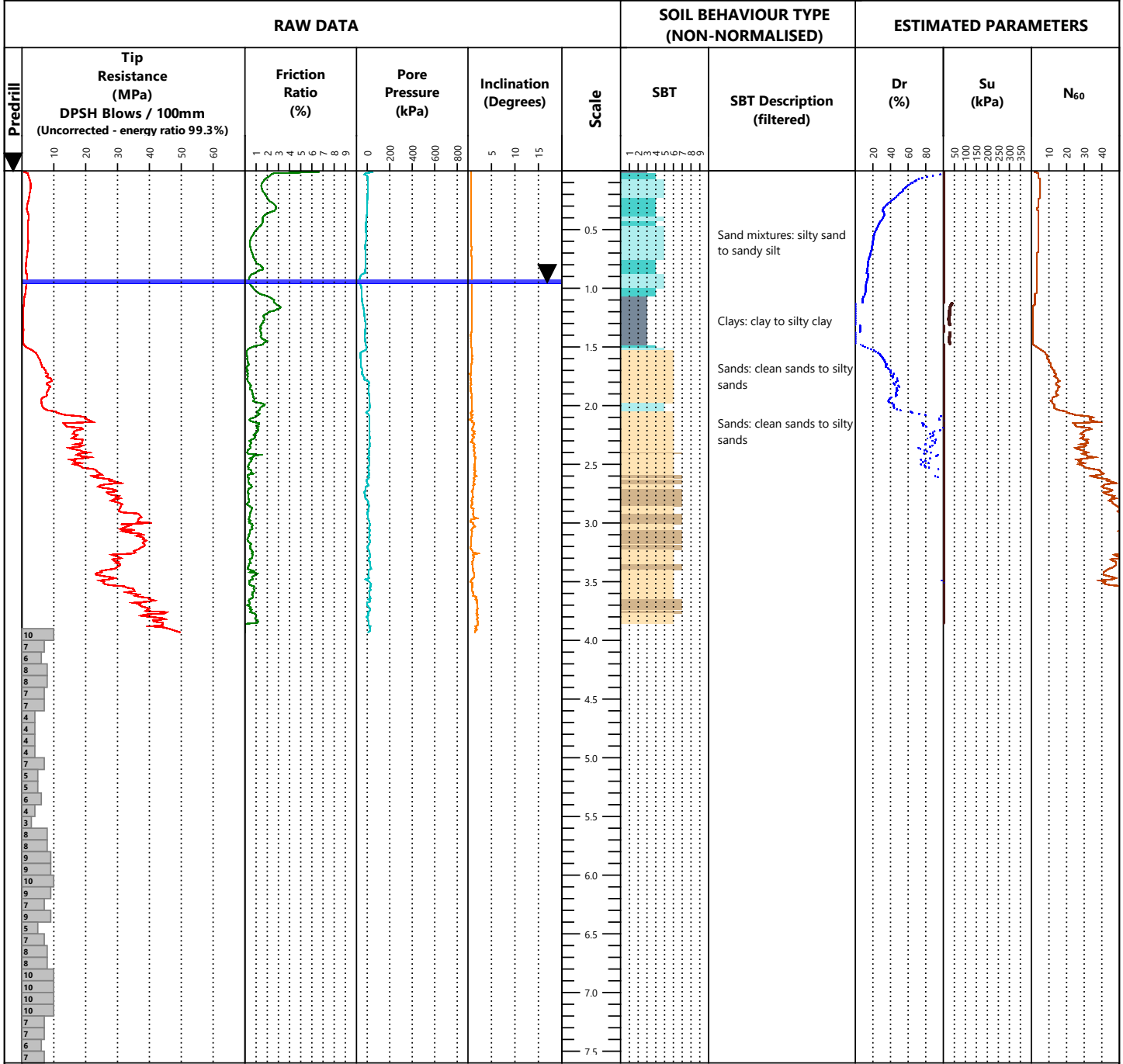
<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.65m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.45m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.4066	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1183		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9587		<b>6</b> Sands: clean sands to silty sands
			<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**



**Site Location:** 2 Glovers Road, Christchurch **Date:** 13/8/2020  
**Grid Reference:** 1565008.77m E, 5172744.63m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.95m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.40m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3708	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1178		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9592		<b>6</b> Sands: clean sands to silty sands
			<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

Sheet 1 of 2



<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu006</b>
<b>Project:</b>	2 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

<b>Site Location:</b> 2 Glovers Road, Christchurch	<b>Date:</b> 13/8/2020
<b>Grid Reference:</b> 1565008.77m E, 5172744.63m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> B. Wilson
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150

RAW DATA					SOIL BEHAVIOUR TYPE (NON-NORMALISED)		ESTIMATED PARAMETERS			
Predrill	Tip Resistance (MPa) DPSH Blows / 100mm (Uncorrected - energy ratio 99.3%)	Friction Ratio (%)	Pore Pressure (kPa)	Inclination (Degrees)	Scale	SBT	SBT Description (filtered)	ESTIMATED PARAMETERS		
								Dr (%)	Su (kPa)	N <sub>60</sub>
5	10	1	0	5	8.0	5		20	50	10
6	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
11	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
11	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
10	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
6	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
10	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
4	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
6	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
12	10	1	0	5	8.0	5		20	50	10
12	10	1	0	5	8.0	5		20	50	10
12	10	1	0	5	8.0	5		20	50	10
10	10	1	0	5	8.0	5		20	50	10
11	10	1	0	5	8.0	5		20	50	10
14	10	1	0	5	8.0	5		20	50	10
13	10	1	0	5	8.0	5		20	50	10
16	10	1	0	5	8.0	5		20	50	10
17	10	1	0	5	8.0	5		20	50	10
14	10	1	0	5	8.0	5		20	50	10
15	10	1	0	5	8.0	5		20	50	10
17	10	1	0	5	8.0	5		20	50	10
16	10	1	0	5	8.0	5		20	50	10
17	10	1	0	5	8.0	5		20	50	10
21	10	1	0	5	8.0	5		20	50	10

EOH: 12.7m

<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.95m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.40m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3708	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1178		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9592		<b>6</b> Sands: clean sands to silty sands
	0.9542		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

<b>Notes &amp; Limitations</b>	<b>Remarks</b>
Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	
	Sheet 2 of 2

## TEST DETAIL

PointID: CPTu001  
Sounding: 1

**Operator:** E. Diaz  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKS711  
**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	20.4528	20.369
<b>Local Friction</b>	0.2535	0.2535
<b>Pore Pressure</b>	3.0597	3.0579

**Date:** 18/8/2020  
**Predrill:** -  
**Water Level:** 1.45m  
**Collapse:** 1.60m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu002  
Sounding: 1

**Operator:** E. Diaz  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKS711  
**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	20.4004	20.348
<b>Local Friction</b>	0.2537	0.2536
<b>Pore Pressure</b>	3.0612	3.0605

**Date:** 17/8/2020  
**Predrill:** -  
**Water Level:** 1.05m  
**Collapse:** 2.45m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu003  
Sounding: 1

**Operator:** B. Wilson  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKJ328  
**Cone Area Ratio:** 0.80

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.3554	11.3094
<b>Local Friction</b>	0.1187	0.1186
<b>Pore Pressure</b>	0.9596	0.9557

**Date:** 13/8/2020  
**Predrill:** -  
**Water Level:** 1.8m  
**Collapse:** 2.70m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu004  
Sounding: 1

**Operator:** B. Wilson  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKJ328  
**Cone Area Ratio:** 0.80

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.3452	11.2685
<b>Local Friction</b>	0.1186	0.1191
<b>Pore Pressure</b>	0.9595	0.9554

**Date:** 19/8/2020  
**Predrill:** -  
**Water Level:** 0.6m  
**Collapse:** 1.95m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu005  
Sounding: 1

**Operator:** B. Wilson  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKJ328  
**Cone Area Ratio:** 0.80

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.4066	11.2583
<b>Local Friction</b>	0.1183	0.1192
<b>Pore Pressure</b>	0.9587	0.9583

**Date:** 19/8/2020  
**Predrill:** -  
**Water Level:** 0.65m  
**Collapse:** 1.45m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

# TEST DETAIL

---

PointID: CPTu006

Sounding: 1

**Operator:** B. Wilson

**Cone Type:** Pagani Piezocone - Compression

**Cone Reference:** MKJ328

**Cone Area Ratio:** 0.80

**Date:** 13/8/2020

**Predrill:** -

**Water Level:** 0.95m

**Collapse:** 1.40m

**Termination**

**Target Depth:**

**Effective Refusal**

Tip:

Gauge:

Inclinometer:

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.3708	11.2634
<b>Local Friction</b>	0.1178	0.119
<b>Pore Pressure</b>	0.9592	0.9542

# CPT CALIBRATION AND TECHNICAL NOTES

These notes describe the technical specifications and associated calibration references pertaining to the Pagani piezocone types measuring cone resistance, sleeve friction, inclination and pore pressure (piezocone, 10cm<sup>2</sup>)

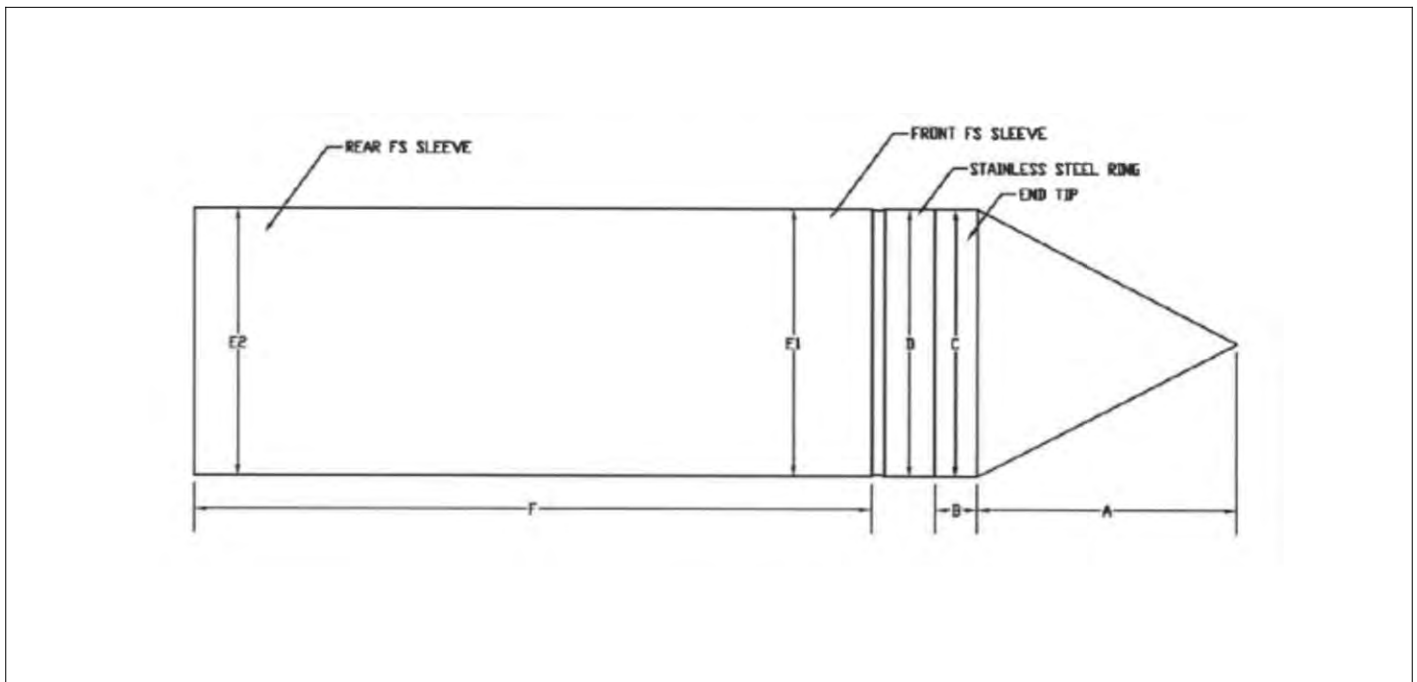
## Dimensions

Dimensional specifications are detailed below. All tolerances are routinely checked prior to testing and measurements taken are electronically recorded. All records are kept on file and available on request.

## Technical specifications

	Tip	Friction	Pore Pressure	Inclination
<b>Maximum Measuring Range:</b>	50 - 100 MPa	1.60 MPa	2.50 MPa	0° - 20°
<b>Resolution:</b>	24 bit	24 bit	24 bit	12 bit
<b>Accuracy:</b>	0.005 MPa	0.04 MPa	0.04 MPa	0.5°

<b>Length:</b>	320 mm	<b>Weight:</b>	1.8 kg
<b>Diameter:</b>	35.8 mm	<b>Opening angle of bit:</b>	60°
<b>Cone base area:</b>	10 cm <sup>2</sup>	<b>Side sleeve surfaces:</b>	150 cm <sup>2</sup>
<b>Cone area ratio:</b>	0.80	<b>Tip and Local Friction sensor displacement:</b>	80 mm





**CONE CALIBRATION CERTIFICATE**  
N° Z087/19

Calibrated system (Sistema tarato):  
 Serial number **Mkj328**  
 Sensor  
 Max. Capacity [MPa]: **100**  
 Scaling Factor: **195500**  
 Tip net area ratio (a<sub>n</sub>): **0,80**  
 Sleeve net ratio (b<sub>n</sub>): **0,00**

Addressee (destinatario):  
 LANDTEST  
 307 Cashel street, Christchurch  
 New Zealand

Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 200 kN  
 Serial Number 138913  
 Power press:  
 Manufacturer Easydur Italiana  
 Model Aura 20T  
 Serial Number 29084

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)

Last verification date: 15/01/2019  
 Certificate N. LAT 091 2019-014  
 Temperature of calibration 22°C  
 Humidity 53%

Factory calibration in accordance with ASTM D5778-13



**CONE CALIBRATION CERTIFICATE**  
N° Z087/19

Calibrated system (Sistema tarato):  
 Serial number **Mkj328**  
 Sensor **SLEEVE FRICTION**  
 Max. Capacity [kPa]: **1600**  
 Scaling Factor: **30696**

Addressee (destinatario):  
 LANDTEST  
 307 Cashel street, Christchurch  
 New Zealand

Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 50 kN  
 Serial Number 65495  
 Power press:  
 Manufacturer Easydur Italiana  
 Model Aura 10T  
 Serial Number 29002

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)

The adapted calibration procedure has been developed according to the suggestions given by Prof. Paul W. Mayne (Georges Institute of Technology) and Prof. Diego La Presti (University of Pisa)

Cone calibrated by **Cludio C.**

Date of issue 27/06/2019



**CONE CALIBRATION CERTIFICATE**  
N° Z087/19

Calibrated system (Sistema tarato):  
 Serial number **Mkj328**  
 Sensor **PORE PRESSURE**  
 Max. Capacity [kPa]: **2500**  
 Scaling Factor: **16963**  
 Sensor **TILT ANGLE**  
 Max. Inclination [°]: **20**  
 Scaling Factor: **140137**

Addressee (destinatario):  
 LANDTEST  
 307 Cashel street, Christchurch  
 New Zealand

Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Pressure Generator:  
 Manufacturer AEP transducers  
 Model GPM500  
 Digital Indicator:  
 Manufacturer AEP transducers  
 Model LAB DMM  
 Serial Number 301796

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)



# CONE CERTIFICATES



## CONE CALIBRATION CERTIFICATE N° 2024/20

Calibrated system (Sistema tarato):  
 Serial number **Mks711**  
 Sensor  
 Max. Capacity [MPa]: **100**  
 Sealing Factor: **190780**  
 Tip net area ratio (a<sub>b</sub>): **0,79**  
 Sleeve net ratio (b<sub>s</sub>): **0,00**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 200 kN  
 Serial Number 138913  
 Power press: Easydur Italiana  
 Model Aura 20T  
 Serial Number 29084

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 Certificate N. LAT 091 2020-015  
 Temperature of calibration 22°C  
 Humidity 45%  
 Factory calibration in accordance with ASTM D5778-12



## CONE CALIBRATION CERTIFICATE N° 2024/20

Calibrated system (Sistema tarato):  
 Serial number **Mks711**  
 Sensor **SLEEVE FRICTION**  
 Max. Capacity [kPa]: **1600**  
 Sealing Factor: **31343**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 50 kN  
 Serial Number 65495  
 Power press: Easydur Italiana  
 Model Aura 10T  
 Serial Number 29002

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 The adopted calibration procedure has been developed acc Prof. Paul W. Mayne (Georgia Institute of technology) and  
 Cone calibrated by



## CONE CALIBRATION CERTIFICATE N° 2024/20

Calibrated system (Sistema tarato):  
 Serial number **Mks711**  
 Sensor **PORE PRESSURE**  
 Max. Capacity [kPa]: **2500**  
 Sealing Factor: **10298**  
 Sensor **TILT ANGLE**  
 Max. Inclination [°]: **20**  
 Sealing Factor: **280277**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Pressure Generator:  
 Manufacturer MENSOR  
 Model CPC 4000  
 Serial Number 41000V56  
 Sensor Descri Silicon Pressure Transducer  
 Sensor Serial Number 41000SYF

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 28/02/2019  
 Certificate N. 162632  
 Temperature of calibration 22°C  
 Humidity 45%  
 Factory calibration in accordance with ASTM D5778-12

# **CONE PENETRATION TEST (CPT) REPORT**

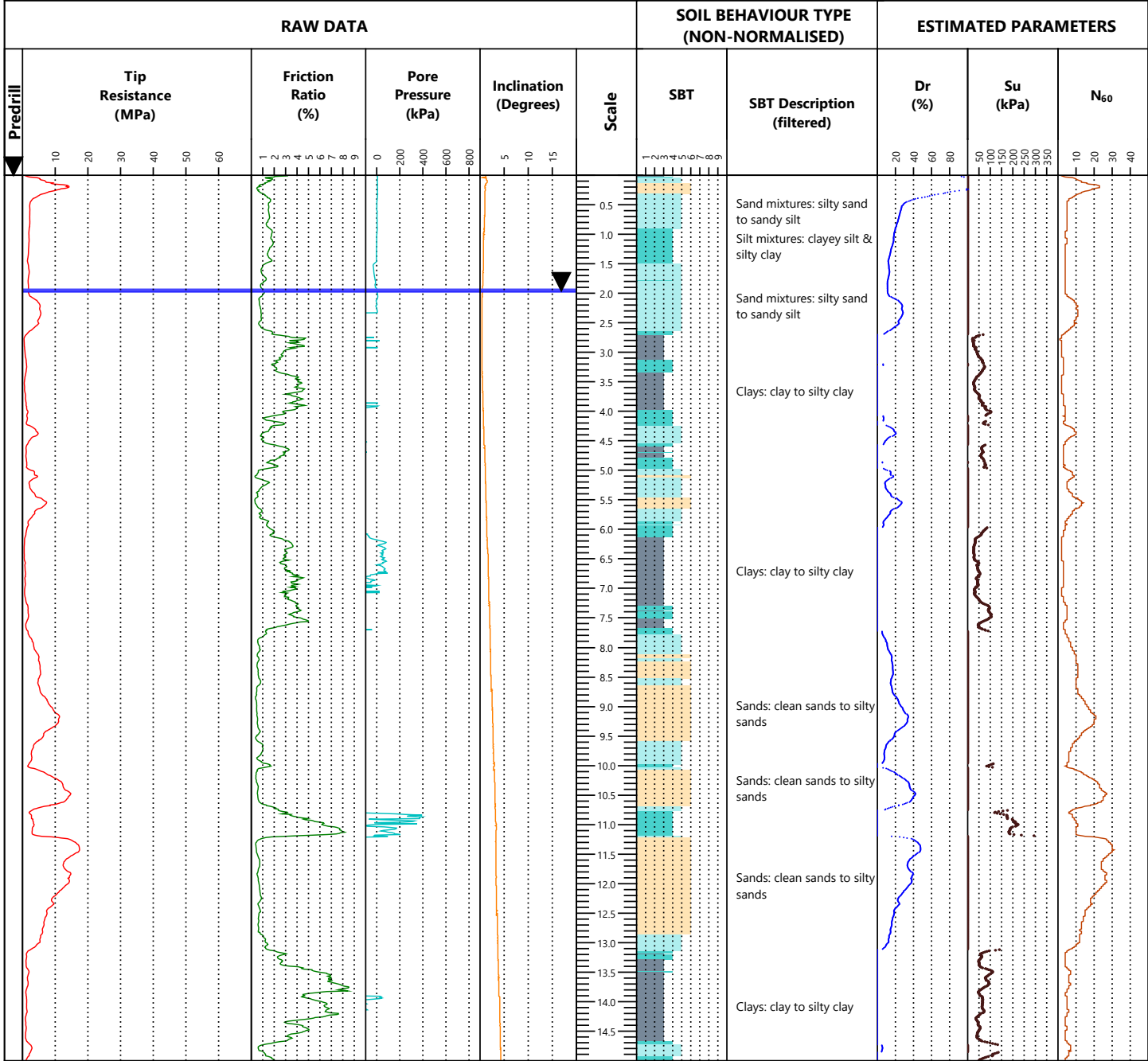


**Client: Miyamoto International NZ**

**Location: 2-4 Glovers Road, Christchurch**

**Printed: 29/09/2020**

**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 24/9/2020  
**Grid Reference:** 1564970.4m E, 5173158.32m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ329	<b>Water Level:</b> 1.96m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 2.0m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.9412	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1606		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	1.4594		<b>6</b> Sands: clean sands to silty sands
	1.262		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**  
 Invalid pore water pressure data from 2.33m.

<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu008</b>
<b>Project:</b>	2-4 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

**Site Location:** 2-4 Glovers Road, Christchurch

**Date:** 24/9/2020

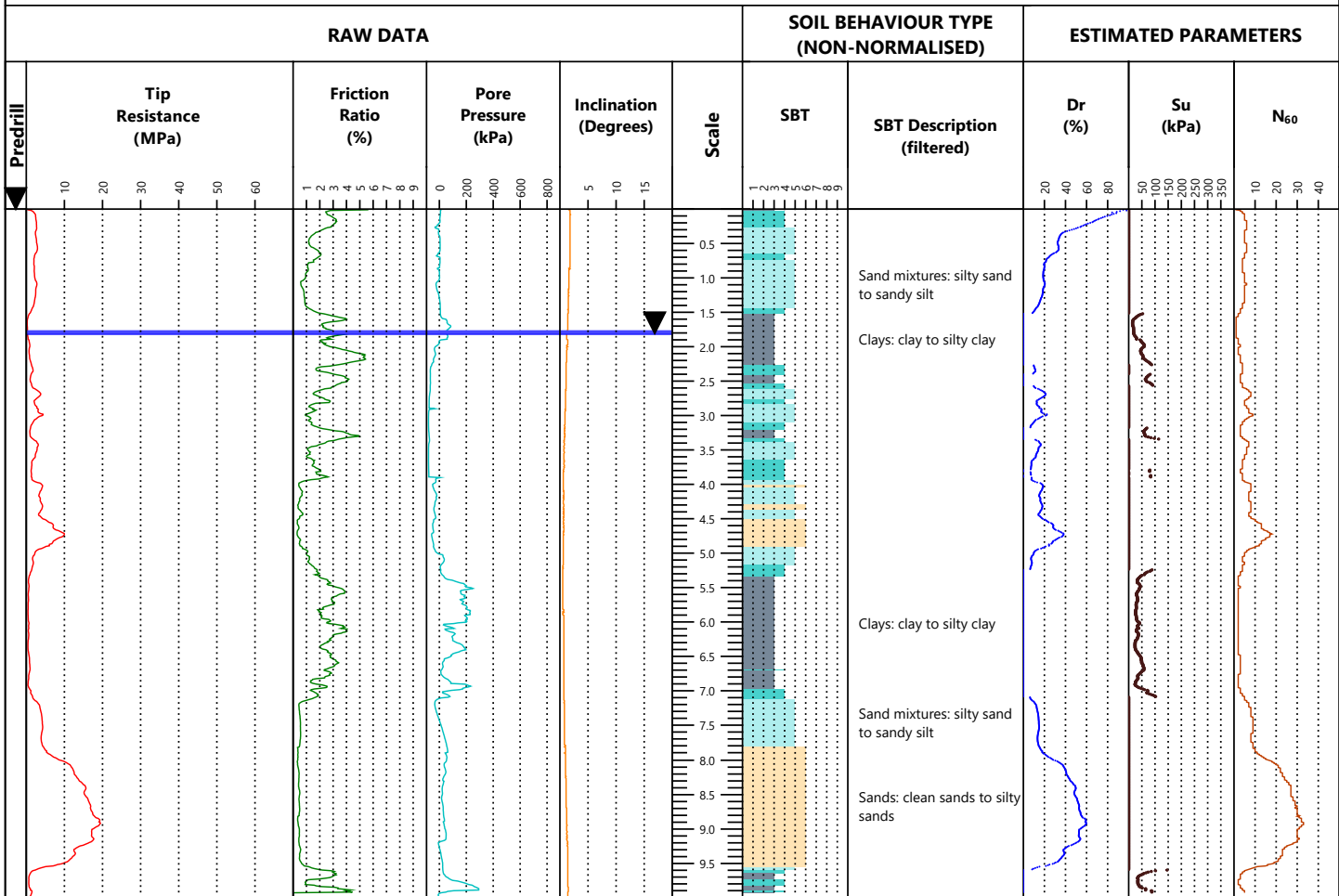
**Grid Reference:** 1565034.78m E, 5173124.87m N (NZTM) - Map or aerial photograph

**Rig Operator:** E. Diaz

**Elevation:** 0.00m

**Datum:** Ground

**Equipment:** Pagani TG63-150



EOH: 10m

**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKJ329  
**Cone Area Ratio:** 0.79  
**Standards:** ISO 22476-1:2012

**Predrill:** -  
**Water Level:** 1.8m  
**Collapse:** 2.2m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
 Tip:   
 Gauge:   
 Inclinator:

**Soil Behaviour Type (SBT) - Robertson et al. 1986**

<b>0</b> Undefined	<b>5</b> Sand mixtures: silty sand to sandy silt
<b>1</b> Sensitive fine-grained	<b>6</b> Sands: clean sands to silty sands
<b>2</b> Clay - organic soil	<b>7</b> Dense sand to gravelly sand
<b>3</b> Clays: clay to silty clay	<b>8</b> Stiff sand to clayey sand
<b>4</b> Silt mixtures: clayey silt & silty clay	<b>9</b> Stiff fine-grained

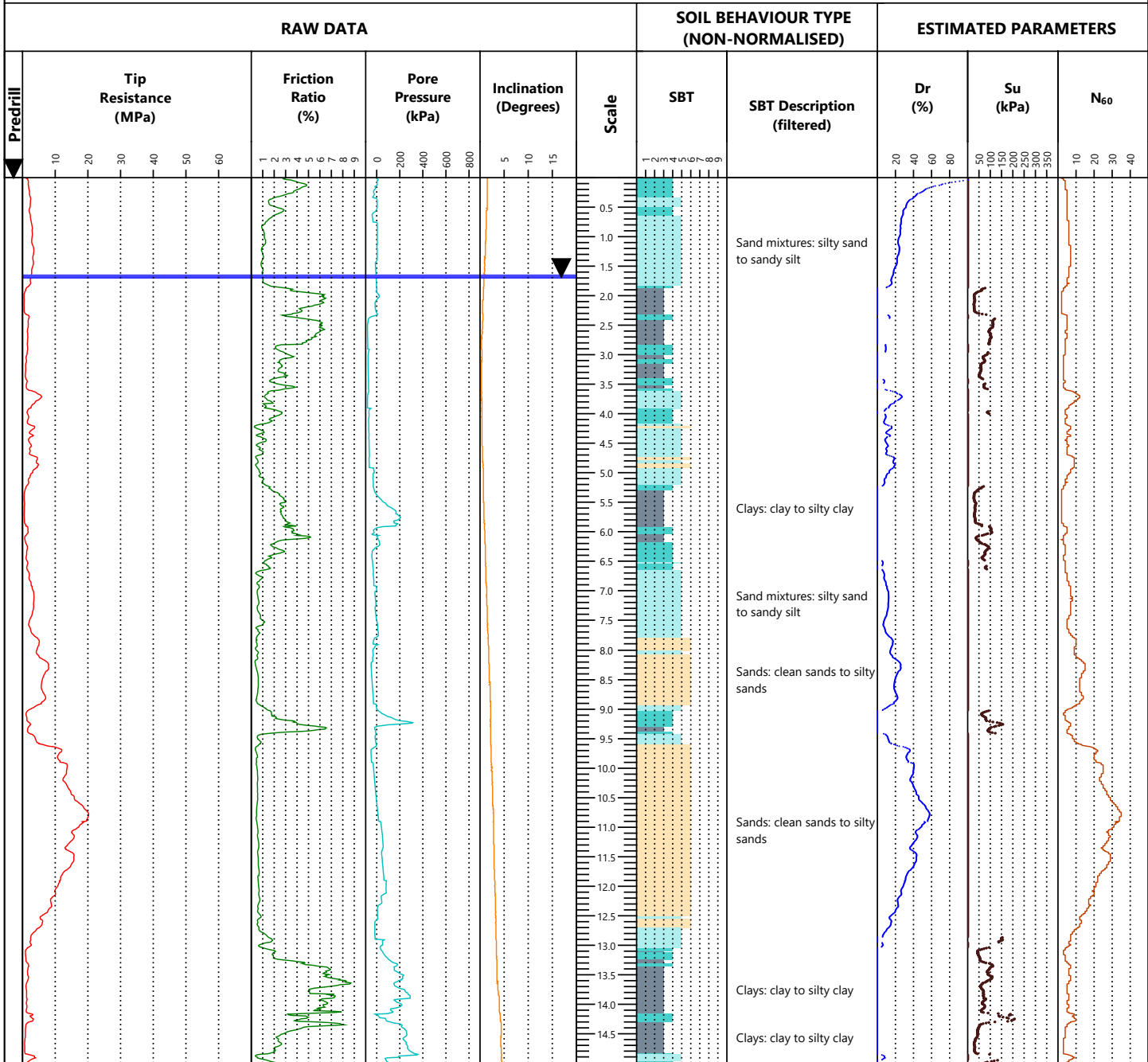
Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.9516	11.8425
<b>Local Friction</b>	0.1609	0.1614
<b>Pore Pressure</b>	1.459	1.4561

**Notes & Limitations**

Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 24/9/2020  
**Grid Reference:** 1564969.64m E, 5173086.81m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



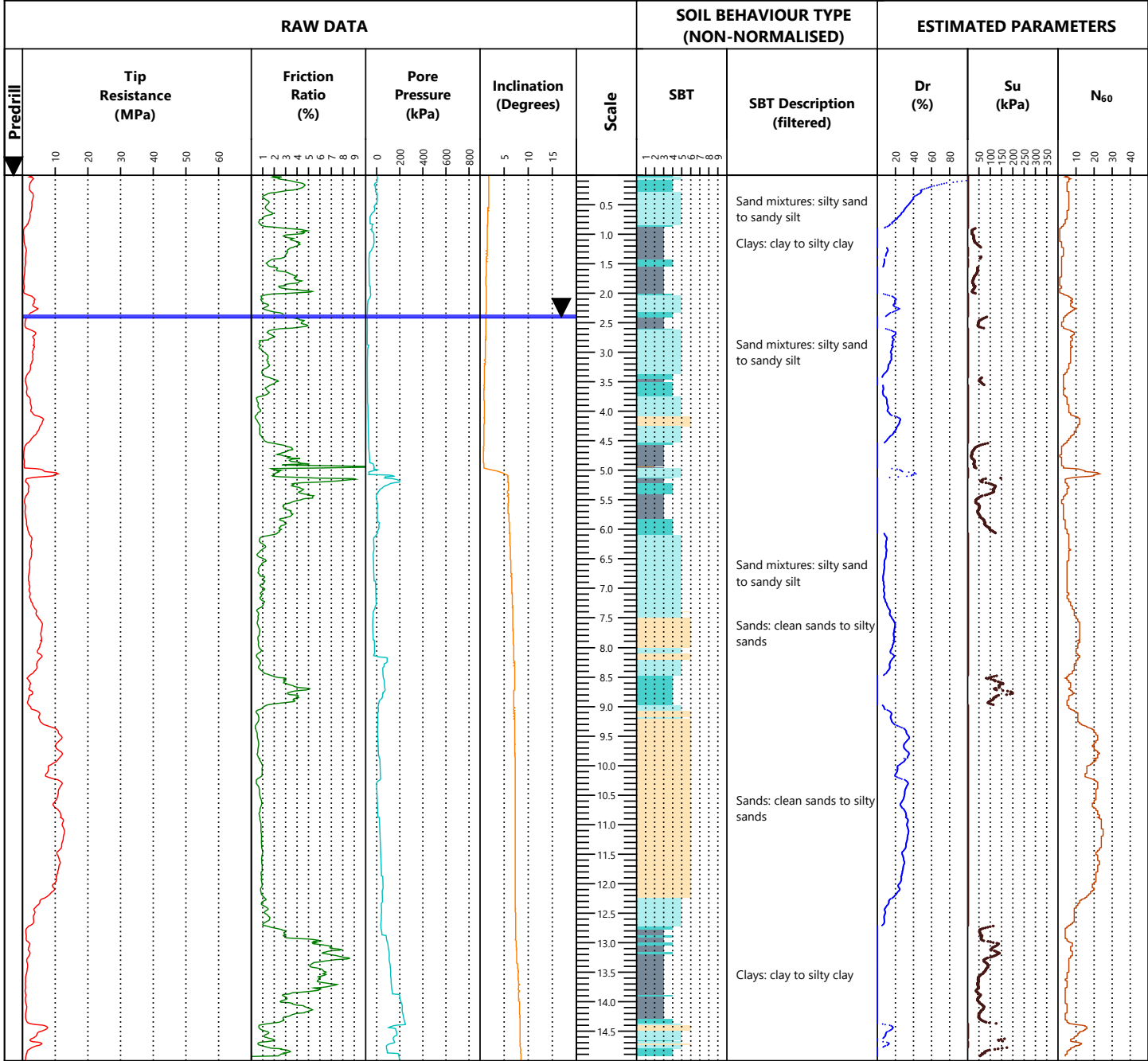
<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ329	<b>Water Level:</b> 1.68m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 1.80m	<b>Effective Refusal</b>	<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>6</b> Sands: clean sands to silty sands
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>7</b> Dense sand to gravelly sand
<b>Tip Resistance</b>	11.9464	Inclinometer: <input type="checkbox"/>	<b>8</b> Stiff sand to clayey sand
<b>Local Friction</b>	0.1604		<b>9</b> Stiff fine-grained
<b>Pore Pressure</b>	1.4592		

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

Sheet 1 of 1

**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 25/9/2020  
**Grid Reference:** 1565043.16m E, 5173036.65m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150

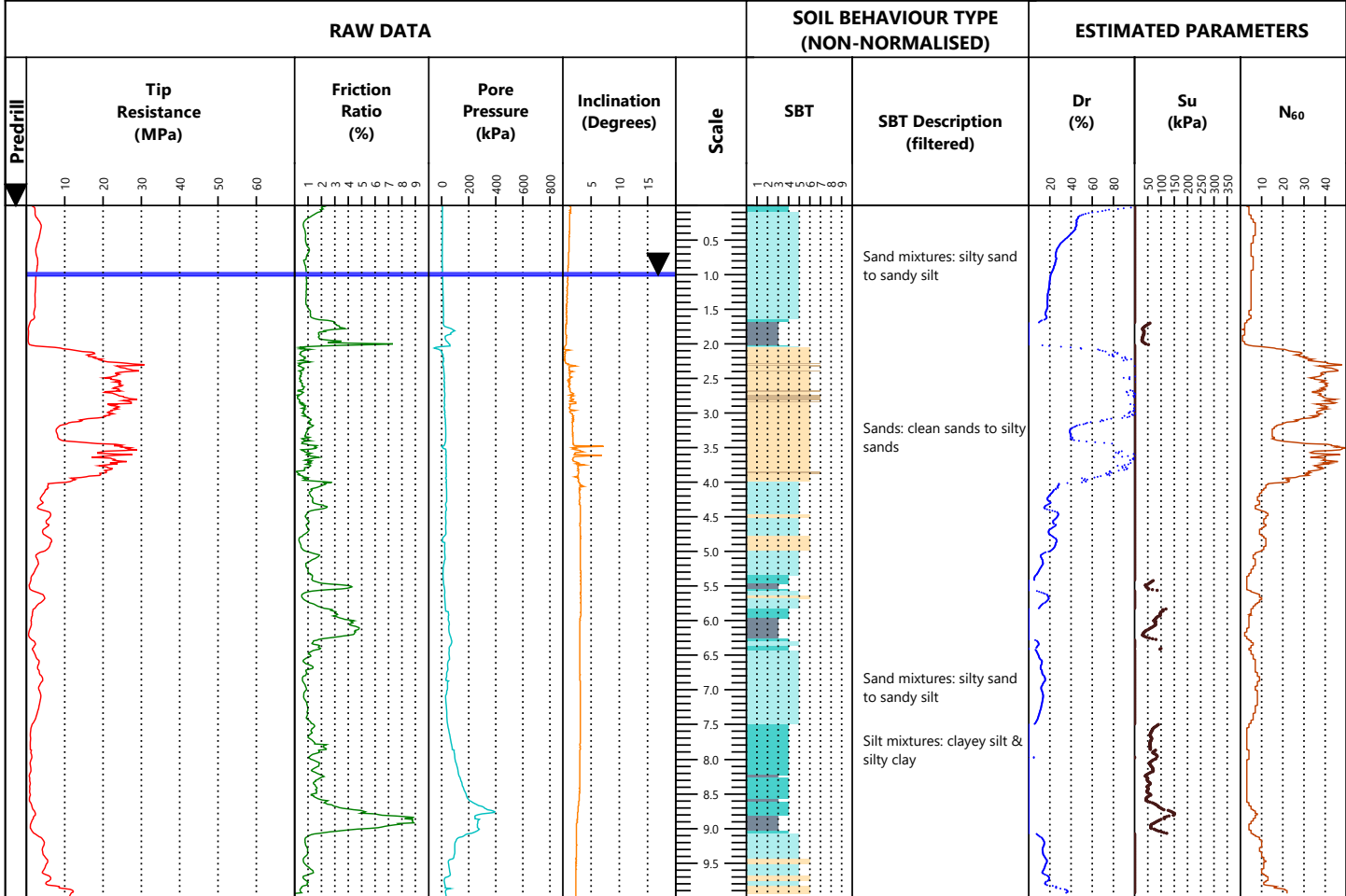


<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ329	<b>Water Level:</b> 2.4m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 2.50m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.9568	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1618		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	1.4599		<b>6</b> Sands: clean sands to silty sands
	1.4582		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 25/9/2020  
**Grid Reference:** 1565055.15m E, 5172937.04m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



EOH: 10m

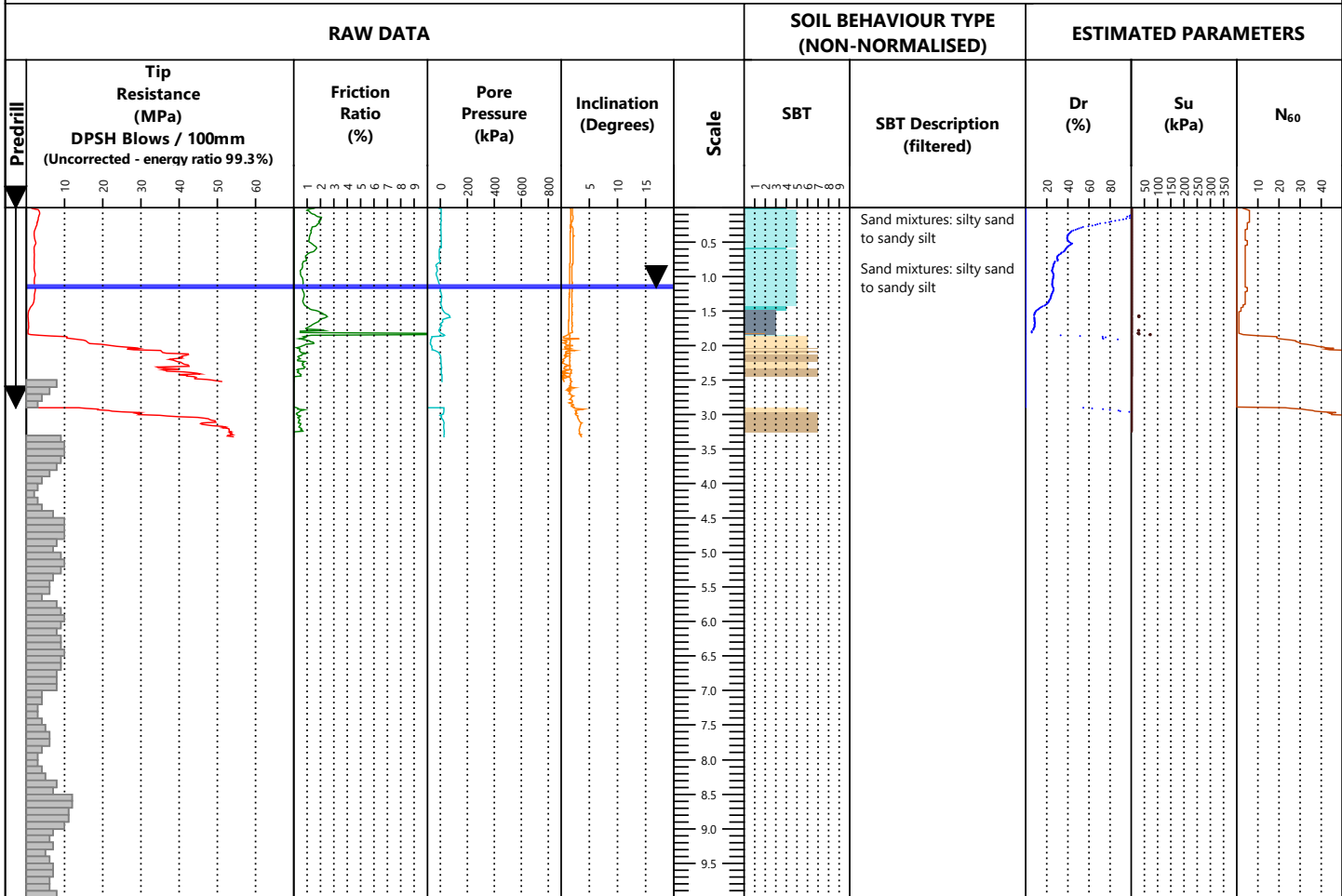
<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ329 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012	<b>Predrill:</b> - <b>Water Level:</b> 1m <b>Collapse:</b> 5.1m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <b>0</b> Undefined <b>1</b> Sensitive fine-grained <b>2</b> Clay - organic soil <b>3</b> Clays: clay to silty clay <b>4</b> Silt mixtures: clayey silt & silty clay <b>5</b> Sand mixtures: silty sand to sandy silt <b>6</b> Sands: clean sands to silty sands <b>7</b> Dense sand to gravelly sand <b>8</b> Stiff sand to clayey sand <b>9</b> Stiff fine-grained
<b>Zero load outputs (MPa)</b> <b>Tip Resistance</b> 11.9464 <b>Local Friction</b> 0.1615 <b>Pore Pressure</b> 1.4598	<b>Before test</b> 11.8166 0.1621 1.455	<b>After test</b> 11.8166 0.1621 1.455	<b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

Sheet 1 of 1

<b>Site Location:</b> 2-4 Glovers Road, Christchurch	<b>Date:</b> 29/9/2020
<b>Grid Reference:</b> 1565058.83m E, 5172852.91m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> E. Diaz
<b>Elevation:</b> 0.00m <b>Datum:</b> Ground	<b>Equipment:</b> Pagani TG63-150



EOH: 10m

<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ329 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012  <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <th>Zero load outputs (MPa)</th> <th>Before test</th> <th>After test</th> </tr> <tr> <td><b>Tip Resistance</b></td> <td>11.8737</td> <td>11.8321</td> </tr> <tr> <td><b>Local Friction</b></td> <td>0.1612</td> <td>0.1611</td> </tr> <tr> <td><b>Pore Pressure</b></td> <td>1.4542</td> <td>1.4556</td> </tr> </table>	Zero load outputs (MPa)	Before test	After test	<b>Tip Resistance</b>	11.8737	11.8321	<b>Local Friction</b>	0.1612	0.1611	<b>Pore Pressure</b>	1.4542	1.4556	<b>Predrill:</b> 2.9m <b>Water Level:</b> 1.15m <b>Collapse:</b> 2.2m  <b>Termination</b> <b>Target Depth:</b> <input type="checkbox"/>  <b>Effective Refusal</b> Tip: <input checked="" type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td style="background-color: black; color: white;">0</td> <td>Undefined</td> <td style="background-color: #90EE90;">5</td> <td>Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td style="background-color: #FF0000;">1</td> <td>Sensitive fine-grained</td> <td style="background-color: #FFD700;">6</td> <td>Sands: clean sands to silty sands</td> </tr> <tr> <td style="background-color: #FF8C00;">2</td> <td>Clay - organic soil</td> <td style="background-color: #8B4513;">7</td> <td>Dense sand to gravelly sand</td> </tr> <tr> <td style="background-color: #4682B4;">3</td> <td>Clays: clay to silty clay</td> <td style="background-color: #808080;">8</td> <td>Stiff sand to clayey sand</td> </tr> <tr> <td style="background-color: #00CED1;">4</td> <td>Silt mixtures: clayey silt &amp; silty clay</td> <td style="background-color: #404040;">9</td> <td>Stiff fine-grained</td> </tr> </table>	0	Undefined	5	Sand mixtures: silty sand to sandy silt	1	Sensitive fine-grained	6	Sands: clean sands to silty sands	2	Clay - organic soil	7	Dense sand to gravelly sand	3	Clays: clay to silty clay	8	Stiff sand to clayey sand	4	Silt mixtures: clayey silt & silty clay	9	Stiff fine-grained
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<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>   <div style="text-align: right;">Sheet 1 of 1</div>
--	--



## TEST DETAIL

PointID: CPTu007

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9412	11.8737
Local Friction	0.1606	0.161
Pore Pressure	1.4594	1.262

Date: 24/9/2020

Predrill: -

Water Level: 1.96m

Collapse: 2.0m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu008

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9516	11.8425
Local Friction	0.1609	0.1614
Pore Pressure	1.459	1.4561

Date: 24/9/2020

Predrill: -

Water Level: 1.8m

Collapse: 2.2m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu009

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9464	11.801
Local Friction	0.1604	0.1611
Pore Pressure	1.4592	1.4568

Date: 24/9/2020

Predrill: -

Water Level: 1.68m

Collapse: 1.80m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu010

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9568	11.8166
Local Friction	0.1618	0.1622
Pore Pressure	1.4599	1.4582

Date: 25/9/2020

Predrill: -

Water Level: 2.4m

Collapse: 2.50m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu011

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9464	11.8166
Local Friction	0.1615	0.1621
Pore Pressure	1.4598	1.455

Date: 25/9/2020

Predrill: -

Water Level: 1m

Collapse: 5.1m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

## TEST DETAIL

---

PointID: CPTu012

Sounding: 1

**Operator:** E. Diaz

**Cone Type:** Pagani Piezocone - Compression

**Cone Reference:** MKJ329

**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.9568	11.8062
<b>Local Friction</b>	0.1607	0.1609
<b>Pore Pressure</b>	1.4567	1.4562

**Date:** 29/9/2020

**Predrill:** -

**Water Level:** -

**Collapse:** -

**Termination**

**Target Depth:**

**Effective Refusal**

Tip:

Gauge:

Inclinometer:

Sounding: 2

**Operator:** E. Diaz

**Cone Type:** Pagani Piezocone - Compression

**Cone Reference:** MKJ329

**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.8737	11.8321
<b>Local Friction</b>	0.1612	0.1611
<b>Pore Pressure</b>	1.4542	1.4556

**Date:** 29/9/2020

**Predrill:** 2.9m

**Water Level:** 1.15m

**Collapse:** 2.2m

**Termination**

**Target Depth:**

**Effective Refusal**

Tip:

Gauge:

Inclinometer:

# CPT CALIBRATION AND TECHNICAL NOTES

These notes describe the technical specifications and associated calibration references pertaining to the Pagani piezocone types measuring cone resistance, sleeve friction, inclination and pore pressure (piezocone, 10cm<sup>2</sup>)

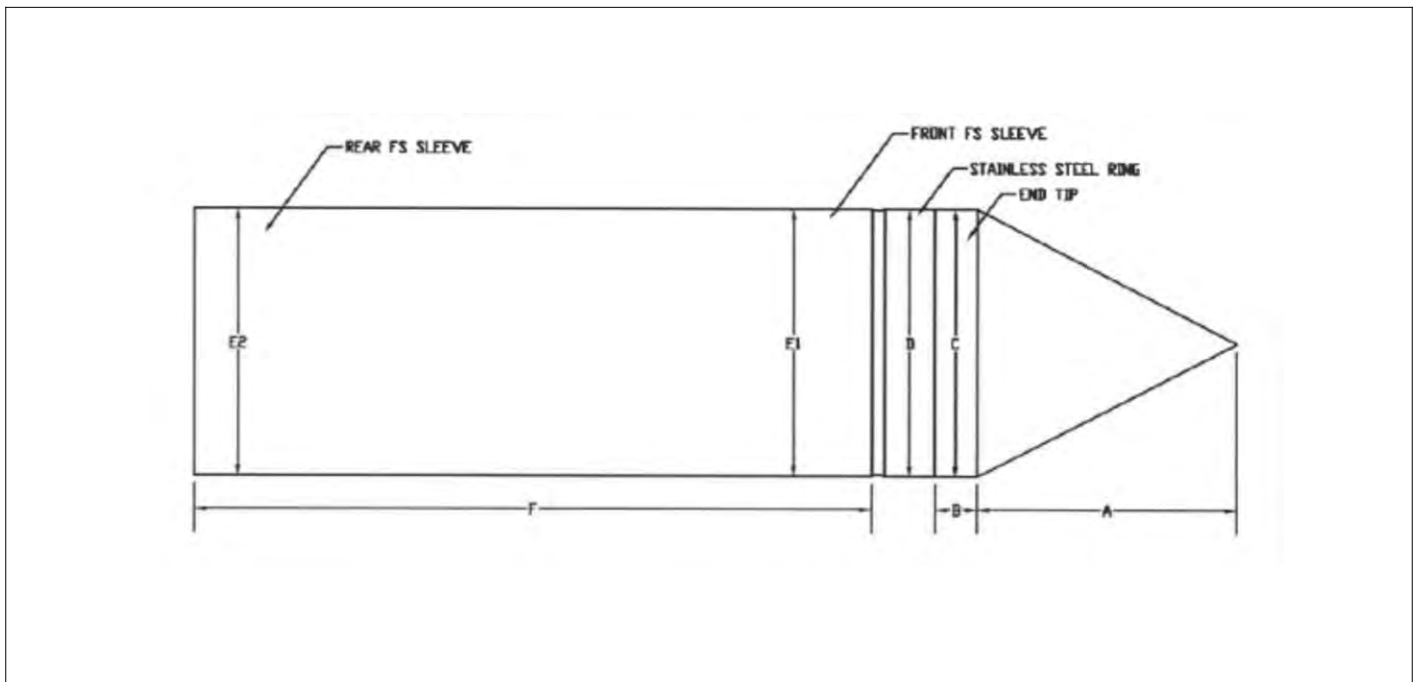
## Dimensions

Dimensional specifications are detailed below. All tolerances are routinely checked prior to testing and measurements taken are electronically recorded. All records are kept on file and available on request.

## Technical specifications

	Tip	Friction	Pore Pressure	Inclination
<b>Maximum Measuring Range:</b>	50 - 100 MPa	1.60 MPa	2.50 MPa	0° - 20°
<b>Resolution:</b>	24 bit	24 bit	24 bit	12 bit
<b>Accuracy:</b>	0.005 MPa	0.04 MPa	0.04 MPa	0.5°

<b>Length:</b>	320 mm	<b>Weight:</b>	1.8 kg
<b>Diameter:</b>	35.8 mm	<b>Opening angle of bit:</b>	60°
<b>Cone base area:</b>	10 cm <sup>2</sup>	<b>Side sleeve surfaces:</b>	150 cm <sup>2</sup>
<b>Cone area ratio:</b>	0.80	<b>Tip and Local Friction sensor displacement:</b>	80 mm





**CONE CALIBRATION CERTIFICATE**  
N° Z023/20

Calibrated system (Sistema tarato):  
 Serial number **Mkj329**  
 Sensor **TIP RESISTANCE**  
 Max. Capacity [MPa]: **100**  
 Scaling Factor: **192610**  
 Tip net area ratio (a<sub>t</sub>): **0,79**  
 Sleeve net ratio (b<sub>s</sub>): **0,00**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 200 KN  
 Serial Number 138913  
 Power press: Easydur Italiana  
 Model Aura 20T  
 Serial Number 29084  
 The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 Certificate N. LAT 091 2020-015  
 Temperature of calibration 22°C  
 Humidity 45%  
 Factory calibration in accordance with **ASTM D5778-12**



**CONE CALIBRATION CERTIFICATE**  
N° Z023/20

Calibrated system (Sistema tarato):  
 Serial number **Mkj329**  
 Sensor **SLEEVE FRICTION**  
 Max. Capacity [kPa]: **1600**  
 Scaling Factor: **30794**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 50 kN  
 Serial Number 65495  
 Power press: Easydur Italiana  
 Model Aura 10T  
 Serial Number 29002  
 The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 The adopted calibration procedure has been developed according to the suggestions given by Prof. Paul W. Mayne (Georgia Institute of Technology) and Prof. Diego Lo Presti (University of Pisa)

*PLS*



**CONE CALIBRATION CERTIFICATE**  
N° Z023/20

Calibrated system (Sistema tarato):  
 Serial number **Mkj329**  
 Sensor **PORE PRESSURE**  
 Max. Capacity [kPa]: **2500**  
 Scaling Factor: **10657**  
 Sensor **TILT ANGLE**  
 Max. Inclination [°]: **20**  
 Scaling Factor: **151152**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Pressure Generator:  
 Manufacturer MENSOR  
 Model CPC 4000  
 Serial Number 41000V56  
 Sensor Descr Silicon Pressure Transducer  
 Sensor Serial Number 41000SYF  
 The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 28/02/2019

Date of issue 05/02/2020

## D. Southern Geophysical MASW and GPR Report



October 2020

# Geophysical Site Investigation:

2-4 Glovers Road, Christchurch

Report prepared for Miyamoto International NZ Ltd

# GEOPHYSICAL REPORT



**Southern**  
**Geophysical**

3/28 Tanya St, Bromley, Christchurch 8062

Ph: 03 384 4302

Web: [www.southerngeophysical.com](http://www.southerngeophysical.com)

Data collected and report prepared for Southern Geophysical Ltd by:

Christian Ruegg, MSc, Geophysicist

Nick McConachie, BSc, Geologist

Report internally reviewed for Southern Geophysical by:

Mike Finnemore, PhD, Senior Geophysicist

## Table of Contents

Summary: .....	2
Methodology: .....	2
Results: .....	3
Conclusions:.....	3
Disclaimer: .....	5

SGL Reference: 2050

Report Version 1



## **Summary:**

Southern Geophysical Ltd was contracted to undertake a geophysical survey using Multi-channel Analysis of Surface Waves (MASW) at 2-4 Glovers Road, Christchurch. The geophysical survey was conducted on September 24<sup>th</sup>, 2020 and includes three MASW lines (Figure 1). The aim of the survey was to assess the shear-wave velocities and structure of the subsurface to a depth of over 20 m. The MASW results show low shear-wave velocities to a depth of 10 m in the northern part of the site (100 m/s to 150 m/s), with higher velocities to the south (100 m/s to 300 m/s). The boundary between these two zones is a feature characteristic of the edge of a paleochannel, buried valley, or dipping volcanic strata, crossing the site east to west and dipping to the north. It is possible that high velocities imaged by the MASW survey to the south (>500 m/s from approximately 20 m depth) are associated with volcanic rock, but there are no boreholes available for ground truthing to that depth.

## **Methodology:**

MASW is a geophysical technique that uses the dispersive nature of surface waves to model shear-wave velocity versus depth.

A MASW survey is undertaken as a series of lines or points across the surface of the site. The MASW points in this survey were collected using a 24-channel towed seismic array, with 4.5 Hz geophones. The geophone spacing was 1 m and the source offset was 10 m. The seismic source was a 16 lb sledgehammer impacting an aluminium plate. Recording parameters for the MASW survey were set with a 0.125 ms sample interval, 1.5 s record length, 24 dB gains, and a geophone trigger system.

The field records were processed using the Kansas Geological Survey software package SurfSeis6++ ©. The geometry for each point was set according to the survey parameters and the dispersion curves were generated and edited. The inversions were run using a 10 layer variable depth model. The velocity data was interpolated into 2D profiles showing  $V_s$  variations with depth (Figures 2 to 3). The output shear-wave velocity data is included as data files (CSV format), supplementary to this report.

Supplementary to the MASW profiles, a series of Ground Penetrating Radar lines were acquired with a GSSI 200 MHz antenna (Figure 1). The radargrams are included in (Figures 4 and 5).



Survey positions were recorded using a Geo 7X Trimble GNSS system with a Tornado antenna. The GNSS positions were differentially corrected using a local GeoNet base station. The GNSS points were output in NZTM2000, with heights in Mean Sea Level (MSL). The accuracy of the survey positions is +/- 0.1 m. The site had no significant topographic changes, and the lines have not been corrected for elevation.

### **Results:**

A total of three MASW lines were acquired at the site with a total MASW survey length of approximately 1 km (Figure 1). The ground surface was well compacted farm tracks and farm yards. A series of GPR lines were acquired along each MASW line to provide a high resolution image of the substrate (Figures 4 and 5).

In homogenous soils, with gradually increasing shear-wave velocities and no sharp lateral discontinuities, the accuracy of the shear-wave velocities derived from the MASW processing is considered to be +/- 10%.<sup>1</sup> The quality of the seismic data and the dispersion curves used in this report is very good, with a good signal-to-noise ratio. If there is a velocity inversion present in the shear-wave profile (decreasing velocity with depth), the shear-wave velocity of the reduced velocity zone and the thickness of that zone can often be underestimated by the inversion process.

### **Conclusions:**

The MASW survey was considered to be of good quality, with modelled shear-wave velocities accurate to +/- 10%. The velocities in the top 5 m are likely to be more accurate than the deeper velocities, due to the presence of multiple velocity inversions. The MASW survey indicates a horizontal layer defined by a sharp increase in shear-wave velocity (180 m/s to 220 m/s) at around 5 m depth in the southern part of the site, consistent with the surface of dense gravels or sands. In the northern part of the site a similar 180 m/s to 220 m/s surface was observed at 20 m depth. There is a well-defined dipping surface dividing the south and the north, possibly associated with a buried valley edge, paleochannel, or

---

<sup>1</sup> Stephenson, W.J., Louie, J.N., Pullammanappallil, S., Williams, R.A., and Odum, J.K. 2005. Blind Shear-wave Velocity Comparison of ReMi and MASW Results with Boreholes to 200 m in Santa Clara Valley: Implications for Earthquake Ground-Motion Assessment. *Bulletin of the Seismological Society of America*, Vol. 95, pp. 2506-2516.

bedrock interface. This edge feature is apparent in both MASW 1 and MASW 3, as well as GPR 4 and GPR 10.

While the limitations of the MASW method should be considered when evaluating these results, the quality of the data collected at the site and the confidence in the shear-wave velocities derived from the MASW data is good.

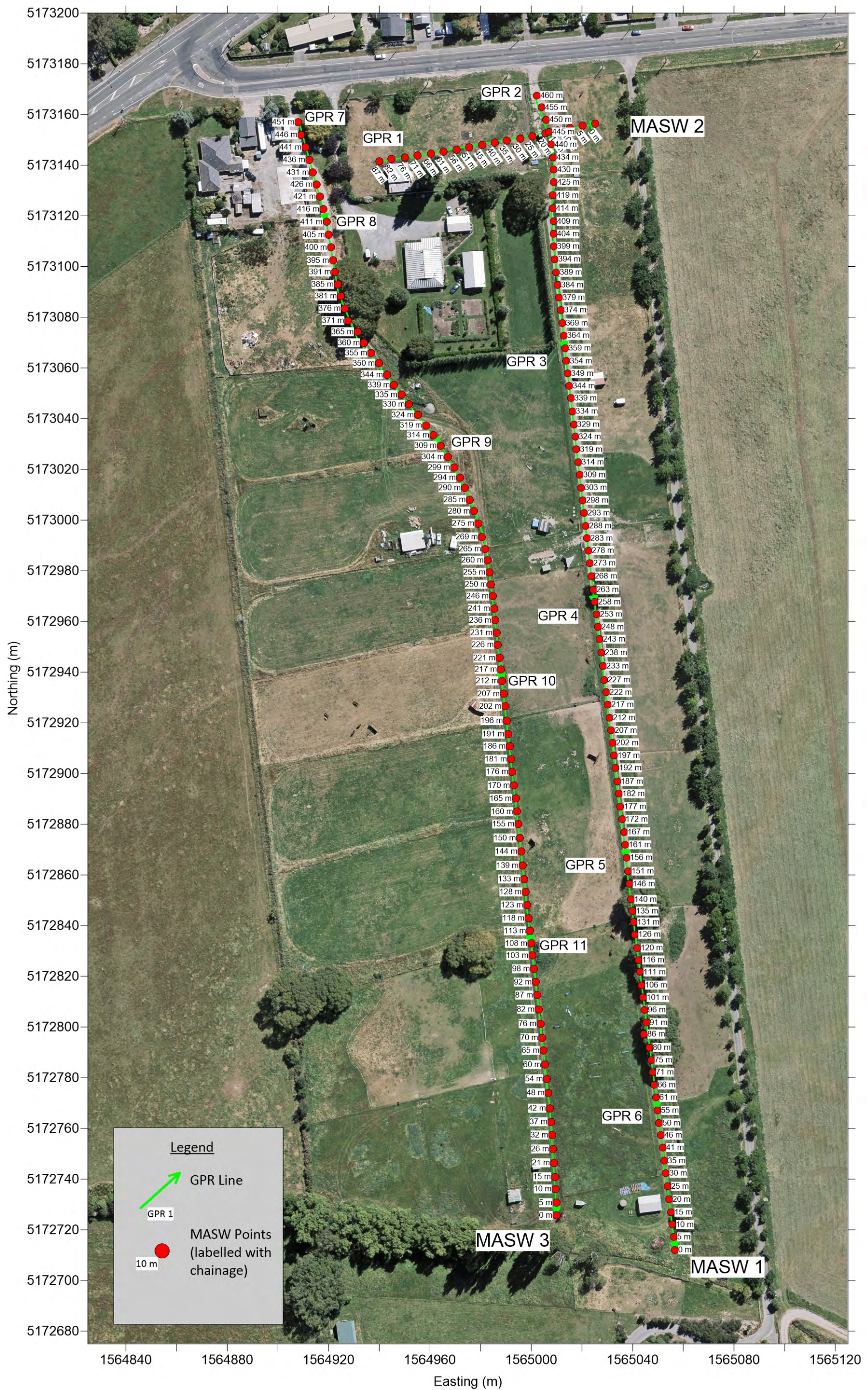
**Disclaimer:**

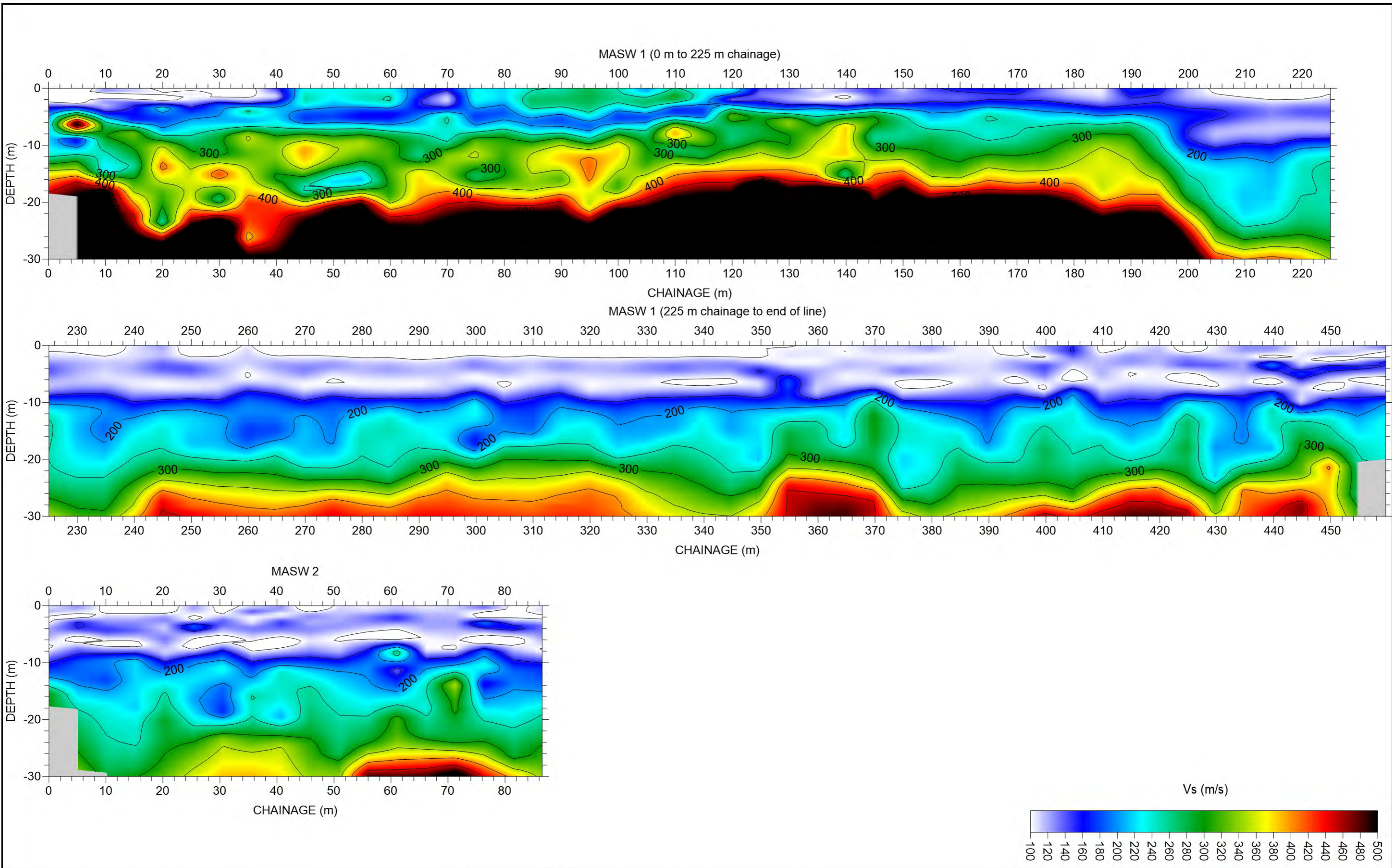
This document has been provided by Southern Geophysical Ltd subject to the following:

Non-invasive geophysical testing has limitations and is not a complete source of testing. Often there is a need to couple non-invasive methods with invasive testing methods, such as drilling, especially in cases where the non-invasive testing indicates anomalies.

This document has been prepared for the particular purpose outlined in the project proposal and no responsibility is accepted for the use of this document, in whole or in part, in other contexts or for any other purpose. Southern Geophysical Ltd did not perform a complete assessment of all possible conditions or circumstances that may exist at the site. Conditions may exist which were undetectable given the limited nature of the enquiry Southern Geophysical Ltd was retained to undertake with respect to the site. Variations in conditions often occur between investigatory locations, and there may be special conditions pertaining to the site which have not been revealed by the investigation and which have not therefore been taken into account. Accordingly, additional studies and actions may be required by the client.

We collected our data and based our report on information which was collected at a specific point in time. The passage of time affects the information and assessment provided by Southern Geophysical Ltd. It is understood that the services provided allowed Southern Geophysical Ltd to form no more than an opinion of the actual conditions of the site at the time the site was visited and cannot be used to assess the effect of any subsequent changes for whatever reason. Where data is supplied by the client or other sources, including where previous site investigation data have been used, it has been assumed that the information is correct. No responsibility is accepted by Southern Geophysical Ltd for incomplete or inaccurate data supplied by others. This document is provided for sole use by the client and is confidential to that client and its professional advisers. No responsibility whatsoever for the contents of this document will be accepted to any person other than the client. Any use which a third party makes of this document, or any reliance on or decisions to be made based on it, is the responsibility of such third parties. Southern Geophysical Ltd accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this document.





DRAWING- **Figure 2: MASW 1 and 2**

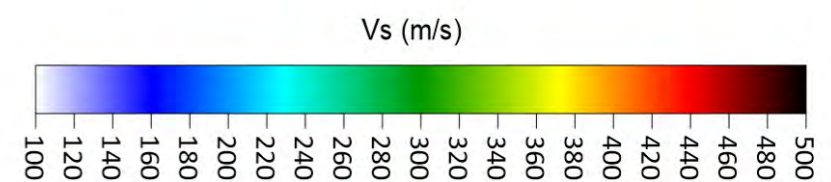
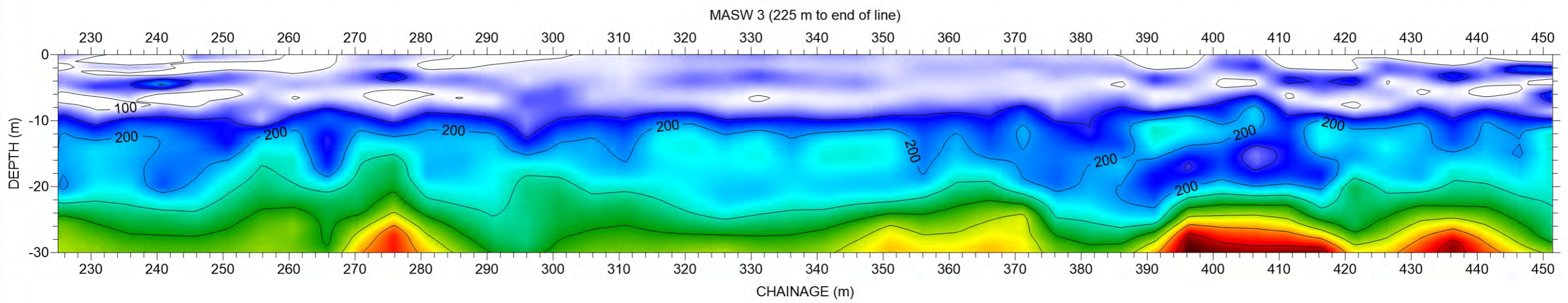
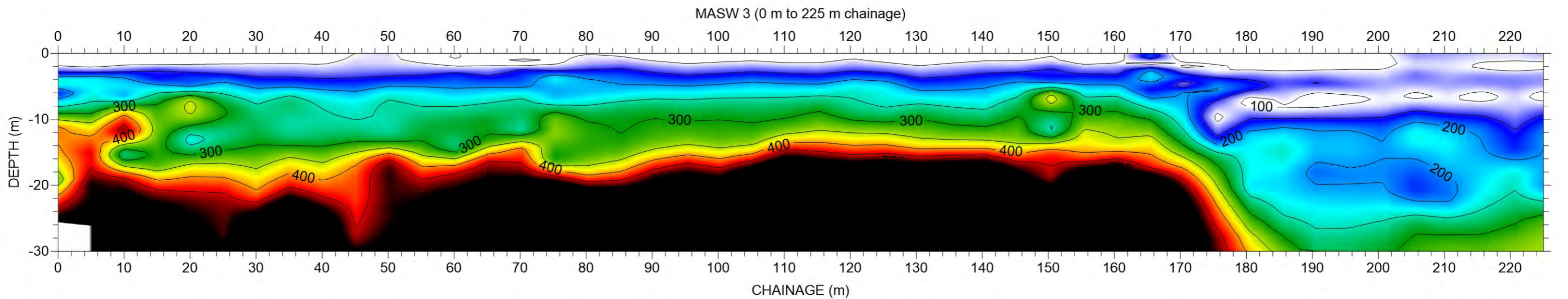
LOCATION- **2-4 Glovers Road, Christchurch**

NOTES MASW Vs profile has contour intervals of 50 m/s (Vs).

See site map for location of points.

A3

**Southern Geophysical Ltd**  
www.southerngeophysical.com



DRAWING- **Figure 3: MASW 3**

LOCATION- **2-4 Glover Street, Christchurch**

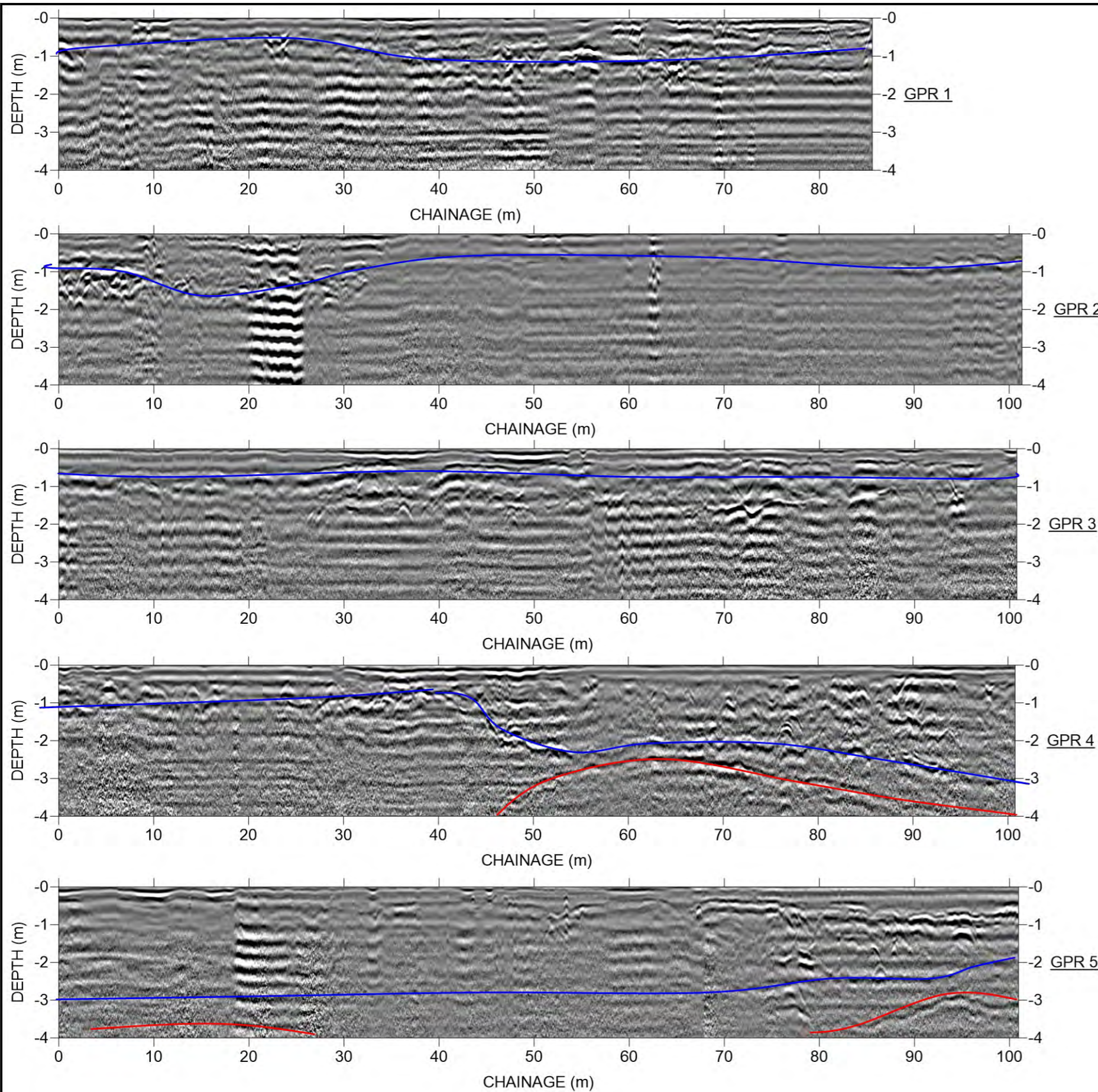
NOTES MASW Vs profile has contour intervals of 50 m/s (Vs).

See site map for location of points.

**Southern Geophysical Ltd**

[www.southerngeophysical.com](http://www.southerngeophysical.com)

A3

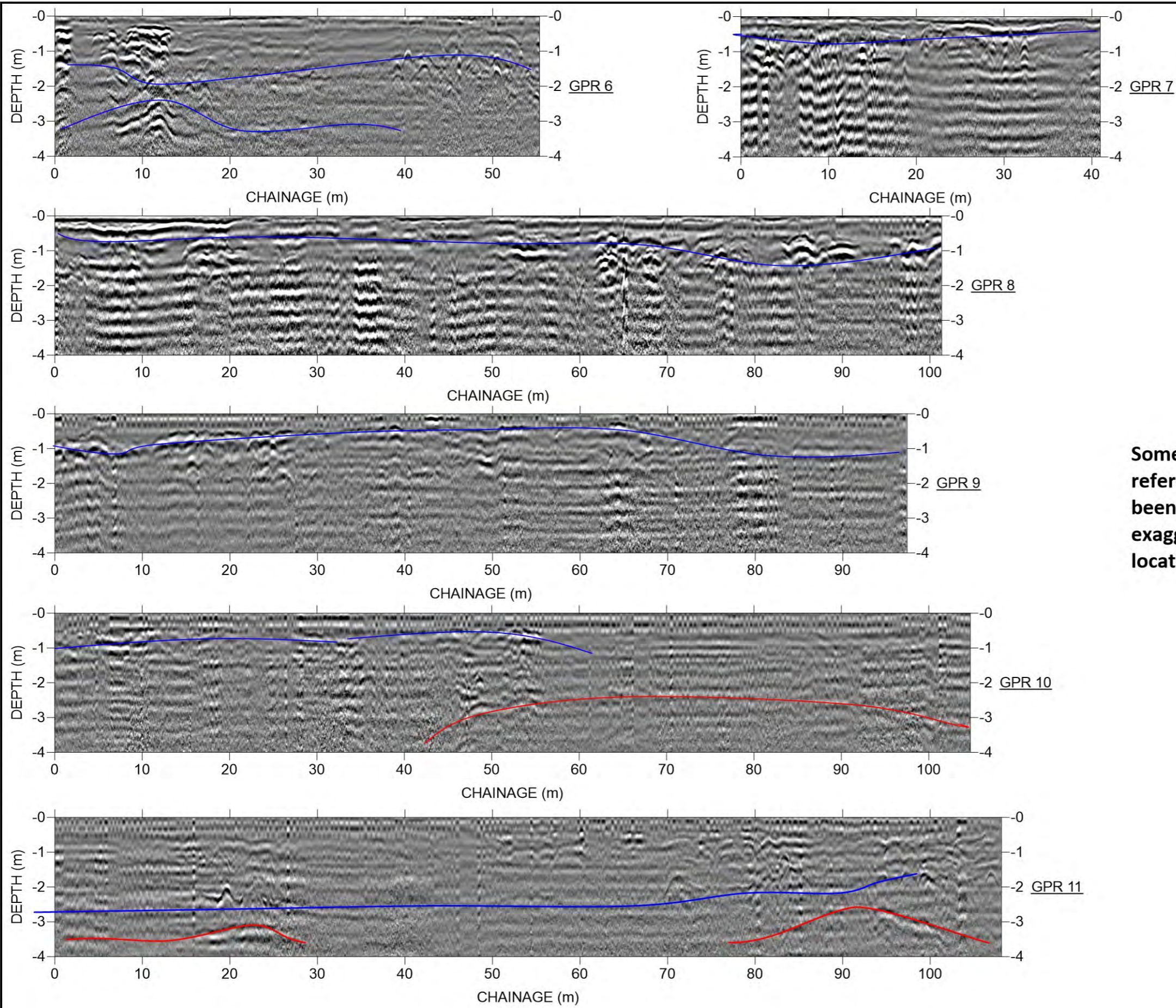


Some reflectors are annotated for reference. Note the profiles have been plotted with a 4:1 vertical exaggeration. See site map for line locations.

DRAWING- **Figure 4: GPR Radargrams 1 to 5**

LOCATION- **2-4 Glover Street, Christchurch**

NOTES



Some reflectors are annotated for reference. Note the profiles have been plotted with a 4:1 vertical exaggeration. See site map for line locations.

DRAWING- **Figure 5: GPR Radargrams 6 to 11**

LOCATION- **2-4 Glover Street, Christchurch**

NOTES

**Southern**  
**Geophysical Ltd**  
[www.southerngeophysical.com](http://www.southerngeophysical.com)

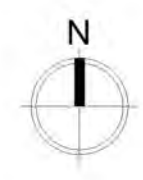
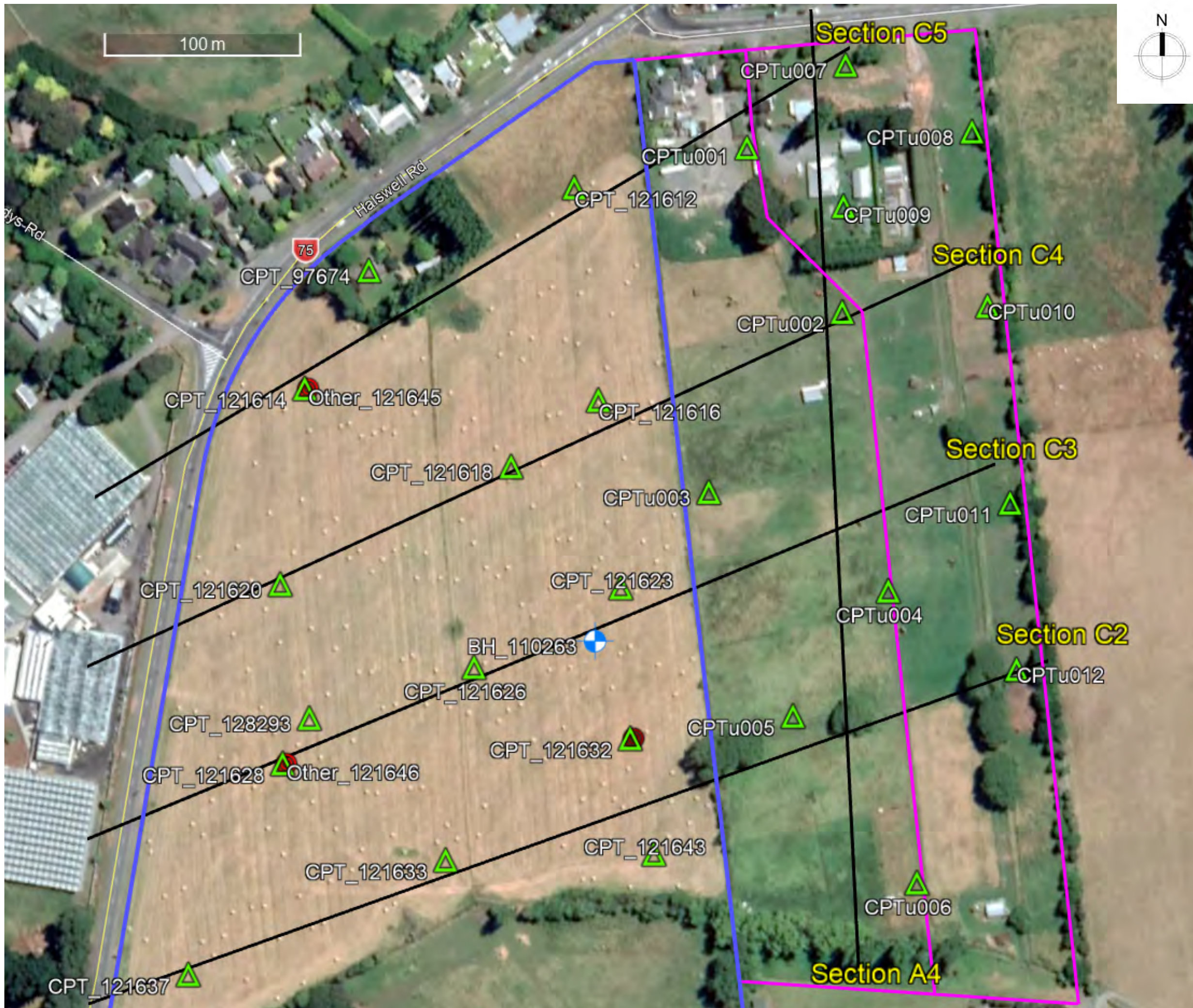


## E. Geotechnical Cross Sections



## PROJECT No: 200357 GEOTECHNICAL CROSS SECTIONS FOR 2&4 GLOVERS ROAD, HALSWELL, CHRISTCHURCH 8025

SHEET LIST		
SHEET N°	SHEET NAME	REV.
S1	LOCATION PLAN	1
S2.1	GEOTECHNICAL CROSS-SECTION 1	1
S2.2	GEOTECHNICAL CROSS-SECTION 2	1
S2.3	GEOTECHNICAL CROSS-SECTION 3	1



100 m

**miyamoto.**

236 Hereford Street,  
PO BOX 137 Cashel Street  
Christchurch 8011

T: 64 03 377 4095  
miyamoto.nz  
projects@miyamoto.nz

**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**

REVISION HISTORY		
REV	DATE	DESCRIPTION
1	19/10/20	FINAL

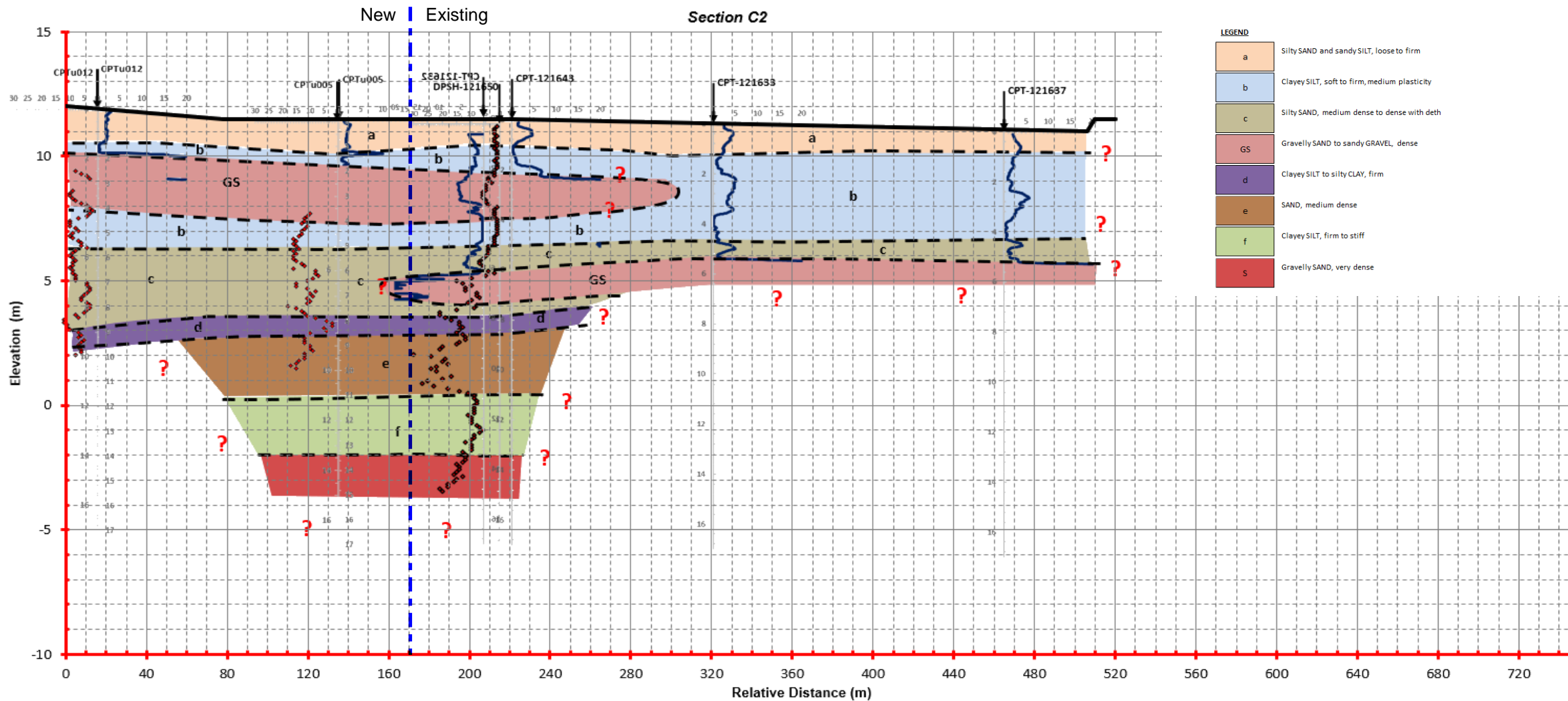
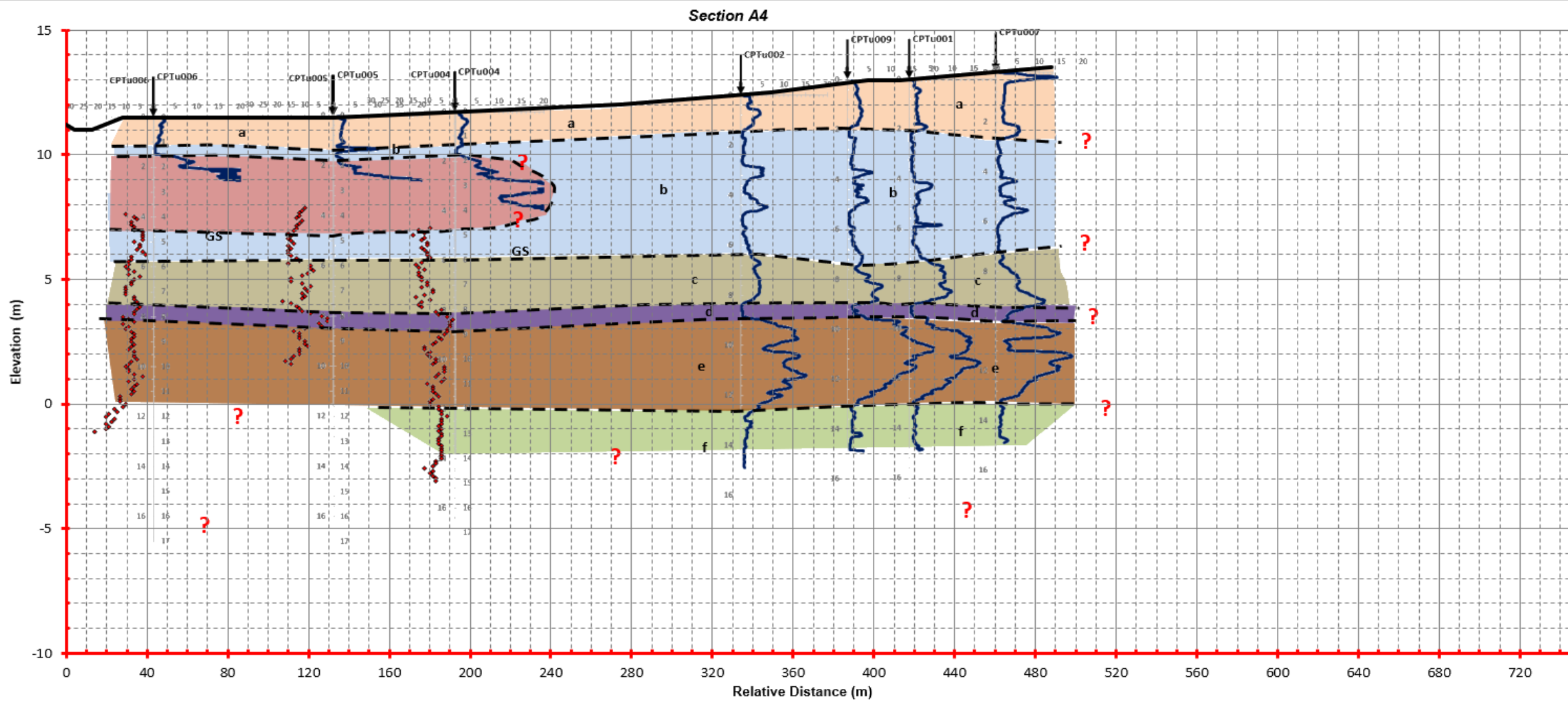
CLIENT:	YOURSECTION LTD
PROJECT No.:	200357
VERSION DATE:	16/10/2020
DRAWN:	CG
ENGINEER:	CG
APPROVED:	AG

SIZE: A3

**LOCATION PLAN**

SHEET No.: S1 REV. 1

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**LEGEND**

a	Silty SAND and sandy SILT, loose to firm
b	Clayey SILT, soft to firm, medium plasticity
c	Silty SAND, medium dense to dense with deth
GS	Gravelly SAND to sandy GRAVEL, dense
d	Clayey SILT to silty CLAY, firm
e	SAND, medium dense
f	Clayey SILT, firm to stiff
s	Gravelly SAND, very dense

**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**

**REVISION HISTORY**

REV	DATE	DESCRIPTION
1	19/10/20	FINAL

CLIENT: YOURSECTION LTD  
 PROJECT No.: 200357  
 VERSION DATE: 16/10/2020  
 DRAWN: CG  
 ENGINEER: CG  
 APPROVED: AG

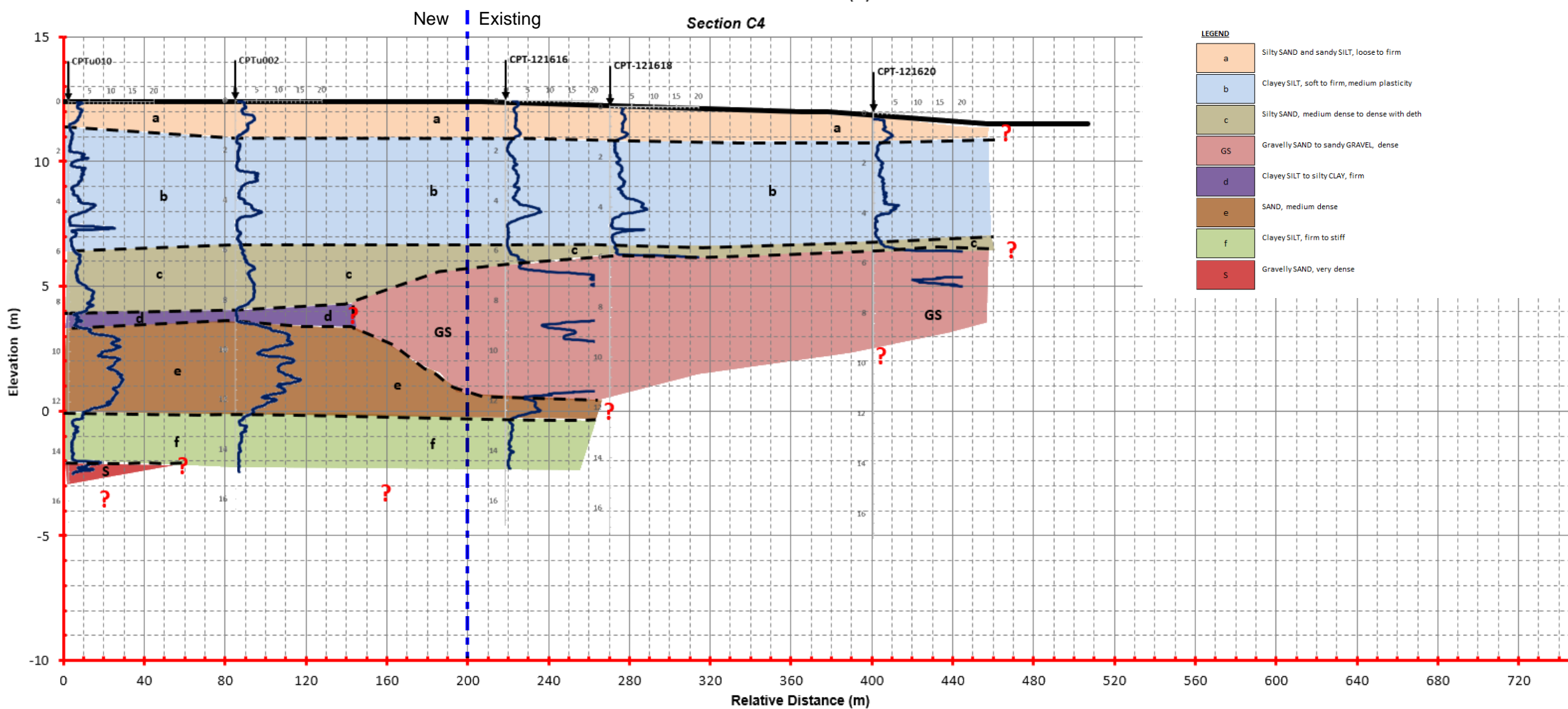
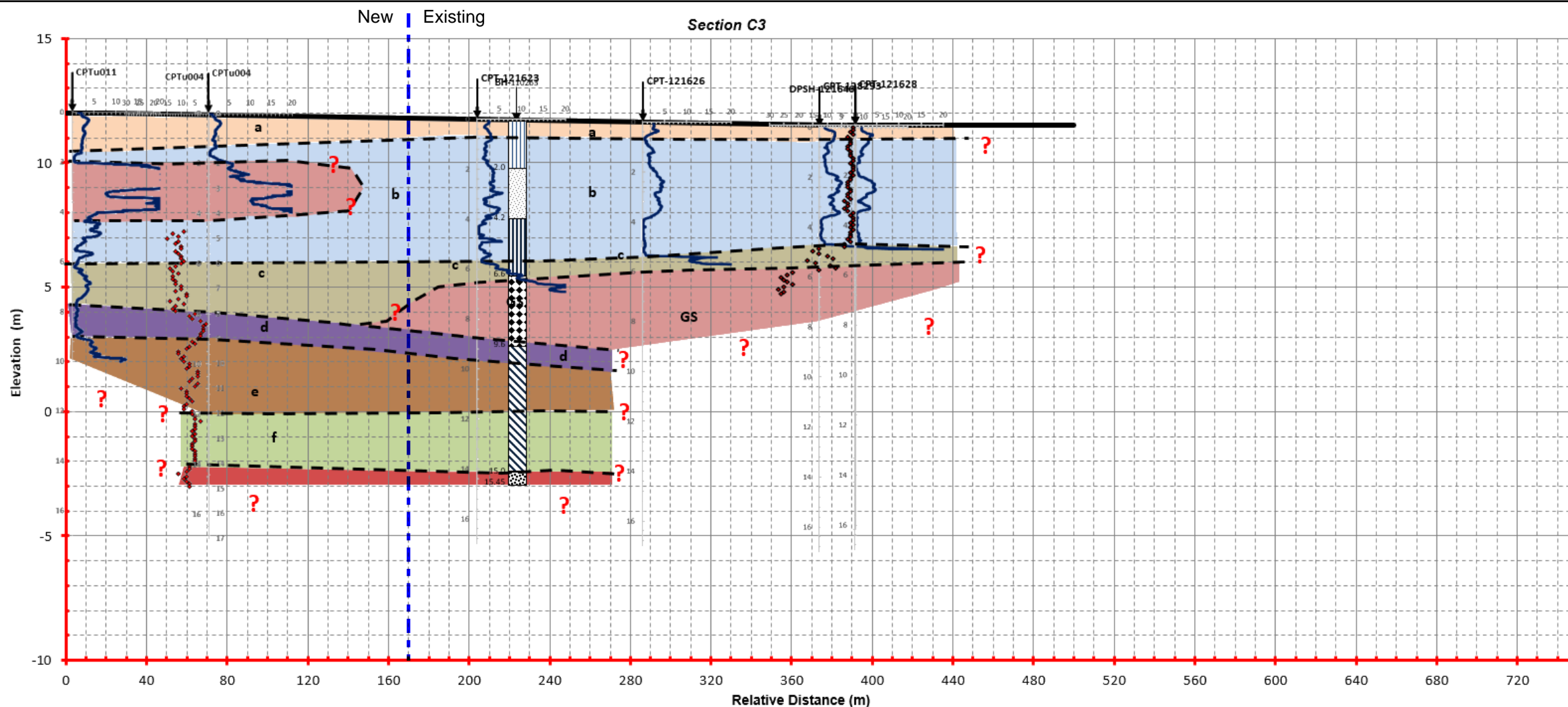
SIZE: A3  
**GROUND MODEL SHEET 1**

SHEET No.: S2.1 REV. 1

**miyamoto.**

T: 64 03 377 4095  
 miyamoto.nz  
 236 Hereford Street,  
 PO BOX 137 Cashel Street  
 Christchurch 8011  
 projects@miyamoto.nz

**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**



**LEGEND**

a	Silty SAND and sandy SILT, loose to firm
b	Clayey SILT, soft to firm, medium plasticity
c	Silty SAND, medium dense to dense with deth
GS	Gravelly SAND to sandy GRAVEL, dense
d	Clayey SILT to silty CLAY, firm
e	SAND, medium dense
f	Clayey SILT, firm to stiff
s	Gravelly SAND, very dense

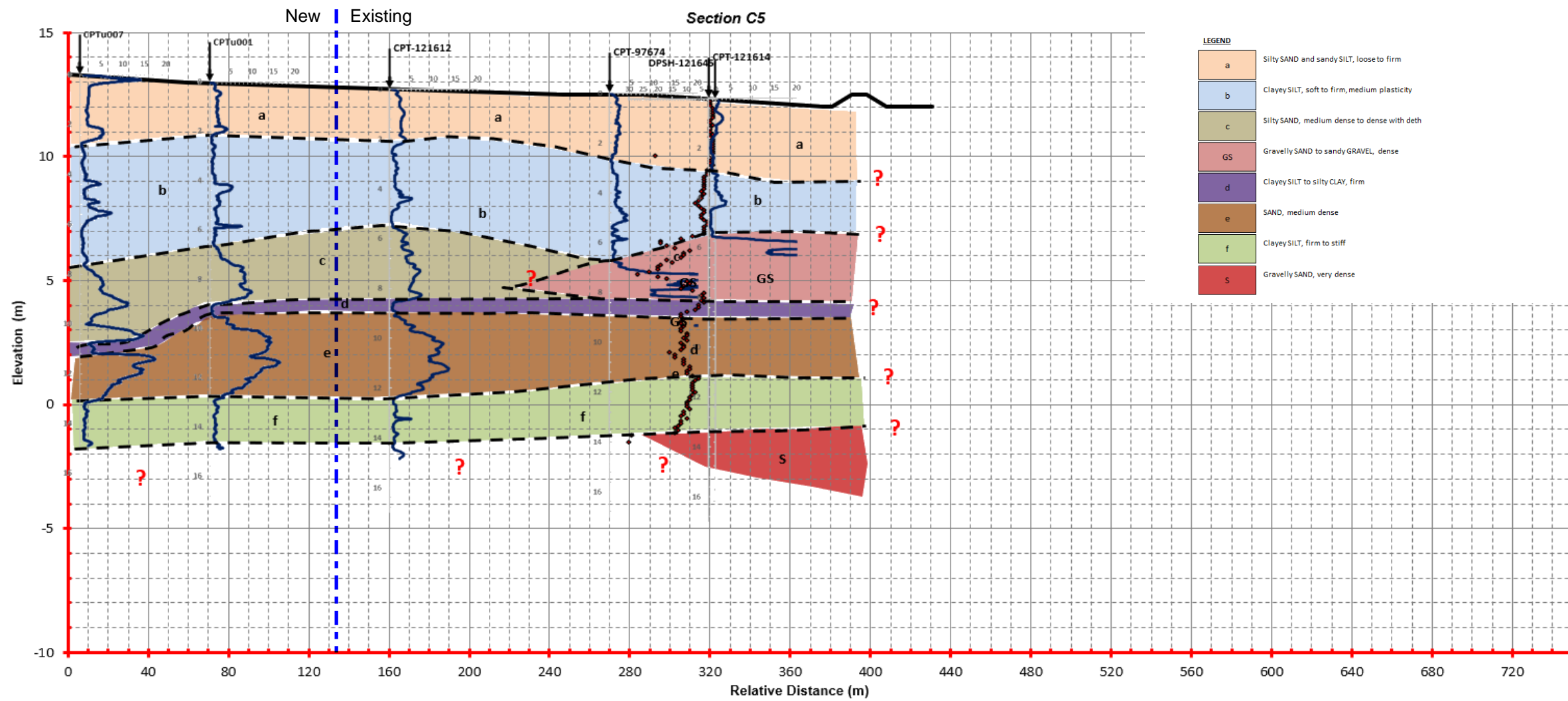
**REVISION HISTORY**

REV	DATE	DESCRIPTION
1	19/10/20	FINAL

CLIENT: YOURSECTION LTD  
PROJECT No.: 200357  
VERSION DATE: 16/10/2020  
DRAWN: CG  
ENGINEER: CG  
APPROVED: AG

SIZE: A3  
**GROUND MODEL SHEET 2**

SHEET No.: S2.2 REV. 1



# miyamoto.

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**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**

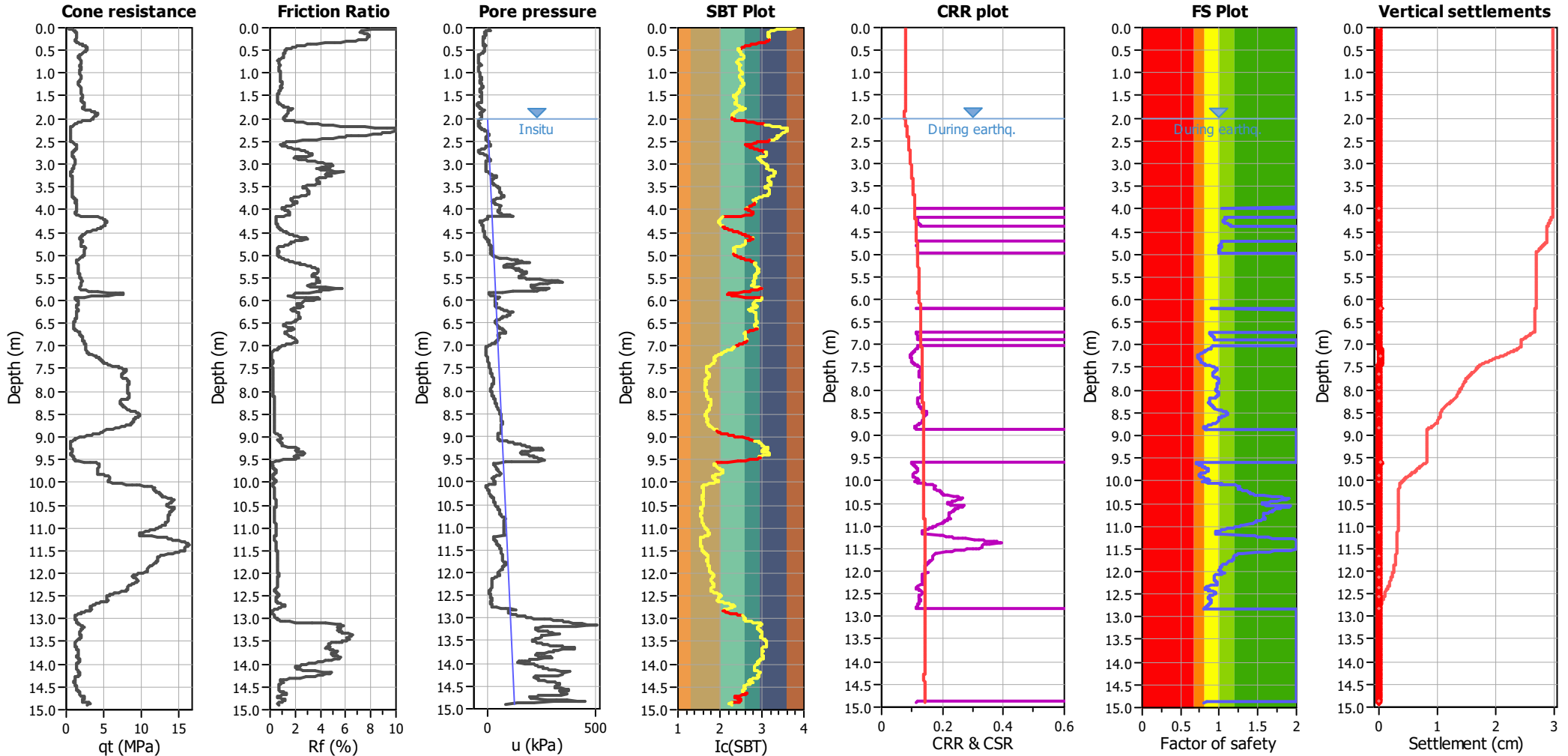
REVISION HISTORY		
REV	DATE	DESCRIPTION
1	19/10/20	FINAL

CLIENT:	YOURSECTION LTD
PROJECT No.:	200357
VERSION DATE:	16/10/2020
DRAWN:	CG
ENGINEER:	CG
APPROVED:	AG

SIZE: A3  
**GROUND MODEL**  
**SHEET 3**  
 SHEET No.: S2.3 REV. 1

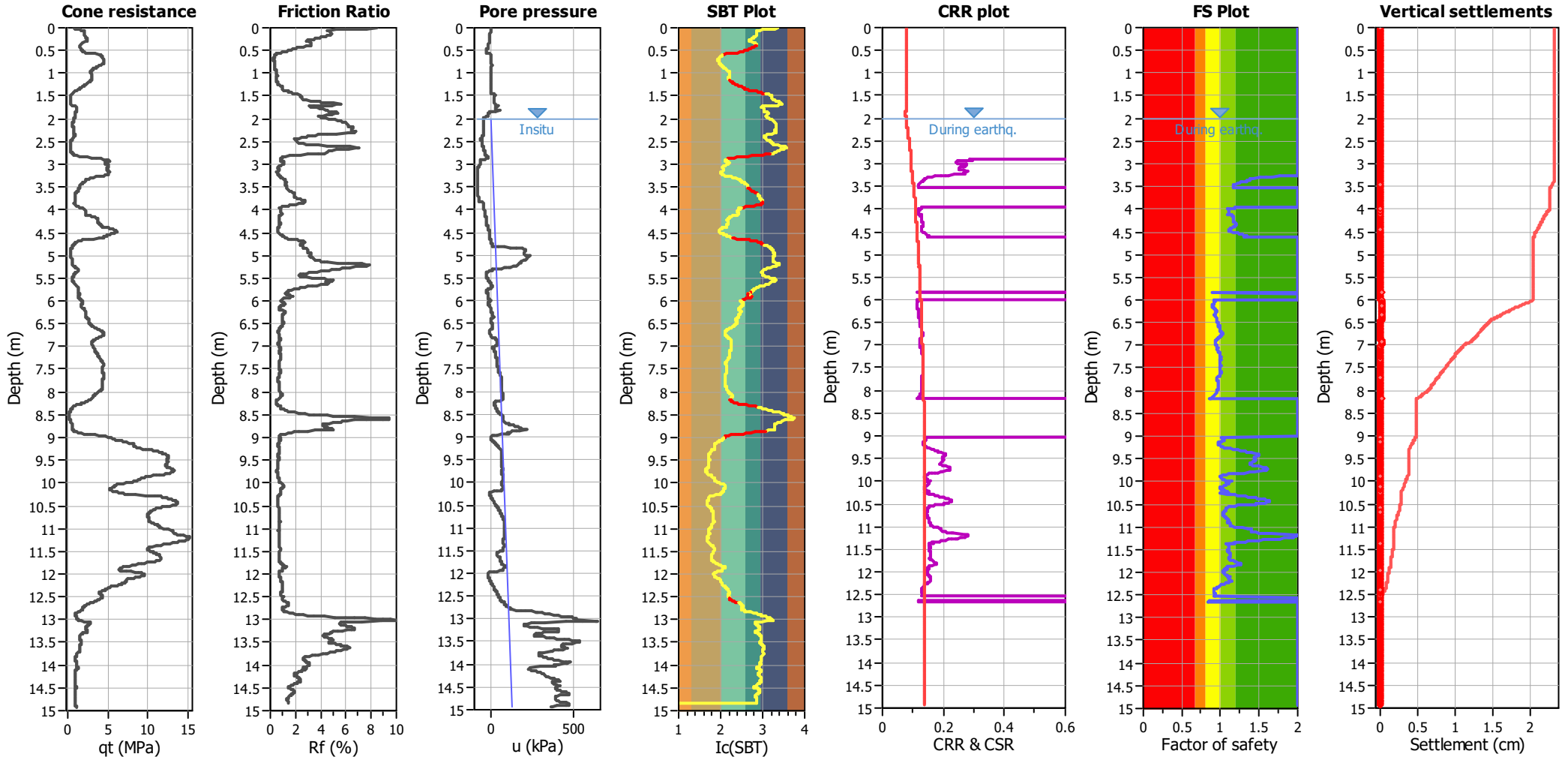
## F. Liquefaction Analyses



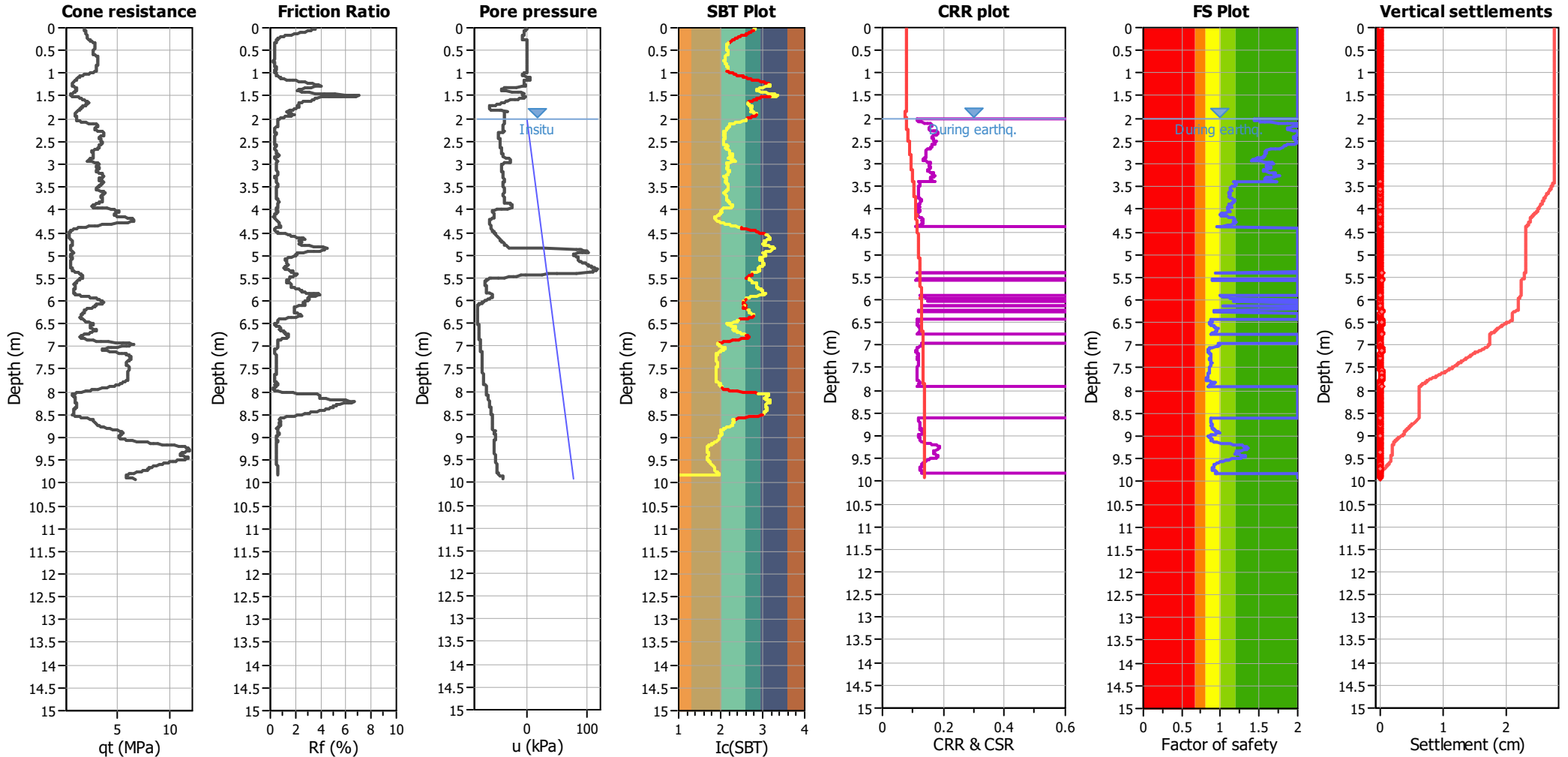


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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

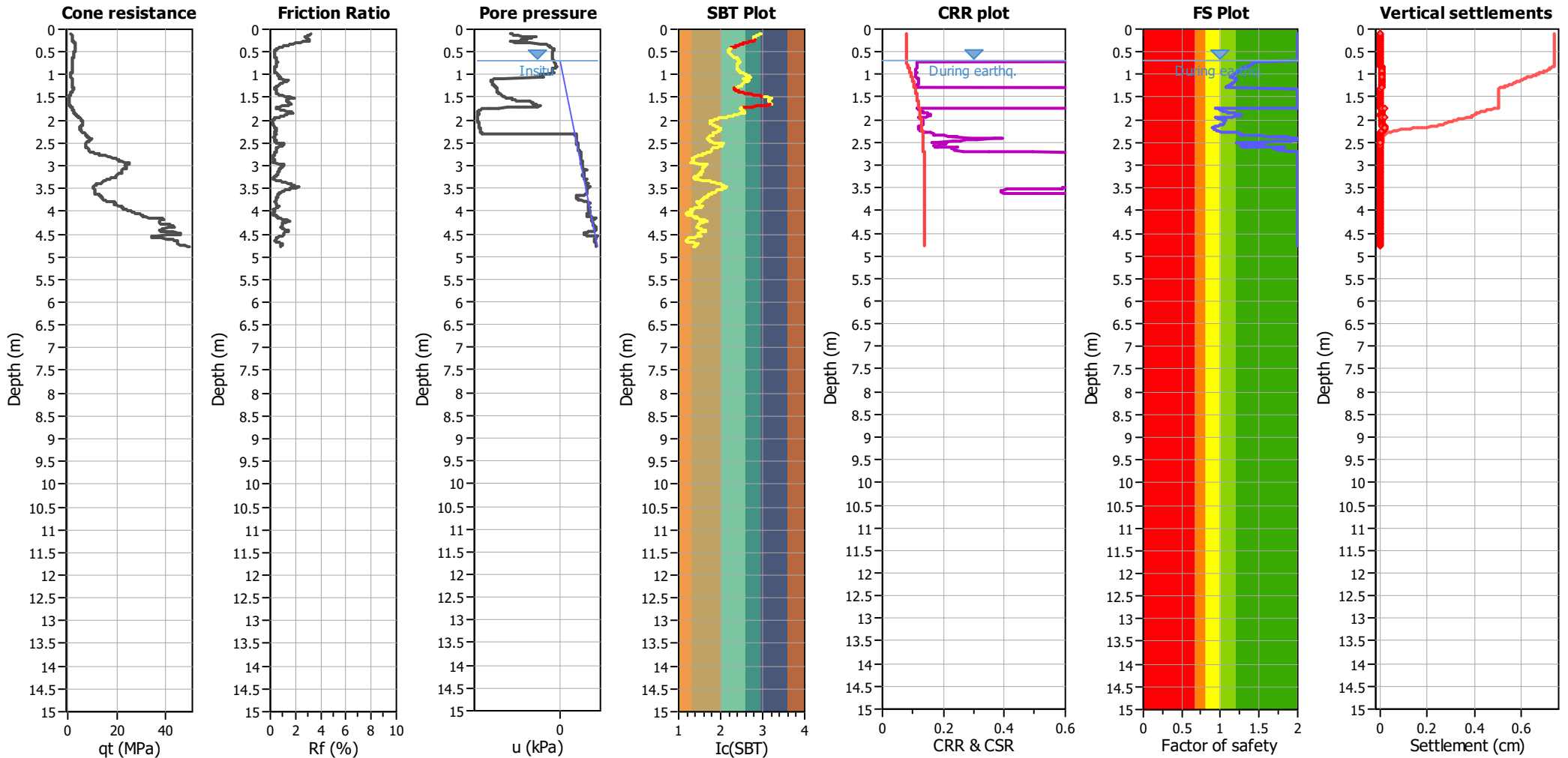




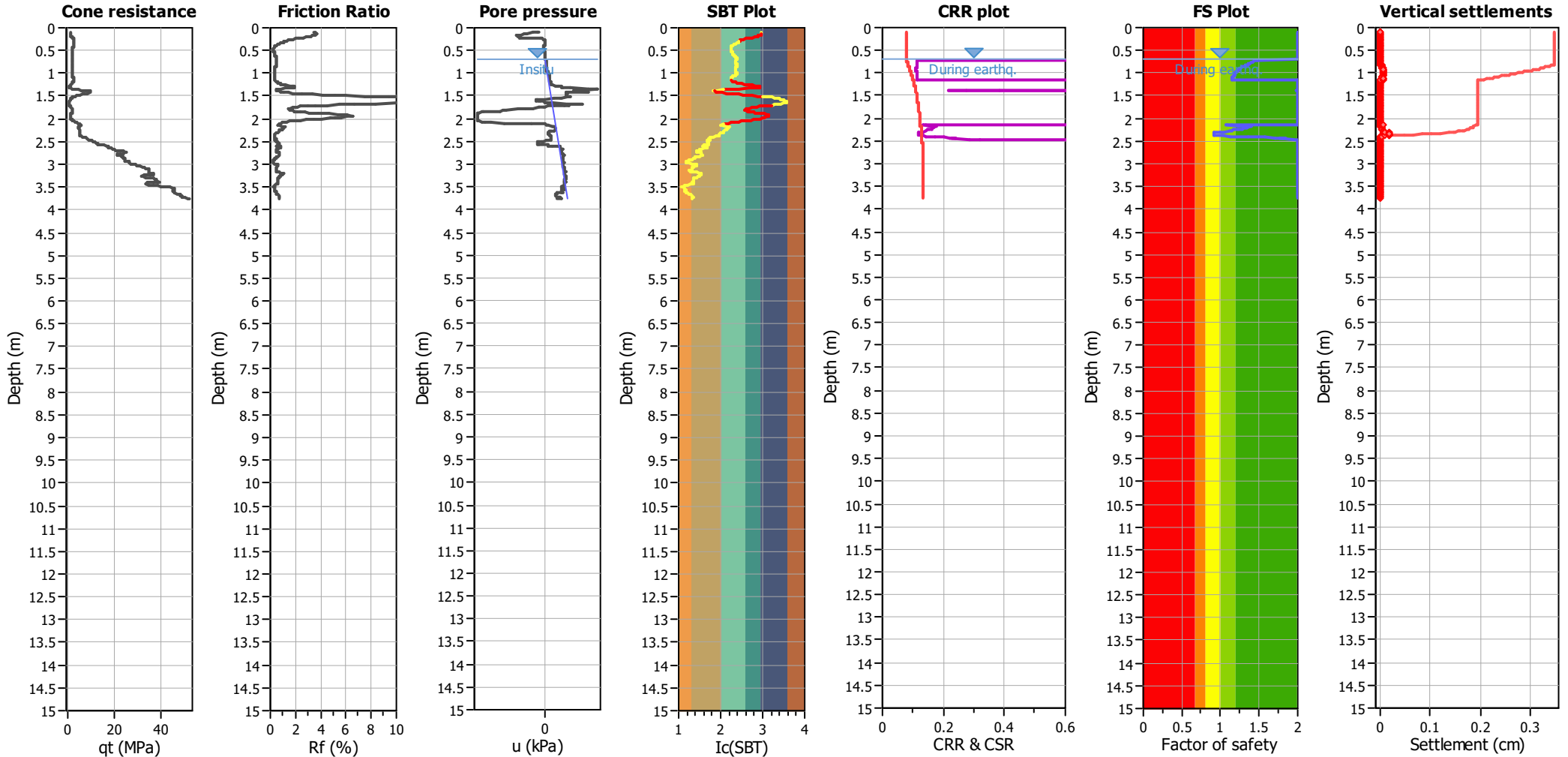
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



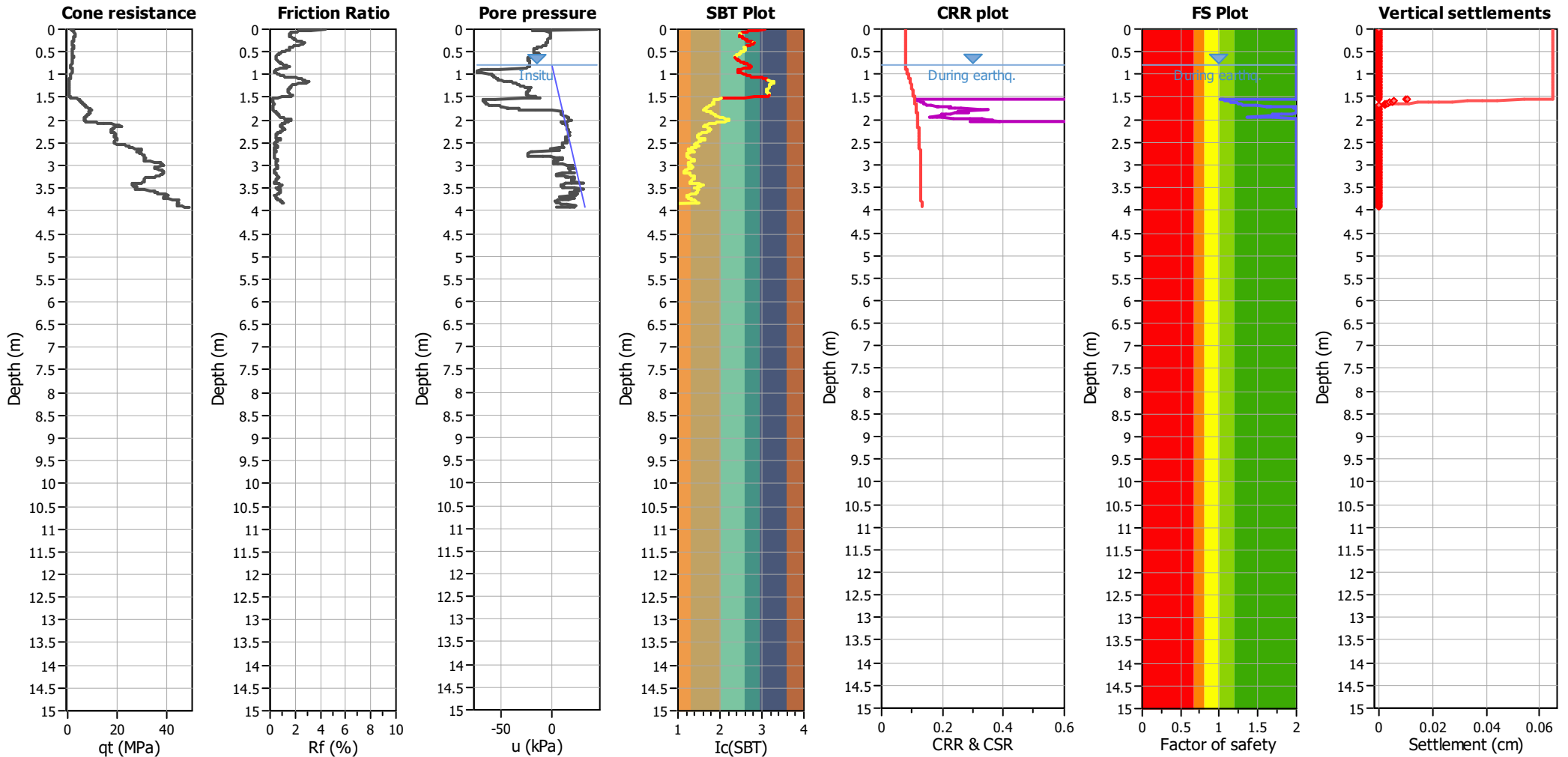
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



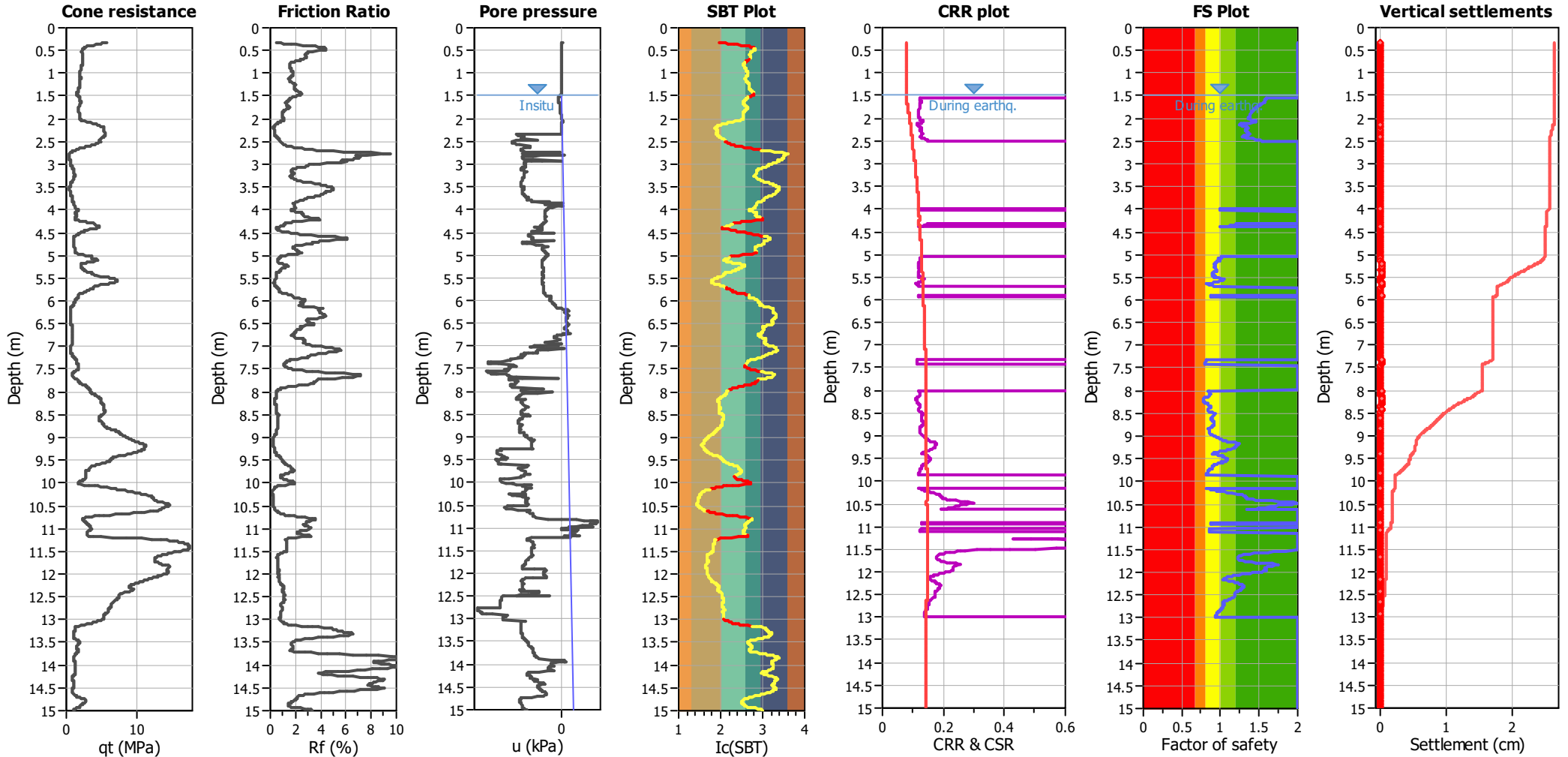
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



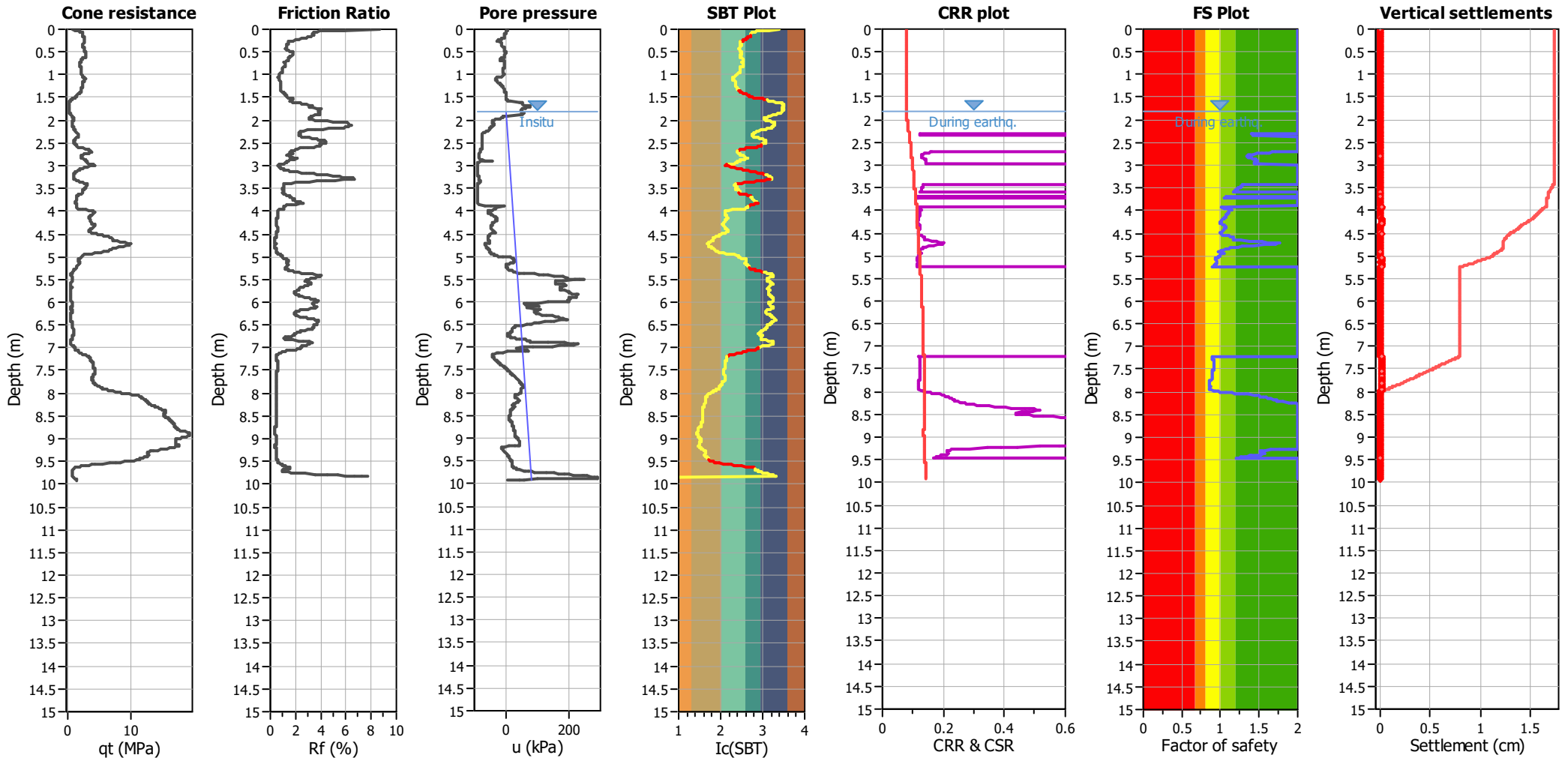
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



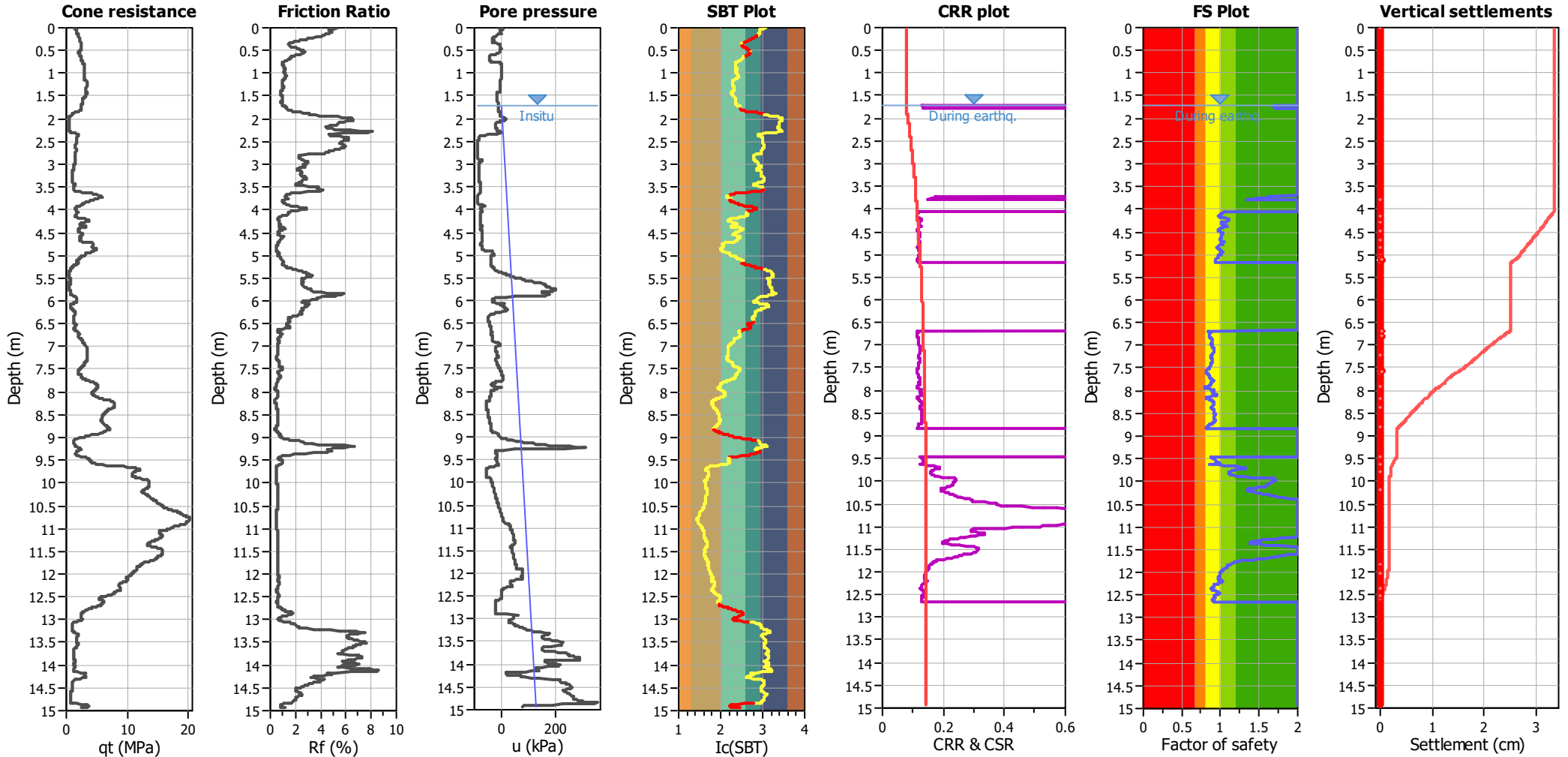
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.50 m	Use fill:	No	Clay like behavior	
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

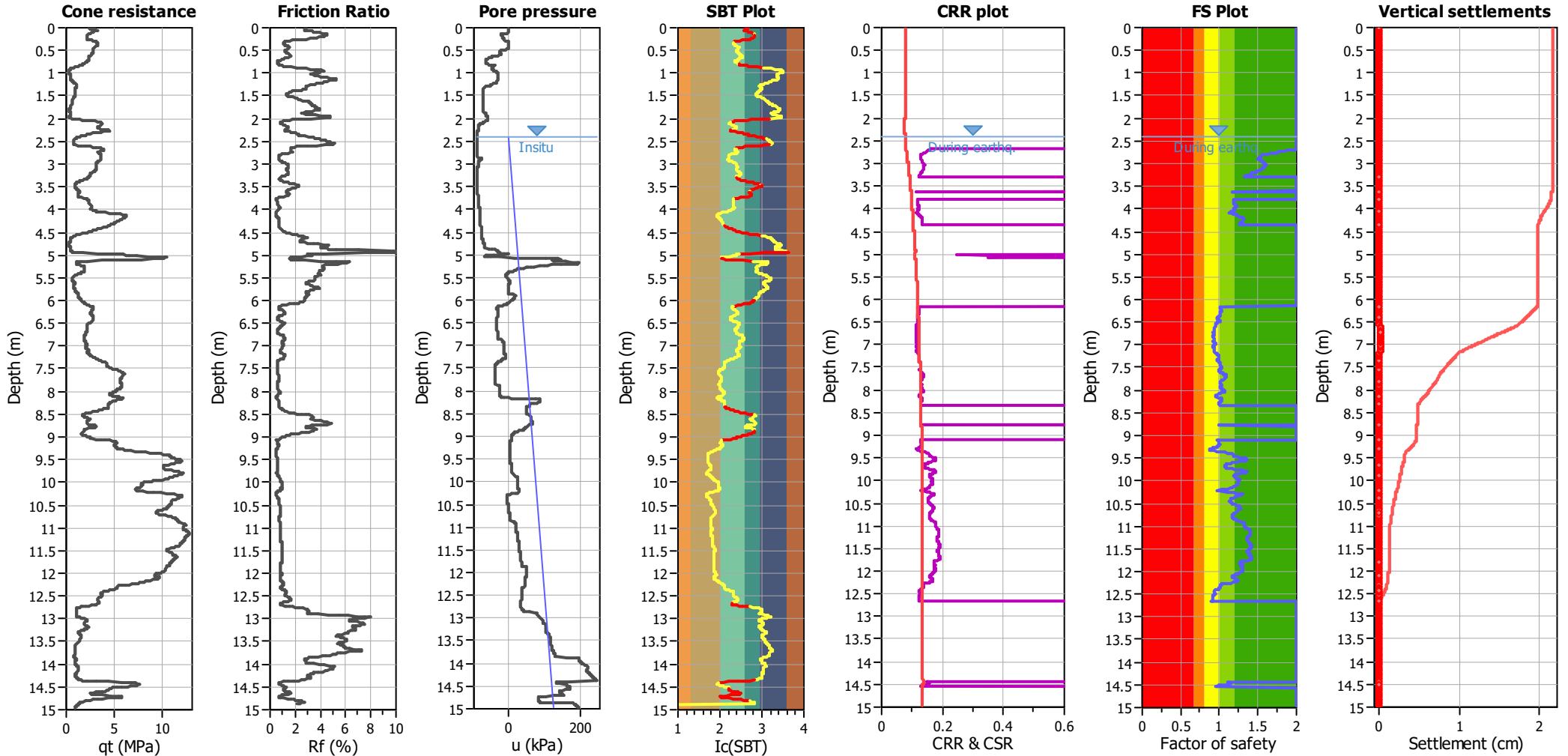


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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

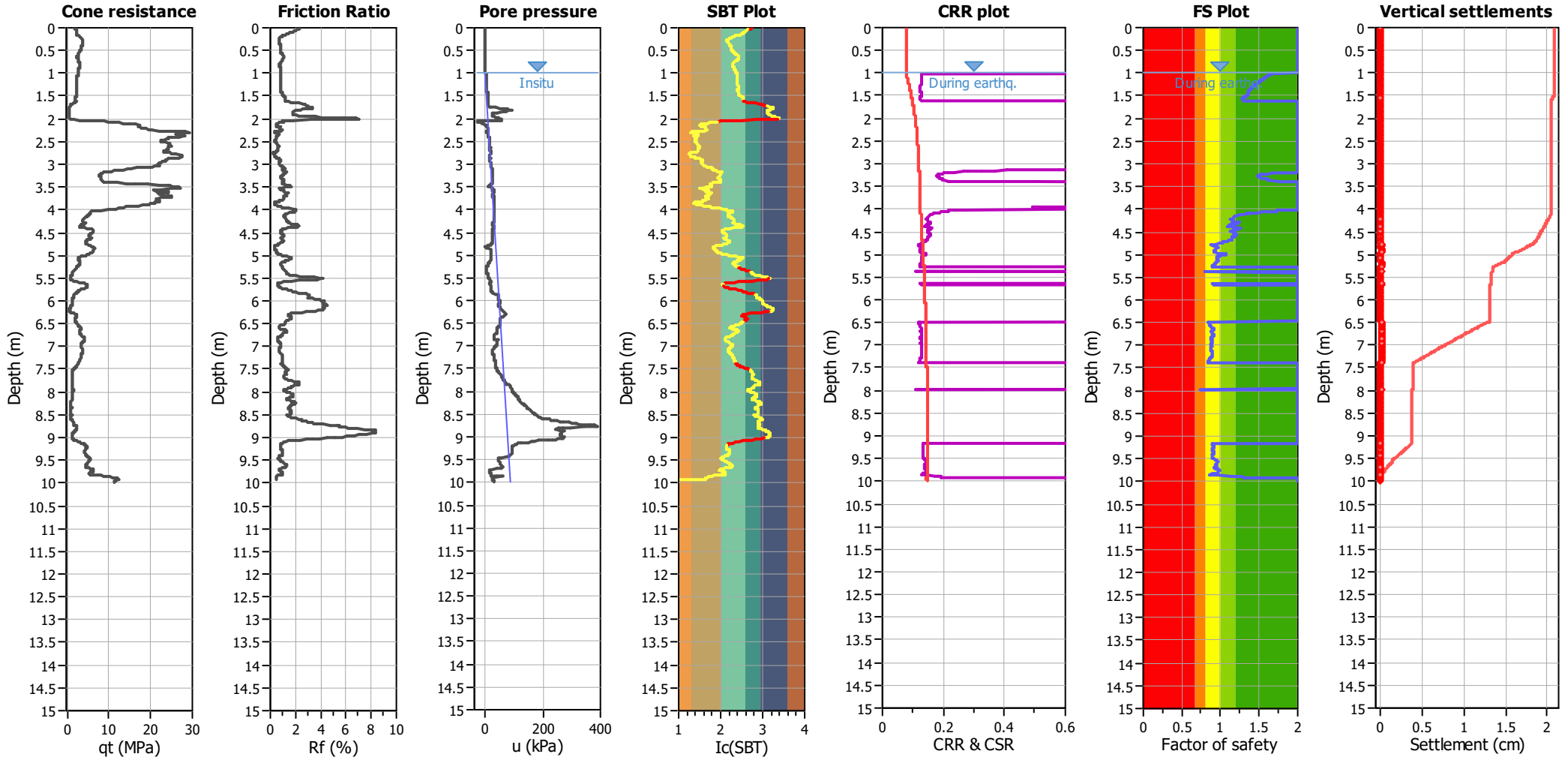


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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_\sigma$ applied:	Yes	MSF method:	Method based

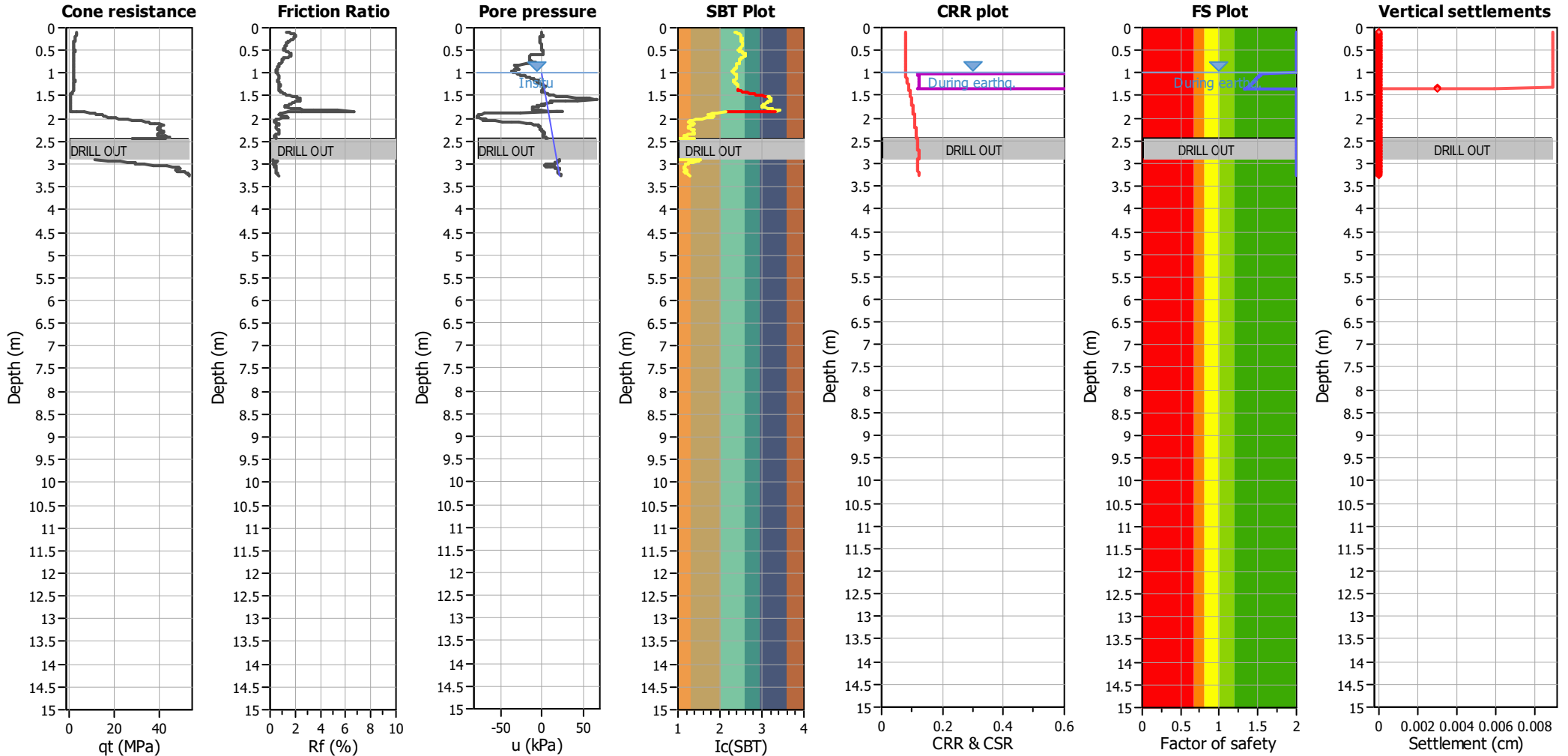




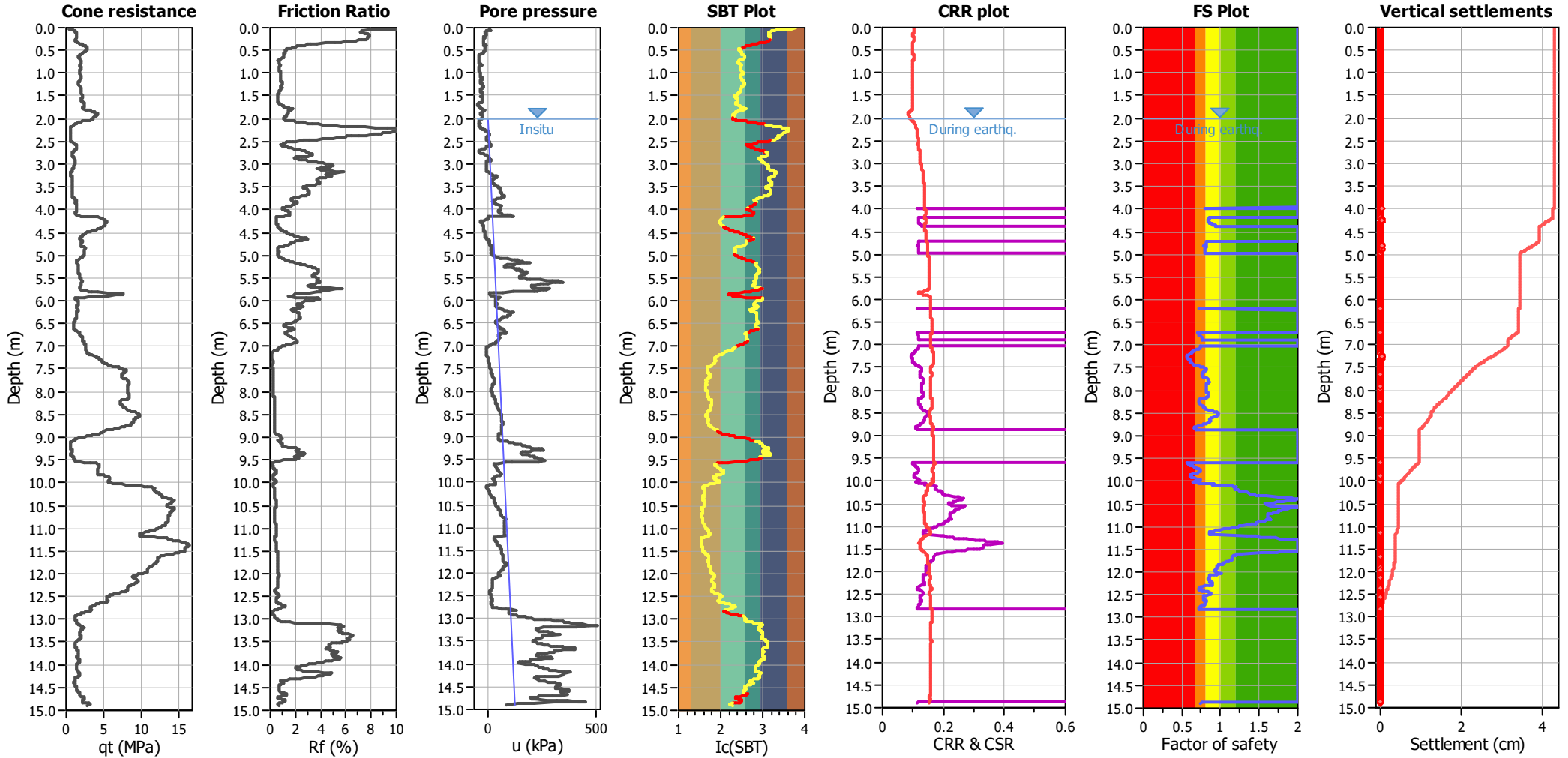
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



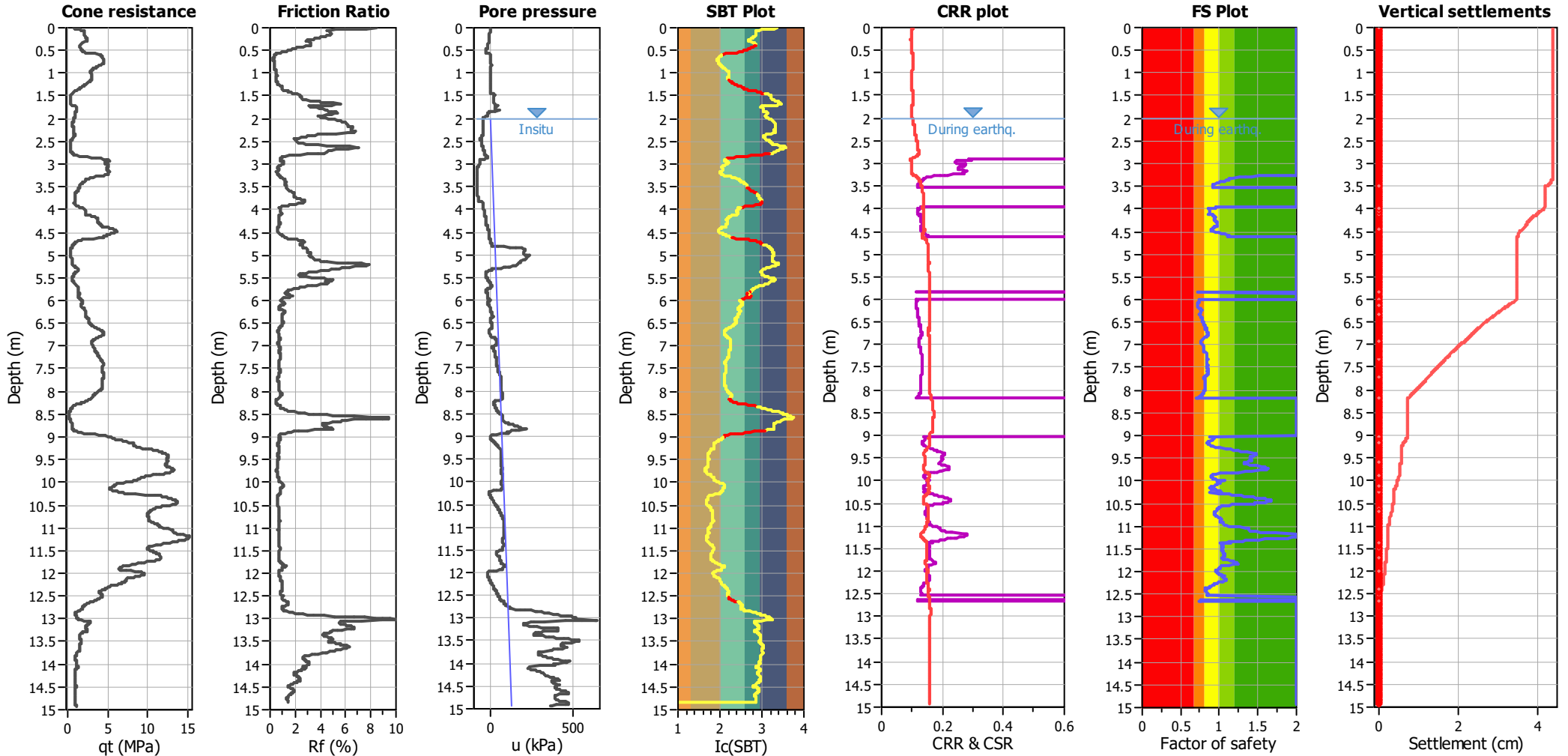
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



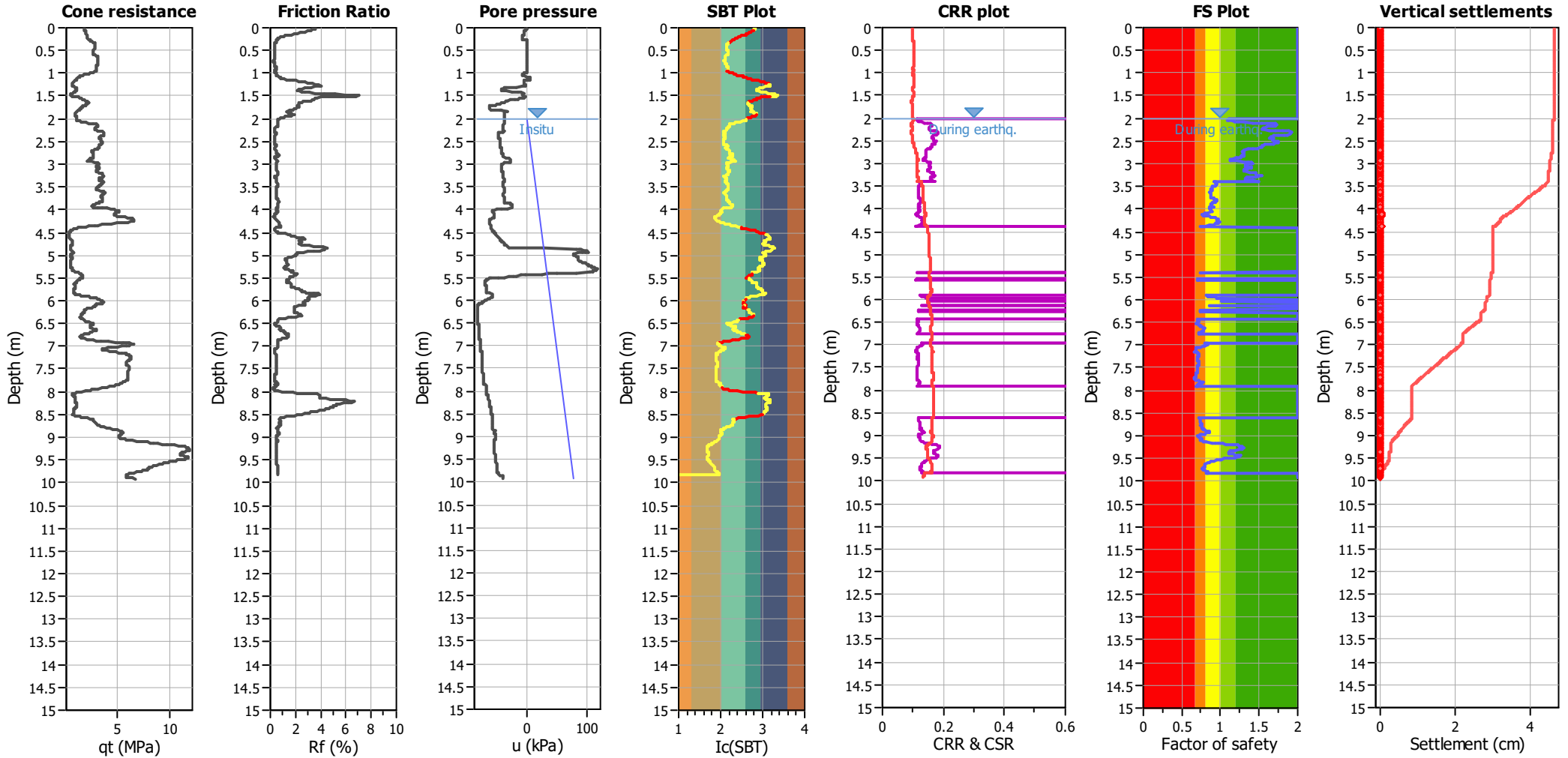
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



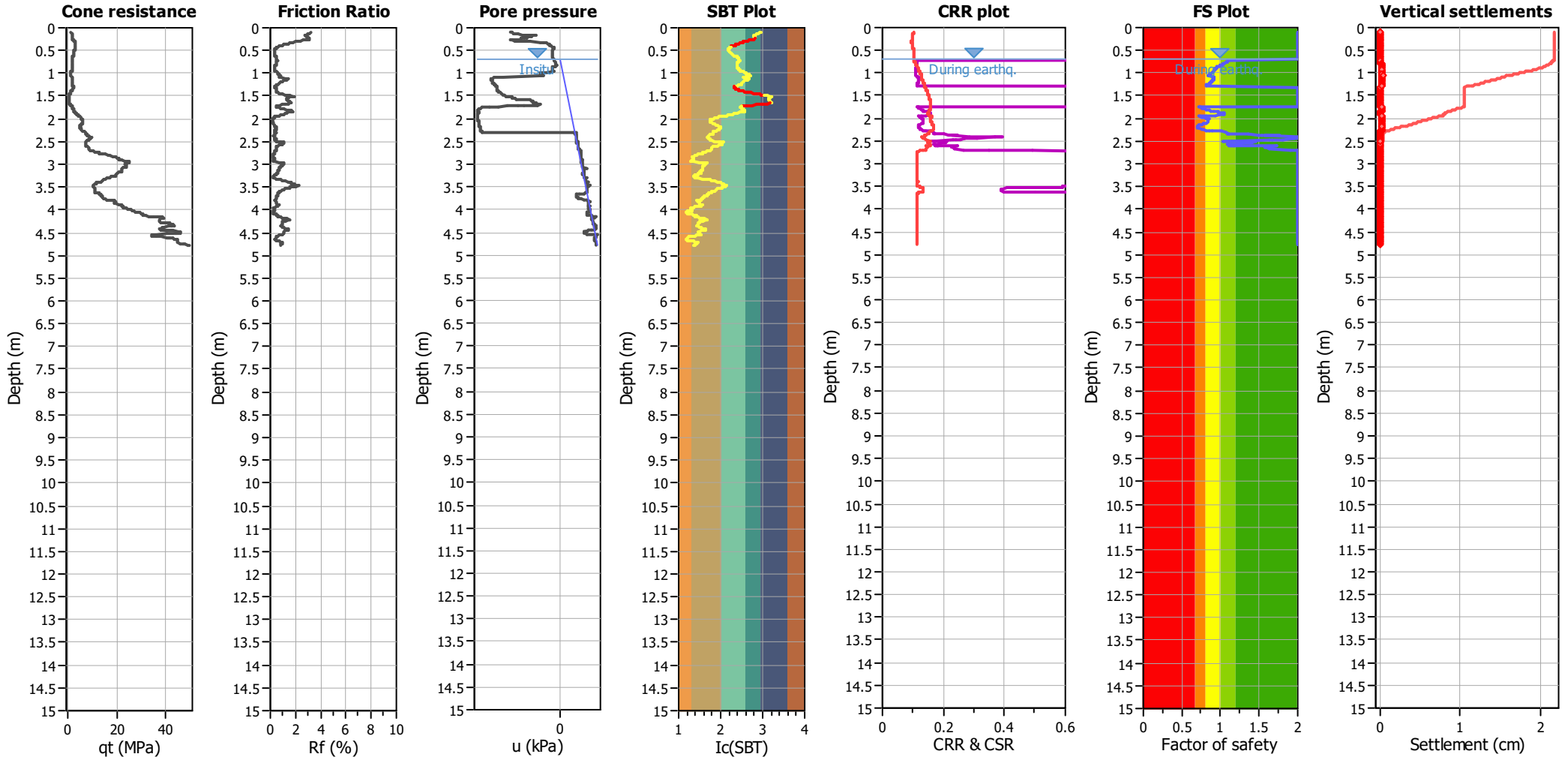
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



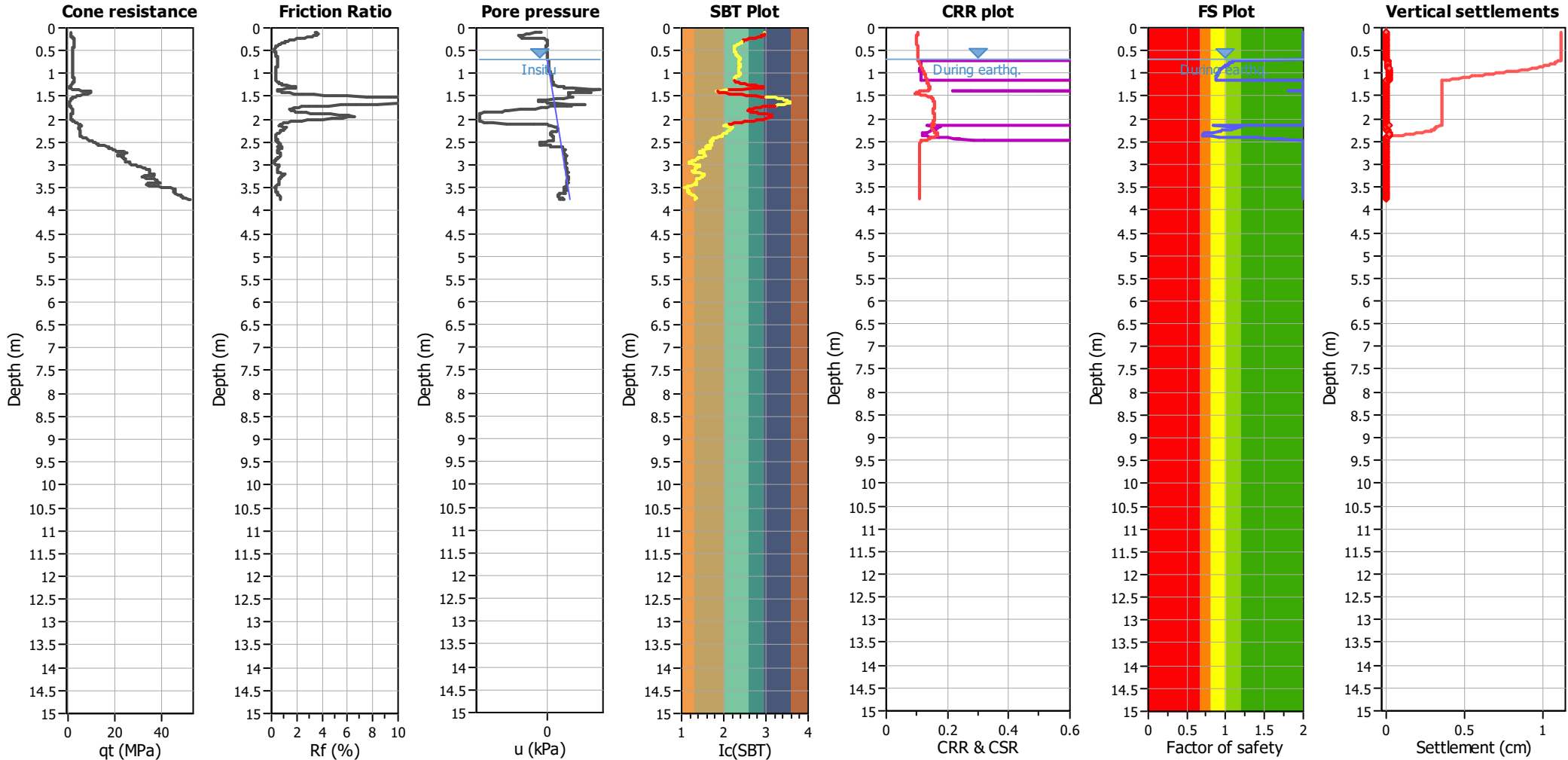
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.00 m	Use fill:	No	Clay like behavior	
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

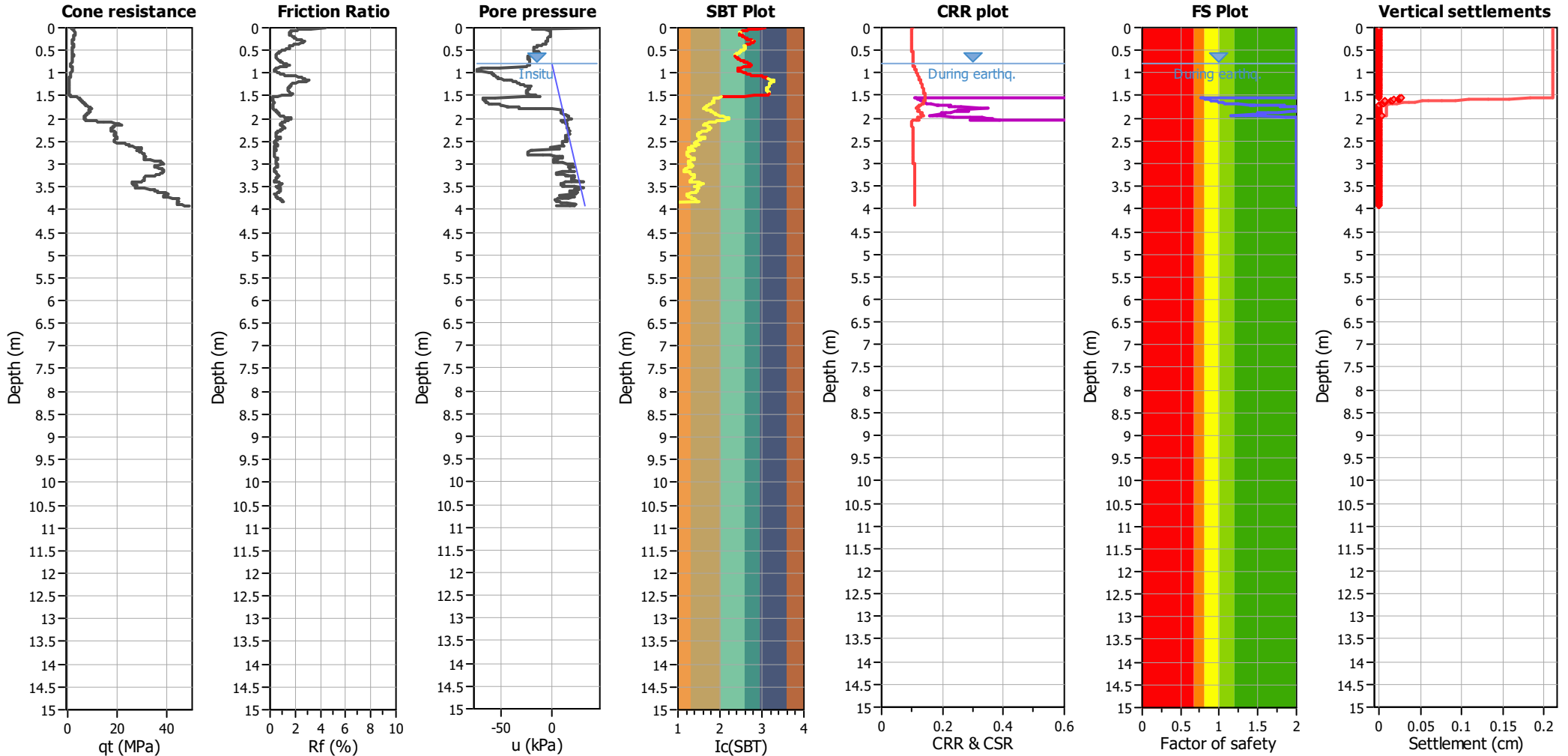


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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

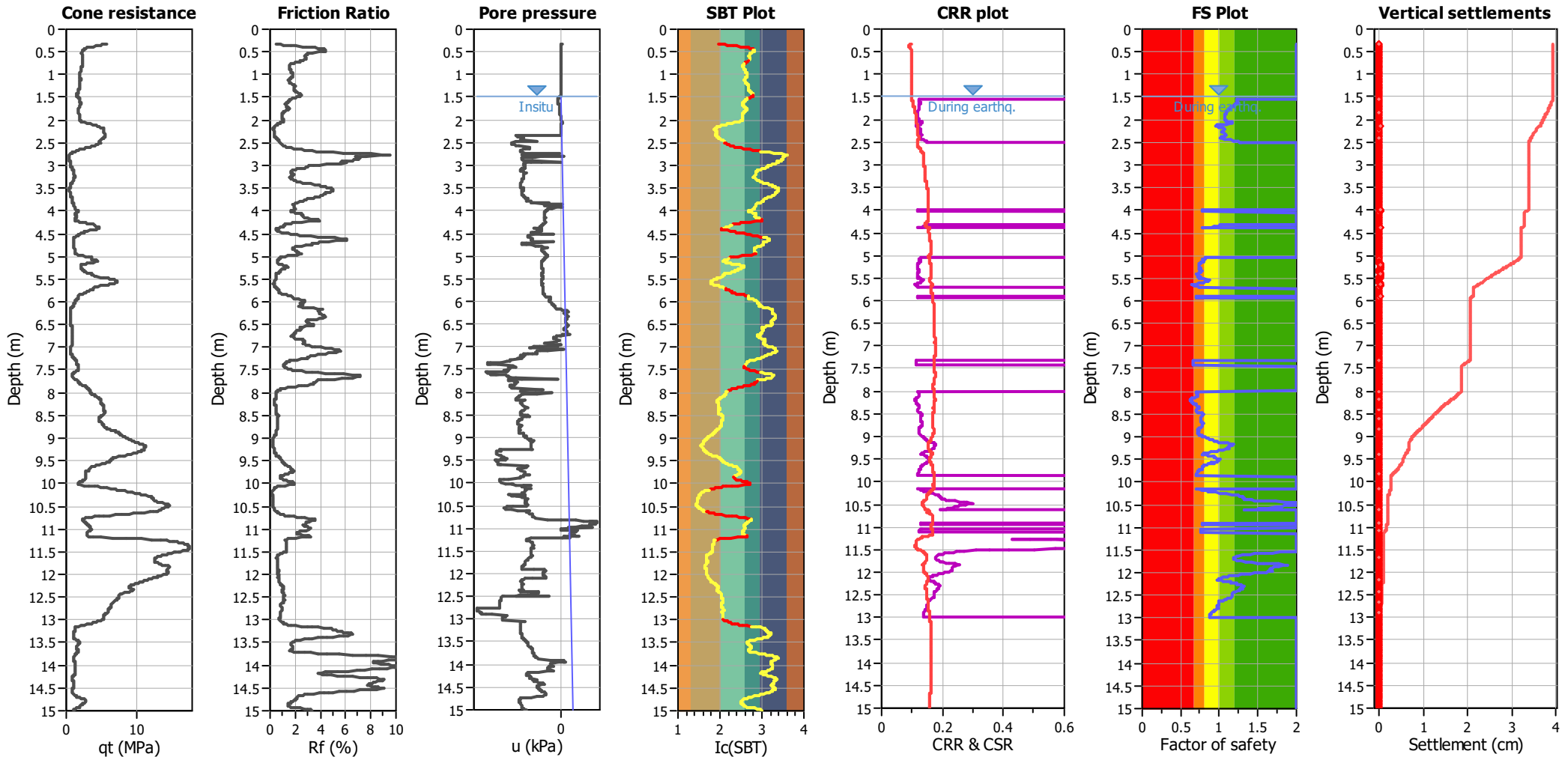


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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

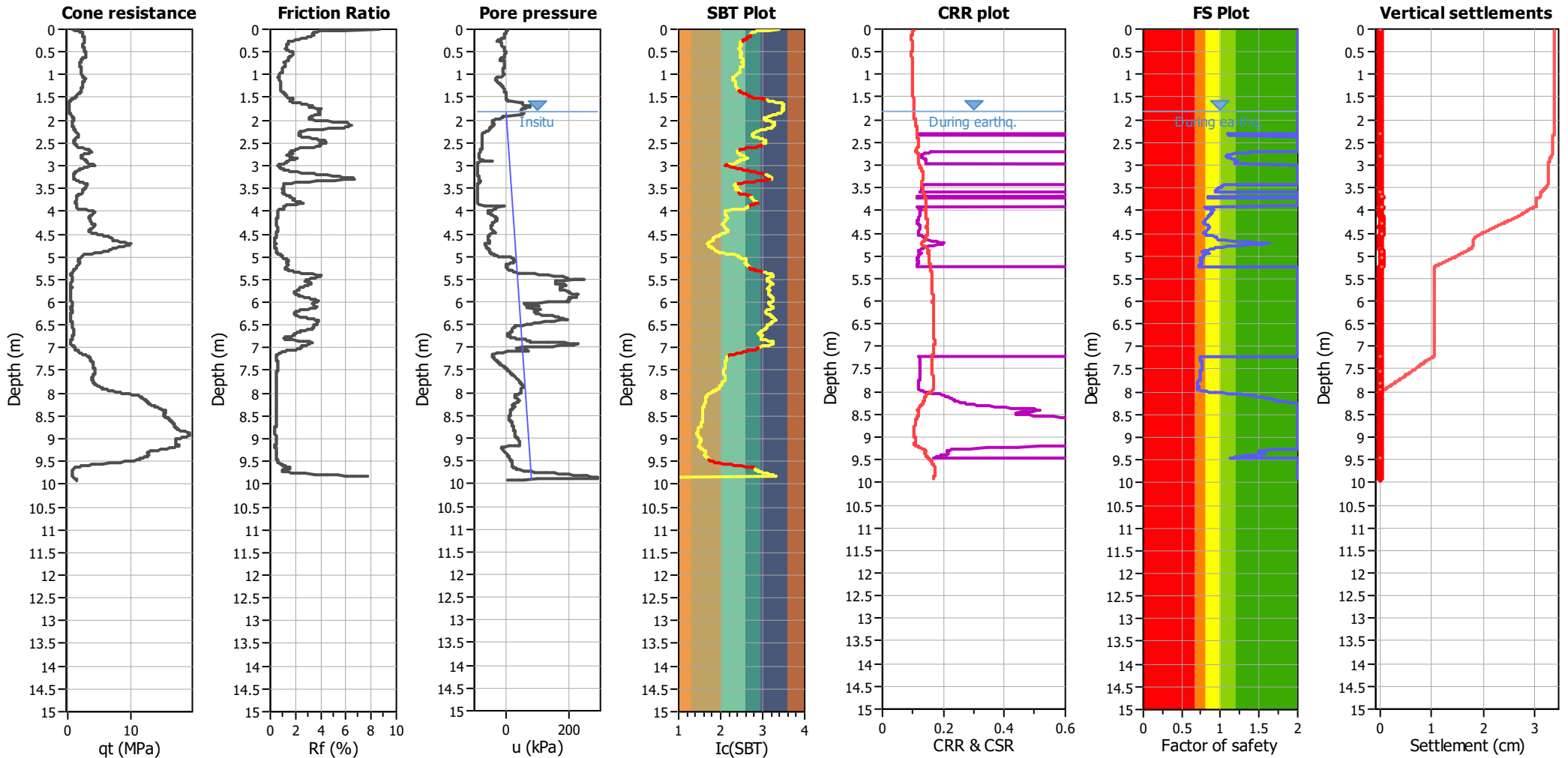




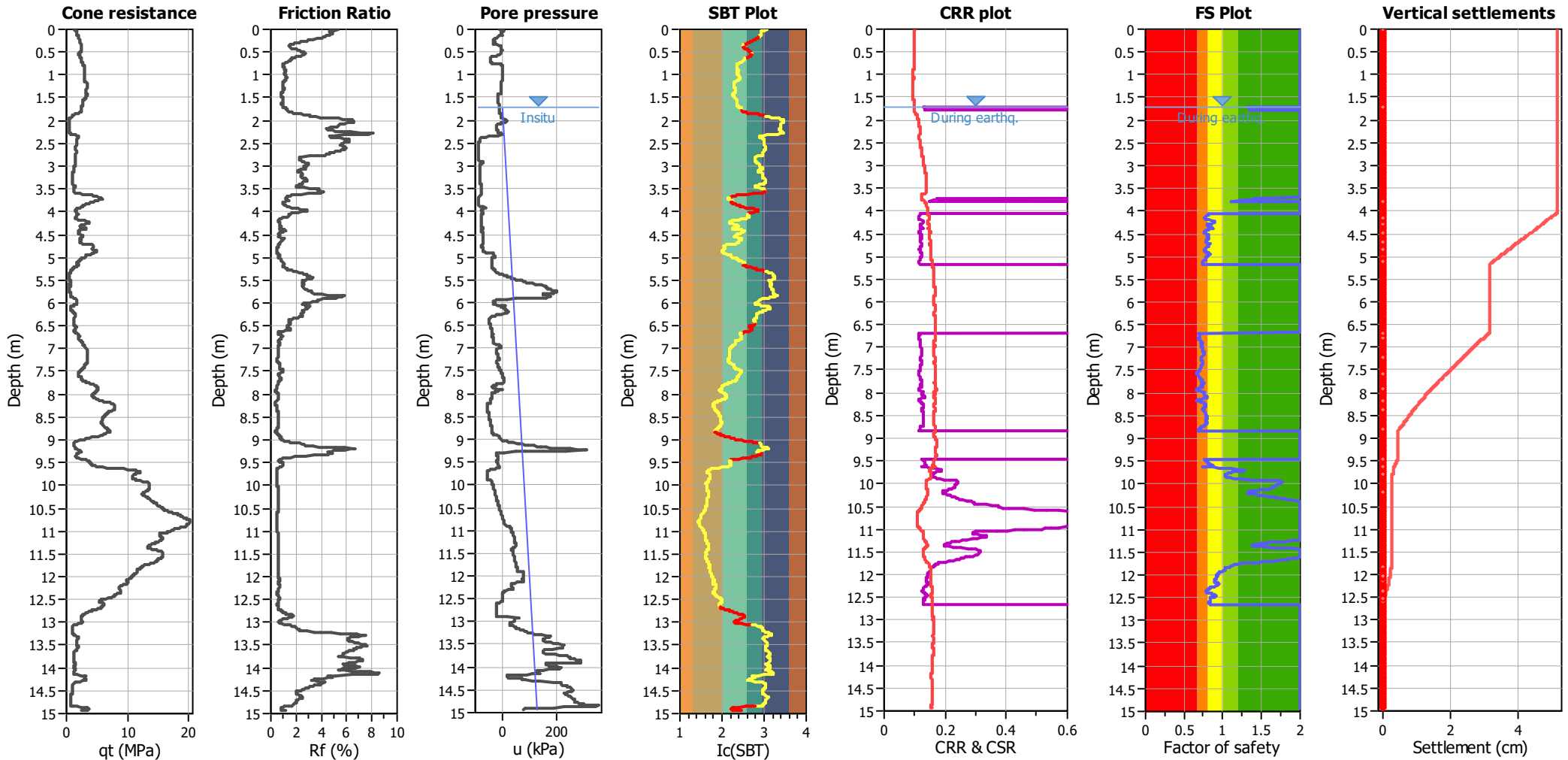
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



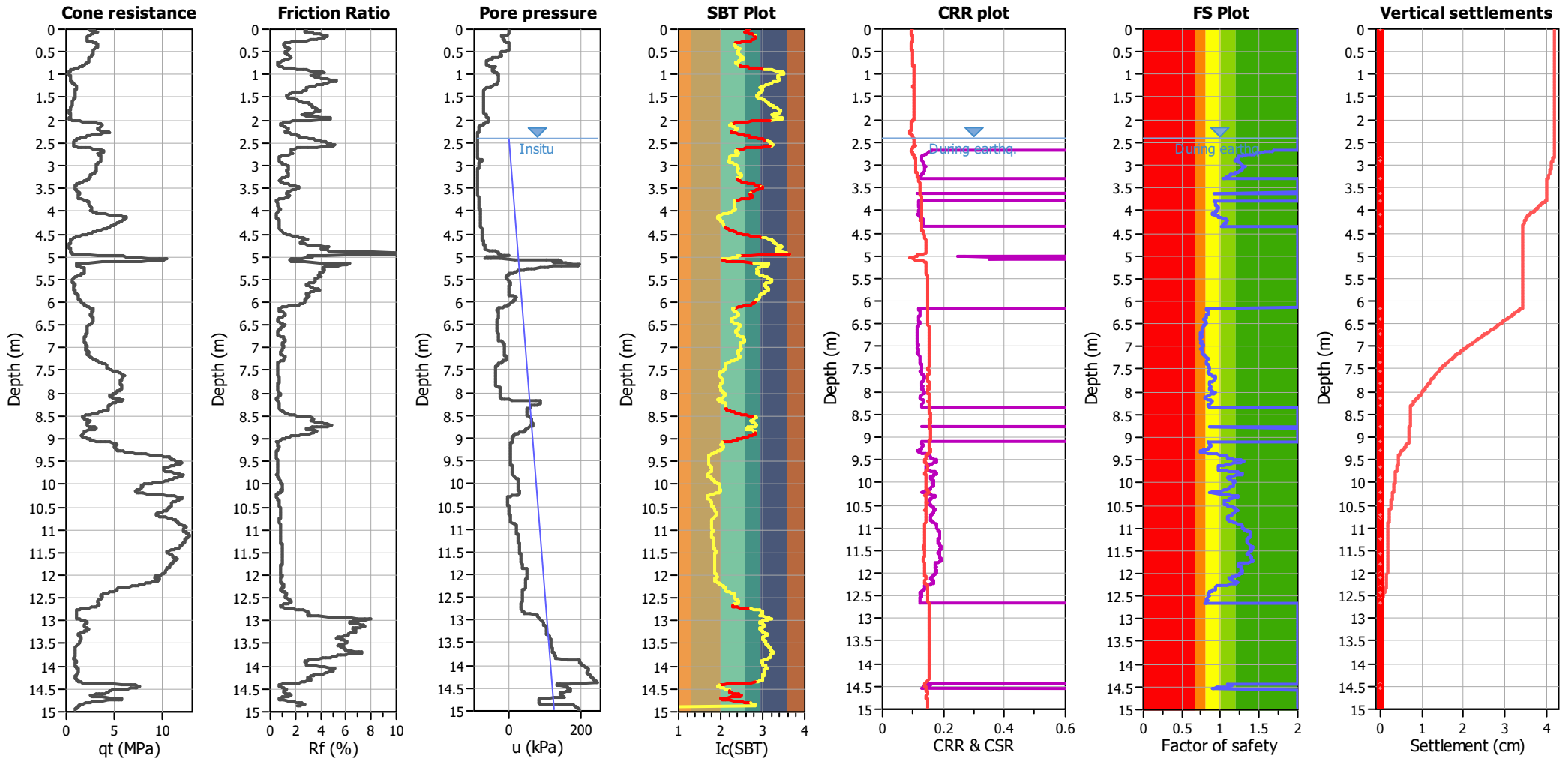
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



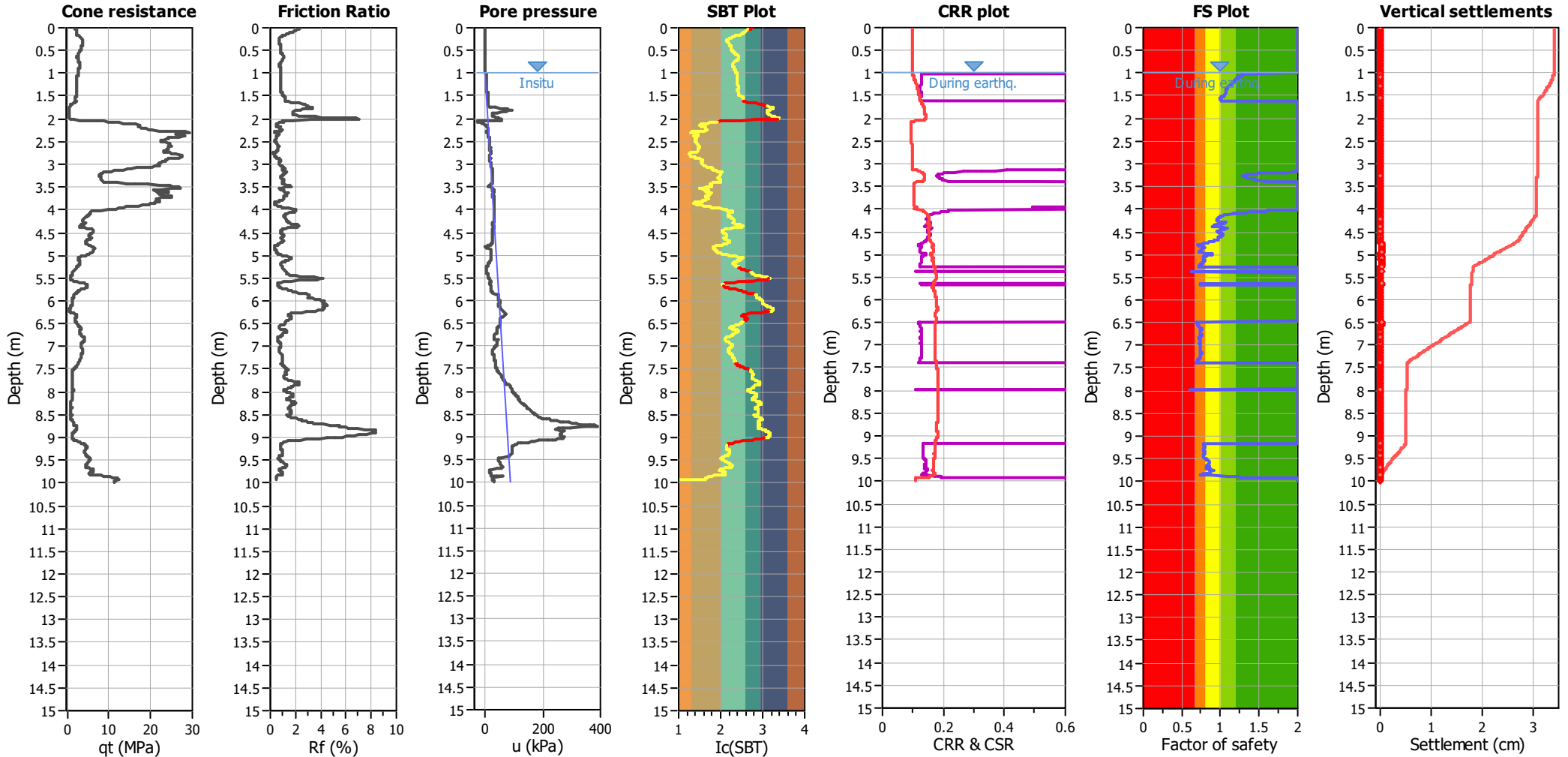
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



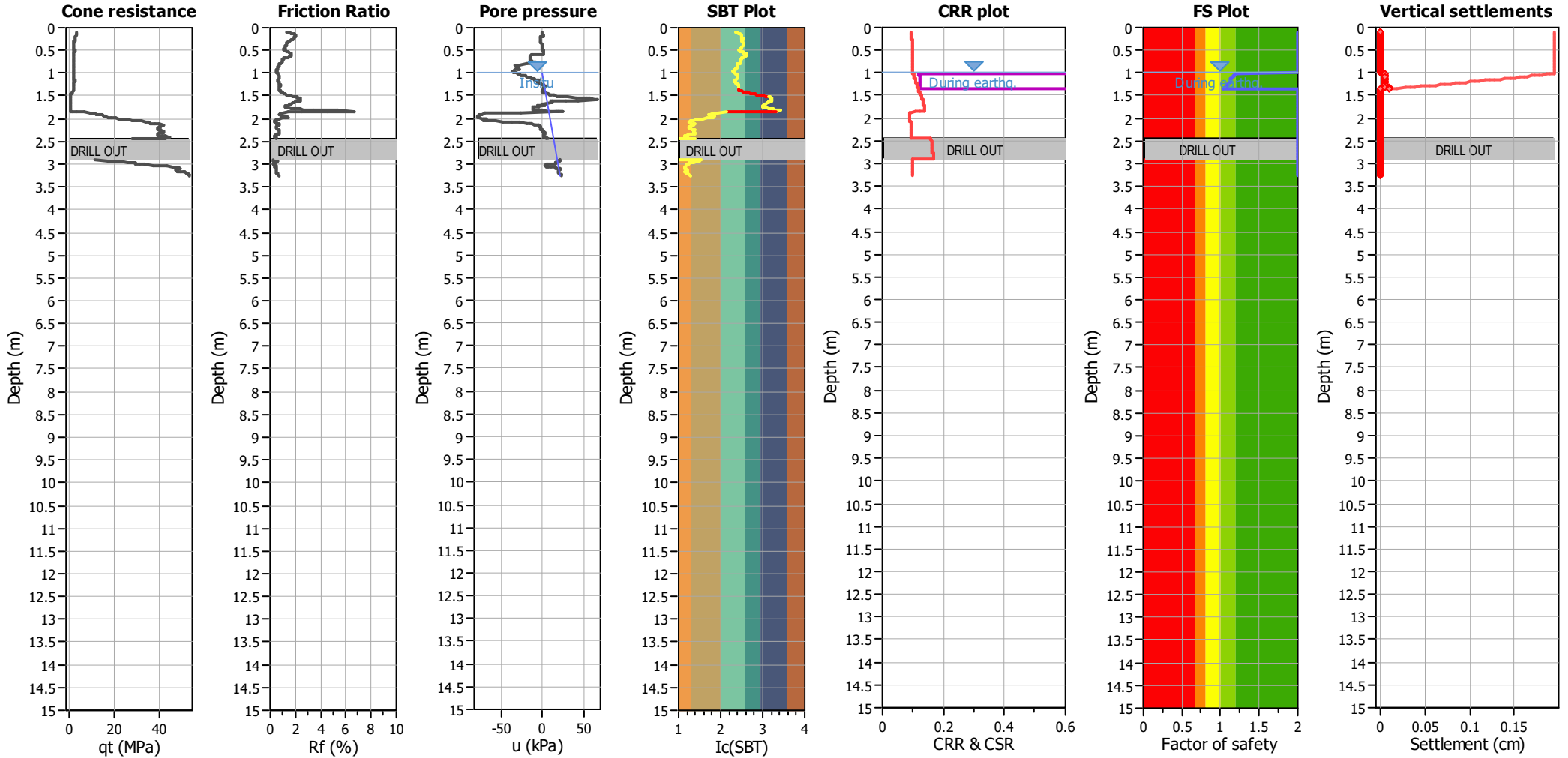
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



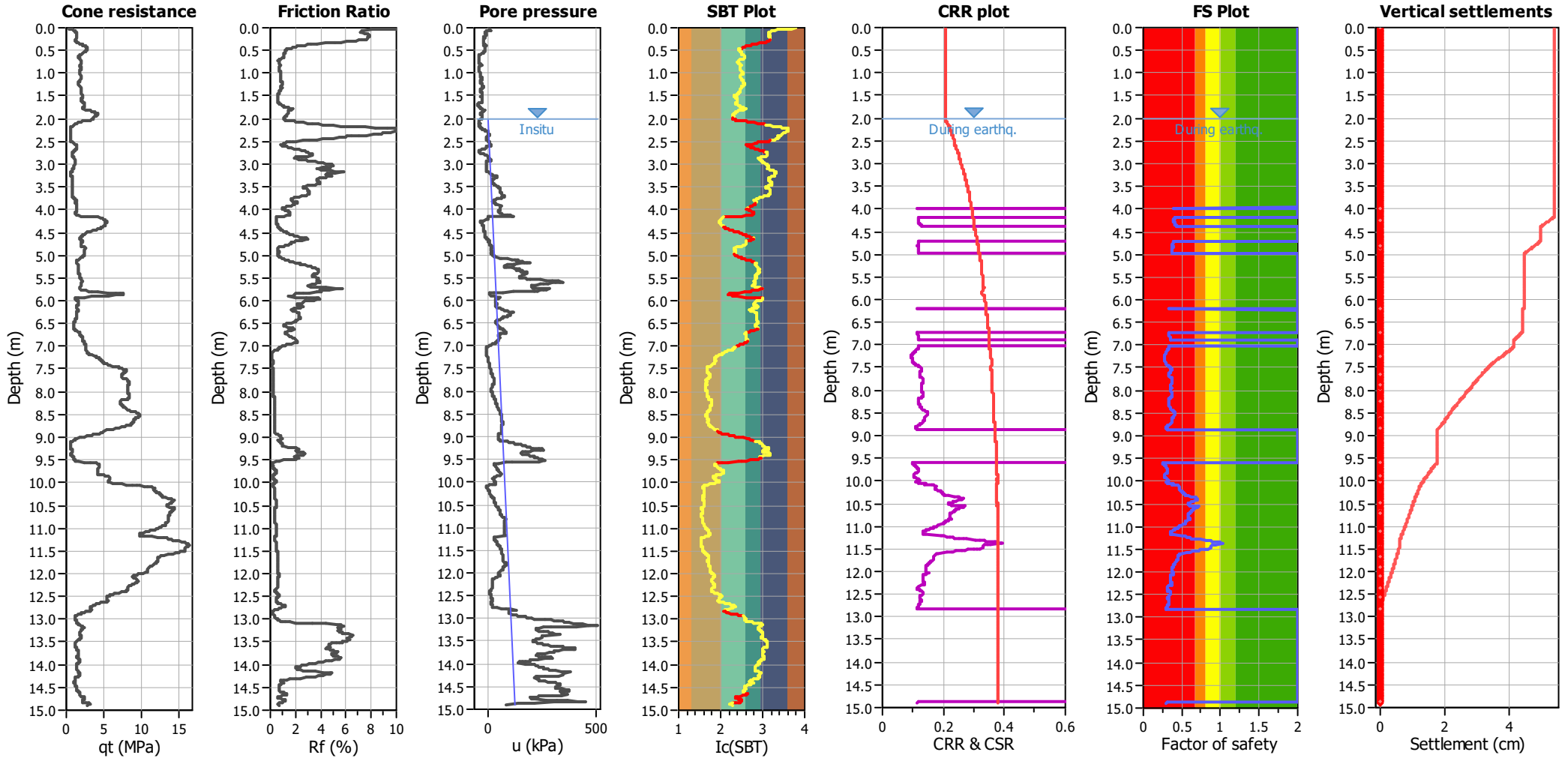
Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.40 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.40 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

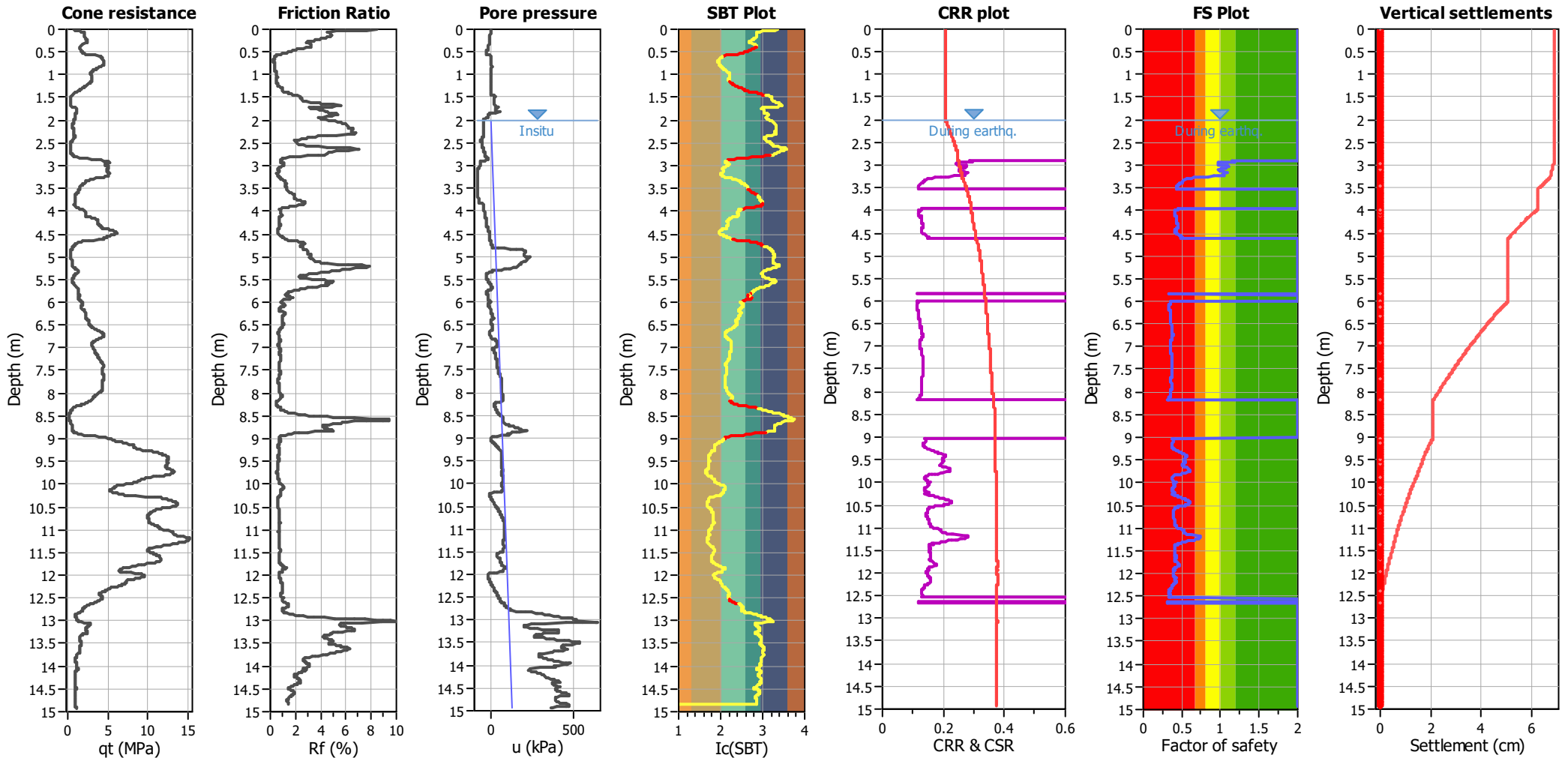


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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

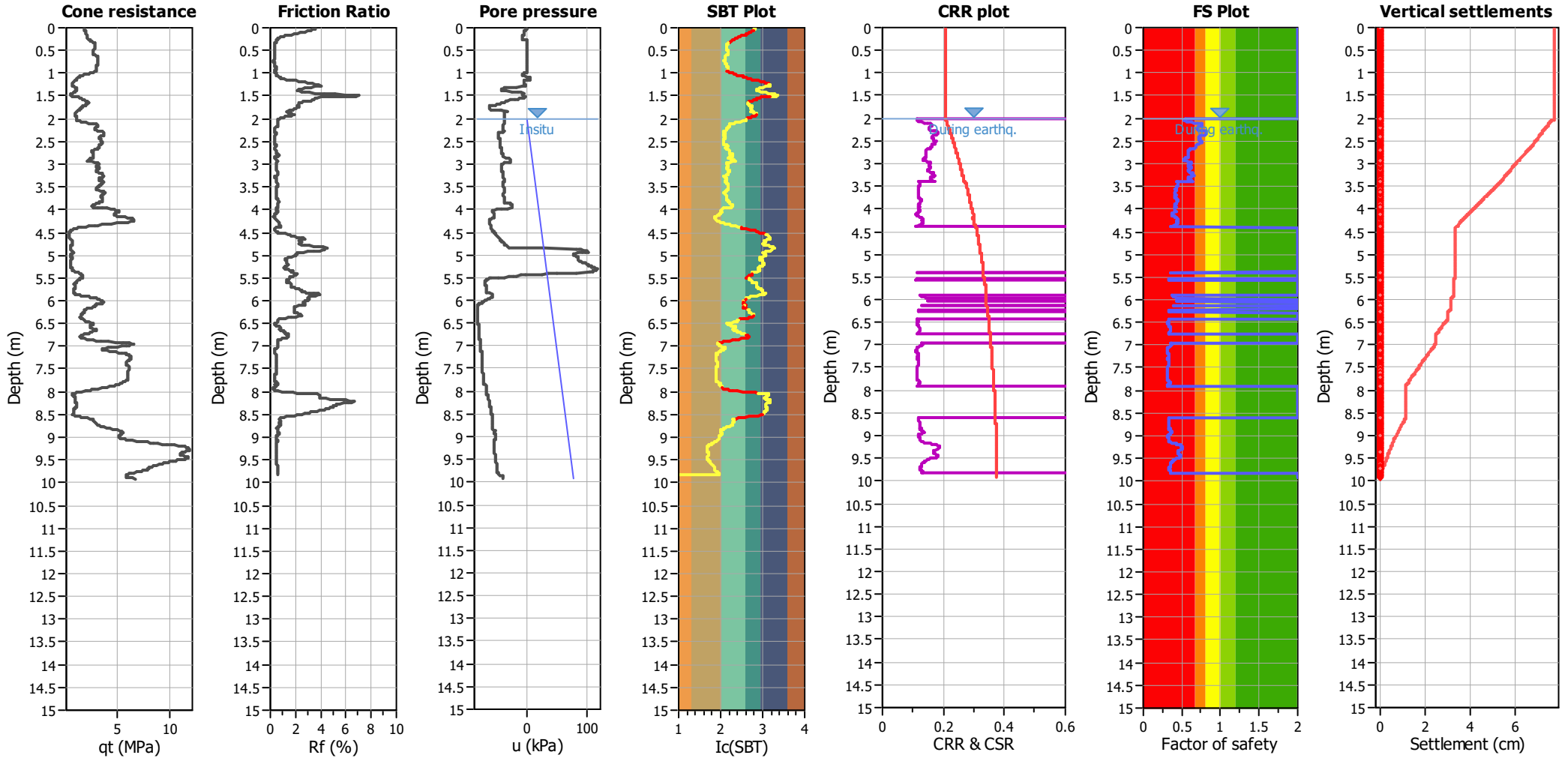


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Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

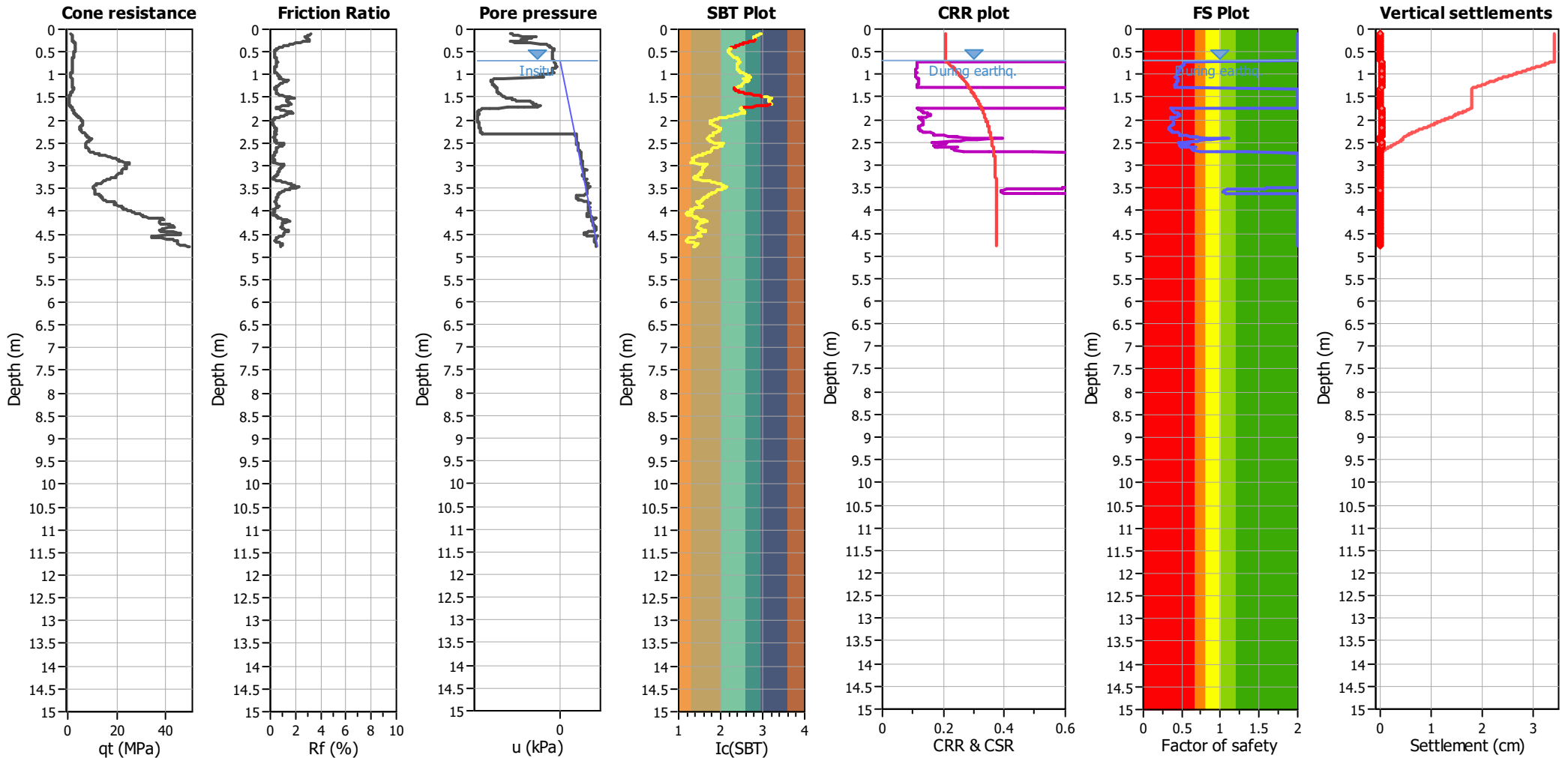




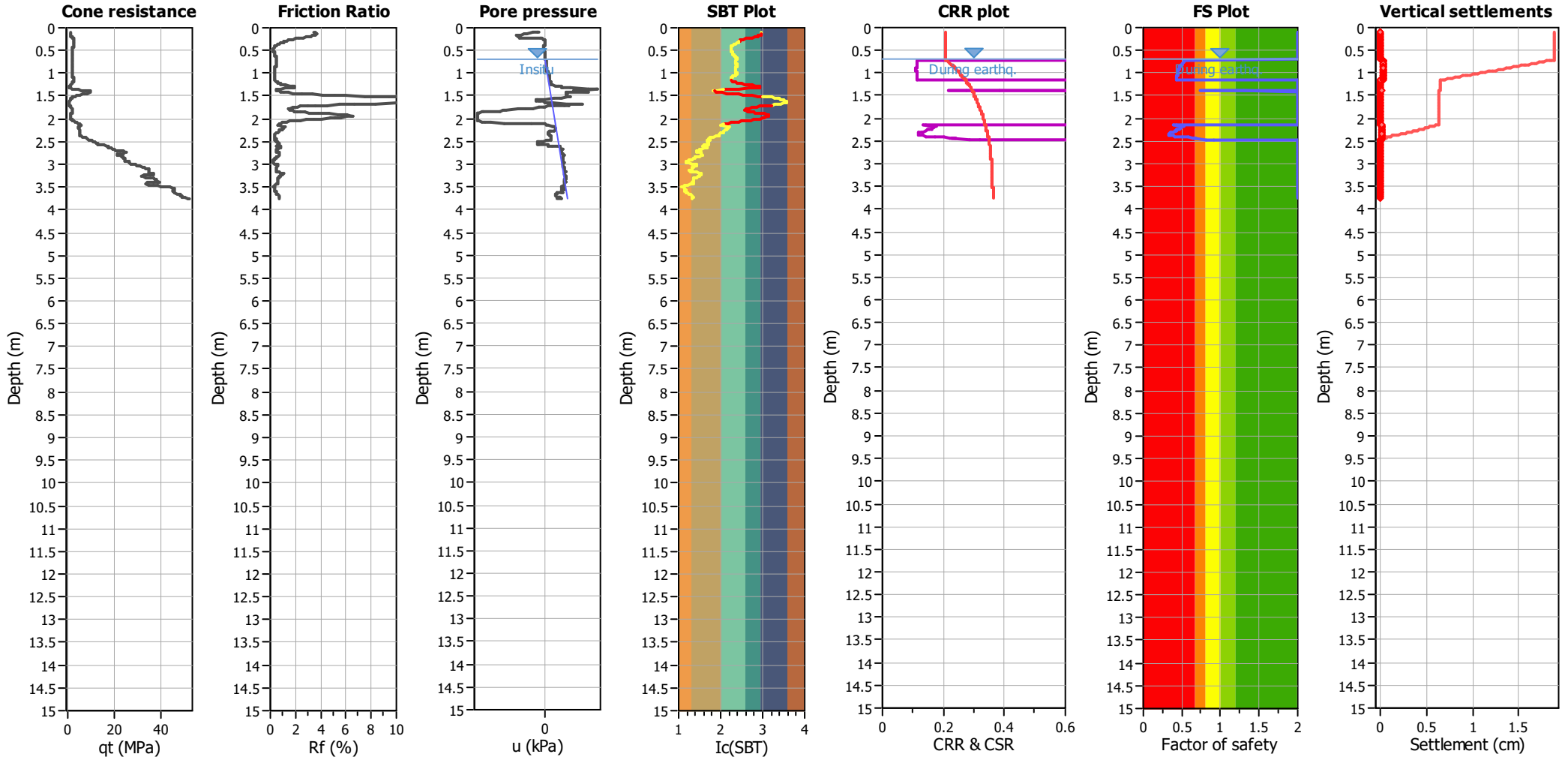
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



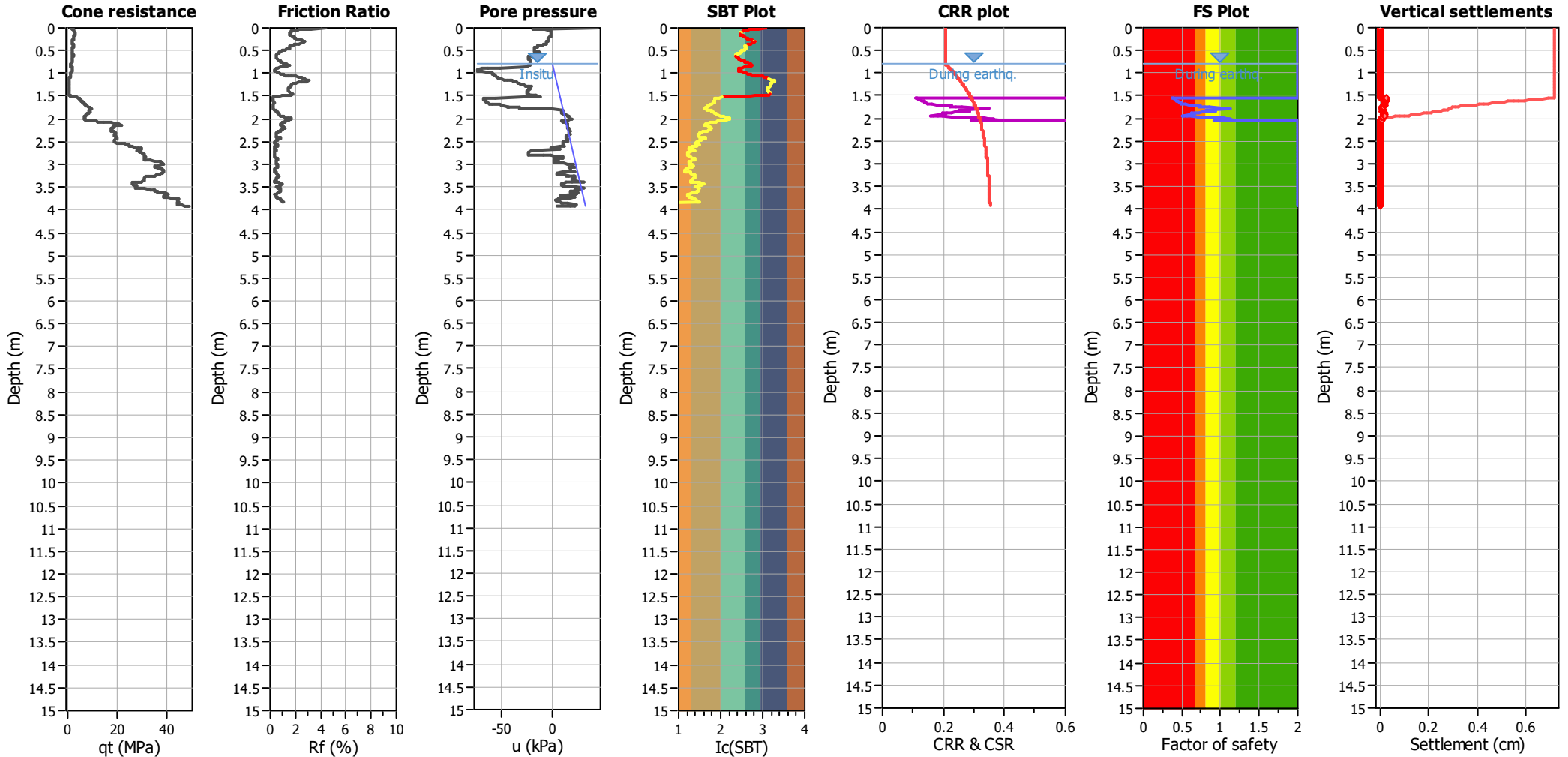
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_\sigma$ applied:	Yes	MSF method:	Method based



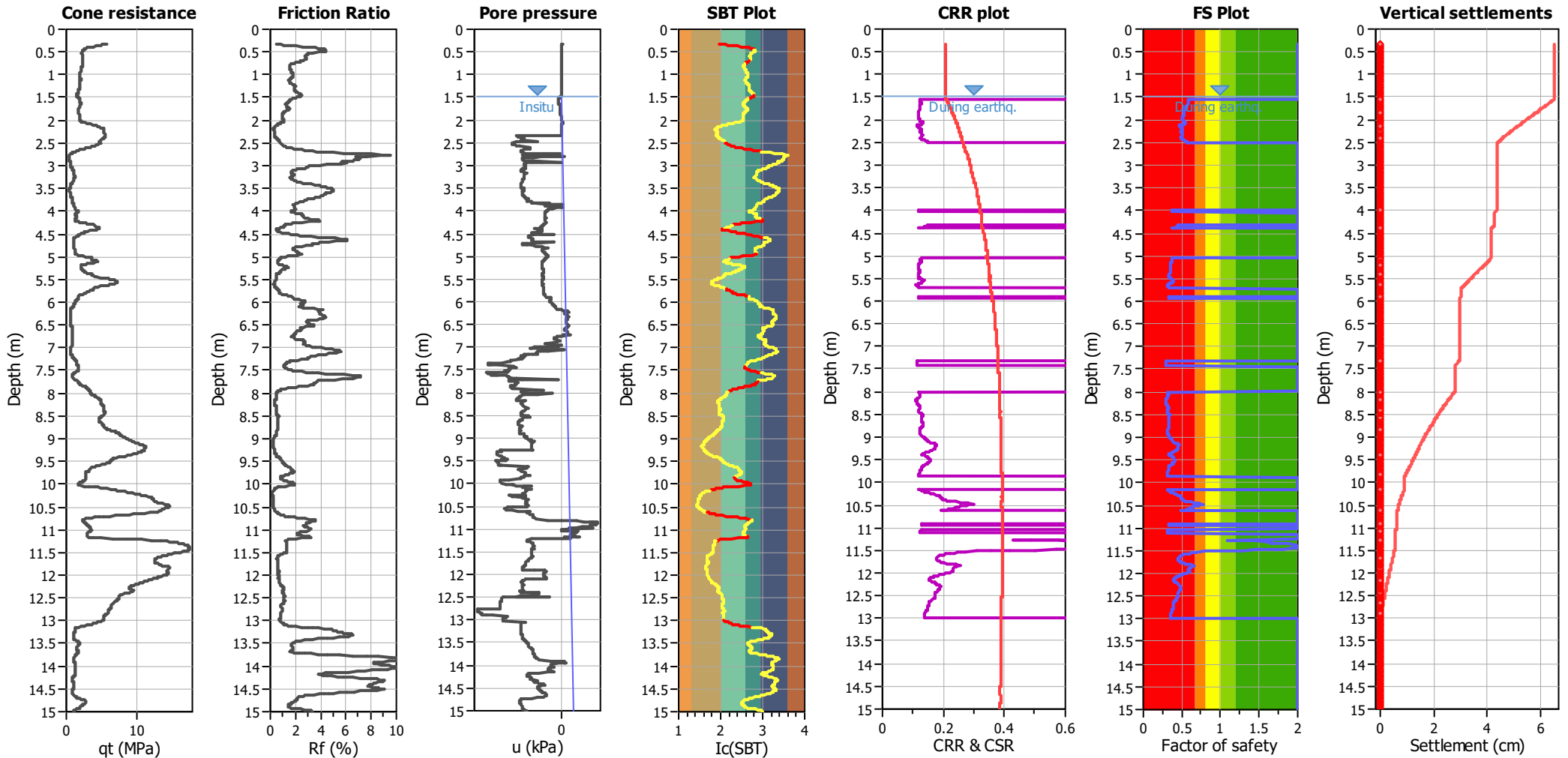
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



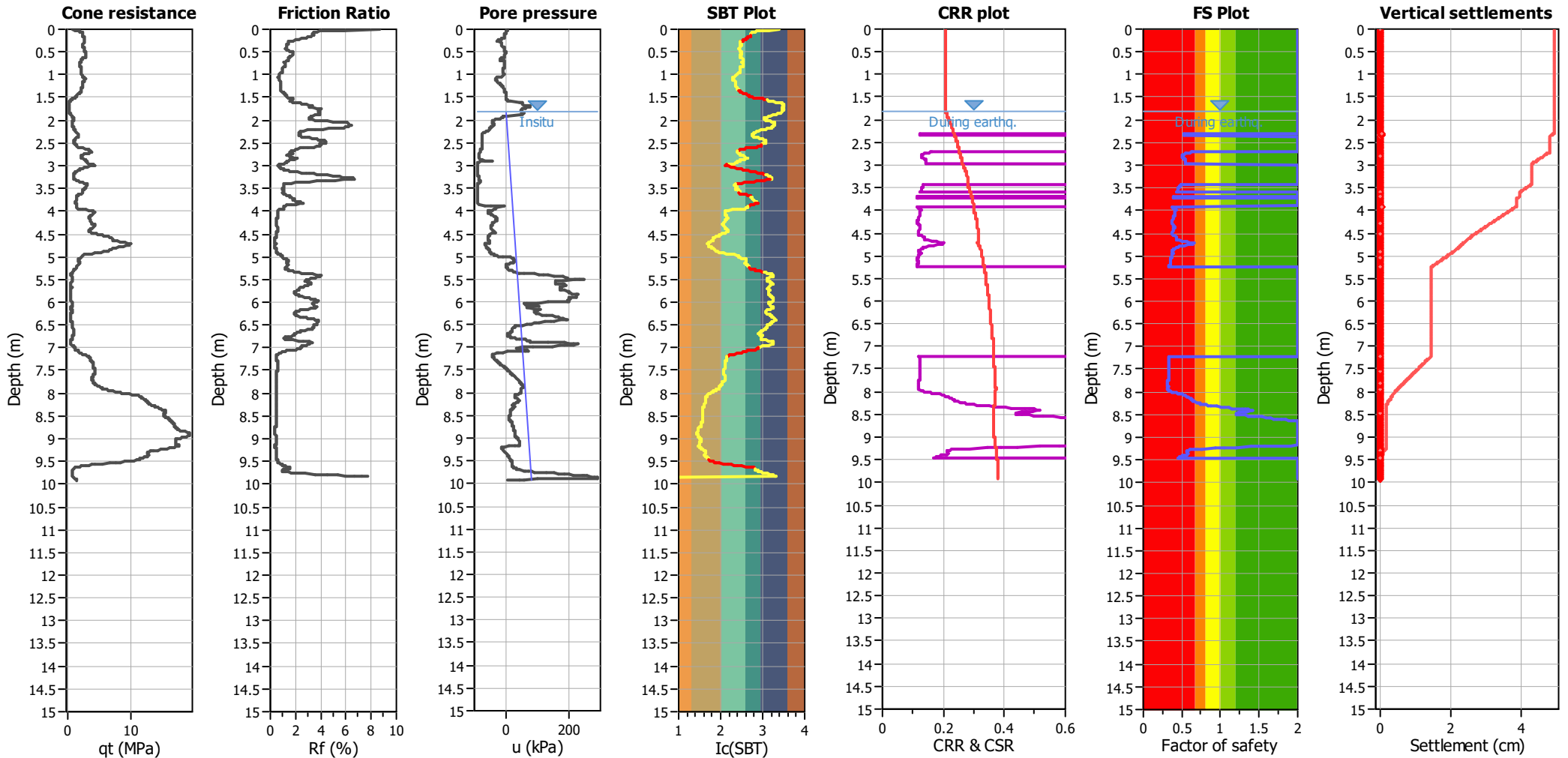
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



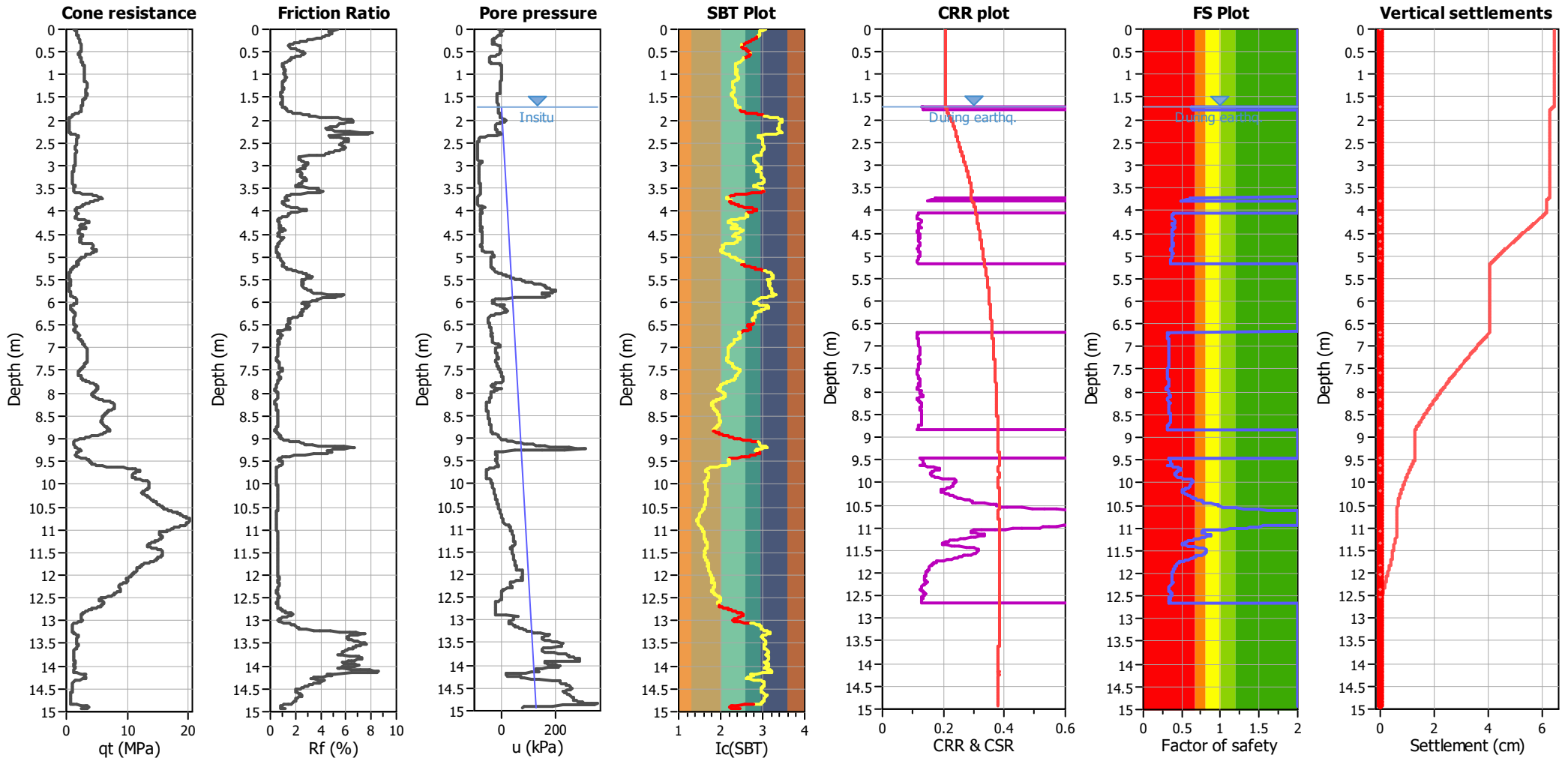
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.50 m	Use fill:	No	Clay like behavior	
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Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

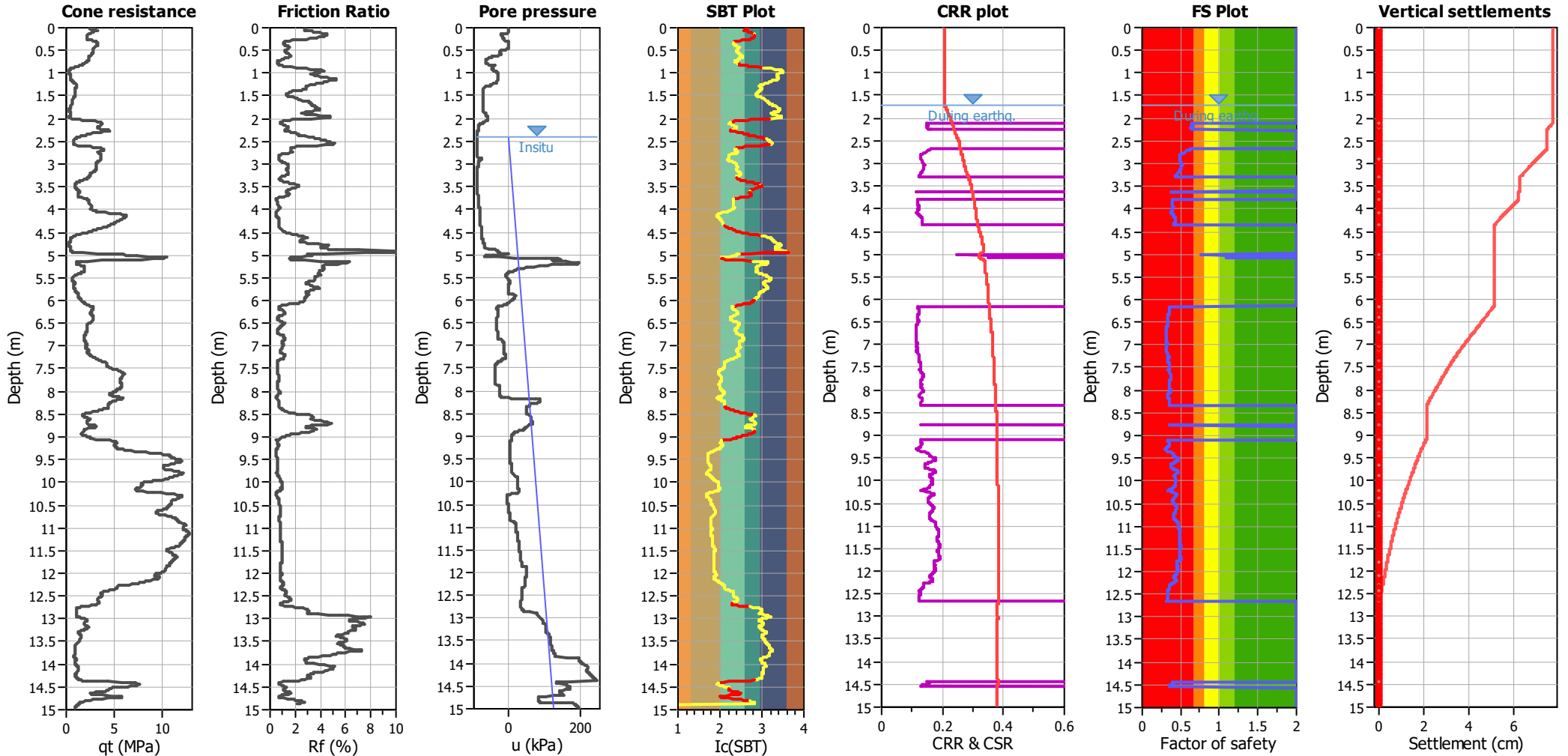


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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

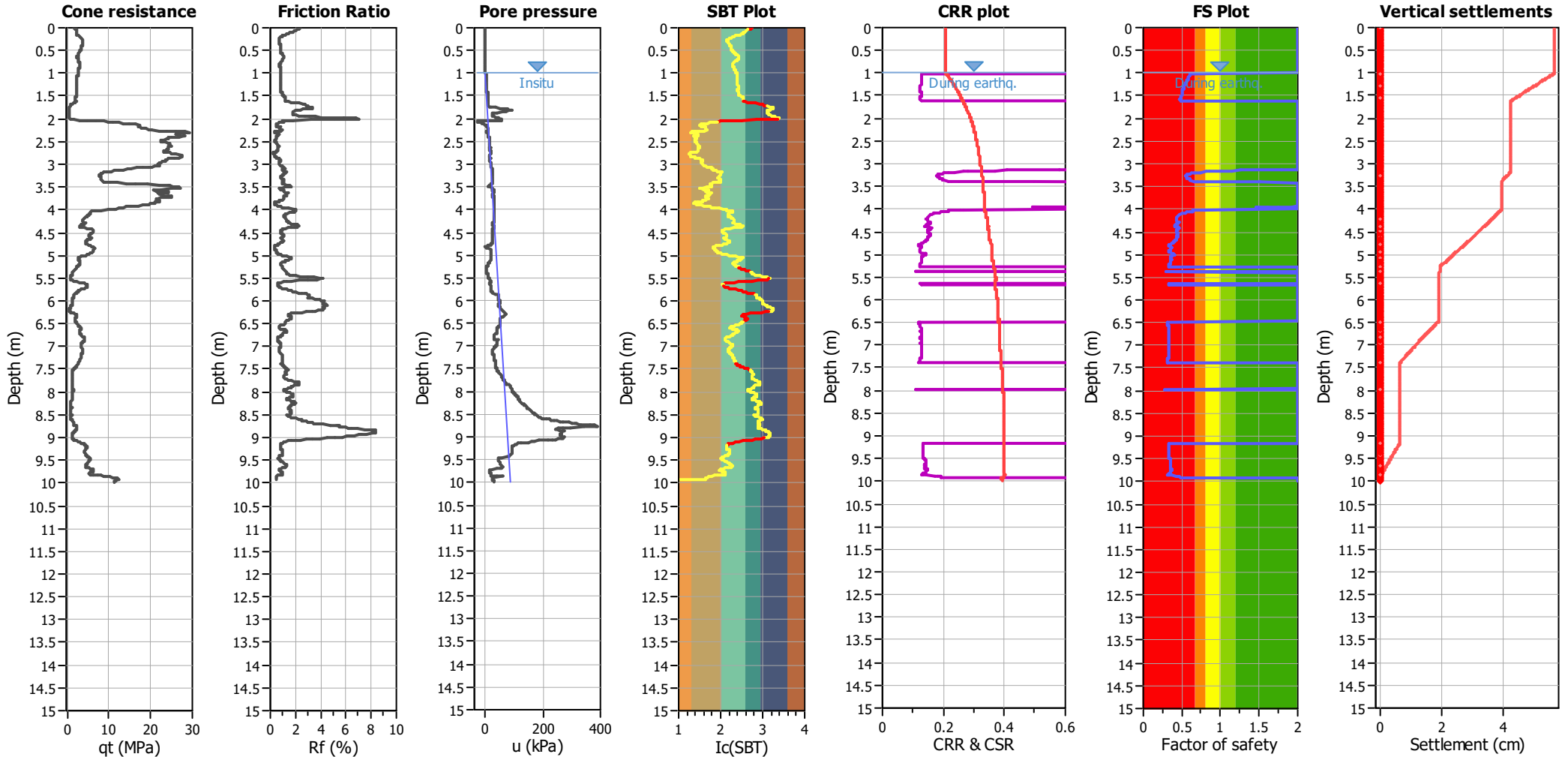


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Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

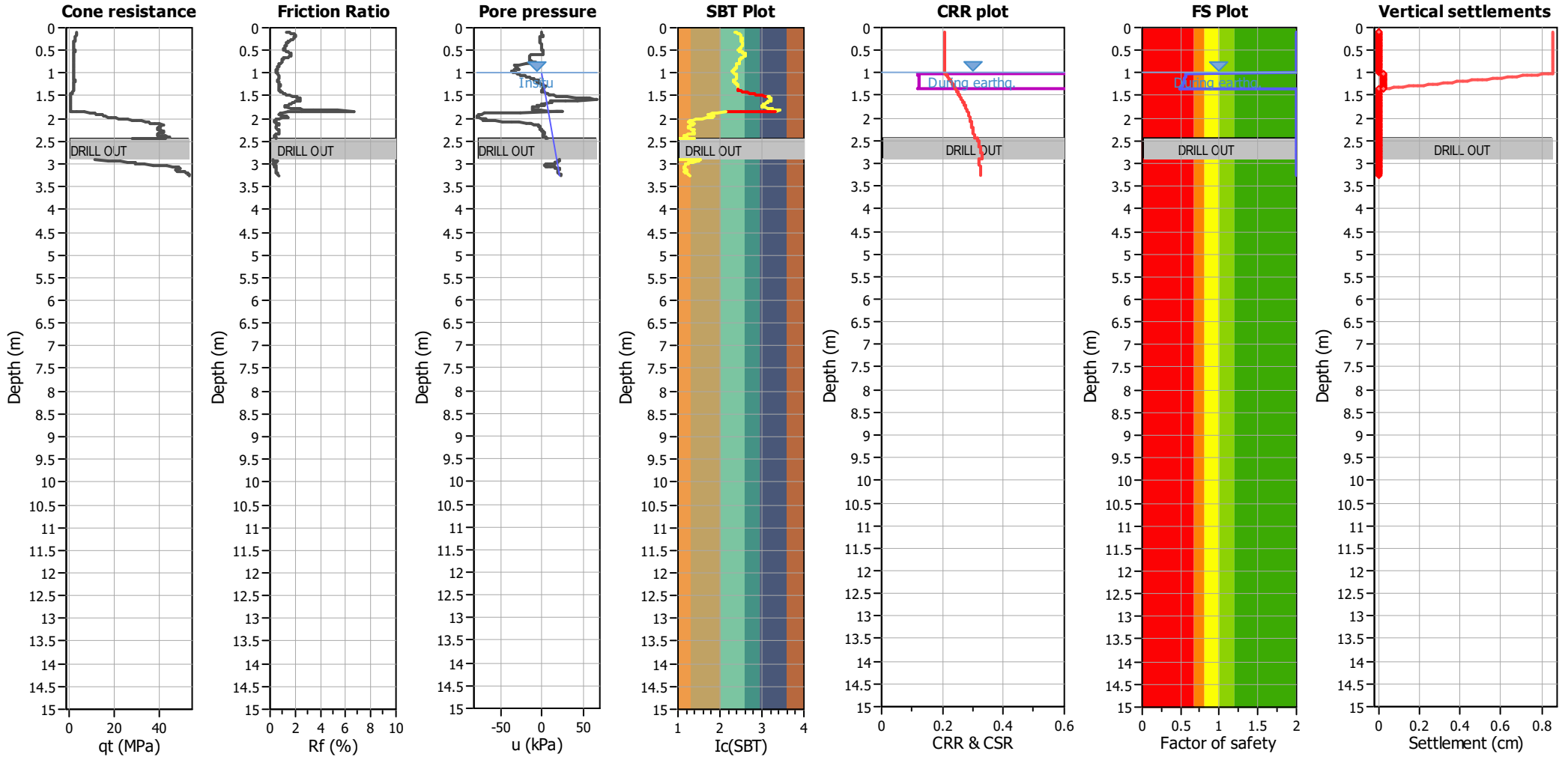




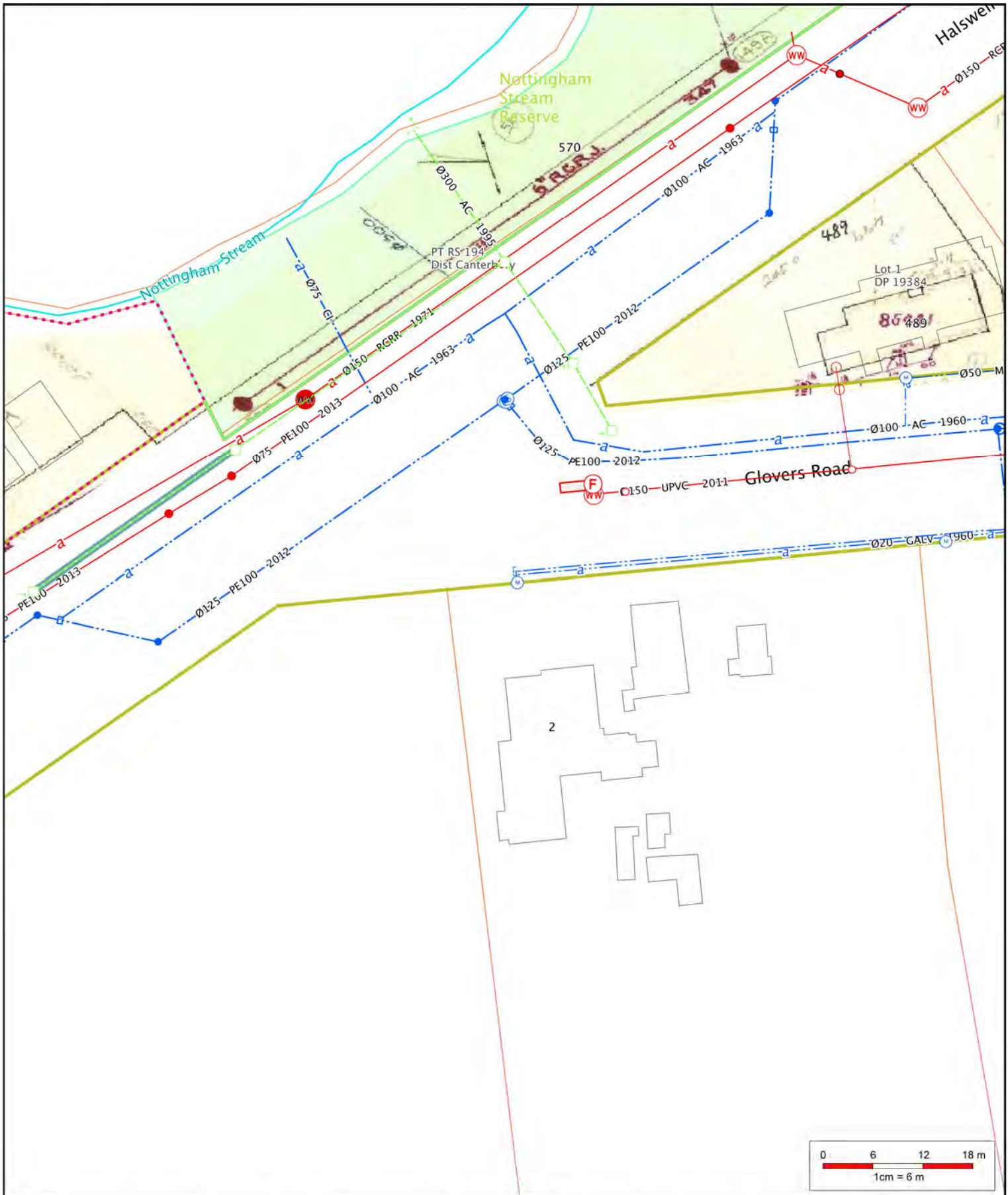
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Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
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Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

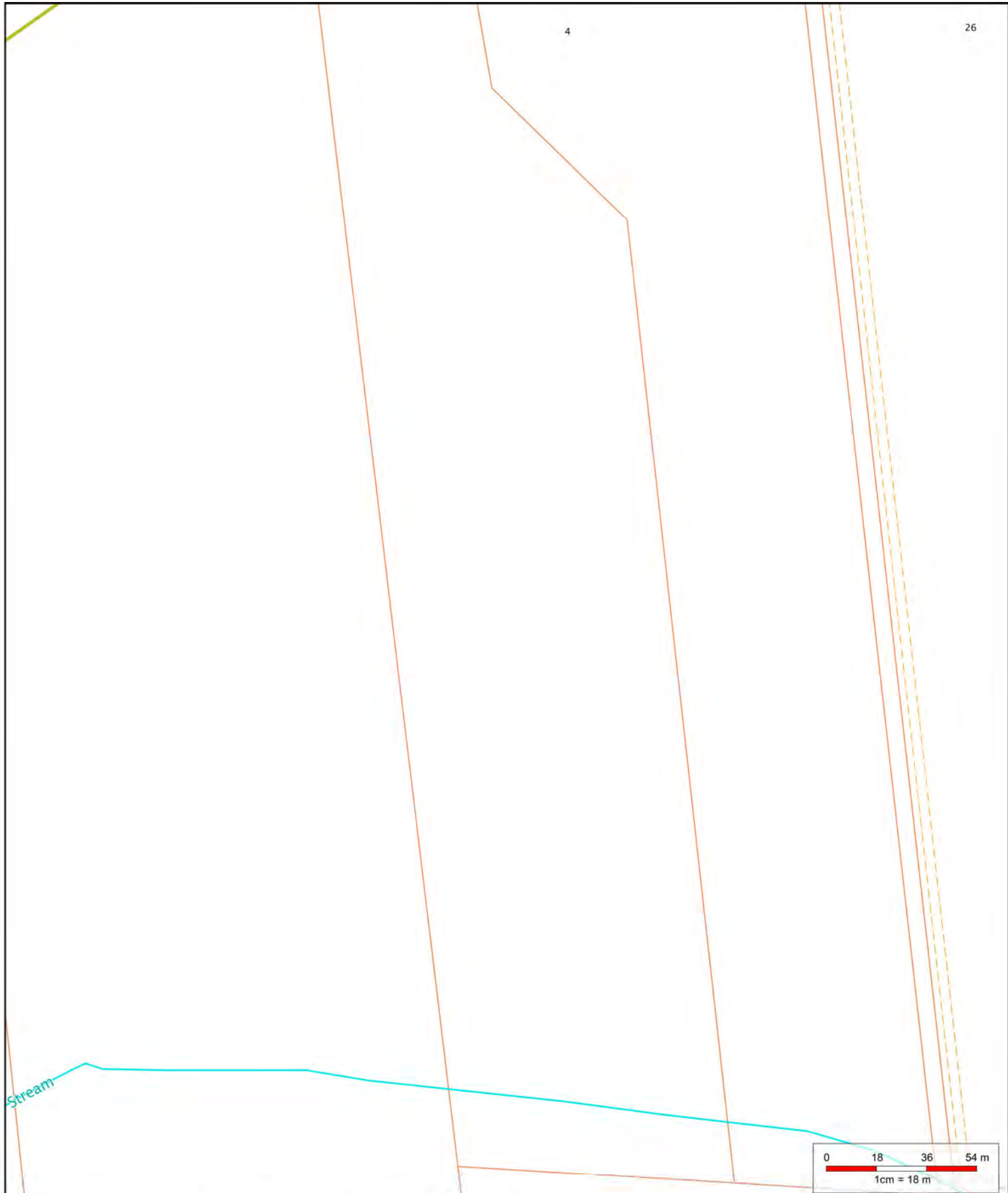


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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based




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 ph: 941-8300 fax: 941-8385  
 Accuracy not guaranteed. Onsite verification required. Display of data scale dependent, full detail available at 1:500.  
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Private Drainage		Water Intake/Supply	Wastewater	Wastewater	Stormwater	Stormwater
<b>Standard Infrastructure</b>  Bio Gas  Condensate Trap  End Cap  Inlet  Outlet  Valve  Main  Cable	 Inlet  Meter  Outlet  Pump  Restrictor  Valve  Air Release  Butterfly  Flow restriction  Gate  Pressure Activated  Sluice  Valve  Reservoir  Structure  Lateral  Main  Sub Main	 End Cap  Valve  Air Gap Separator  Vent  Eye  Eye (Vertical)  Outfall  Pump  Junction  Access  Flush Manhole  Inspection Point  Standard Manhole  Trap  Vented Manhole  Lateral  Main  Pressure Main	 Lateral Fitting <b>Local Pressure</b>  Control Panel  Boundary Kit  Tank System  Site  Vacuum Chamber  Vacuum Breather <b>Stormwater</b>  Bend  Change  Eye  Flow Restriction  Inlet  Dome Sump  Double Sump  Gross Debris Trap	 Inlet  Inlet Headwall  Pipe End  Silt Trap  Single Sump  Soak Pit  Triple Sump  Junction  Standard Manhole  Outlet  Pump  Structure  Basin  Lateral  Main  Lateral Fitting  Double Sump	<b>All services</b>  Pipe Protection  Abandoned  Proposed  Out of service <b>Landbase</b>  Easement	



1 : 1,800 on A4  
18/06/2021 9:23:37 AM

ph: 941-8300 fax: 941-8385

Accuracy not guaranteed. Onsite verification required. Display of data scale dependent, full detail available at 1:500.

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**Private Drainage**

- Standard Infrastructure**
- Bio Gas
  - Condensate Trap
  - End Cap
  - Inlet
  - Outlet
  - Valve
  - Main
  - Cable
- Water Intake/Supply**
- Connector
  - Ballows
  - Connector
  - Hydrant

**Water Intake/Supply**

- Inlet
- Meter
- Outlet
- Pump
- Restrictor
- Valve
- Air Release
- Butterfly
- Flow restriction
- Gate
- Pressure Activated
- Sluice
- Valve
- Reservoir
- Structure
- Lateral
- Main
- Sub Main

**Wastewater**

- End Cap
- Valve
- Air Gap Separator
- Vent
- Eye
- Eye (Vertical)
- Outfall
- Pump
- Junction
- Access
- Flush Manhole
- Inspection Point
- Standard Manhole
- Trap
- Vented Manhole
- Lateral
- Main
- Pressure Main

**Wastewater**

- Local Pressure
- Lateral Fitting
  - Control Panel
  - Boundary Kit
  - Tank System
  - Site
  - Vacuum Chamber
  - Vacuum Breather
- Stormwater**
- Bend
  - Change
  - Eye
  - Flow Restriction
  - Inlet
  - Dome Sump
  - Double Sump
  - Gross Debris Trap

**Stormwater**

- Inlet
- Inlet Headwall
- Pipe End
- Silt Trap
- Single Sump
- Soak Pit
- Triple Sump
- Junction
- Standard Manhole
- Outlet
- Pump
- Structure
- Basin
- Lateral
- Main
- Lateral Fitting
- Double Sump

**Stormwater**

- Lateral Fitting
  - Single Sump
  - Soak Pit
  - Inspection point
  - Manhole
- All services**
- Pipe Protection
  - Abandoned
  - Proposed
  - Out of service
- Landbase**
- Easement

CHRISTCHURCH CITY COUNCIL - DRAINAGE PICK UP



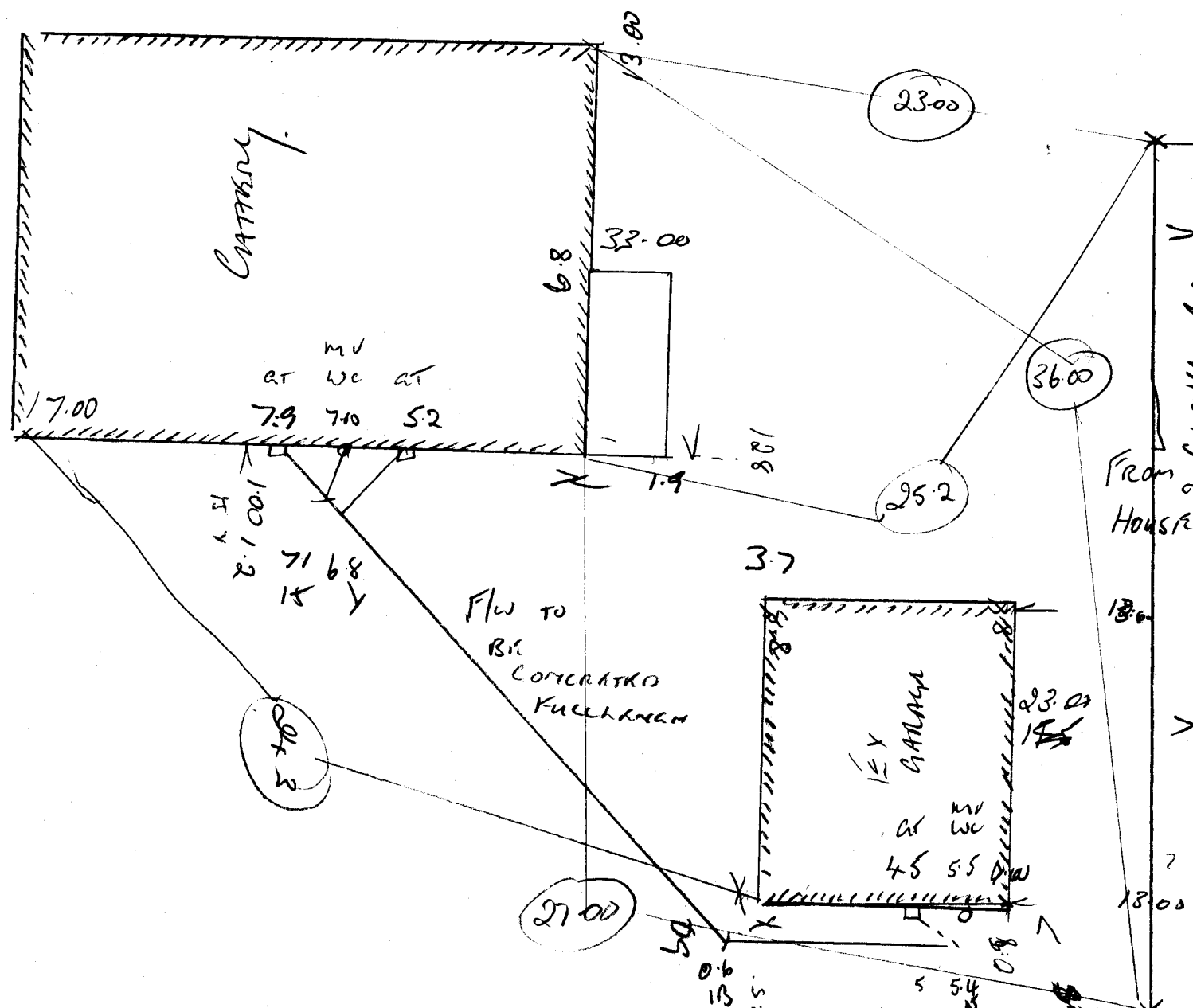
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 LEGAL DESCRIPTION:  
 PROJECT No.: 94006454  
 DATE: 2-11-94

OWNER: BLAIR  
 DRAINLAYER: M. SPAIN  
 PLUMBER:  
 FIELD OFFICER: O'Hara

RECEIVED: 21 NOV 1994  
 BLOCK PLAN: HAL 43  
 PLOTTED: / /  
 EYE BOOK:

CONNECTION NUMBER

Flow only





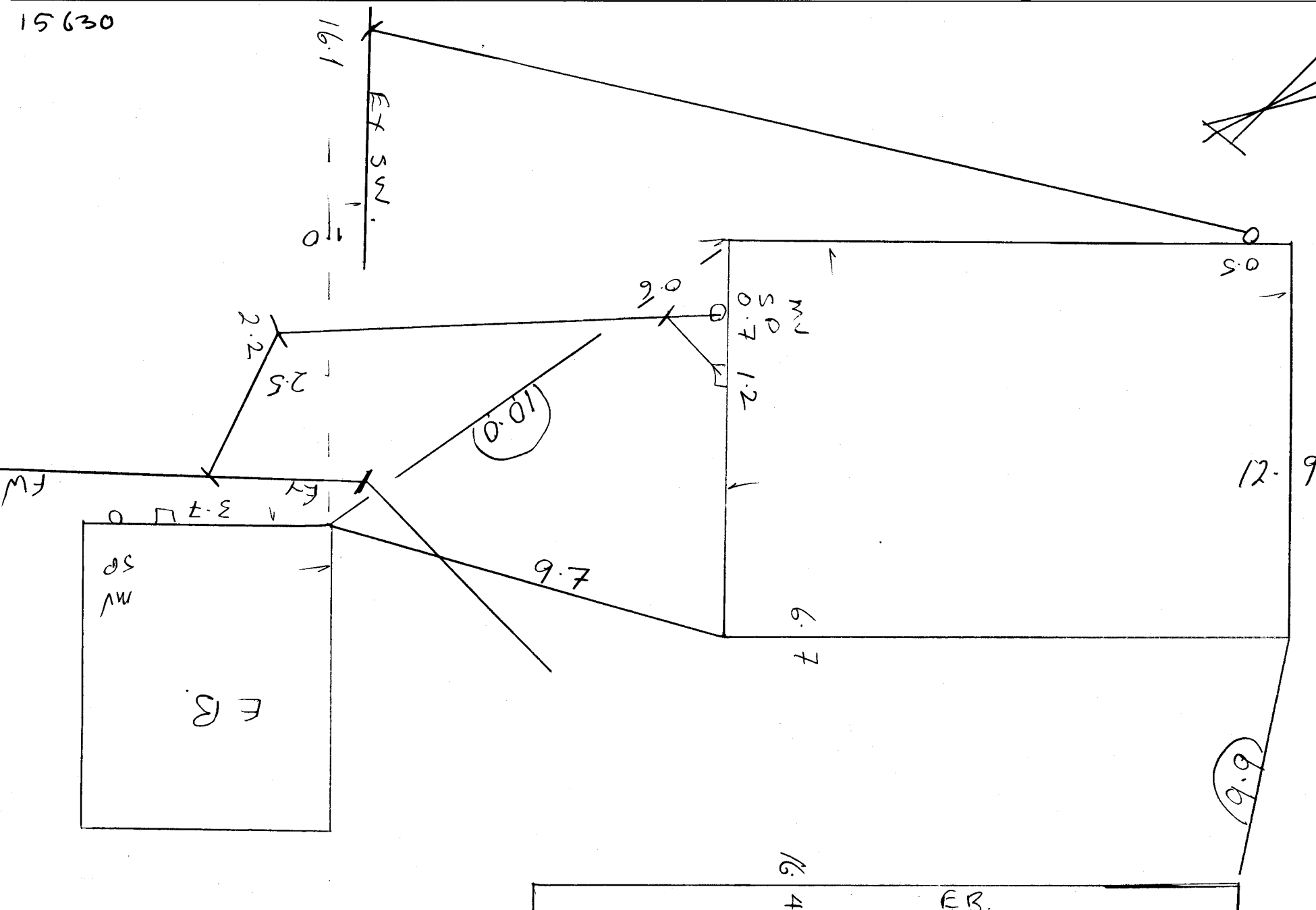
ADDRESS: 2 GLOVERS  
 LEGAL DESCRIPTION:  
 PROJECT No: 98003663  
 DATE: 14.9.98

OWNER:  
 DRAINLAYER: T MCKAY  
 PLUMBER:  
 FIELD OFFICER: STURBS

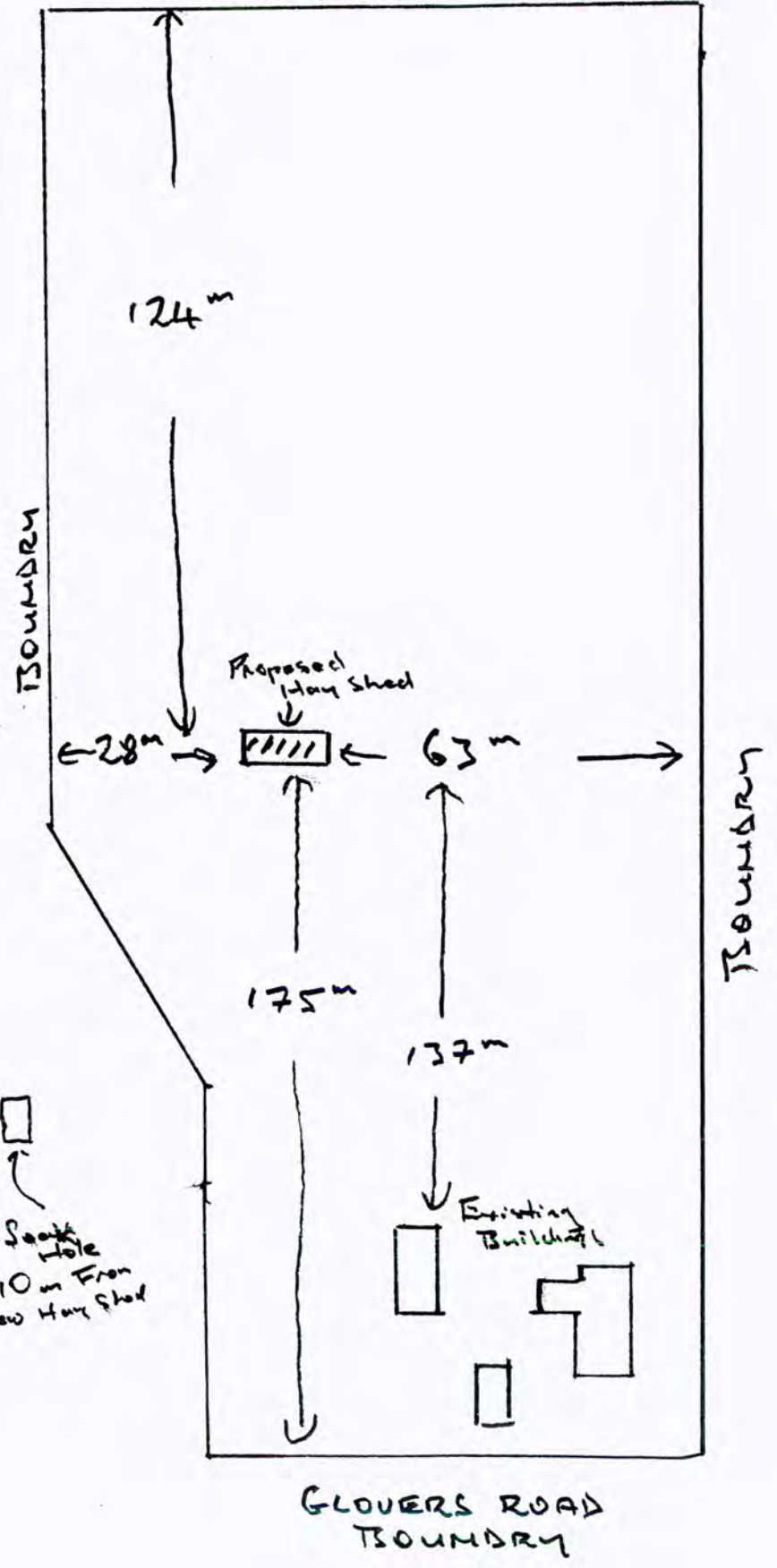
RECEIVED: 30 SEP 1998  
 BLOCK PLAN: HALL 43  
 PLOTTED: / /  
 EYE BOOK:

CONNECTION NUMBER

15630

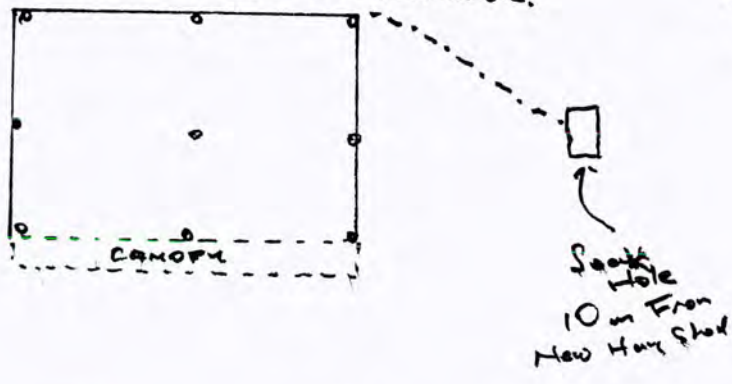


# Diagram of Lot 1 Showing Distances from Boundary & Nearest Building BOUNDARY



CHRISTCHURCH CITY COUNCIL  
**CONSENT DOCUMENT**  
 18 AUG 2001  
 All building work shall comply with the New Zealand Building Code notwithstanding any inconsistencies which may occur in the drawings and specifications.

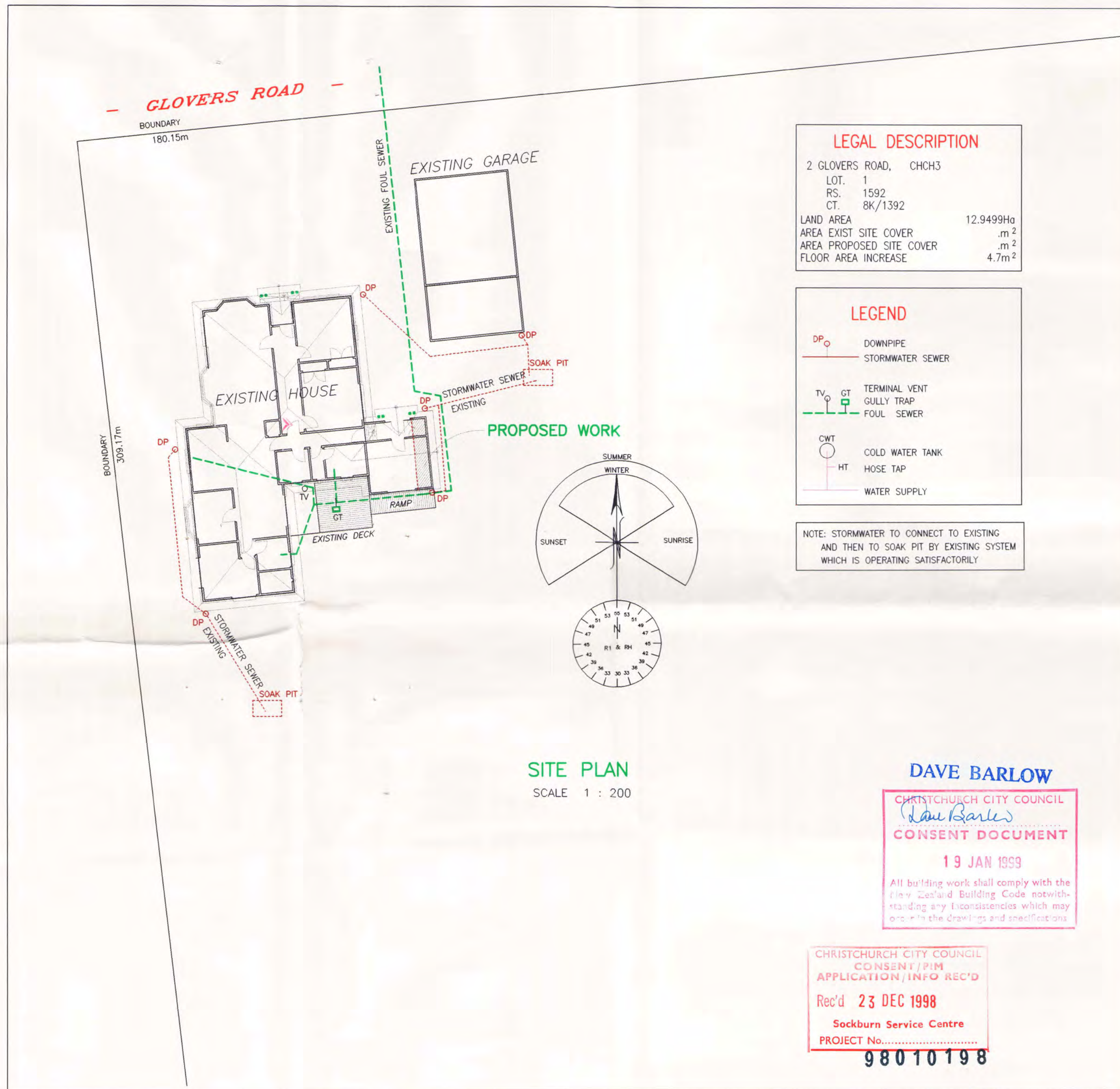
## Diagram showing STORM WATER DRAINAGE.



FILE COPY

10017967





**LEGAL DESCRIPTION**

2 GLOVERS ROAD, CHCH3	
LOT.	1
RS.	1592
CT.	8K/1392
LAND AREA	12.9499Ha
AREA EXIST SITE COVER	.m <sup>2</sup>
AREA PROPOSED SITE COVER	.m <sup>2</sup>
FLOOR AREA INCREASE	4.7m <sup>2</sup>

**LEGEND**

	DOWNPIPE
	STORMWATER SEWER
	TERMINAL VENT GULLY TRAP
	FOUL SEWER
	COLD WATER TANK
	HOSE TAP
	WATER SUPPLY

NOTE: STORMWATER TO CONNECT TO EXISTING AND THEN TO SOAK PIT BY EXISTING SYSTEM WHICH IS OPERATING SATISFACTORILY

**DAVE BARLOW**

CHRISTCHURCH CITY COUNCIL  
*(Signature)*  
**CONSENT DOCUMENT**  
**19 JAN 1999**  
All building work shall comply with the New Zealand Building Code notwithstanding any inconsistencies which may occur in the drawings and specifications.

CHRISTCHURCH CITY COUNCIL  
CONSENT/PIM  
APPLICATION/INFO REC'D  
Rec'd **23 DEC 1998**  
Sockburn Service Centre  
PROJECT No.....  
**98010198**

BUILDER TO CHECK ALL DIMENSIONS

**FILE COPY**



**SITE PLAN**  
SCALE 1 : 200

PROPOSED KELLY DWELLING ALTERATIONS  
GORDAN & HEATHER KELLY  
2 GLOVERS ROAD HALSWELL

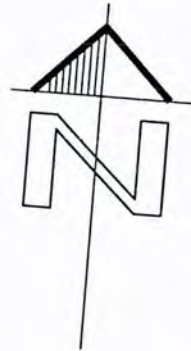
DRAWN	M.J.M	JOB No.	419-KELLY
DATE	17-12-98	SHEET	1
CHECKED		Amt.	

HALSWELL RD

GLOVERS RD



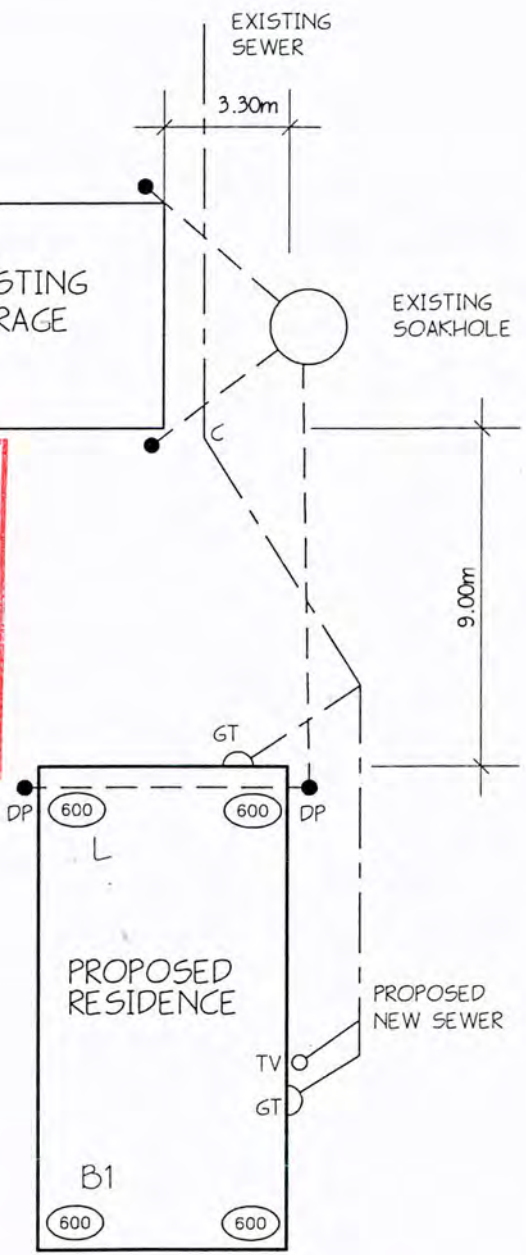
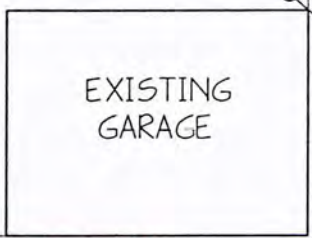
LOCALITY PLAN  
N.T.S.



LEGAL DESCRIPTION  
 LOT 1  
 DP 54911

**CHRISTCHURCH CITY COUNCIL**  
*P. J. Bevan*  
**CONSENT DOCUMENT**  
**22 MAY 1998**  
 All building work shall comply with the New Zealand Building Code notwithstanding any inconsistencies which may occur in the drawings and specifications.

EXISTING CATTERY



**CHRISTCHURCH CITY COUNCIL**  
**P.I.M. APPLICATION**  
 Rec'd 19 MAY 1998  
 Sockburn Service Centre  
 PROJECT No. 98003663

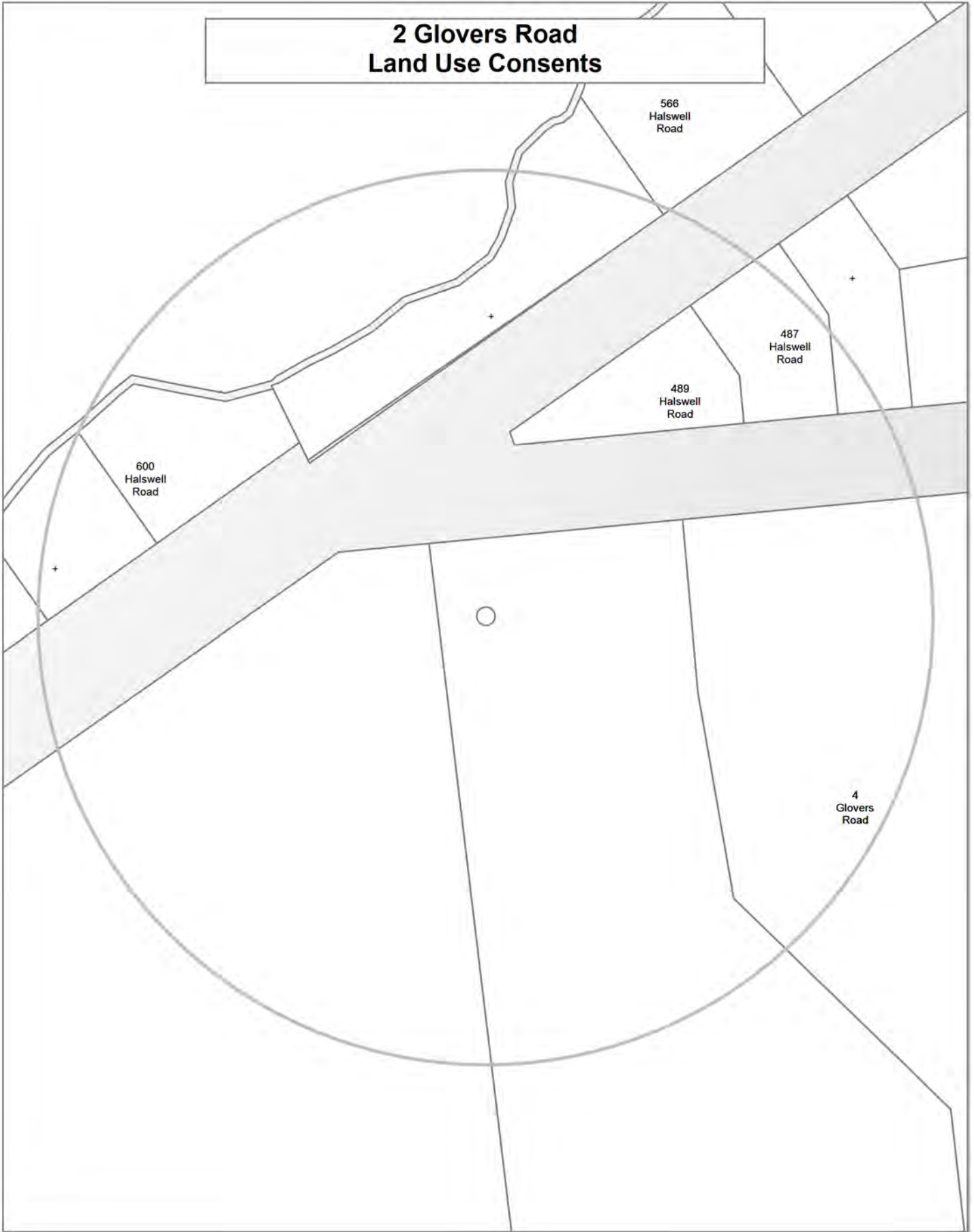
**FILE COPY**

SITE PLAN

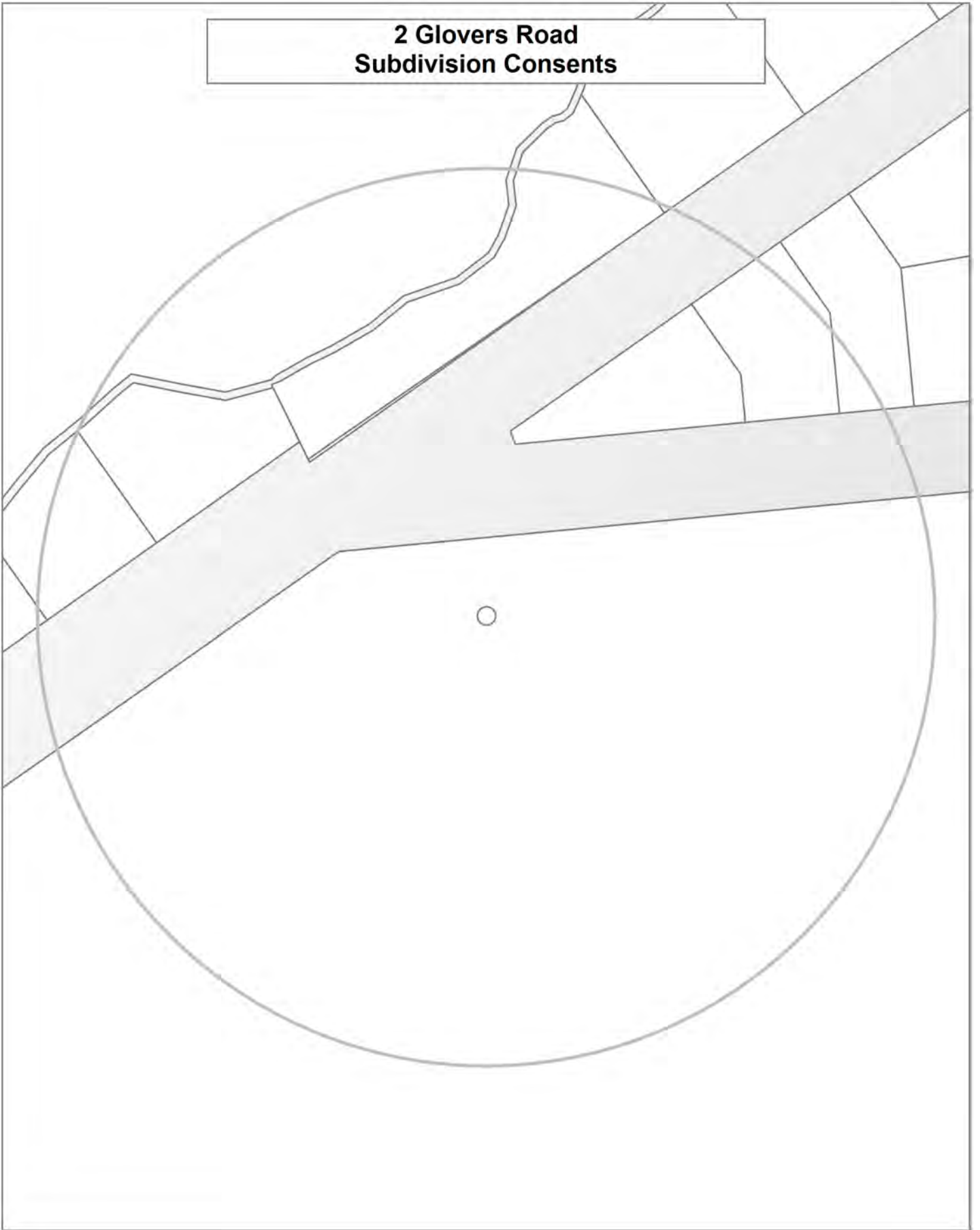
DRAWN KB	<b>KEITH HAY</b> <b>HOMES</b> ©COPYRIGHT 1997	CUSTOMER.....CONTRACTOR.....	
DATE 17/04/98		NAME A. & L. BLAIR	
CHECKED DB.		AREA	SCALES 1:200
			1

C:\CAD\BRANCHES

## 2 Glovers Road Land Use Consents



**2 Glovers Road  
Subdivision Consents**



## Land Use Resource Consents within 100 metres of 2 Glovers Road

Note: This list does not include subdivision Consents and Certificates of Compliance issued under the Resource Management Act.

---

### 4 Glovers Road

RMA/2003/1909

Application to convert an existing studio into a family flat - Historical Reference RMA20014216

Processing complete

Applied 25/07/2003

Decision issued 13/08/2003

Granted 13/08/2003

RMA/2017/1463

To establish a Temporary Storage Yard

Processing complete

Applied 26/06/2017

Decision issued 13/02/2019

Granted 13/02/2019

RMA/2020/2557

Remediation of contaminated soils

Processing complete

Applied 06/11/2020

Decision issued 09/12/2020

Granted 09/12/2020

RMA/2020/2770

To conduct earthworks and stockpiling on site

Processing complete

Applied 27/11/2020

Decision issued 27/01/2021

Granted 27/01/2021

RMA/2020/3076

To subdivide 4 allotments to create 87 residential allotments. Land use consent for earthworks and under the NES for contaminated land.

On hold - waiting for response from applicant

Applied 22/12/2020

## 487 Halswell Road

RMA/1994/527

Consent to erect a garage over 40m<sup>2</sup> in the front yard, and to erect a studio in the front yard. - Historical Reference RES94001092

Processing complete

Applied 30/06/1994

Decision issued 25/07/1994

Granted 25/07/1994

## 489 Halswell Road

RMA/1995/2290

Application for reduced setback for garage - Historical Reference RES953485

Processing complete

Applied 16/08/1995

Decision issued 07/09/1995

Granted 07/09/1995

RMA/2001/351

Appication for a garage addition to be attached to the existing dwelling with non compliances with street setback; length of wall and queuing space - Historical Reference RMA20004203

Processing complete

Applied 09/02/2001

Decision issued 01/03/2001

Granted 01/03/2001

## 511 Halswell Road

RMA/2020/163

Earthworks for residential development

Processing complete

Applied 29/01/2020

Decision issued 10/02/2020

Granted 10/02/2020

RMA/2020/2770

To conduct earthworks and stockpiling on site

Processing complete

Applied 27/11/2020

Decision issued 27/01/2021

Granted 27/01/2021

RMA/2020/3076

To subdivide 4 allotments to create 87 residential allotments. Land use consent for earthworks and under the NES for contaminated land.

On hold - waiting for response from applicant

Applied 22/12/2020

RMA/2021/733

Earthworks - Associated with the formation of vehicle crossings

Processing complete

Applied 24/03/2021

Decision issued 11/06/2021

Granted 11/06/2021

## 566 Halswell Road

RMA/1998/3055

A site which does not comply with number of vehicle crossings allowed under the Proposed District Plan. - Historical Reference RES990037

Processing complete

Applied 06/12/1998

Decision issued 12/01/1999

Granted 12/01/1999

RMA/1998/891

Application to erect a dwelling within 15m setback required from the Nottingham Stream in terms of the Proposed Plan. - Historical Reference RES980953

Processing complete

Applied 14/04/1998

Decision issued 03/06/1998

Granted 03/06/1998

## 600 Halswell Road

RMA/1985/400

Carport adjoining existing shed - Historical Reference RES9207116

Processing complete

Applied 12/06/1985

Decision issued 20/06/1985

Granted 20/06/1985

## 604 Halswell Road

RMA/2000/2667

Application for alterations to and the erection of additions to a dwelling to create a family flat and alterations to an existing garage - Historical Reference RMA20003424

Processing complete

Applied 25/10/2000

Decision issued 09/11/2000

Granted 08/11/2000

## Data Quality Statement

### Land Use Consents

All resource consents are shown for sites that have been labelled with an address. For sites that have been labelled with a cross (+) no resource consents have been found. Sites that have no label have not been checked for resource consents. This will be particularly noticeable on the margins of the search radius. If there are such sites and you would like them included in the check, please ask for the LIM spatial query to be rerun accordingly. This will be done free of charge although there may be a short delay. Resource consents which are on land occupied by roads, railways or rivers are not, and currently cannot be displayed, either on the map or in the list. Resource consents that relate to land that has since been subdivided, will be shown in the list, but not on the map. They will be under the address of the land as it was at the time the resource consent was applied for. Resource consents that are listed as Non-notified and are current, may in fact be notified resource consents that have not yet been through the notification process. If in doubt. Please phone (03)941 8999.

The term "resource consents" in this context means land use consents. Subdivision consents and certificates of compliance are excluded.

### Subdivision Consents

All subdivision consents are shown for the sites that have been labelled with consent details. For Sites that have been labelled with a cross (+) no records have been found. Sites that have no label have not been checked for subdivision consents. This will be particularly noticeable on the margins of the search radius. If there are such sites and you would like them included in the check, please ask for the LIM spatial query to be rerun accordingly. This will be done free of charge although there may be a short delay.

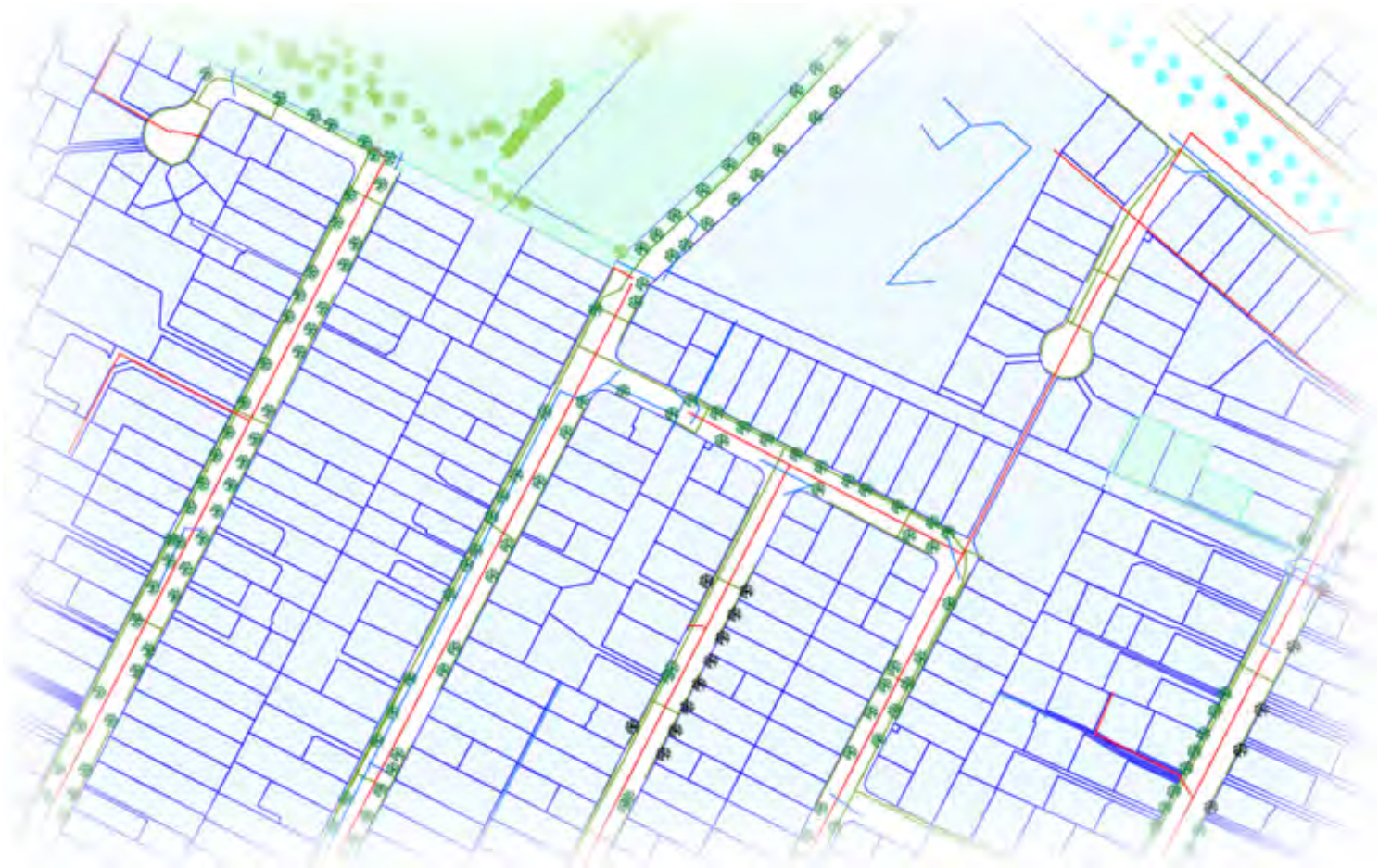
The term "subdivision consents" in this context means a resource consent application to subdivide land. Non subdivision land use resource consents and certificates of compliance are excluded.

This report will only record those subdivision applications which have not been completed i.e once a subdivision has been given effect to and the new lots/properties have been established the application which created those lots will not be shown

All subdivision consent information is contained on the map and no separate list is supplied



# Land Information Memorandum



Property address:  
4 Grovers Road

LIM number: 70247283  
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Christchurch City Council  
53 Hereford Street, PO Box 73015  
Christchurch 8154, New Zealand  
Tel 64 3 941 8999  
Fax 64 3 941 8984  
[www.ccc.govt.nz](http://www.ccc.govt.nz)

## Application details

Please supply to YOURSECTION RS LTD  
Client reference RIVERSTONE  
Phone number  
Fax number  
Date issued 18 June 2021  
Date received 10 June 2021

## Property details

Property address 4 Glovers Road  
Valuation roll number 23562 09301  
Valuation information Capital Value: \$3000000  
Land Value: \$2300000  
Improvements Value: \$700000  
*Please note: these values are intended for Rating purposes*  
Legal description Lot 2 DP 83635  
Existing owner Yoursection RS Limited  
PO Box 9301  
TOWER JUNCTION  
CHRISTCHURCH 8149

## Council references

Debtor number 4188171  
Rate account ID 73049823  
LIM number 70247283  
Property ID 1020795

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## Document information

This Land Information Memorandum (LIM) has been prepared for the purpose of section 44A of the Local Government Official Information and Meetings Act 1987 (LGOIMA). It is a summary of the information that we hold on the property. Each heading or "clause" in this LIM corresponds to a part of section 44A.

Sections 1 to 10 contain all of the information known to the Christchurch City Council that must be included under section 44A(2) LGOIMA. Any other information concerning the land as the Council considers, at its discretion, to be relevant is included at section 11 of this LIM (section 44A(3) LGOIMA). If there are no comments or information provided in these sections this means that the Council does not hold information on the property that corresponds to that part of section 44A.

The information included in this LIM is based on a search of Council records only and there may be other information relating to the land which is unknown to the Council. Please note that other agencies may also hold information relevant to the property, or administer legislation relevant to the use of the land, for example, the Regional Council (Ecan), Heritage New Zealand Pouhere Taonga, and Land Information New Zealand.

Council records may not show illegal or unauthorised building or works on the property. The applicant is solely responsible for ensuring that the land is suitable for a particular purpose.

A LIM is only valid at the date of issue as information is based only upon information the Council held at the time of that LIM request being made.

## Property file service

This Land Information Memorandum does not contain all information held on a property file. Customers may request property files by phoning the Council's Customer Call Centre on (03) 941 8999, or visiting any of the Council Service Centres. For further information please visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

To enable the Council to measure the accuracy of this LIM document based on our current records, we would appreciate your response should you find any information contained therein which may be considered to be incorrect or omitted. Please telephone the Customer Call Centre on (03) 941 8999.

A search of records held by the Council has revealed the following information:

## 1. Special features and characteristics of the land

*Section 44A(2)(a) LGOIMA. This is information known to the Council but not apparent from the district scheme under the Town and Country Planning Act 1977 or a district plan under the Resource Management Act 1991. It identifies each (if any) special feature or characteristic of the land concerned, including but not limited to potential erosion, avulsion, falling debris, subsidence, slippage, alluvion, or inundation, or likely presence of hazardous contaminants.*

( For enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### ┆ Consultant Report Available

Land Information New Zealand (LINZ) engaged Tonkin and Taylor to provide a Geotechnical Report on Ground Movements that occurred as a result of the Canterbury Earthquake Sequence. The report indicates this property may have been effected by a degree of earthquake induced subsidence. The report obtained by LINZ can be accessed on their website at <https://www.linz.govt.nz/land/surveying/earthquakes/canterbury-earthquakes/information-for-canterbury-surveyors>

### ┆ Liquefaction Vulnerability

Christchurch City Council holds indicative information on liquefaction hazard for Christchurch. Information on liquefaction, including an interactive web tool, can be found on the Council website at [ccc.govt.nz/liquefaction](http://ccc.govt.nz/liquefaction). Depending on the liquefaction potential of the area that the property is in, the Council may require site-specific investigations before granting future subdivision or building consent for the property.

### ┆ Softground

Council records show that site contains Soft Ground. Predominant Ground Material: N/A Reason for Assessment: Subdivision Should further buildings be proposed on this site, specific foundation design may be required.

## Related information

┆ There is attached a sub division soil investigation report covering this property.

## 2. Private and public stormwater and sewerage drains

Section 44A(2)(b) LGOIMA. This is information about private and public stormwater and sewerage drains as shown in the Council's records.

( For stormwater and sewerage enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### 1 Property within Local Pressurised Sewer System Zone

This property is in a local pressure sewer system catchment within the Christchurch wastewater network. If there is a house on the property, there will already be a wastewater pressure pump and tank. If a house is yet to be built, a new wastewater pressure pump and tank will need to be installed. General information about pressure sewer systems can be found on the Council website. More detailed information can be obtained by contacting Council Customer Services on 03 941 8999.

### Related information

- 1 The property is shown to be served by an on-site septic tank disposal system.
- 1 No details of the private stormwater system serving this property are shown on the plan or on Council records.
- 1 This property has been identified as being in a pressurised wastewater system zone and attached is a copy of the systems user guide. For more information you can refer to <https://ccc.govt.nz/services/water-and-drainage/wastewater/about-wastewater/types-of-wastewater-systems> or contact Christchurch City Councils 3 waters unit on (03) 941-8999.

### 3. Drinking Water Supply

*Section 44A(2)(ba) and (bb) LGOIMA. This is information notified to the Council about whether the land is supplied with drinking water, whether the supplier is the owner of the land or a networked supplier, any conditions that are applicable, and any information the Council has about the supply.*

Please note the council does not guarantee a particular water quality to its customers. If you require information on current water quality at this property please contact the Three Waters & Waste Unit.

( For water supply queries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

#### Water Supply

Christchurch City Council is the networked supplier of water to this property. This property is connected to the Christchurch City Council Water Supply. The conditions of supply are set out in the Christchurch City Council Water Supply, Wastewater & Stormwater Bylaw (2014), refer to [www.ccc.govt.nz](http://www.ccc.govt.nz).

## 4. Rates

Section 44A(2)(c) LGOIMA. This is information on any rates owing in relation to the land.

( For rates enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (a) Annual rates

Annual rates to 30/06/2021: \$ 18,496.32

	Instalment Amount	Date Due
Instalment 1	\$ 4,623.98	31/08/2020
Instalment 2	\$ 4,623.98	30/11/2020
Instalment 3	\$ 4,623.98	28/02/2021
Instalment 4	\$ 4,624.38	31/05/2021

Rates owing as at 18/06/2021: \$ 0.00

### (b) Excess water charges

\$ 0.00

( For water charge enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (c) Final water meter reading required?

No Reading Required

( To arrange a final water meter reading, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

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4 Glovers Road

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[www.ccc.govt.nz](http://www.ccc.govt.nz)

## 5. Consents, certificates, notices, orders, or requisitions affecting the land and buildings

*Section 44A(2)(d) LGOIMA. This is information concerning any consent, certificate, notice, order, or requisition, affecting the land or any building on the land, previously issued by the Council.* The information in this section may also cover building consent and/or code compliance information issued by building certifiers under the Building Act 1991 and building consent authorities that are not the Council under the Building Act 2004.

You can check the property file to identify whether any consent or certificate was issued by a building certifier under the Building Act 1991.

*Section 44A(2)(da) LGOIMA. The information required to be provided to a territorial authority under section 362T(2) of the Building Act 2004. There is currently no information required to be provided by a building contractor to a territorial authority under section 362T(2) of the Building Act 2004. The Building (Residential Consumer Rights and Remedies) Regulations 2014 only prescribed the information that must be given to the clients of a building contractor.*

( For building enquiries, please phone (03) 941 8999, email [EPADutyBCO@ccc.govt.nz](mailto:EPADutyBCO@ccc.govt.nz) or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (a) Consents

- | BCN/2003/2479 Applied: 07/04/2003 Status: Completed  
4 Glovers Road Halswell  
Accepted for processing 07/04/2003  
PIM Granted 22/04/2003  
PIM Issued 22/04/2003  
Building consent granted 22/08/2003  
Building consent issued 02/09/2003  
Code Compliance Certificate Granted 30/10/2003  
Code Compliance Certificate Issued 30/10/2003  
ALTER TO FAMILY FLAT- Historical Reference ABA10033765

### (b) Certificates

*Note: Code Compliance Certificates were only issued by the Christchurch City Council since January 1993.*

### (c) Notices

### (d) Orders

### (e) Requisitions

## Related information

- | Council holds no record of building permit/consent for dwelling at this address. No information is held by Council relating to the materials, construction or year the dwelling was built.
- | The Council has previously issued other consents, certificates, notices, orders, and/ or requisitions for this property that have been resolved or are no longer current or relate to a building that is no longer on the land. For further information please contact the compliance and investigation team on 941 8999 and reference CSR92185809.

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## 6. Certificates issued by a building certifier

Section 44A(2)(e) LGOIMA. This is information notified to the Council concerning any certificate issued by a building certifier pursuant to the Building Act 1991 or the Building Act 2004.

( For building enquiries, please phone (03) 941 8999, email [EPADutyBCO@ccc.govt.nz](mailto:EPADutyBCO@ccc.govt.nz) or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

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## 7. Weathertightness

*Section 44A(2)(ea) LGOIMA. This is information notified to the Council under section 124 of the Weathertight Homes Resolution Services Act 2006.*

( For weathertight homes enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

*If there is no information below this means Council is unaware of any formal Weathertight Homes Resolution Services claim lodged against this property.*

## 8. Land use and conditions

Section 44A(2)(f) LGOIMA. This is information relating to the use to which the land may be put and conditions attached to that use. The planning information provided below is not exhaustive and reference to the Christchurch District Plan and any notified proposed changes to that plan is recommended: <https://ccc.govt.nz/the-council/plans-strategies-policies-and-bylaws/plans/christchurch-district-plan/>.

There maybe some provisions of the Christchurch City Plan or Banks Peninsula District Plan that affect this property that are still operative.

( For planning queries, please phone (03) 941 8999, email [DutyPlanner@ccc.govt.nz](mailto:DutyPlanner@ccc.govt.nz) or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### ┆ **Regional plan or bylaw**

There may be objectives, policies or rules in a regional plan or a regional bylaw that regulate land use and activities on this site. Please direct enquiries to Canterbury Regional Council (Environment Canterbury).

### ┆ **Waterway Provisions for Other Councils**

A resource consent or permit may also be required from the Canterbury Regional Council or other territorial authority, particularly with respect to water bodies managed by those authorities. Please refer to the relevant regional plan and any relevant bylaws, and contact the Christchurch City Council if you are uncertain which authority manages the water body in question.

## **(a) (i) Christchurch City Plan & Banks Peninsula District Plan**

### **(ii) Christchurch District Plan**

#### ┆ **Liquefaction Management Area (LMA)**

Property or part of property within the Liquefaction Management Area (LMA) Overlay which is operative.

#### ┆ **Outline Development Plan**

Property or part of property is within an Outline Development Plan area which is affected by specific provisions that are operative.

#### ┆ **Remainder Slope Instability Management Area**

Property or part of property within the Christchurch District Plan Remainder of Port Hills and Banks Peninsula Slope Instability Management Area overlay.

#### ┆ **Waterway Provisions**

This property or part of this property is close to at least one waterway. It may be within the setback for an Environmental Asset Waterway. Within that setback, District Plan rules apply to activities including buildings, earthworks, fences and impervious surfacing. Any part of the property within the setback will be affected by those rules.

#### ┆ **Development Constraint Conditions**

Council records show there is a specific condition on the use of this site: Well on Property

#### ┆ **Development Constraint Conditions**

Council records show there is a specific condition on the use of this site: Specific Site Level required

† **Flood Management Area**

Property or part of property within the Flood Management Area (FMA) Overlay which is operative.

† **District Plan Zone**

Property or part of property within the Residential New Neighbourhood Zone which is operative.

**(b) Resource consents**

If there are any land use resource consents issued for this property the Council recommends that you check those resource consents on the property file. There may be conditions attached to those resource consents for the property that are still required to be complied with.

† RMA/2003/1909 - Land Use Consent

4 Glovers Road Halswell

Application to convert an existing studio into a family flat - Historical Reference RMA20014216

Status: Processing complete

Applied 25/07/2003

Decision issued 13/08/2003

Granted 13/08/2003

† RMA/2017/1463 - Land Use Consent

4 Glovers Road Halswell

To establish a Temporary Storage Yard

Status: Processing complete

Applied 26/06/2017

Granted 13/02/2019

Decision issued 13/02/2019

† RMA/2020/2557 - Land Use Consent

2 Glovers Road Halswell

Remediation of contaminated soils

Status: Processing complete

Applied 06/11/2020

Granted 09/12/2020

Decision issued 09/12/2020

† RMA/2020/2770 - Land Use Consent

511 Halswell Road Halswell

To conduct earthworks and stockpiling on site

Status: Processing complete

Applied 27/11/2020

Granted 27/01/2021

Decision issued 27/01/2021

Property address:

4 Glovers Road

- | RMA/2020/3076 - Combined subdivision / land use consent  
511 Halswell Road Halswell  
To subdivide 4 allotments to create 87 residential allotments. Land use consent for earthworks and under the NES for contaminated land.  
Status: On hold - waiting for response from applicant  
Applied 22/12/2020
  
- | RMA/1999/5158 - Subdivision Consent  
Fee Simple SUBDIVISION - Historical Reference RMA4366  
Status: Processing complete  
Applied 30/04/1999
  
- | RMA/2000/1933 - Subdivision Consent  
2 LOT FEE SIMPLE APP 223 recieved 29/9/00 certified 9/10/00 224 REQUESTED 08/03/01 Issued 13/3/01 DP 83635  
- Historical Reference RMA20002667  
Status: Processing complete  
Applied 02/08/2000  
Granted 22/08/2000  
Decision issued 22/08/2000

## Related information

- | Council records show that there is a current/on hold monitoring job in our system. This monitoring is to ensure that the resource consent conditions have been met. For further information you can contact the Compliance & Investigation team A on 941 8999 or email: [rcmon@ccc.govt.nz](mailto:rcmon@ccc.govt.nz) and reference to resource consent RMA/2020/2770 - RMA/2020/2557.

## 9. Other land and building classifications

*Section 44A(2)(g) LGOIMA. This is information notified to the Council by any statutory organisation having the power to classify land or buildings for any purpose.*

( For land and building enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

Please refer to Section 1 for details

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## 10. Network utility information

*Section 44A(2)(h) LGOIMA. This is information notified to the Council by any network utility operator pursuant to the Building Act 1991 or the Building Act 2004.*

( For network enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

! **None recorded for this property**

## 11. Other information

Section 44A(3) LGOIMA. This is information concerning the land that the Council has the discretion to include if it considers it to be relevant.

( For any enquiries, please phone (03) 941 8999 or visit [www.ccc.govt.nz](http://www.ccc.govt.nz).

### (a) Kerbside waste collection

- | Your recycling is collected Fortnightly on the Week 2 collection cycle on a Tuesday. Please leave your recycling at the Kerbside by 6:00 a.m. Your nearest recycling depot is the Parkhouse Road EcoDrop.
- | Your refuse is collected Fortnightly on the Week 2 collection cycle on a Tuesday. Please leave your rubbish at the Kerbside by 6:00 a.m. Your nearest rubbish depot is the Parkhouse Road EcoDrop.
- | Your organics are collected Weekly on Tuesday. Please leave your organics at the Kerbside by 6:00 a.m.

### (b) Other

#### | Floor Levels Information

Christchurch City Council holds a variety of information relevant to building/property development across the city. This includes minimum finished floor levels that need to be set to meet the surface water requirements in clause E1.3.2 of the building code (where this applies), and the requirements of the Christchurch District Plan (where a property is in the Flood Management Area). Where this information has been processed for your site, it can be viewed at <https://ccc.govt.nz/floorlevelmap/>, otherwise site specific advice can be obtained by emailing [floorlevels@ccc.govt.nz](mailto:floorlevels@ccc.govt.nz).

#### | Community Board

Property located in Halswell-Hornby-Riccarton Community Board.

#### | Guest Accommodation

Guest accommodation (including whole unit listings on Airbnb; BookaBach; etc.) generally requires a resource consent in this zone when the owner is not residing on the site. For more information, please refer to: <https://ccc.govt.nz/providing-guest-accommodation/>.

#### | Tsunami Evacuation Zone

This property is not in a tsunami evacuation zone. It is not necessary to evacuate in a long or strong earthquake or during an official Civil Defence tsunami warning. Residents may wish to offer to open their home to family or friends who need to evacuate from a tsunami zone, and should plan with potential guests to do so in advance. More information can be found at <https://ccc.govt.nz/services/civil-defence/hazards/tsunami-evacuation-zones-and-routes/>

#### | Electoral Ward

Property located in Halswell Electoral Ward

#### | Listed Land Use Register

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Hazardous activities and industries involve the use, storage or disposal of hazardous substances. These substances can sometimes contaminate the soil. Environment Canterbury identifies land that is used or has been used for hazardous activities and industries. This information is held on a publically available database called the Listed Land Use Register (LLUR). The Christchurch City Council may not hold information that is held on the LLUR. Therefore, it is recommended that you check Environment Canterbury's online database at [www.llur.ecan.govt.nz](http://www.llur.ecan.govt.nz)

## I **Spatial Query Report**

A copy of the spatial query report is attached at the end of this LIM. The spatial query report lists land use resource consents that have been granted within 100 metres of this property.

# Geotechnical Investigation and Assessment Report for Subdivision

Riverstone Subdivision, 2 & 4 Glovers Road, Halswell, Christchurch

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Issue Date: **20 October 2020**



Document Ref: **200357-RP-001[A]**

Prepared for: **Yoursection Ltd**

**Report Tracking - 2 & 4 Glovers Road, Halswell, Christchurch**

Revision	Status	Date	Prepared by	Reviewed by
A	Final	20 October 2020	C. Gibbens	A. Giannakogiorgos

**Authorisation**

<b>Author's Signature</b>		<b>Approver's Signature</b>	
<b>Name</b>	Clem Gibbens	<b>Name</b>	Andreas Giannakogiorgos
<b>Title</b>	Engineering Geologist BSc MSc (Hons) MEngNZ	<b>Title</b>	Chartered Professional Engineer (Geotechnical) BSc MSc DIC CMEngNZ CPEng IntPE (NZ)

**Miyamoto International New Zealand Ltd**  
Level 1, 236 Hereford Street | Christchurch 8011

[www.miyamoto.nz](http://www.miyamoto.nz)

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## Executive Summary

Miyamoto International NZ Ltd (MINZ) has been engaged by Yoursection Ltd to undertake a geotechnical land suitability assessment for the proposed residential subdivision at 2 & 4 Glovers Road, Halswell, Christchurch. The key findings of our evaluation and assessment are outlined below.

<b>GROUND CONDITIONS</b>	<b>Ground profile</b>	The sub-surface conditions comprise mainly topsoil over sand-silt mixtures underlain by soft clayey silts and shallow gravel. The ground conditions are variable in horizontal and vertical spread.	
	<b>Soil classification as per NZS 1170.5:2004</b>	Residential Subdivision Area: Class 'D' (deep or soft soil site)	
	<b>Depth to water table</b>	Perched water tables and shallow saturated soils were encountered within the top 1.0 to 2.0m bgl. Permanent ground water is anticipated below the soft silts within the underlying sands and gravels.	
<b>SEISMIC ASSESSMENT</b>	<b>Design Earthquake Event</b>	<b>SLS/SLS2</b>	<b>ULS</b>
	<b>Estimated "free-field" Index post-liquefaction volumetric settlements</b>	< 50mm	< 80mm
	<b>Liquefaction Severity Number (LSN) Value</b>	< 15 Little to minor expression of liquefaction	< 25 Little to moderate expression of liquefaction
	<b>MBIE Technical Categorization (TC)</b>	<b>Mapped MBIE</b>	Rural & Unmapped
		<b>Site Specific Foundation TC</b>	TC2
<b>GEOTECHNICAL CONSIDERATIONS</b>	<p>Our assessment of the site under RMA Section 106 found that the subsidence hazard is present on-site due to presence of soft/loose soil layers and liquefiable deposits, though these hazards can be mitigated by the options listed in this report.</p> <p>As the site is located within an FMA set out by CCC, a portion of the site will require filling to raise the ground level to a suitable level for the proposed development by around 1.0m close to Green's Stream. Filling of the site will likely cause static some consolidation settlements in the soft compressible soils underlying the site, though this is not expected to be a significant risk to the development, based on the pre-loading trial undertaken by MINZ previously. A period of monitoring of the site filling works during the raising of the site levels and for a period (~6 months) is advised to be safeguard against the anticipated static settlements.</p>		

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### Appendices

- A. Updated Indicative Subdivision Plan (Davie Lovell Smith)
- B. ECan Listed Land Use Register Files
- C. Geotechnical Investigation Results
- D. Southern Geophysical MASW and GPR Report
- E. Geotechnical Cross Sections
- F. Liquefaction Analyses

## 1. Introduction

Miyamoto International NZ Ltd (Miyamoto) has been engaged by Yoursection Ltd to undertake a geotechnical evaluation and assessment as part of a land suitability assessment for the proposed new extension of the residential Riverstone Subdivision at 2 & 4 Glovers Road, Halswell, Christchurch.

Miyamoto have previously completed a geotechnical assessment for resource consenting purposes for the initial stage of the Riverstone Subdivision located at 511 Halswell Road, Christchurch (190666-RP-001[A] – 511 Halswell Road, dated 10 October 2019), as well as undertaking a trial pre-load assessment for the same property (190666-TM-001[A]\_511 Halswell Road\_Pre-load Trial, dated 28 January 2020). Both documents are referenced as part of this assessment, with this report supplementing and expanding on the work already undertaken.

The scope of this geotechnical engineering assessment was to evaluate the geotechnical conditions at the site and to provide preliminary recommendations for development of the sections. This assessment comprised the following:

- Research of the available information from the New Zealand Geotechnical Database (NZGD), Christchurch City Council (CCC) and Environment Canterbury (ECan);
- Site walkover inspection of the land;
- Shallow field investigation comprising hand-augered boreholes (HA) with associated dynamic cone penetrometer (DCP) and shear vane (SV) tests;
- Deep field investigation comprising Cone Penetration Tests (CPT) with accompanying Dynamic Probe Super Heavy (DPSH) testing;
- Multichannel Analysis of Surface Waves (MASW) geophysical survey;
- Ground Penetrating Radar (GPR) geophysical survey;
- Liquefaction analyses using CPT-based liquefaction triggering procedures;
- Reporting of the findings.

The geotechnical investigation and assessment were carried out considering the Ministry of Business, Innovation & Employment (MBIE) Guidance documents “Planning and engineering guidance for potentially liquefaction-prone land” - Version 1, dated September 2017, “Repairing and rebuilding houses affected by the Canterbury earthquakes” - Version 3, dated December 2012, and “Earthquake geotechnical engineering practice - Modules 2 & 3”. This report presents our findings and conclusions which are provided to facilitate the development of the extended subdivision plan for the site.

## 2. Site Description

The site, legally described as Lot 1 (2 Glovers) and Lot 2 (4 Glovers) DP 83635, is in Halswell, Christchurch and is approximately 8.3 hectares (ha) in total area. There is an approximate elevation change of 2.0m over 460m at an average gradient of 0.4%. The site generally slopes from north to south, with the low point at the southern boundary of both sections. The property is bound by Glovers Road along the northern boundaries and is bound by rural

properties on the south and east boundaries, and the 511 Halswell Road section to the west. Green's Stream runs through the southern end of both sections.

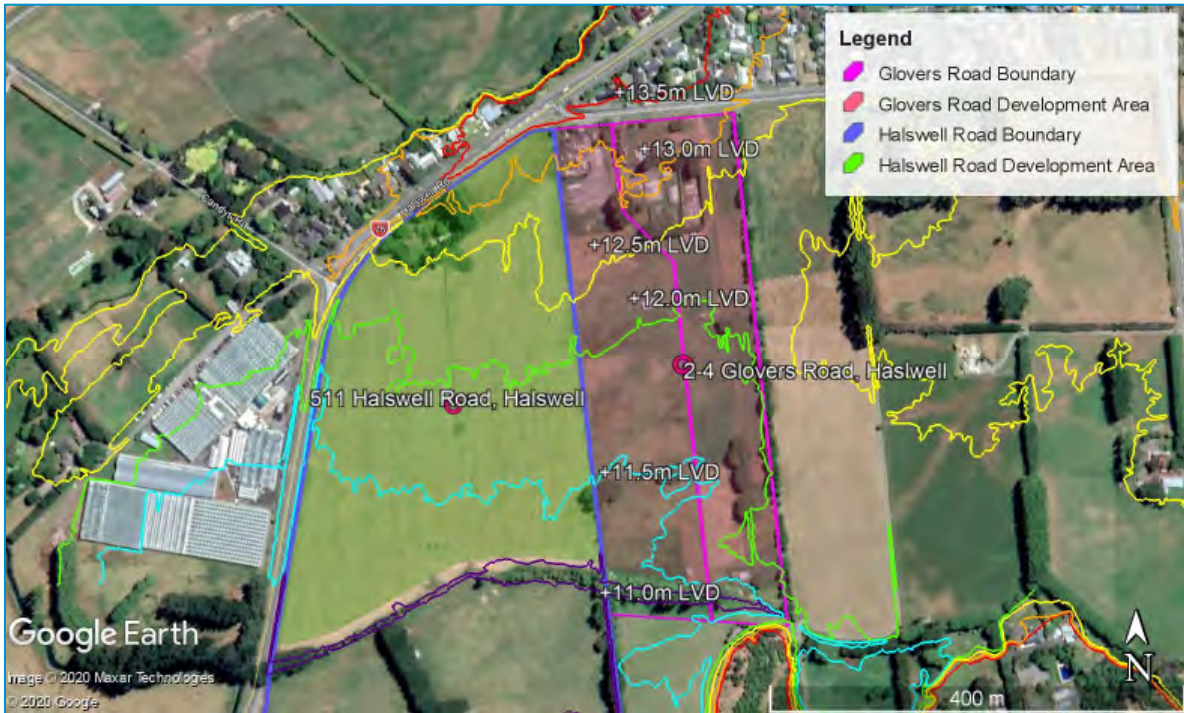


Figure 1: Proposed Site Layout with (Scale as Shown)

The property is located within the “Rural and Unmapped” category listed under the MBIE Technical Categories Map. The site location with reference to the MBIE Technical Categories is shown in Figure 2.

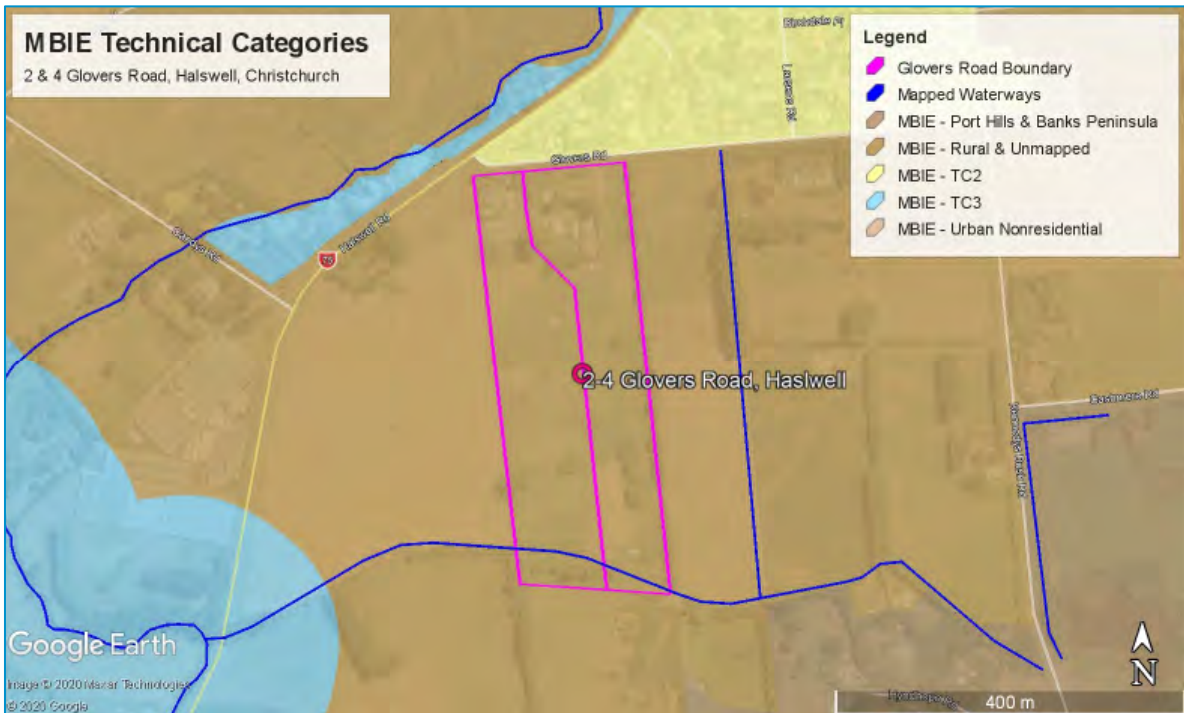


Figure 2: Site Location Plan Showing MBIE Technical Categories and Mapped Waterways (Scale as Shown)

The Riverstone Subdivision is proposed to, currently, be comprised of 239 residential lots with reserves located throughout. A draft plan of the subdivision, including the Glovers Road properties, is presented in Appendix A.

### 3. Desk Study

The following sources of third-party information were considered and are referenced in this report:

- New Zealand Geotechnical Database (NZGD);
- Environment Canterbury (ECan);
- Christchurch City Council (CCC).

#### New Zealand Geotechnical Database

The NZGD website was reviewed to identify any additional information related to the extent of land damage after the CES on the site and in the immediate surrounding areas. The results of this review indicate that no significant land damage was observed across the site. Table 1 provides a summary of the information obtained from our review of the NZGD.

Table 1: Desk Study Information Summary (NZGD)

	September 2010 (M <sub>w</sub> 7.1)	February 2011 (M <sub>w</sub> 6.2)	June 2011 (M <sub>w</sub> 6.0)	December 2011 (M <sub>w</sub> 5.9)
<i>Aerial Photography Review</i>	Outside of photographed area	Areas of likely ejecta identified in the central and northern areas of both properties, though mainly confined to 2 Glovers Road	Outside of photographed area	Outside of photographed area
<i>Land damage observations</i>	Minor ground cracking but no observed ejected liquefied material was recorded on the properties on the opposite side of Glovers Road in the September 2010 CES event and along Halswell Road and sections of Glovers Road during the June 2011 CES event.			
<i>Observed ground cracking</i>	No cracks mapped on the properties, 10mm – 200mm ground cracks mapped ~65m west of the northernmost boundary of the site within the residential area on the opposite side of Halswell Road			
<i>PGA (g) ± SD</i>	0.294 ± 0.390	0.356 ± 0.435	0.145 ± 0.465	0.139 ± 0.250
<i>Scaled PGA<sub>7.5</sub> PGA<sub>16%ile</sub> to PGA<sub>84%ile</sub><sup>(1)</sup> (g)</i>	0.179 to 0.394	0.164 to 0.391	0.061 to 0.156	0.071 to 0.117

(1) Scaled to M7.5 using Idriss and Boulanger recommendations (2008); 68% confidence PGA<sub>7.5</sub> range



## Contaminated Land Considerations

The ECan Listed Land Use Register (LLUR) was reviewed and holds records of potentially Hazardous Activities and Industrial List (HAIL) sites. At this time, a small area that intersects the southern end of both sections is listed as a potential HAIL site. The LLUR lists this small area (in the vicinity of a storage shed) as an A10-classified area, which relates to “persistent pesticide bulk storage or use including sports turfs, market gardens, orchards, glass houses or spray sheds”, though this has not been investigated by ECan. The property reports for both sections are included in Appendix B.

An environmental assessment is outside the scope of this assessment and has been undertaken by others.

## Flood Hazard

Christchurch is a low-lying city and there have always been areas that are prone to flooding during heavy rainfall. The CES has worsened flood risk in many areas of the city through damage to waterways and land. Flood Management Areas (FMAs) have been identified by CCC in the District Plan and take into consideration the impacts of the CES.

At the time of writing this report the site is located within a FMA as indicated by the CCC District Plan.

It is understood that a Finished Floor Level (FFL) of 21.25m above Christchurch Drainage Datum (CDD) is a requirement for development of the site.

## Ground Motion

Using the MBIE and Bradley & Hughes (2012) procedures, we have found that the site was “sufficiently tested” to the Serviceability Limit State (SLS) level of earthquake demand during the September 2010 and February 2011 events of the CES. This indicates that land and building damage in a future SLS event is likely to be similar to these individual events.

Additionally, based on the SLS2 level of shaking ( $M_w$  6.0 and PGA of 0.19g) which was introduced by MBIE following the updated liquefaction triggering CPT-based procedure by Boulanger & Idriss (2014), it is our opinion the site was “sufficiently tested” to the SLS2 level of earthquake demand during the September 2010 and February 2011 events of the CES.

Utilising a derivation of the Bradley and Hughes method, we can suggest that the site was not tested to Ultimate Limit State (ULS) level of shaking during the CES. Based on the probabilistic analysis of the PGAs experienced at the site, the nature of land and building damage is likely to be more severe during a future ULS event than that already experienced during the individual CES events.

## 4. Subsurface Conditions

### Geological Setting

The geological map of the area (GNS 1:250,000 QMap) indicates that most of the site has surface geology consisting of “modern (Quaternary) river floodplain and low-level degradation terraces (<2° slopes) comprised of unweathered, variably sorted gravel/sand/silt/clay”.

## Field Investigations

The NZGD website was reviewed to identify relevant geotechnical investigations completed within the site vicinity, additional to the data identified for use in the original site assessment for the neighbouring section, though nothing for inclusion was identified.

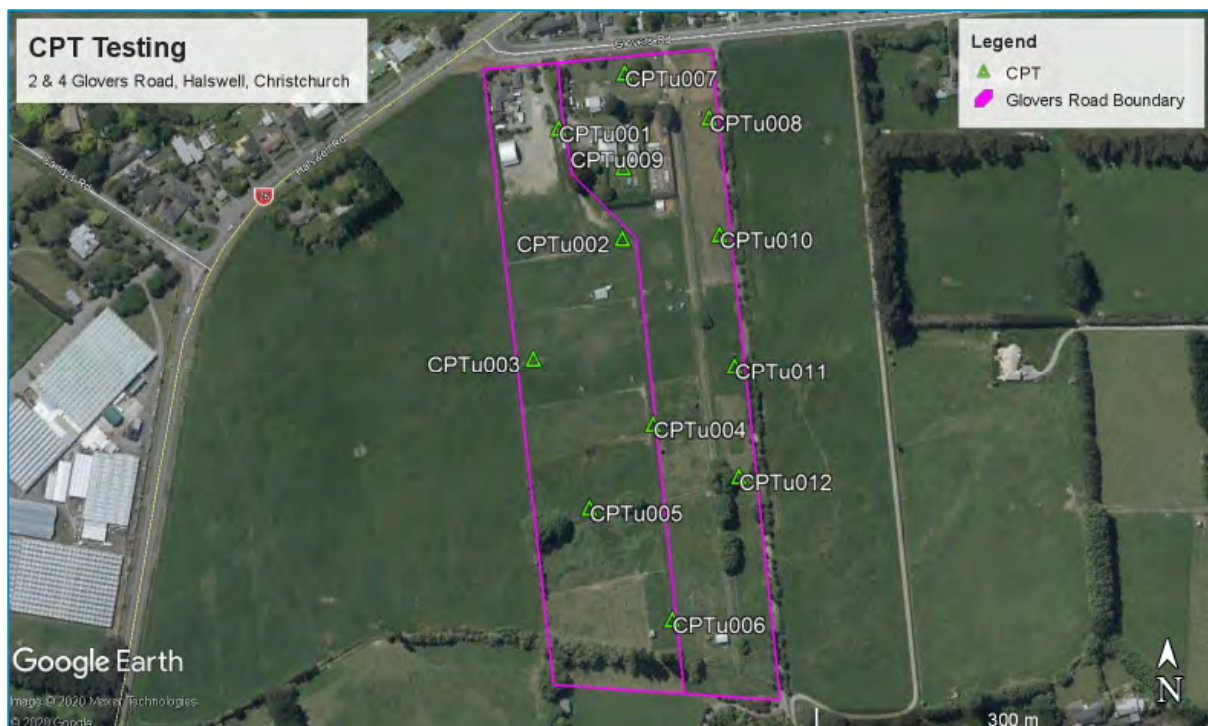
Miyamoto undertook the following site-specific ground investigations and testing:

- Five (5) hand-augered boreholes (referenced HA1 to HA5) with in-situ shear vane testing;
- Five (5) Dynamic Cone Penetrometer (DCP) tests (referenced DCP1 to DCP5);
- Laboratory testing including fines content (FC) and Atterberg Limits;
- Twelve (12) Cone Penetration Tests (CPTu) with porewater pressure measurements;
- Multichannel Analysis of Surface Waves (MASW) geophysical survey;
- Ground Penetrating Radar (GPR) geophysical survey.

The general details of the ground investigations are summarised in Table 2, the test locations are shown in Figure 3 and Figure 4, and the HA/DCP logs and CPT plots are presented in Appendix C and the geophysical survey report is presented in Appendix D.

**Table 2: Summary of Ground Investigations**

Test Ref.	Source	Source Ref.	Test Type	Depth (m bgl)
HA1/DCP1 to HA5/DCP5	MINZ	200357	Hand Auger/ DCP	1.8 to 3.9
CPTu001 to CPTu012	LandTest	19096	CPT	10.0 to 15.0
MASW 1 to MASW 3	Southern Geophysical Ltd	2050	MASW	Up to 40.0
GPR 1 to GPR 11			GPR	Up to 4.0



**Figure 3: CPT Investigation Location Plan (Scale as Shown)**

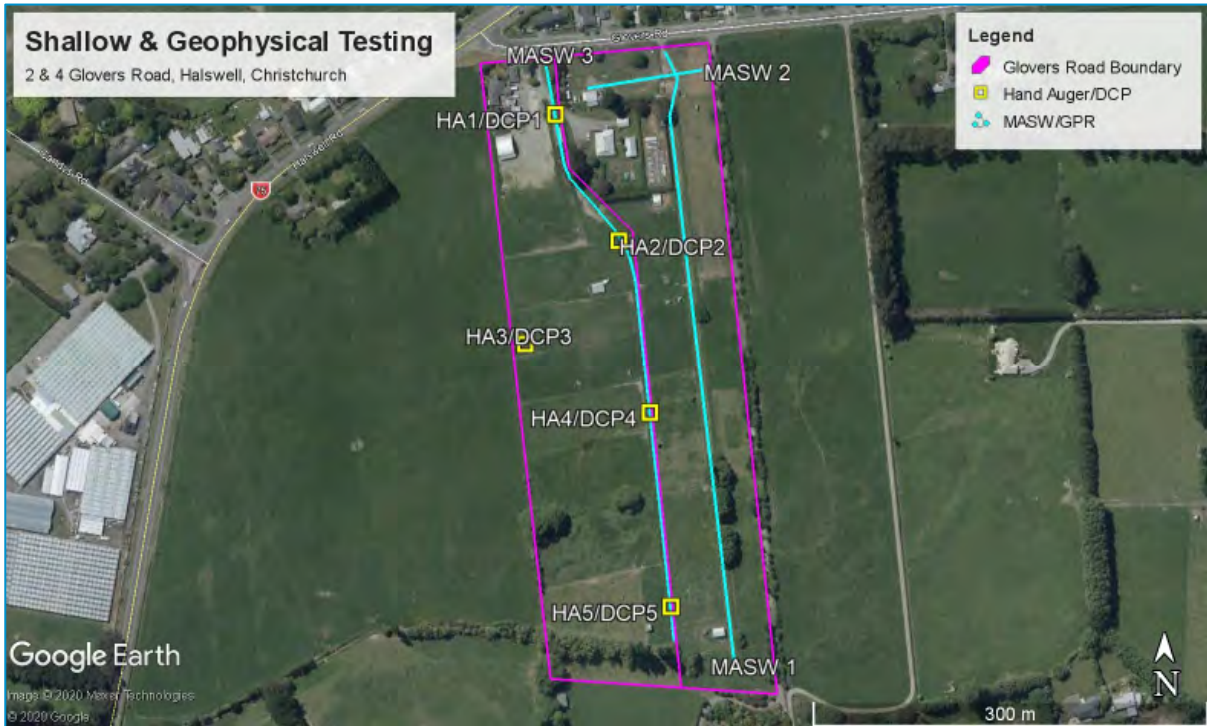


Figure 4: Other Geotechnical Investigation Location Plan (Scale as Shown)

### Laboratory Test Results

Laboratory testing was undertaken on samples obtained from our shallow ground investigation to assess the soil characteristics across the site. The testing undertaken includes wet sieving to determine the fines content, and Atterberg limits tests to determine the plastic and liquid limits. A summary of the test results is presented in Table 3, with the full results presented in Appendix C.

Table 3: Laboratory Test Results

Sample Ref.	Depth of sample (m)	Soil Description	Plasticity Index	% Passing		
				0.3 mm	0.15 mm	0.063 mm
C20-319	HA1 1.5m – 2.3m	Silty SAND, brownish grey, wet, non-plastic	-	100	90	49
C20-320	HA1 2.3m – 3.8m	Silty SAND, brownish grey, saturated, non-plastic	-	100	91	49
C20-321	HA2 2.7m – 4.0m	Silty CLAY, some sand, dark grey, saturated, low plasticity	9	99	96	85
C20-312	HA3 2.0m – 3.4m	Sandy SILT, dark grey, saturated, non-plastic	NP	100	99	59
C20-323	HA5 1.5m – 1.8m	Silty SAND, brownish grey, wet, non-plastic	-	99	77	42

## Ground Conditions

The ground conditions interpreted from the existing data and investigations undertaken as part of this assessment are presented graphically in the geotechnical cross sections included in Appendix E and the basic soil descriptions are outlined in Table 4.

A near-surface paleo-feature (old river terrace or paleochannel) was identified during the site testing with the CPT's completed at the southern end of the site (CPTu004 to CPTu006 and CPTu012) refusing in dense soils within the upper 5m, before testing was continued with the DPSH. The shallow investigation (HA5/DCP5) also refused at a shallow depth due to dense soils. The testing at the northern end of the site all reached the target depths and were consistent in their findings.

Table 4: Ground Conditions Summary

Layer	Soil Name
a	Silty SAND and Sandy SILT, loose to firm
b	Clayey SILT, soft to firm, medium plasticity
c	Silty SAND, medium dense to dense with increasing depth
GS	Gravelly SAND to Sandy GRAVEL, dense
d	Clayey SILT to silty CLAY, firm
e	Medium dense SAND with silt and gravels
f	Clayey SILT, firm to stiff
S	Silty SAND to Sandy SILT, medium dense to very stiff

## MASW & GPR Geophysical Survey

The shear wave velocity ( $V_s$ ) measurement was assessed with a MASW survey. The results of the survey were used to refine the boundaries and extents between the shallow, softer soils and denser sandy/gravelly layers with the MASW survey reflecting the findings of the intrusive investigations, with 2 clearly defined areas for the north and south of the site. The soils in the northern part of the site had a generally lower shear wave velocity ( $V_s < 180\text{m/s}$ ) to approximately 20.0m depth, though discrete layers of denser, higher  $V_s$  soils were identified above this depth before becoming lower velocity again. For the southern part of the site, the lower  $V_s$  soils are generally terminated shallower (<5m depth) before the  $V_s$  increased in the gravelly dense material.

Additionally, the measured cone tip resistance ( $q_c$ ) and interpreted shear wave velocity from the CPT data generally shows a consistent pattern with the recorded values from the MASW survey as seen in the CPT profiles in Appendix C. It should be noted that due to the high velocity layers towards the south, thin lower velocity layers were not picked up as seen in the DPSH data. This is reflected in the cross sections presented in Appendix E.

The GPR survey was undertaken to further supplement the MASW surveys for the near-surface soils. The primary objective of this survey was to assist in identifying softer or denser layers that may not have been picked up in the MASW survey. The results generally show a consistent correlation with the MASW survey. The softer soils generally had a poor reflection, with denser material showing a clearer reflection. The shallow gravelly soils at the southern end of the site were also clear within the upper 4.0m of the soil profile.

## Groundwater

Our site-specific shallow investigation encountered groundwater levels between 1.0m and 1.8m bgl, however the cohesive soils below the recorded depth were noted to not be saturated, indicating that a perched water table is likely present on-site. The CPT data shows variable piezometric conditions indicating a groundwater table depth between 0.7m and 2.4m bgl, due to the differing depth of cohesive soils in the upper soil profile and different elevations. The shallower groundwater depths were generally confined to the lower elevations of the property.

Based on the above, a groundwater depth range of between 0.7m to 2.4m bgl was adopted for the liquefaction triggering and free-field settlement assessment, depending on the location of the test across the site.

## Site Subsoil Class

Based on the site-specific investigation, geological maps and other available information, the site is classified as a Class D (deep or soft soil) site.

## Shallow Soils

The geotechnical investigations indicate the existence of low velocity ( $V_s \leq 180\text{m/s}$ ), soils between approximately 4.0m and 20.0m depth, with the lower  $V_s$  soils encountered at greater depths towards the north of the sections. There are also locations where denser pockets of material were identified within these lower  $V_s$  layers. Those layers have lower strength and have the potential for long-term consolidation settlements from loads, such as residential dwellings. This is further discussed later in this report.

# 5. Liquefaction Assessment

## Methodology

An assessment of the earthquake-induced free-field post-liquefaction volumetric settlement at the site has been carried out in accordance with the MBIE Guidance and using proprietary liquefaction assessment software, for SLS and ULS earthquake scenarios.

The seismic design requirements adopted for use in the analyses are defined in MBIE/NZGS Earthquake Geotechnical Engineering Practice Module 3 (May 2016), and Part C of the MBIE Guidelines “Repairing and rebuilding houses affected by the Canterbury earthquakes” and its subsequent updates - clarifications. These are:

- Buildings of normal use (Importance Level 2);
- Deep or soft soil sites (Class D) as specified previously;

- Boulanger and Idriss (2014) methodology for liquefaction triggering, as per the MBIE Guidance subsequent updates (Issue 7, October 2014);
- Zhang et al. (2002) post-liquefaction volumetric strain calculation for estimating the free-field settlements;

Calculations were performed for the full depth of the CPTs and the upper 10m of the soil profile (as per the MBIE Guidance “index value” estimations). It should be noted that the settlement estimates only account for the free-field component of the expected settlement. Actual total settlements under SLS or ULS earthquake loading may be greater or less.

The Liquefaction Severity Number (LSN<sup>1</sup>) has been calculated and used in our assessment as it tends to better reflect the more damaging effects of shallow liquefaction, which is more critical for shallow founded structures. The level of ground damage associated with LSN is summarised in Table 5.

**Table 5: Liquefaction Severity Number Ranges and Related Effects**

LSN Value	Observed Performance
<10	Little to no expression of liquefaction, minor effects
10 – 20	Minor expression of liquefaction, some sand boils
20 – 30	Moderate expression of liquefaction, with sand boils and some structural damage
30 – 40	Moderate to severe expression of liquefaction, settlement can cause structural damage
40 – 50	Major expression of liquefaction, undulations and damage to ground surface, sever total and differential settlement of structures
>50	Severe damage, extensive evidence of liquefaction at surface, sever total and differential settlements affecting structures, damage to services

### Liquefaction Assessment Results

Due to the rapid changes at the interface between fine and coarse-grained soils, a layer correction was applied. The cone tip penetration, and subsequently, the ability to resist liquefaction of a sandy material, is reduced by the surrounding silty layers, while the  $I_c^2$  of the silt layers is reduced due to the presence of the surrounding sandy layers and hence the susceptibility of the fine layers is overestimated. For our analysis, an  $I_c$  change of >0.05 per 10mm has been adopted, which eliminates the liquefaction potential for the layer.

The results of our liquefaction triggering analyses utilising the CPT data are presented in Appendix F and summarised in Table 6.

<sup>1</sup> **LSN = Liquefaction Severity Number.** LSN (van Ballegooy et al., 2014) is a vulnerability indicator (damage index) quantifying liquefaction-induced damage developed to reflect more damaging effects of shallow liquefaction on residential land and foundations following the Canterbury Earthquakes (2010-11). LSN considers depth weighted calculated volumetric densification strain within soil layers as a proxy for the severity of liquefaction land damage likely at the ground surface.

<sup>2</sup>  **$I_c$  = Soil Behaviour Classification Index** - Robertson & Wride 1998.

Table 6: Estimated “Free-Field” Post-Liquefaction Volumetric Ground Surface Settlements

Earthquake scenario	Moment magnitude ( $M_w$ ) / PGA (g)	MBIE “Index Value” (mm)	MBIE Technical Category	LSN Values
GWD = varying (in-situ) and 0.5m to 1.2m (earthquake); Layer transition applied				
SLS	7.5/0.13	< 35	TC2	1 – 5
SLS2	6.0/0.19	5 – 50	TC2	2 – 16
ULS	7.5/0.35	5 – 80	TC2	5 – 25

In accordance with the MBIE Guidance, the analysis indicates that under SLS and ULS loading conditions the predicted index value settlements fall within the expected future land performance values for a TC2 category site. The higher settlements were located on the land at the northern area of the 2 Glovers Road section, which generally correlates with observed liquefaction ejecta in the aerial photographs.

Based on the LSN estimated for the design events, ‘little to minor’ expression of liquefaction may be expected for a future SLS design event, and ‘little to moderate’ expression of liquefaction may be expected for a future ULS design event. The values of LSN at the upper end of the ranges estimated are generally located in the central portion of the development area (where ejecta has been observed following the CES events).

### Lateral Spreading

Given the generally flat topography of the site, and the assumption that the site will be levelled further during the development of the subdivision, there is unlikely to be significant height differences, apart from the area immediately adjacent to Green’s Stream. As the area needs to be developed with the FMA in mind, and land levels lifted, there is the potential for a more pronounced ‘free-face’ that could create a risk of lateral spreading. Options to address this are discussed later in the report.

## 6. Site Designation Assessment

Based on the findings of our desk study, our site-specific ground investigation and observations, and assessment of the performance of the land, we consider the MBIE TC2 category generally appropriate for the site. Despite the deformation characteristics of TC2, the land does not meet the definition of ‘Good Ground’ as per the New Zealand Standards without modification to standard foundation systems and specific engineering design to account for this due to the soft soils.

## 7. Geotechnical Considerations for Subdivision

### Geotechnical Hazards

The most significant geotechnical hazards at the site comprise the potential for earthquake-induced soil liquefaction and potential static subsidence of the soft compressible soils. These hazards can be partly mitigated by providing strengthened foundations, which reduce the potential for differential settlement of the buildings and are designed to be re-levellable.

However, as part of the land development it is understood that, in order to meet the CCC FFL requirements, the site grade will need to be raised by filling. Site filling works can induce

additional loading of the underlying soft compressible deposits and potentially lead to consolidation settlement of the fill and / or construction above. To assess the likely influence of filling, a pre-load trial was undertaken by Miyamoto. This trial indicates that static settlements are not believed to pose a significant risk to the Halswell Road section of the development. Given the similar soil conditions found, it is our professional opinion that this statement also applies to the Glovers Road properties. It is still recommended that settlement plates are installed during the site filling works and these should be founded at the base of the fill with upstands extending through the top of the fill. It is advised that the settlement plates are monitored during the raising of the site levels and for a period (up to 6 months) to assess any static settlements and ensure performance is in line with the pre-loading trial findings.

The current subdivision plan for the entire site is not currently finalised and until it is further developed, specific detailed recommendations cannot be provided, however, the following sections outline general considerations for future development.

### Development Considerations

Based on the land survey data (provided by others), a maximum level of approximately 22.3m CDD was identified at the northern extent of property. The land drops to approximately 19.6m CDD next to Green's Stream, though the development does not extend to this point. The low point of the development area is at approximately 20.4m CDD. As discussed above, the site will require filling to meet the CCC FFL requirements (FFL = 21.25m CDD based on the Halswell Road site), particularly if the preferred foundation options comprise concrete slab foundations. It is anticipated that maximum filling would be in the proximity of 1.2m.

Currently, there is no indication of cutting or removal of material to the north of the site. All earthworks should be undertaken in accordance with NZS 4431:1989 (code of practice for earth fill for residential development) prior to the construction of any foundations. The monitoring scheme (mentioned earlier) should be fully developed once the final details of the proposed earthworks are known.

The southern extent of the filling (in proximity of Green's Stream) will be the maximum height of fill required and will require detailed design to ensure stability. It is our understanding the development area is to extend to within 15m of Green's Stream. A shallow vegetated slope is considered suitable given the height of filling is not likely to exceed 1.2m, and provided the slope is not at a gradient exceeding 1.0m vertical to 2.0m horizontal.

Based on the above and the previously completed works, the following foundation solutions would be considered suitable for the construction of NZS3604 compliant structures for the subdivision:

- MBIE TC2 (Options 1 to 4) enhanced foundation slab;
- Specifically designed, enhanced NZS 3604 perimeter foundation wall and shallow piles.



Based on development works proposed, a geotechnical ultimate bearing capacity of 200kPa can be assumed at a high level, though this value is indicative only. The available bearing capacity must be confirmed on-site prior to construction works at the time of any building consent application.

The foundation types detailed above are also preliminary and should be further developed and optimised in collaboration with the structural engineer once further details of any proposed structure are finalised.

### Stormwater Management

Stormwater management is outside the scope of our works. However, it is understood the southern section of the Halswell Road site (area south of Green's Stream) will be utilised for stormwater detention and treatment for the Riverstone subdivision as a whole, with shallow basins excavated through this area. As mentioned in the initial assessment undertaken, this material is unlikely to be suitable for filling of the development area.

### Services

Buried services are vulnerable to ground deformations when located within and/or in proximity of potentially liquefiable and compressible soils. Services for the residential development should be designed by a suitably qualified person in collaboration with the geotechnical engineers to accommodate the likelihood of future ground deformations.

### Pavement/Roading Infrastructure

As for the services at the site, pavements will require detailed design by a suitably experienced person in collaboration with the geotechnical engineer, the finished ground levels and compaction characteristics of the filling material.

It is currently understood that the new areas of development will link into the Halswell Road property as well as having its own access onto Glovers Road, and it is assumed that filling in this area will be required to raise the grade. The underlying soils in this area are generally typical for the site with the upper 1.0m comprising topsoil over soft silt (loosely corresponding to a CBR of ~2 to 3 below the topsoil).

## 8. Assessment Against RMA Section 106

As per the requirements of Section 106 of the Resource Management Act (RMA) (2017), we have undertaken a high-level assessment of the significant geotechnical hazards that may affect the site, outside of the hazards already discussed in this report (i.e. static and earthquake-induced subsidence, and lateral spreading). These hazards include, but are not limited to:

- Erosion;
- Falling debris;
- Slippage;
- Inundation.

At the time of our site visit, there was no evidence of erosion. Likewise, no evidence was observed to suggest that lateral movement is an issue on the site, given the site is generally

flat. Rock Fall or slope movement are also not considered a risk to this area of the development.

As part of the site is identified as being within a Flood Management Area (FMA) as defined by the CCC, inundation is likely to be a risk, as the site currently stands. If the site is built up to ensure the FFLs set by the CCC are met and suitable stormwater drainage is in place, then inundation is not considered an imminent risk to the development.

Based on our assessment, we consider that the “significant” geotechnical hazards may be mitigated to an acceptable standard, provided that the geotechnical recommendations given in this report are followed, and the appropriate engineering measures implemented, we consider that the development is unlikely to be affected nor worsen, accelerate or result in material damage.

## 9. Limitations

This report is subject to the following limitations:

- This report has been prepared by Miyamoto for the Client for the purpose/s agreed with the Client (Purpose). Miyamoto accepts no responsibility for the validity, appropriateness, sufficiency or consequences of the Client using the report for purposes other than for the Purpose.
- This report is not intended for general publication or circulation. This report is not to be reproduced by the Client except in relation to the Purpose, without Miyamoto’s prior written permission. Miyamoto disclaims all risk and all responsibility to any third party.
- This report is provided based on the various assumptions contained in the report.
- Miyamoto’s professional services are performed using a degree of care and skill reasonably exercised by reputable consultants providing the same or similar services as at the date of this report.
- The Client is responsible for ensuring that the design of any foundations ensures the functionality of the building under SLS level loads.
- The sub surface information has been obtained from investigation carried out at discrete locations, which by their nature only provide information about a relatively small volume of subsoils. While Miyamoto has taken reasonable skill and care in carrying out the investigation to determine the subsoil condition, the subsoil condition could differ substantially from the results of any sampling investigation. Miyamoto is not responsible for and does not accept any liability in respect of any difference between the actual subsoil conditions and the results of our investigation.
- Any susceptibility analysis carried out in respect of liquefaction is based on Miyamoto’s current understanding as an experienced professional engineering consultant of the data, methods etc. Future seismic events may change our understanding of liquefaction and its affects, which may affect the content of this report. Miyamoto is not responsible for and does not accept any liability where the content of this report is changed due to a change in industry knowledge of matters relating to liquefaction.
- This report specifically excludes assessment or advice relating to hazardous materials, such as asbestos.

- Where the Client provides information to Miyamoto, including design calculations and drawings of the as-built structure, or where the report indicates that we have obtained and/or relied upon information provided from a third party, Miyamoto has not made any independent verification of this information except as expressly stated in the report. Miyamoto assumes no responsibility for any inaccuracies in, or omissions to, that information.
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If you have any queries or you require any further clarification on any aspects of this report, please do not hesitate to contact Miyamoto International (NZ) Ltd.

## 10. References

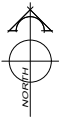
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## Appendices



## A. Updated Indicative Subdivision Plan (Davie Lovell Smith)





**DRAFT**

AMENDMENT	DATE	DESCRIPTION



Total Area : 23.1161 ha  
 Comprised in: RT's CB108/654, CB48C/117 & CB48C/118

**DAVE LOVELL-SMITH**  
 PLANNING SURVEYING ENGINEERING

116 Wrights Road P O Box 679 Christchurch 8140, New Zealand  
 Telephone: 03 379-0793 Website: www.dls.co.nz E-mail: office@dls.co.nz

JOB TITLE: **Halswell Road**

SHEET TITLE: **Proposed Subdivision of Pt RS 1593, RS 772 & Lots 1 & 2 DP 83635**

DRAWING STATUS: **For Discussion Purposes**

SCALE: 1:1000@A1 1:2000@A3 DATE: October 2020  
 CAD FILE: J:\2017\Concept\_R4.dwg REVISION:  
 DRAWING No: **C20017** SHEET No: 1 OF 1 **R6**

- NOTES:
1. Areas and dimensions are approximate only and are subject to final survey and deposit of plans.
  2. Service easements to be created as required.
  3. This plan has been prepared for discussion purposes only. No liability is accepted if the plan is used for any other purposes.
  4. The position of Greens Drain is approximate and subject to survey.

**DRAFT**

Pt RS 5786

Lot 2 DP 490383

Lot 3 DP 83635

## B. ECan Listed Land Use Register Files





Dear Sir/Madam

Thank you for submitting your property enquiry in regards to our Listed Land Use Register (LLUR) which holds information about sites that have been used, or are currently used for activities which have the potential to have caused contamination.

The LLUR statement provided indicates the location of the land parcel(s) you enquired about and provides information regarding any LLUR sites within a radius specified in the statement of this land.

Please note that if a property is not currently entered on the LLUR, it does not mean that an activity with the potential to cause contamination has never occurred, or is not currently occurring there. The LLUR is not complete, and new sites are regularly being added as we receive information and conduct our own investigations into current and historic land uses.

The LLUR only contains information held by Environment Canterbury in relation to contaminated or potentially contaminated land; other information relevant to potential contamination may be held in other files (for example consent and enforcement files).

If your enquiry relates to a farm property, please note that many current and past activities undertaken on farms may not be listed on the LLUR. Activities such as the storage, formulation and disposal of pesticides, offal pits, foot rot troughs, animal dips and underground or above ground fuel tanks have the potential to cause contamination.

Please contact and Environment Canterbury Contaminated Sites Officer if you wish to discuss the contents of the LLUR statement, or if you require additional information. For any other information regarding this land please contact Environment Canterbury Customer Services.

Yours sincerely

**Contaminated Sites Team**

# Property Statement from the Listed Land Use Register

Visit [www.ecan.govt.nz/HAIL](http://www.ecan.govt.nz/HAIL) for more information about land uses.

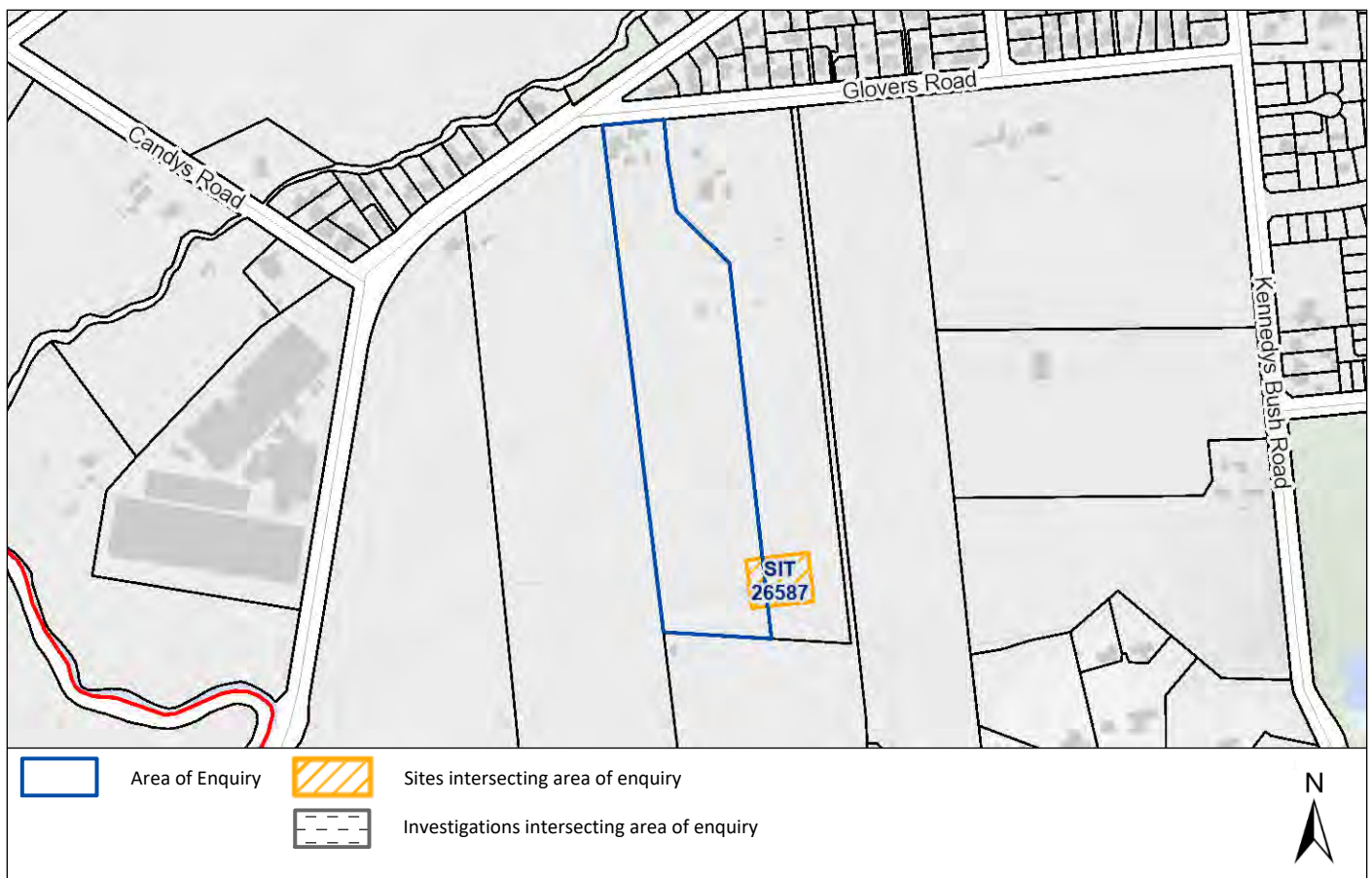
Customer Services  
P. 03 353 9007 or 0800 324 636

PO Box 345  
Christchurch 8140

P. 03 365 3828  
F. 03 365 3194  
E. [ecinfo@ecan.govt.nz](mailto:ecinfo@ecan.govt.nz)

[www.ecan.govt.nz](http://www.ecan.govt.nz)

<b>Date:</b>	13 October 2020	
<b>Land Parcels:</b>	Lot 1 DP 83635	Valuation No(s): 2356209300



*The information presented in this map is specific to the property you have selected. Information on nearby properties may not be shown on this map, even if the property is visible.*

## Summary of sites:

Site ID	Site Name	Location	HAIL Activity(s)	Category
26587	26587	Halswell West	A10 - Persistent pesticide bulk storage or use;	Not Investigated

Please note that the above table represents a summary of sites and HAILS intersecting the area of enquiry only.

## Information held about the sites on the Listed Land Use Register

**Site 26587: 26587** (Intersects enquiry area.)

<b>Site Address:</b>	Halswell West
<b>Legal Description(s):</b>	Lot 1 DP 83635, Lot 2 DP 83635

<b>Site Category:</b>	Not Investigated
<b>Definition:</b>	Verified HAIL has not been investigated.

<b>Land Uses (from HAIL):</b>	<b>Period From</b>	<b>Period To</b>	<b>HAIL land use</b>
	Pre 1994	Pre 2004	Persistent pesticide bulk storage or use including sports turfs, market gardens, orchards, glass houses or spray sheds

**Notes:**

17 Oct 2013                    Area defined from: 1994-2004 ECan Aerial Photographs  
 Note: Multiple glass houses were noted in aerial photographs reviewed.

**Investigations:**

There are no investigations associated with this site.

---

**Information held about other investigations on the Listed Land Use Register**

For further information from Environment Canterbury, contact Customer Services and refer to enquiry number ENQ265562.

**Disclaimer:**        *The enclosed information is derived from Environment Canterbury’s Listed Land Use Register and is made available to you under the Local Government Official Information and Meetings Act 1987 and Environment Canterbury’s Contaminated Land Information Management Strategy (ECan 2009).*

*The information contained in this report reflects the current records held by Environment Canterbury regarding the activities undertaken on the site, its possible contamination and based on that information, the categorisation of the site. Environment Canterbury has not verified the accuracy or completeness of this information. It is released only as a copy of Environment Canterbury's records and is not intended to provide a full, complete or totally accurate assessment of the site. It is provided on the basis that Environment Canterbury makes no warranty or representation regarding the reliability, accuracy or completeness of the information provided or the level of contamination (if any) at the relevant site or that the site is suitable or otherwise for any particular purpose. Environment Canterbury accepts no responsibility for any loss, cost, damage or expense any person may incur as a result of the use, reference to or reliance on the information contained in this report.*

*Any person receiving and using this information is bound by the provisions of the Privacy Act 1993.*

Dear Sir/Madam

Thank you for submitting your property enquiry in regards to our Listed Land Use Register (LLUR) which holds information about sites that have been used, or are currently used for activities which have the potential to have caused contamination.

The LLUR statement provided indicates the location of the land parcel(s) you enquired about and provides information regarding any LLUR sites within a radius specified in the statement of this land.

Please note that if a property is not currently entered on the LLUR, it does not mean that an activity with the potential to cause contamination has never occurred, or is not currently occurring there. The LLUR is not complete, and new sites are regularly being added as we receive information and conduct our own investigations into current and historic land uses.

The LLUR only contains information held by Environment Canterbury in relation to contaminated or potentially contaminated land; other information relevant to potential contamination may be held in other files (for example consent and enforcement files).

If your enquiry relates to a farm property, please note that many current and past activities undertaken on farms may not be listed on the LLUR. Activities such as the storage, formulation and disposal of pesticides, offal pits, foot rot troughs, animal dips and underground or above ground fuel tanks have the potential to cause contamination.

Please contact and Environment Canterbury Contaminated Sites Officer if you wish to discuss the contents of the LLUR statement, or if you require additional information. For any other information regarding this land please contact Environment Canterbury Customer Services.

Yours sincerely

**Contaminated Sites Team**

# Property Statement from the Listed Land Use Register

Visit [www.ecan.govt.nz/HAIL](http://www.ecan.govt.nz/HAIL) for more information about land uses.

Customer Services  
P. 03 353 9007 or 0800 324 636

PO Box 345  
Christchurch 8140

P. 03 365 3828  
F. 03 365 3194  
E. [ecinfo@ecan.govt.nz](mailto:ecinfo@ecan.govt.nz)

[www.ecan.govt.nz](http://www.ecan.govt.nz)

<b>Date:</b>	13 October 2020	
<b>Land Parcels:</b>	Lot 2 DP 83635	Valuation No(s): 2356209301



*The information presented in this map is specific to the property you have selected. Information on nearby properties may not be shown on this map, even if the property is visible.*

## Summary of sites:

Site ID	Site Name	Location	HAIL Activity(s)	Category
26587	26587	Halswell West	A10 - Persistent pesticide bulk storage or use;	Not Investigated

*Please note that the above table represents a summary of sites and HAILS intersecting the area of enquiry only.*

## Information held about the sites on the Listed Land Use Register

**Site 26587: 26587** (Intersects enquiry area.)

<b>Site Address:</b>	Halswell West
<b>Legal Description(s):</b>	Lot 1 DP 83635, Lot 2 DP 83635

<b>Site Category:</b>	Not Investigated
<b>Definition:</b>	Verified HAIL has not been investigated.

Land Uses (from HAIL):	Period From	Period To	HAIL land use
	Pre 1994	Pre 2004	Persistent pesticide bulk storage or use including sports turfs, market gardens, orchards, glass houses or spray sheds

**Notes:**

17 Oct 2013                      Area defined from: 1994-2004 ECan Aerial Photographs  
 Note: Multiple glass houses were noted in aerial photographs reviewed.

**Investigations:**

There are no investigations associated with this site.

---

**Information held about other investigations on the Listed Land Use Register**

For further information from Environment Canterbury, contact Customer Services and refer to enquiry number ENQ265560.

**Disclaimer:**            *The enclosed information is derived from Environment Canterbury’s Listed Land Use Register and is made available to you under the Local Government Official Information and Meetings Act 1987 and Environment Canterbury’s Contaminated Land Information Management Strategy (ECan 2009).*

*The information contained in this report reflects the current records held by Environment Canterbury regarding the activities undertaken on the site, its possible contamination and based on that information, the categorisation of the site. Environment Canterbury has not verified the accuracy or completeness of this information. It is released only as a copy of Environment Canterbury's records and is not intended to provide a full, complete or totally accurate assessment of the site. It is provided on the basis that Environment Canterbury makes no warranty or representation regarding the reliability, accuracy or completeness of the information provided or the level of contamination (if any) at the relevant site or that the site is suitable or otherwise for any particular purpose. Environment Canterbury accepts no responsibility for any loss, cost, damage or expense any person may incur as a result of the use, reference to or reliance on the information contained in this report.*

*Any person receiving and using this information is bound by the provisions of the Privacy Act 1993.*

## C. Geotechnical Investigation Results

MINZ Shallow Investigation Logs

Laboratory Soil Sample Test Results

LandTest CPT/DPSH Plot



## SHALLOW GROUND INVESTIGATION LOG

HA1/DCP1

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
LOGGED BY: CG	TOTAL DEPTH OF HOLE: 2.9 mbgl
PROCESSED BY: CG	HOLE DIAMETER: 50 mm
LOCATION: REFER TO SITE PLAN	DRILLING METHOD: Hand Auger
	SHEAR VANE NUMBER: 2102
	GROUNDWATER LEVEL: 1.65 mbgl
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded	
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size				
							LL	PL	PI	Gr	Sa	FC		WC (%)
0.0 - 0.5	1, 1, 1, 1, 3, 2			SILT: low plasticity, dark brown, moist, with minor rootlets (TOPSOIL)	[Cross-hatch pattern]									
0.5 - 1.5	1, 2, 1, 2, 2, 2, 2, 2, 2, 1			SILT: low plasticity, brown, moist, with minor fine sand	[X pattern]									
1.5 - 2.5	2, 2, 2, 2, 2, 2, 3, 3, 2, 1, 1, 2, 2, 3, 4, 5	1.65		Silty SAND: fine to medium, brown-grey, wet  at 2.0m: becomes blue-grey, saturated	[Dotted pattern]	DIST. SAMPLE					51%	49%		
2.5 - 3.0						DIST. SAMPLE					51%	49%		

...contd on next page

### LEGEND

**ABBREVIATIONS**

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 ...▽... STANDING GWL

**NOTES**

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth



## SHALLOW GROUND INVESTIGATION LOG

HA1/DCP1 (contd.)

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 3.9 mbgl
<b>PROCESSED BY:</b> CG	<b>DRILLING METHOD:</b> Hand Auger
<b>LOCATION:</b> REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b> 1.65 mbgl
<b>HOLE DIAMETER:</b> 50 mm	
<b>SHEAR VANE NUMBER:</b> 2102	
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size				WC (%)	UW
							LL	PL	PI	Gr	Sa	FC			
3.5	9 9 9 9 7 6 6 7 7	1.65m bgl →		Silty SAND: fine to medium, blue-grey, saturated (contd.)		DIST. SAMPLE					51%	49%			
4.0				SILT: low plasticity, blue-grey, saturated											
4.5				EOH (Target Depth Reached)											
5.0															
5.5															

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

## HA2/DCP2

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
<b>LOGGED BY:</b> CG	<b>TOTAL DEPTH OF HOLE:</b> 3.9 mbgl
<b>PROCESSED BY:</b> CG	<b>DRILLING METHOD:</b> Hand Auger
<b>LOCATION:</b> REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b> 1.3 mbgl
<b>HOLE DIAMETER:</b> 50 mm	
<b>SHEAR VANE NUMBER:</b> 2102	
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing							Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size			WC (%)		UW	
							LL	PL	PI	Gr	Sa	FC				
1	1	▽		SILT: non-plastic, dark brown, moist, with some sand and rootlets (TOPSOIL)											66 / 16	
2	2			SILT: low plasticity, yellow-brown, moist, with some sand												
0.5	2															
	3															
	3															
1.0	2															
	2															
	4															
	3															
	2															
	3															
	2															
1.5	2															
	3															
	4															
	3															
	Self Weight			at 1.9m: becomes wet, mottled orange											63 / 16	
2.0	1															
	3															
	3															
	3															
	4															
2.5	4															
	4															
	5															
	5															
	7															
	7															
...contd on next page																

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 ▽ STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA2/DCP2 (contd.)

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
LOGGED BY: CG	TOTAL DEPTH OF HOLE: 3.9 mbgl
PROCESSED BY: CG	HOLE DIAMETER: 50 mm
LOCATION: REFER TO SITE PLAN	DRILLING METHOD: Hand Auger
	SHEAR VANE NUMBER: 2102
	GROUNDWATER LEVEL: 1.3 mbgl
This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size				WC (%)	UW
							LL	PL	PI	Gr	Sa	FC			
3.5	7 7 8 7 7 6 7 8 7	1.3m bgl →		Clayey SILT: low to medium plasticity, grey, saturated, with some sand (contd.)		DIST. SAMPLE	29	20	9	-	15%	85%			
4.0				EOH (Target Depth Reached)											
4.5															
5.0															
5.5															

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
GWL GROUNDWATER LEVEL  
mbgl METERS BELOW GROUND LEVEL  
WC WATER CONTENT

HA HAND AUGER  
UTP UNABLE TO PENETRATE  
EOH END OF HOLE  
UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
PL PLASTIC LIMIT  
PI PLASTICITY INDEX  
NE NOT ENCOUNTERED

Gr GRAVEL  
Sa SAND  
FC FINES CONTENT  
...▽... STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA3/DCP3

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
LOGGED BY: CG	TOTAL DEPTH OF HOLE: 4.1 mbgl
PROCESSED BY: CG	HOLE DIAMETER: 50 mm
LOCATION: REFER TO SITE PLAN	DRILLING METHOD: Hand Auger
	SHEAR VANE NUMBER: 2102
	GROUNDWATER LEVEL: 1.8 mbgl
	This report may only be reproduced in full

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size					
							LL	PL	PI	Gr	Sa	FC		WC (%)	UW
0.0 - 0.5	2			SILT: non-plastic, dark brown, dry, with some sand and rootlets (TOPSOIL)											
0.5 - 1.0	2			SILT: low plasticity, light brown, moist											
1.0 - 1.5	2			SAND: fine to medium, orange brown, moist											
1.5 - 2.0	3			Sandy SILT: low plasticity, orange brown, wet											
2.0 - 2.5	3			SILT: medium plasticity, brown, wet											
2.5 - 3.0	5	...▽...		Sandy SILT: non-plastic, dark grey, saturated		DIST. SAMPLE	Non-Plastic			-	41%	59%			
3.0 - 3.5	2														
3.5 - 4.0	2														
4.0 - 4.5	4														
4.5 - 5.0	4														
5.0 - 5.5	5														
5.5 - 6.0	2														
6.0 - 6.5	4														
6.5 - 7.0	5														

...contd on next page

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
GWL GROUNDWATER LEVEL  
mbgl METERS BELOW GROUND LEVEL  
WC WATER CONTENT

HA HAND AUGER  
UTP UNABLE TO PENETRATE  
EOH END OF HOLE  
UW UNIT WEIGHT (kN/m<sup>3</sup>)

LL LIQUID LIMIT  
PL PLASTIC LIMIT  
PI PLASTICITY INDEX  
NE NOT ENCOUNTERED

Gr GRAVEL  
Sa SAND  
FC FINES CONTENT  
...▽... STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

### HA3/DCP3 (contd.)

PROJECT:	2 & 4 Glovers Road, Halswell, Christchurch		
LOGGED BY:	CG	TOTAL DEPTH OF HOLE:	4.1 mbgl
PROCESSED BY:	CG	DRILLING METHOD:	Hand Auger
LOCATION:	REFER TO SITE PLAN	GROUNDWATER LEVEL:	1.8 mbgl
		HOLE DIAMETER:	50 mm
		SHEAR VANE NUMBER:	2102
		This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing						Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size					
							LL	PL	PI	Gr	Sa	FC		WC (%)	UW
5	5	1.8m bgl -->		Sandy SILT: non-plastic, dark grey, saturated (contd.)	x x	DIST. SAMPLE	Non-Plastic			-	41%	59%			
7	7														
8	8														
8	8														
3.5	8														
7	7														
8	8														
9	9														
10	10														
4.0				EOH (Target Depth Reached)											

LEGEND						NOTES	
ABBREVIATIONS							
DCP	DYNAMIC CONE PENETROMETER	HA	HAND AUGER	LL	LIQUID LIMIT	Gr	GRAVEL
GWL	GROUNDWATER LEVEL	UTP	UNABLE TO PENETRATE	PL	PLASTIC LIMIT	Sa	SAND
mbgl	METERS BELOW GROUND LEVEL	EOH	END OF HOLE	PI	PLASTICITY INDEX	FC	FINES CONTENT
WC	WATER CONTENT	UW	UNIT WEIGHT (kN/m³)	NE	NOT ENCOUNTERED	∇	STANDING GWL
							As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA4/DCP4

<b>PROJECT:</b> 2 & 4 Glovers Road, Halswell, Christchurch	
LOGGED BY: CG	TOTAL DEPTH OF HOLE: 2.9 mbgl
PROCESSED BY: CG	HOLE DIAMETER: 50 mm
LOCATION: REFER TO SITE PLAN	DRILLING METHOD: Hand Auger
	SHEAR VANE NUMBER: 2102
	GROUNDWATER LEVEL: 1.2 mbgl
	This report may only be reproduced in full

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing							Vane shear strength (kPa) peak/remoulded		
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size			WC (%)		UW	
							LL	PL	PI	Gr	Sa	FC				
0.0 - 0.2	2			Sandy SILT: non-plastic, brown, moist, with minor rootlets (TOPSOIL)												
0.2 - 0.8	2			SAND: fine to medium, grey, moist, with some silt												
0.8 - 1.2	2			at 0.8m: becomes wet												
1.2 - 1.9	3	1.2		Sandy SILT: low plasticity, brown-grey, wet, sand is fine												
1.9 - 2.0	3			at 1.2m: becomes saturated												
2.0 - 2.2	3			SILT: low to medium plasticity, blue-grey, saturated												
2.2 - 2.4	4			Silty SAND: fine to medium, grey, saturated												
2.4 - 2.5	4															
			EOH (Target Depth Reached)													

### LEGEND

#### ABBREVIATIONS

DCP DYNAMIC CONE PENETROMETER  
 GWL GROUNDWATER LEVEL  
 mbgl METERS BELOW GROUND LEVEL  
 WC WATER CONTENT

HA HAND AUGER  
 UTP UNABLE TO PENETRATE  
 EOH END OF HOLE  
 (kN/m<sup>3</sup>)  
 UW UNIT WEIGHT

LL LIQUID LIMIT  
 PL PLASTIC LIMIT  
 PI PLASTICITY INDEX  
 NE NOT ENCOUNTERED

Gr GRAVEL  
 Sa SAND  
 FC FINES CONTENT  
 STANDING GWL

#### NOTES

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

## SHALLOW GROUND INVESTIGATION LOG

HA5/DCP5

<b>PROJECT:</b>	2 & 4 Glovers Road, Halswell, Christchurch				
<b>LOGGED BY:</b>	CG	<b>TOTAL DEPTH OF HOLE:</b>	1.9 mbgl	<b>HOLE DIAMETER:</b>	50 mm
<b>PROCESSED BY:</b>	CG	<b>DRILLING METHOD:</b>	Hand Auger	<b>SHEAR VANE NUMBER:</b>	2102
<b>LOCATION:</b>	REFER TO SITE PLAN	<b>GROUNDWATER LEVEL:</b>	1.0 mbgl	This report may only be reproduced in full	

Depth (m)	DCP Test Results (Blows per 100mm)	GWL	Soil Description			Sample Taken	Lab Testing							Vane shear strength (kPa) peak/remoulded					
			USC	Soil Characteristics	Graphic Log		Atterberg Limits			Grain Size			WC (%)		UW				
							LL	PL	PI	Gr	Sa	FC							
0.0 - 0.2	2	▽		SILT: low plasticity, brown, moist, with minor fine sand (TOPSOIL)	[Cross-hatch pattern]														
0.2 - 0.4	1			Sandy SILT: low plasticity, grey, moist, sand is fine	[X pattern]														
0.4 - 0.6	2																		
0.6 - 0.8	2																		
0.8 - 1.0	2																		
1.0 - 1.2	2																		
1.2 - 1.4	2																		
1.4 - 1.6	1			at 1.0m: becomes wet															
1.6 - 1.8	1			at 1.2m: becomes saturated															
1.8 - 2.0	2				Silty SAND: fine to medium, grey, saturated	[Dotted pattern]	DIST. SAMPLE					58%	42%						
2.0 - 2.2	5		at 1.8m: with minor fine to medium gravel																
2.2 - 2.4	11		EOH (Practical Refusal on Gravel)																

### LEGEND

ABBREVIATIONS				NOTES			
DCP	DYNAMIC CONE PENETROMETER	HA	HAND AUGER	LL	LIQUID LIMIT	Gr	GRAVEL
GWL	GROUNDWATER LEVEL	UTP	UNABLE TO PENETRATE	PL	PLASTIC LIMIT	Sa	SAND
mbgl	METERS BELOW GROUND LEVEL	EOH	END OF HOLE	PI	PLASTICITY INDEX	FC	FINES CONTENT
WC	WATER CONTENT	UW	UNIT WEIGHT (kN/m <sup>3</sup> )	NE	NOT ENCOUNTERED	▽	STANDING GWL

As per MINZ policy, the DCP was transferred to the base of the hand auger borehole at 1.9m depth

**SITE INVESTIGATION PLAN**

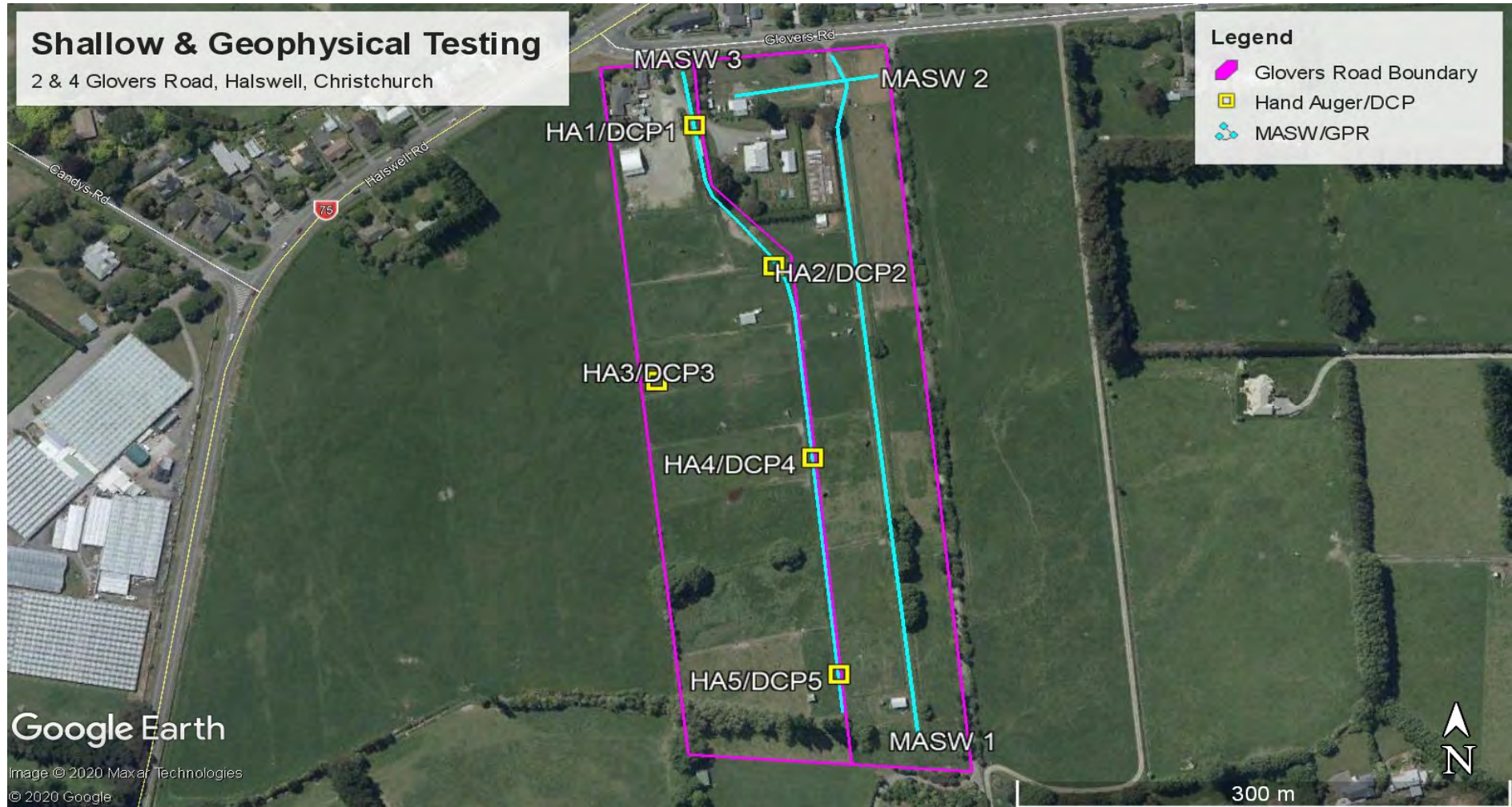
2 & 4 Glovers Road, Halswell, Christchurch

**Shallow & Geophysical Testing**

2 & 4 Glovers Road, Halswell, Christchurch

**Legend**

- Glovers Road Boundary
- Hand Auger/DCP
- MASW/GPR





## TEST REPORT

Lab Job No: 8378-032  
Your ref.: -  
Date of Issue: 14/09/2020  
Date of Re-Issue: -  
Page: 1 of 8

### Test Report

#### C20-450

PROJECT: 2 Glovers Road – Laboratory Testing  
CLIENT: Miyamoto International NZ Ltd,  
518 Colombo Street,  
Christchurch, 8011  
ATTENTION: Clem Gibbens  
INSTRUCTIONS: Determination of Particle-Size Distribution-Wet Sieving method  
Determination of the Liquid & Plastic Limits, Plasticity Index and Water Content  
Determination of the Water Content of Soils  
TEST METHOD: NZS 4402:1986 Test 2.8.1  
NZS 4402:1986 Tests 2.2, 2.3, 2.4  
NZS 4402:1986 Test 2.1  
SAMPLING METHOD: Client - SNA  
TEST RESULTS: As per Laboratory sheets attached



Jeremy Brokenshire  
Laboratory Technician



Nick van Warmerdam  
Approved Signatory



All tests reported herein  
have been performed in  
accordance with the  
laboratory's scope of  
accreditation

-CPT – Aggregates – Soil – Roadings-

This report shall not be reproduced except in full, without written approval of the laboratory



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M: 027 6565 317

DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH

NZS 4402: 1986 Test 2.8.1, 2.8.2

Lab Job No: 8378-032  
Client: Miyamoto International NZ Ltd  
Location: 2 Glovers Road  
HA01 (1.5-2.3m)  
Date Received: 8/09/2020  
Report No: C20-450  
REF: -

Sample No: C20-319  
Tested By: D.P  
Date: 9/09/2020  
Checked By: J.B  
Date: 14/09/2020  
Page: 2 of 8

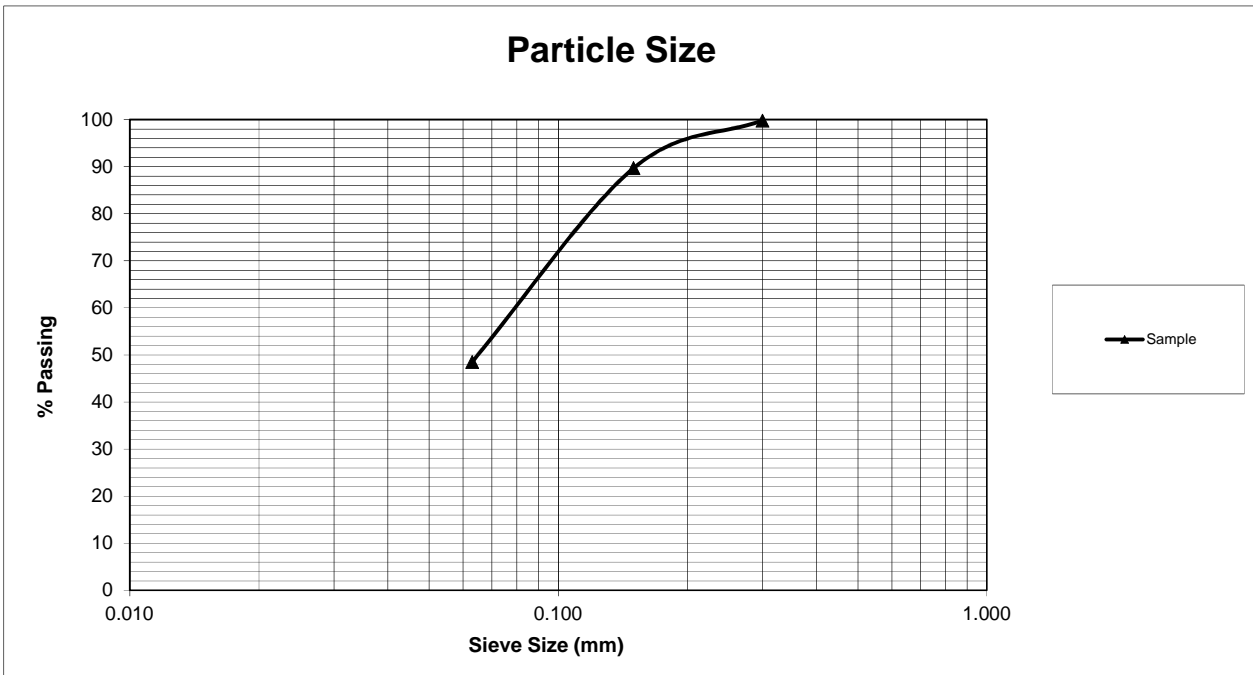
Sampling Method: Sampled by client - SNA  
Date Sampled: 4/09/2020

Sampled By: Client

Test Details: Wet sieving method  
History: Natural

Description of Sample: Silty SAND, brownish grey, wet, no plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	100
0.150	-	-	90
0.063	-	-	49



\*The percentage passing the finest sieve was obtained by difference.

N. van Warmerdam  
Approved Signatory



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DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH

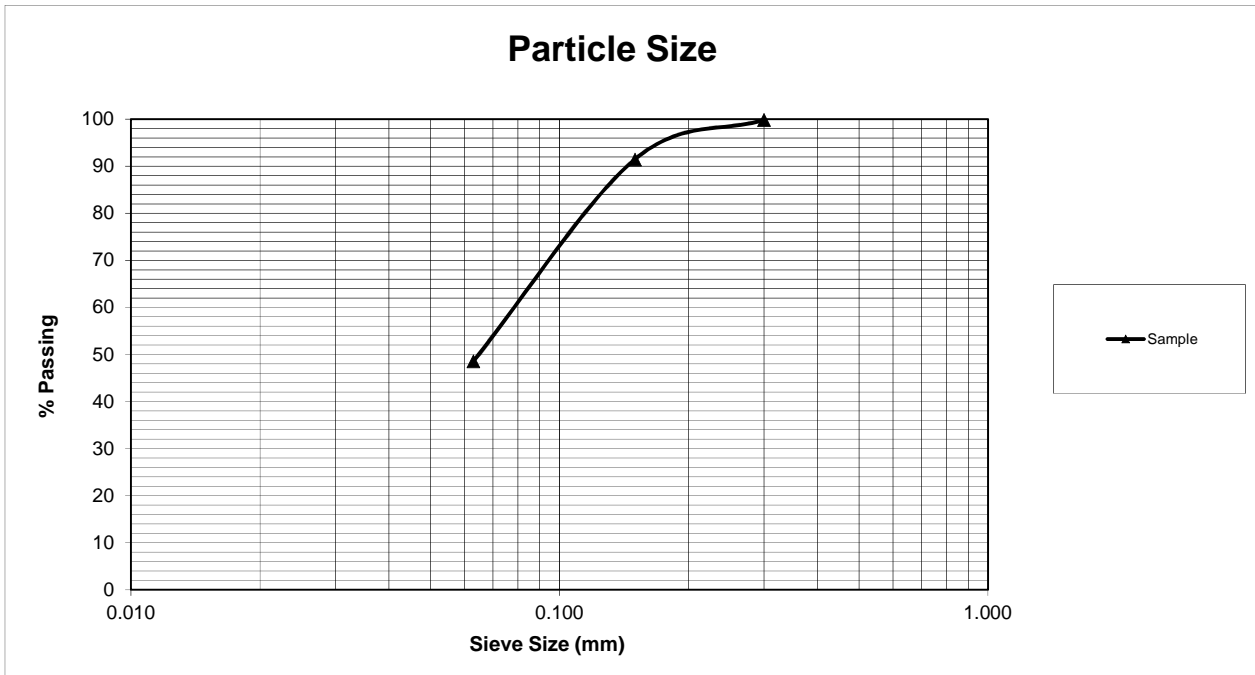
NZS 4402: 1986 Test 2.8.1, 2.8.2

Lab Job No: 8378-032      Sample No: C20-320  
Client: Miyamoto International NZ Ltd      Tested By: D.P  
Location: 2 Glovers Road      Date: 9/09/2020  
          HA01 (2.3-3.8m)      Checked By: J.B  
Date Received: 8/09/2020      Date: 14/09/2020  
Report No: C20-450      Page: 3 of 8  
REF: -  
Sampling Method: Sampled by client - SNA      Sampled By: Client  
Date Sampled: 4/09/2020

Test Details: Wet sieving method  
History: Natural

Description of Sample: Silty SAND, brownish grey, saturated, no plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	100
0.150	-	-	91
0.063	-	-	49



\*The percentage passing the finest sieve was obtained by difference.



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**DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH**

NZS 4402: 1986 Test 2.8.1, 2.8.2

Lab Job No: 8378-032  
Client: Miyamoto International NZ Ltd  
Location: 2 Glovers Road  
HA02 (2.7-4.0m)  
Date Received: 8/09/2020  
Report No: C20-450  
REF: -

Sample No: C20-321  
Tested By: D.P  
Date: 9/09/2020  
Checked By: J.B  
Date: 14/09/2020  
Page: 4 of 8

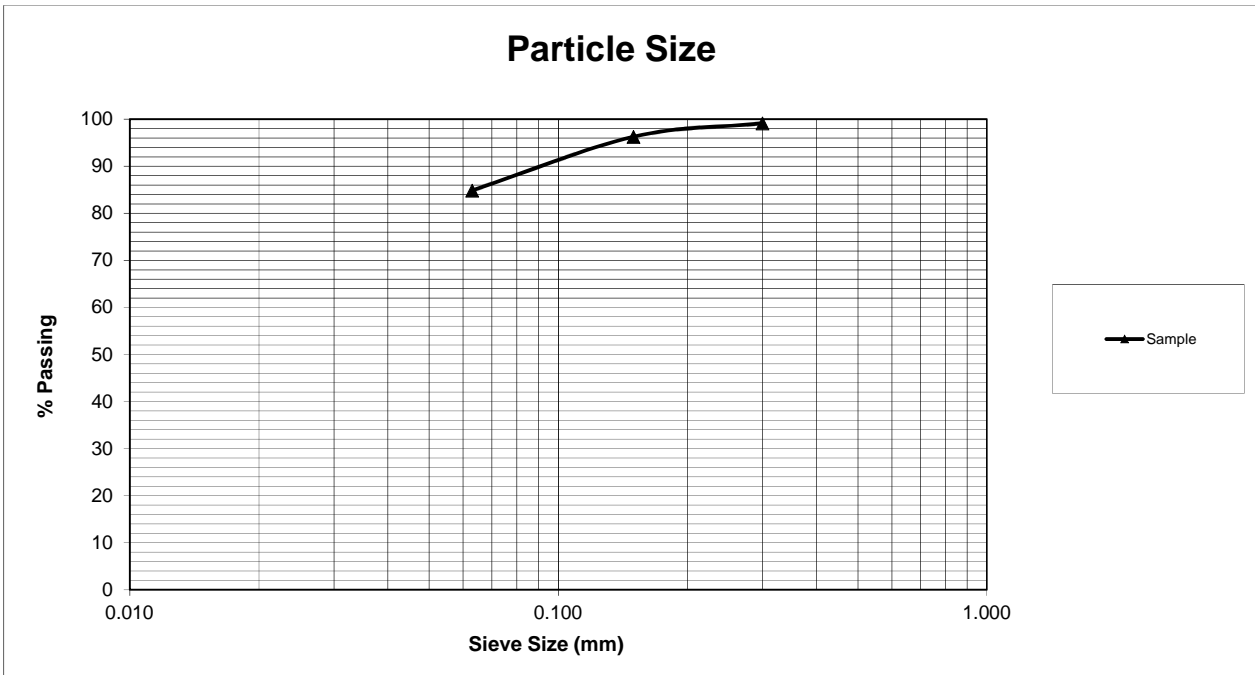
Sampling Method: Sampled by client - SNA  
Date Sampled: 4/09/2020

Sampled By: Client

Test Details: Wet sieving method  
History: Natural

Description of Sample: Silty CLAY, some sand, dark grey saturated, low plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	99
0.150	-	-	96
0.063	-	-	85



\*The percentage passing the finest sieve was obtained by difference.

**DETERMINATION OF THE LIQUID & PLASTIC LIMITS,  
PLASTICITY INDEX & WATER CONTENT**

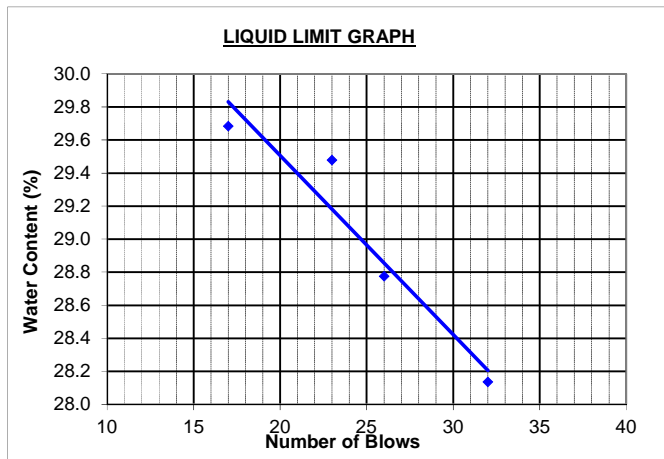
NZS 4402: 1986 Test 2.2, 2.3, 2.4

<b>Lab Job No:</b>	8378-032	<b>Sample No.:</b>	C20-321
<b>Client:</b>	Miyamoto International NZ Ltd	<b>Tested By:</b>	S.P.S
<b>Location:</b>	2 Glovers Road HA02 (2.7-4.0m)	<b>Date Tested:</b>	11/09/2020
<b>Date Received:</b>	8/09/2020	<b>Checked By:</b>	J.B
<b>Report No:</b>	C20-450	<b>Date Checked:</b>	14/09/2020
<b>REF:</b>	-	<b>Page:</b>	5 of 8
<b>Sampling Method:</b>	Sampled by client - SNA	<b>Sampled By:</b>	Client
<b>Date Sampled:</b>	4/09/2020		

**Test Details:**  
 Test performed on: Fraction passing 425mm sieve  
 Sample history: Natural state

**Description of Sample:** Silty CLAY, some sand, dark grey saturated, low plasticity

Liquid Limit				Plastic Limit		NWC	
No. of blows	17	23	26	32			30.5
Water content (%)	29.7	29.5	28.8	28.1	20.0	19.2	29
							20
							9





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DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH

NZS 4402: 1986 Test 2.8.1, 2.8.2

Lab Job No: 8378-032  
Client: Miyamoto International NZ Ltd  
Location: 2 Glovers Road  
HA03 (2.0-3.4m)  
Date Received: 8/09/2020  
Report No: C20-450  
REF: -

Sample No: C20-322  
Tested By: D.P  
Date: 9/09/2020  
Checked By: J.B  
Date: 14/09/2020  
Page: 6 of 8

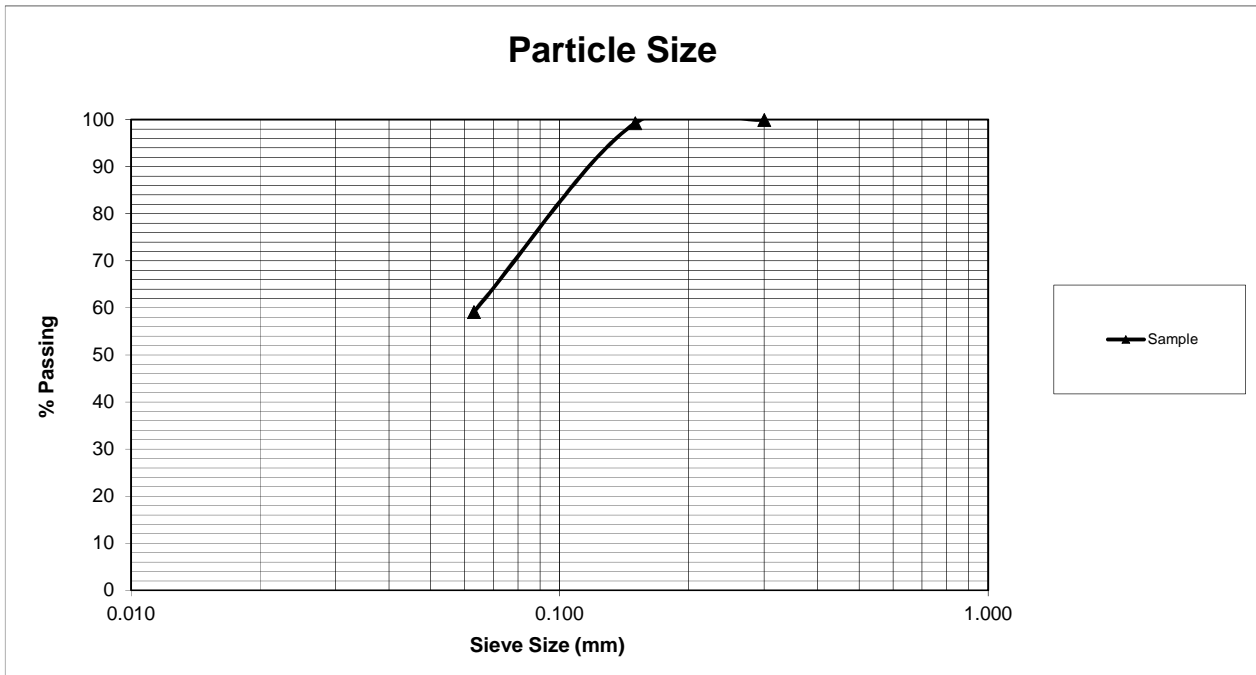
Sampling Method: Sampled by client - SNA  
Date Sampled: 4/09/2020

Sampled By: Client

Test Details: Wet sieving method  
History: Natural

Description of Sample: Sandy SILT, dark grey, saturated, no plasticity

Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	100
0.150	-	-	99
0.063	-	-	59



\*The percentage passing the finest sieve was obtained by difference.

**DETERMINATION OF THE LIQUID & PLASTIC LIMITS,  
PLASTICITY INDEX & WATER CONTENT**

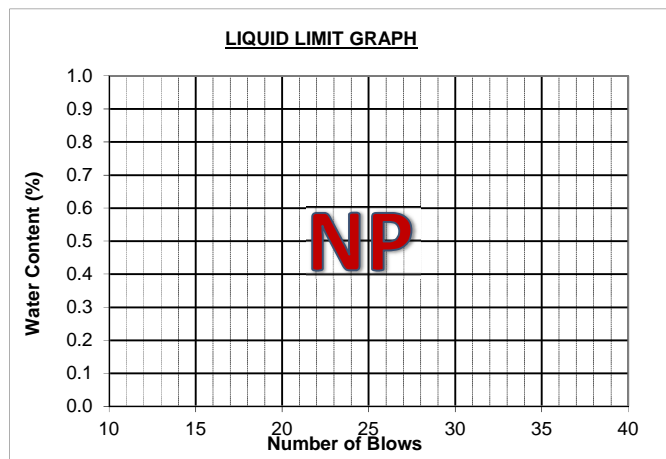
NZS 4402: 1986 Test 2.2, 2.3, 2.4

<b>Lab Job No:</b>	8378-032	<b>Sample No.:</b>	C20-322
<b>Client:</b>	Miyamoto International NZ Ltd	<b>Tested By:</b>	S.P.S
<b>Location:</b>	2 Glovers Road HA03 (2.0-3.4m)	<b>Date Tested:</b>	11/09/2020
<b>Date Received:</b>	8/09/2020	<b>Checked By:</b>	J.B
<b>Report No:</b>	C20-450	<b>Date Checked:</b>	14/09/2020
<b>REF:</b>	-	<b>Page:</b>	7 of 8
<b>Sampling Method:</b>	Sampled by client - SNA	<b>Sampled By:</b>	Client
<b>Date Sampled:</b>	4/09/2020		

**Test Details:**  
 Test performed on: Fraction passing 425mm sieve  
 Sample history: Natural state

**Description of Sample:** Sandy SILT, dark grey, saturated, no plasticity

	<b>Liquid Limit</b>	<b>Plastic Limit</b>	<b>NWC</b>	<b>28.9</b>
<b>No. of blows</b>	<b>NP</b>	<b>NP</b>	<b>Liquid Limit</b>	-
<b>Water content (%)</b>			<b>Plastic Limit</b>	-
			<b>Plasticity Index</b>	-



\*Unable to obtain Liquid Limit or Plastic Limit.



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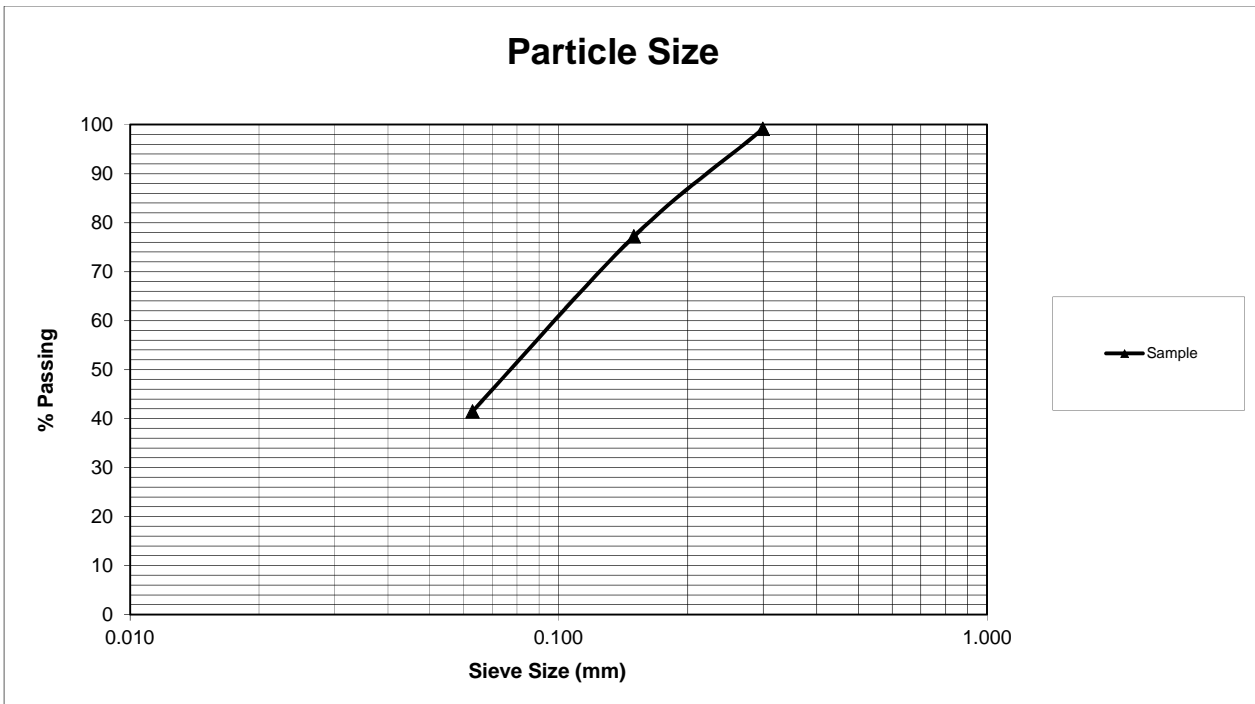
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**DETERMINATION OF THE PARTICLE SIZE DISTRIBUTION - GRAPH**

NZS 4402: 1986 Test 2.8.1, 2.8.2

<b>Lab Job No:</b>	8378-032	<b>Sample No:</b>	C20-323
<b>Client:</b>	Miyamoto International NZ Ltd	<b>Tested By:</b>	D.P
<b>Location:</b>	2 Glovers Road HA05 (1.5-1.8m)	<b>Date:</b>	9/09/2020
<b>Date Received:</b>	8/09/2020	<b>Checked By:</b>	J.B
<b>Report No:</b>	C20-450	<b>Date:</b>	14/09/2020
<b>REF:</b>	-	<b>Page:</b>	8 of 8
<b>Sampling Method:</b>	Sampled by client - SNA	<b>Sampled By:</b>	Client
<b>Date Sampled:</b>	4/09/2020		
<b>Test Details:</b>	Wet sieving method		
<b>History:</b>	Natural		
<b>Description of Sample:</b>	Silty SAND, brownish grey, wet, no plasticity		

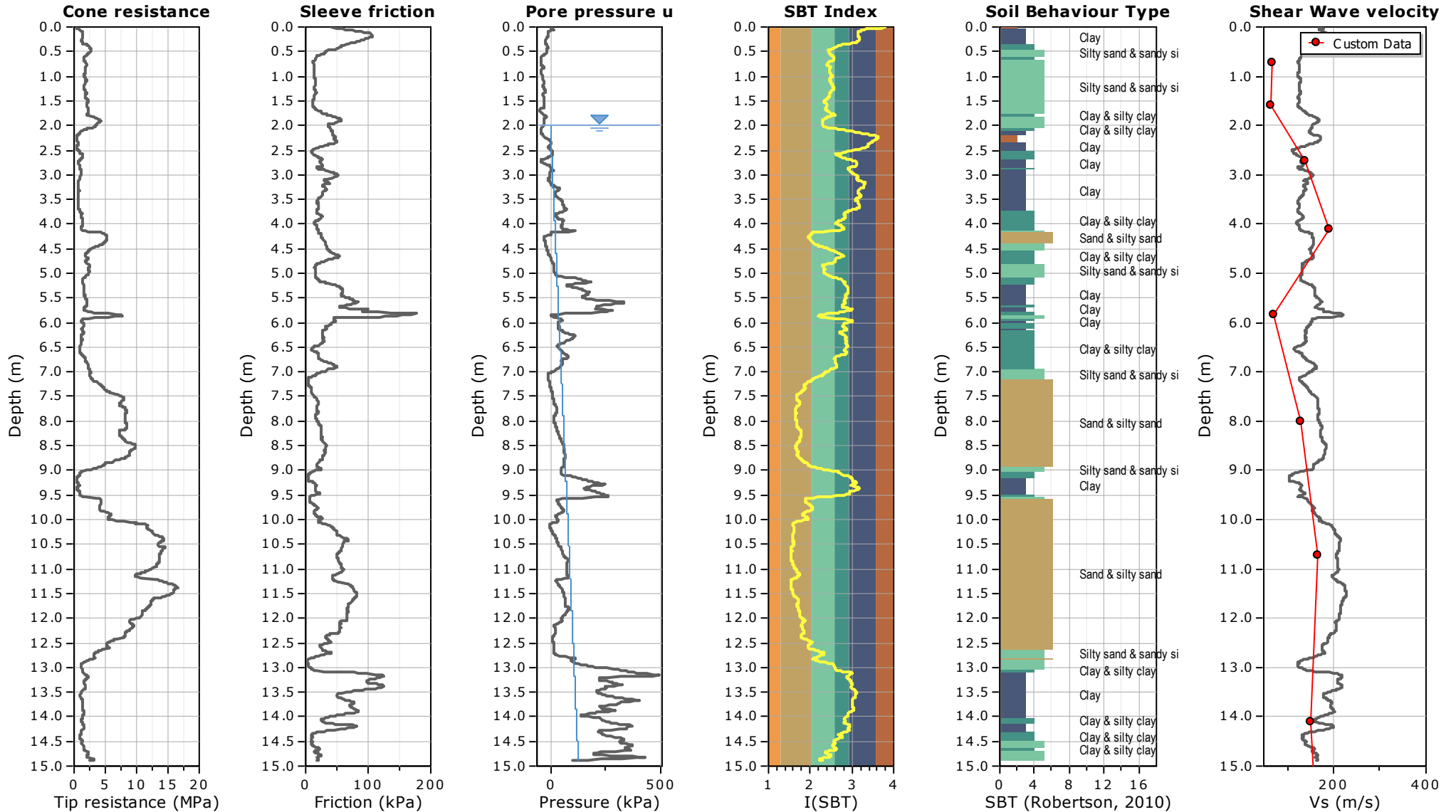
Sieve Size	% Passing		
	Max	Min	Sample
0.300	-	-	99
0.150	-	-	77
0.063	-	-	42



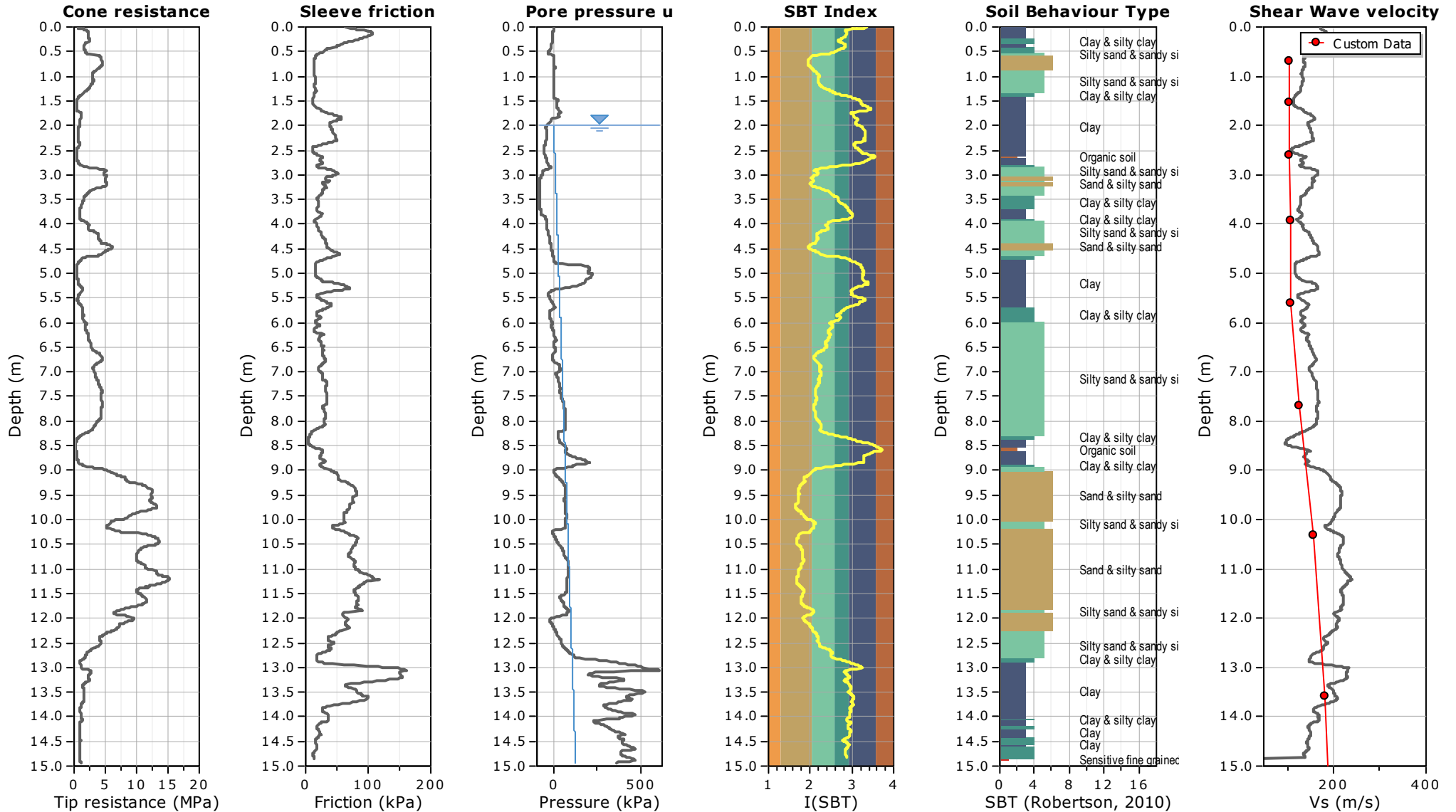
\*The percentage passing the finest sieve was obtained by difference.



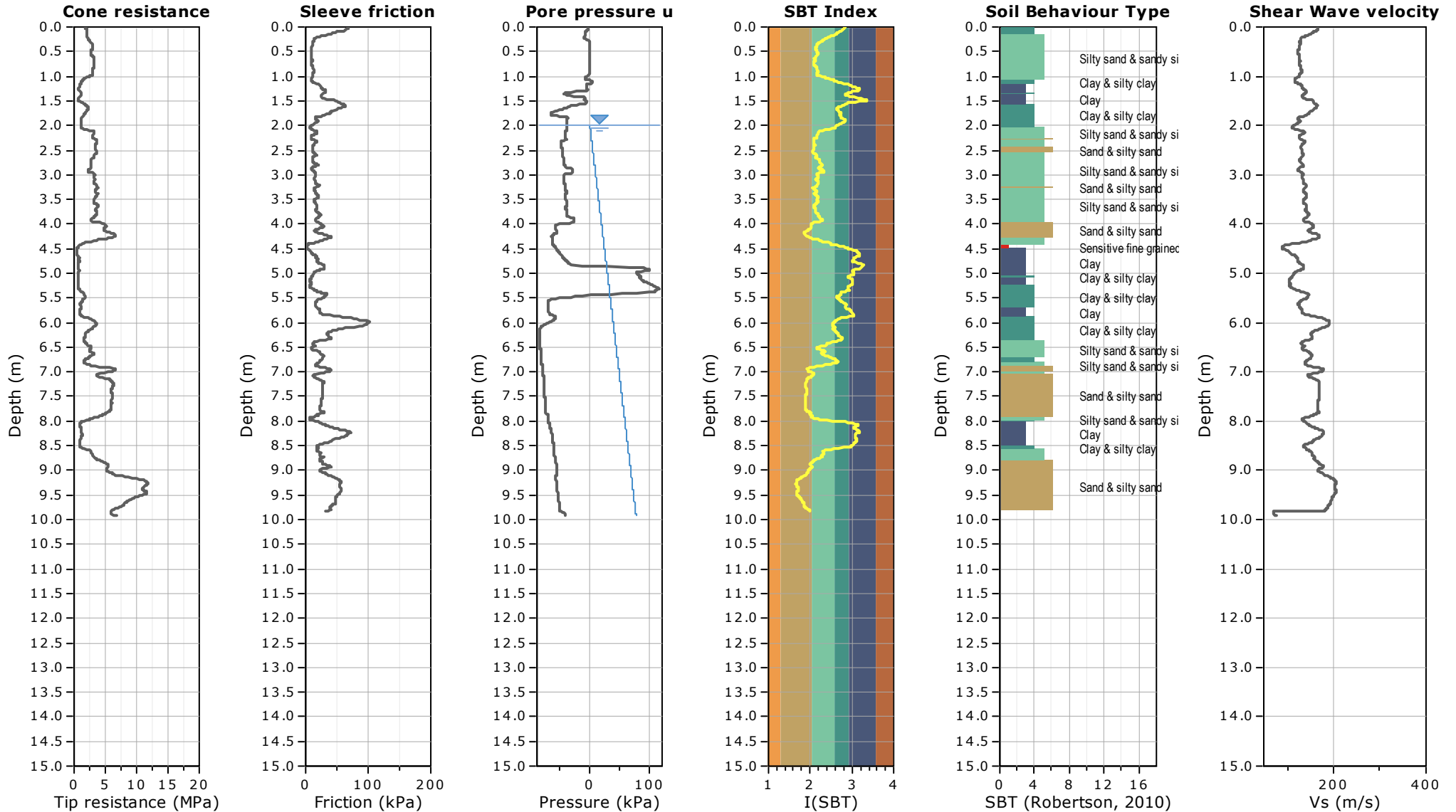
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



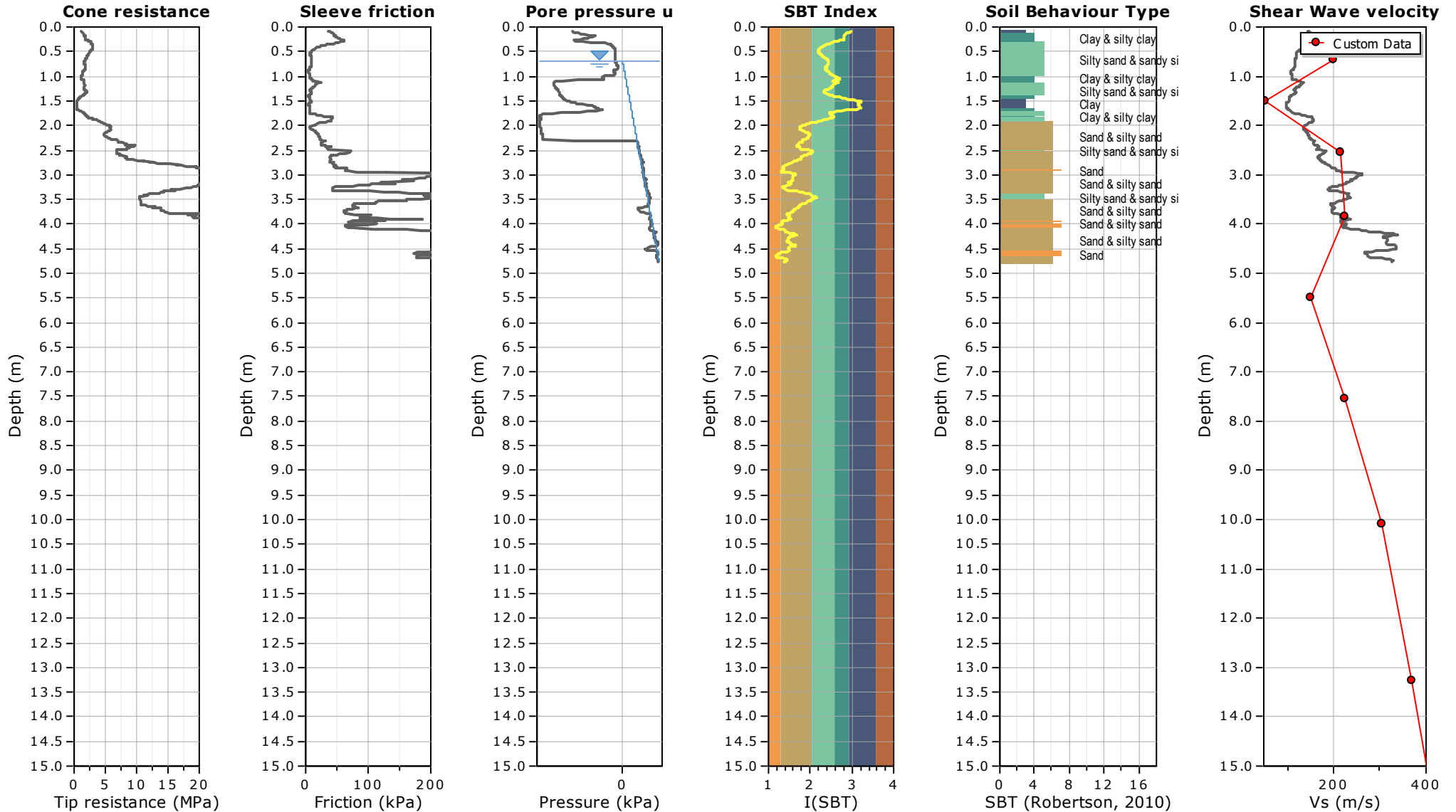
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



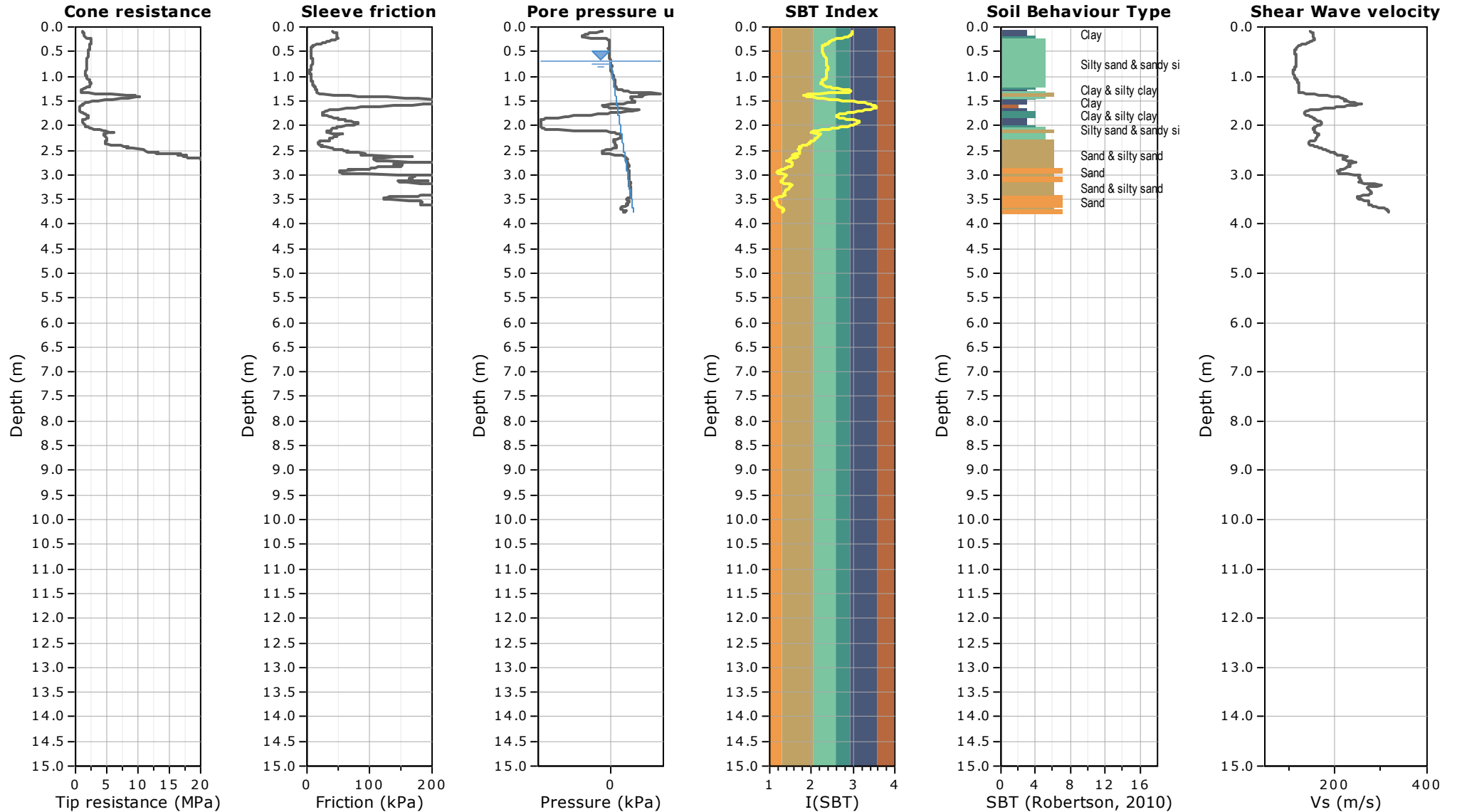
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



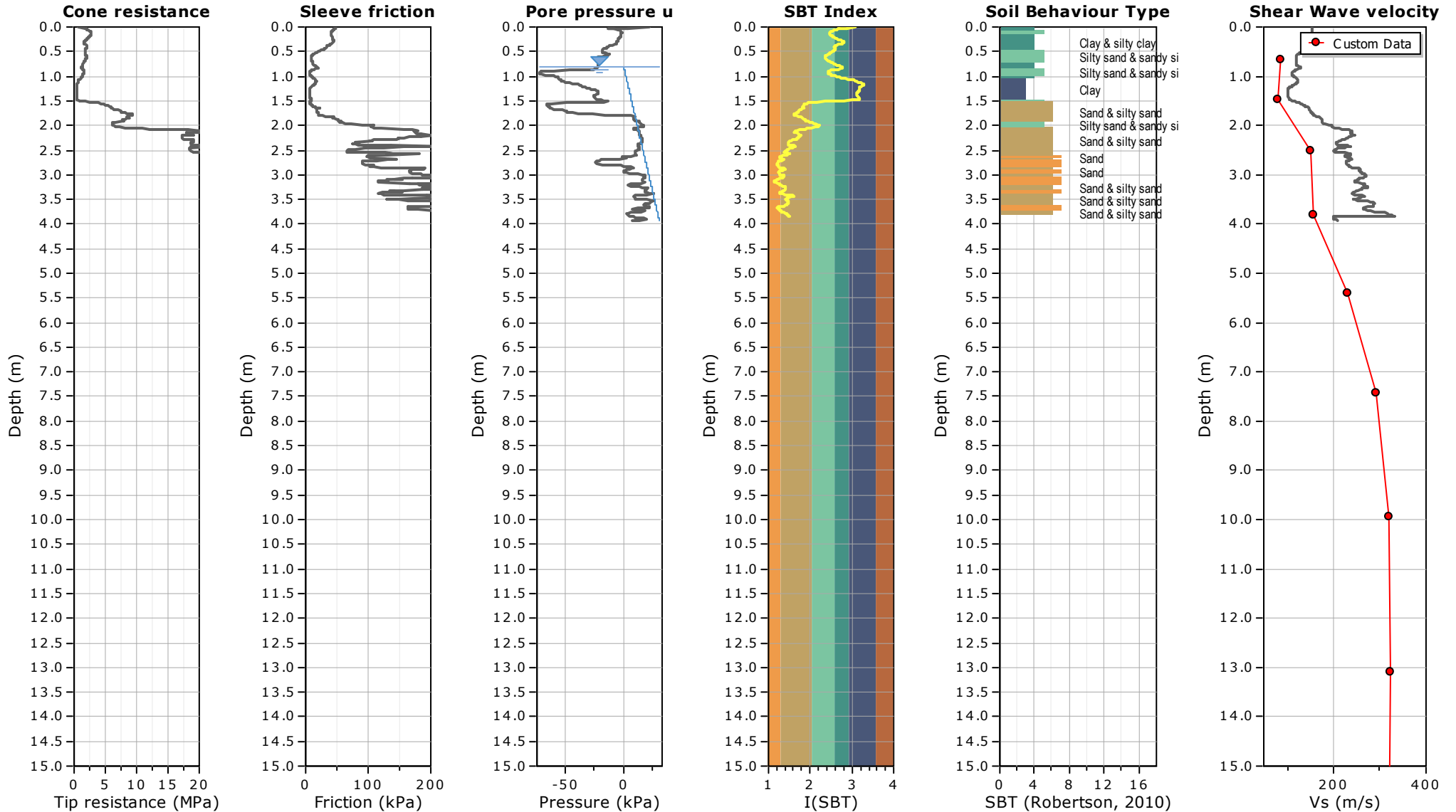
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



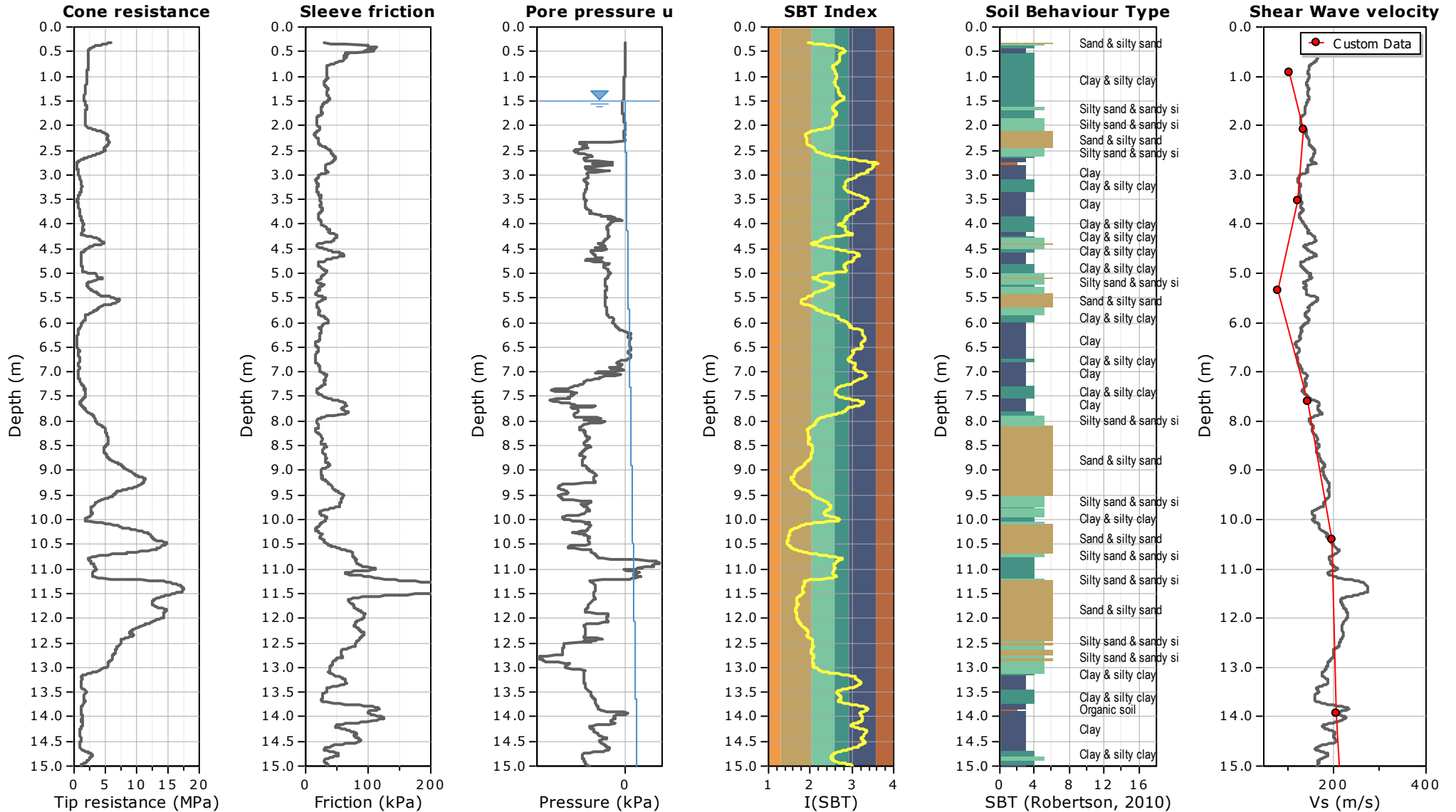
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



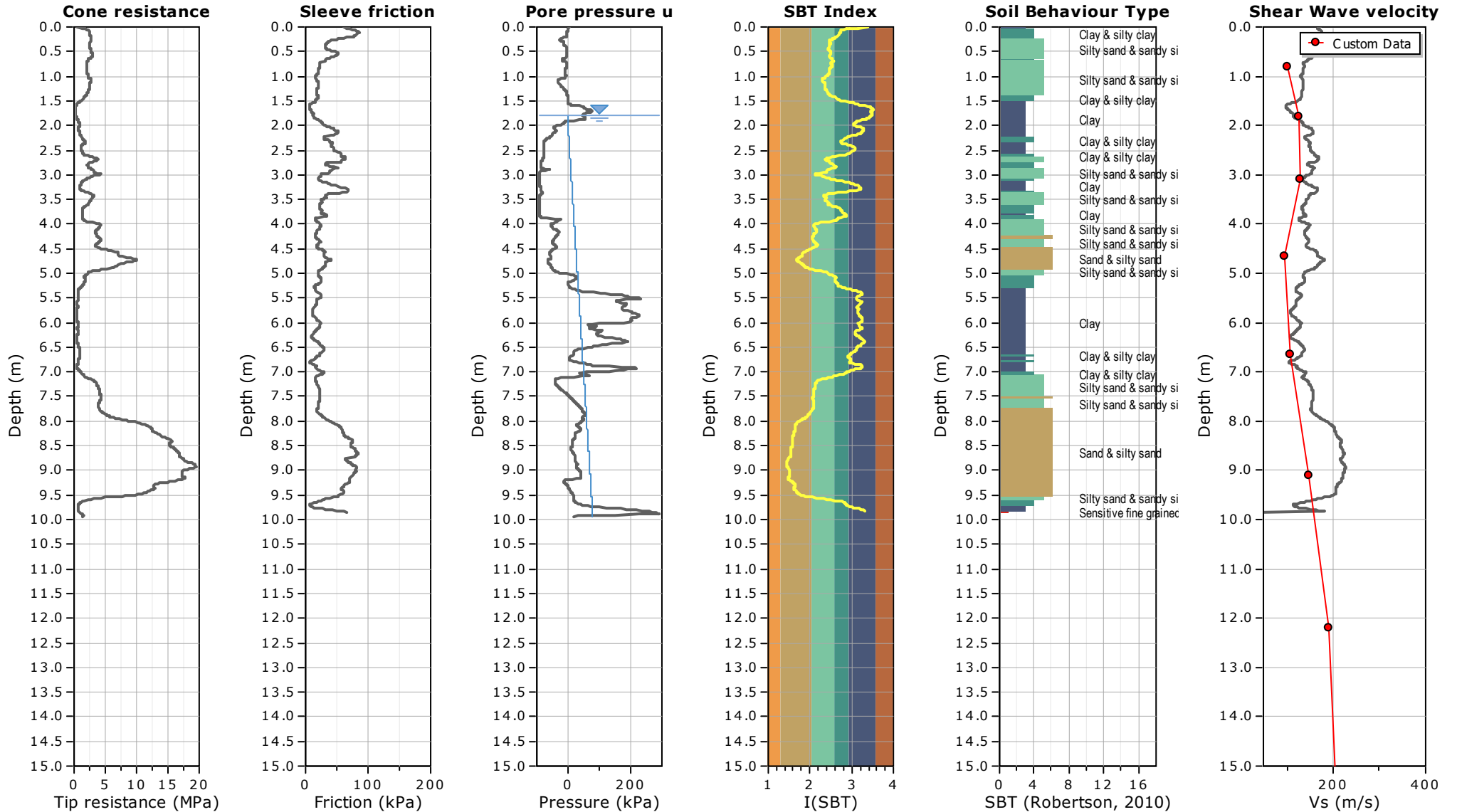
**Project: MINZ200357 - Geotechnical Investigation and Assessment**  
**Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch**



Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch

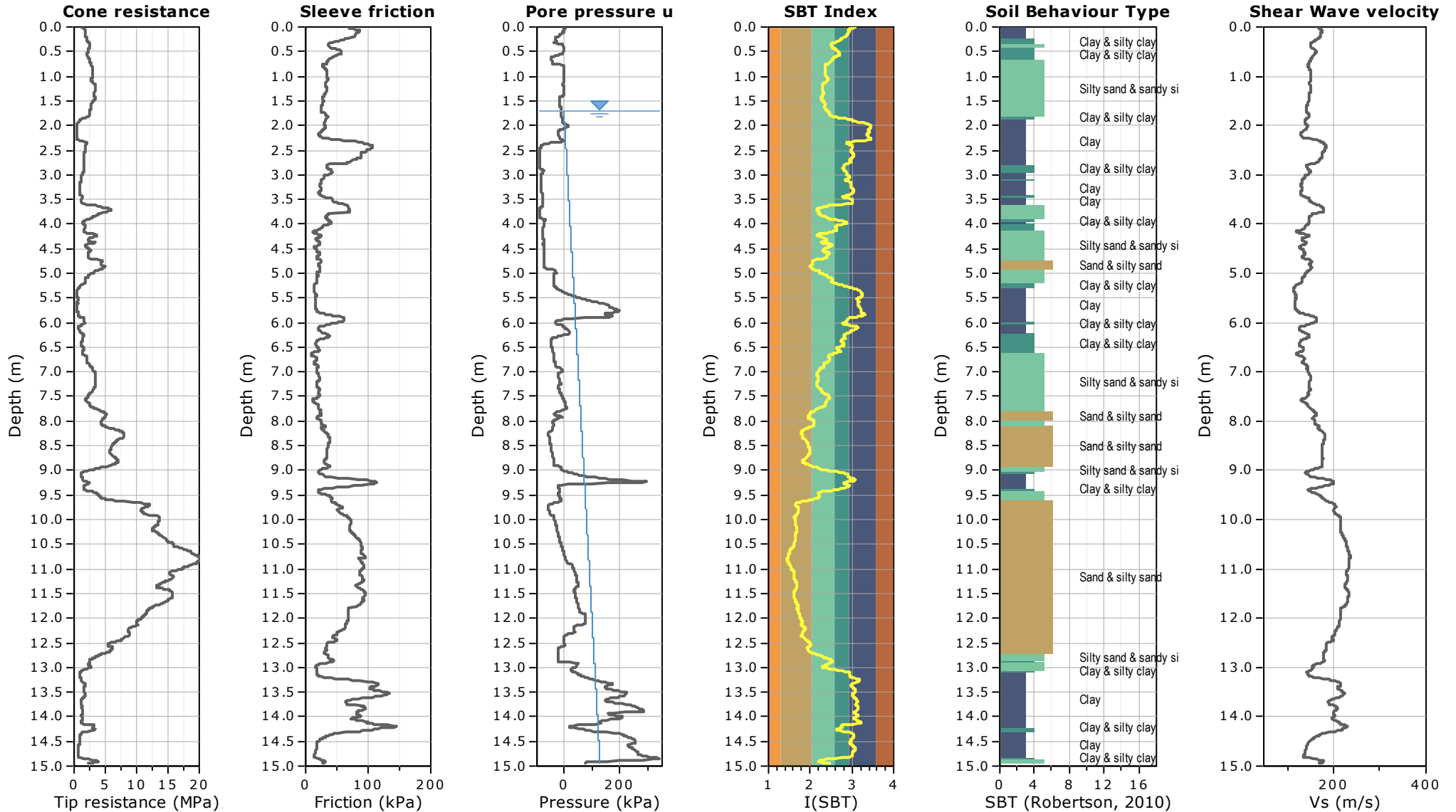


Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch

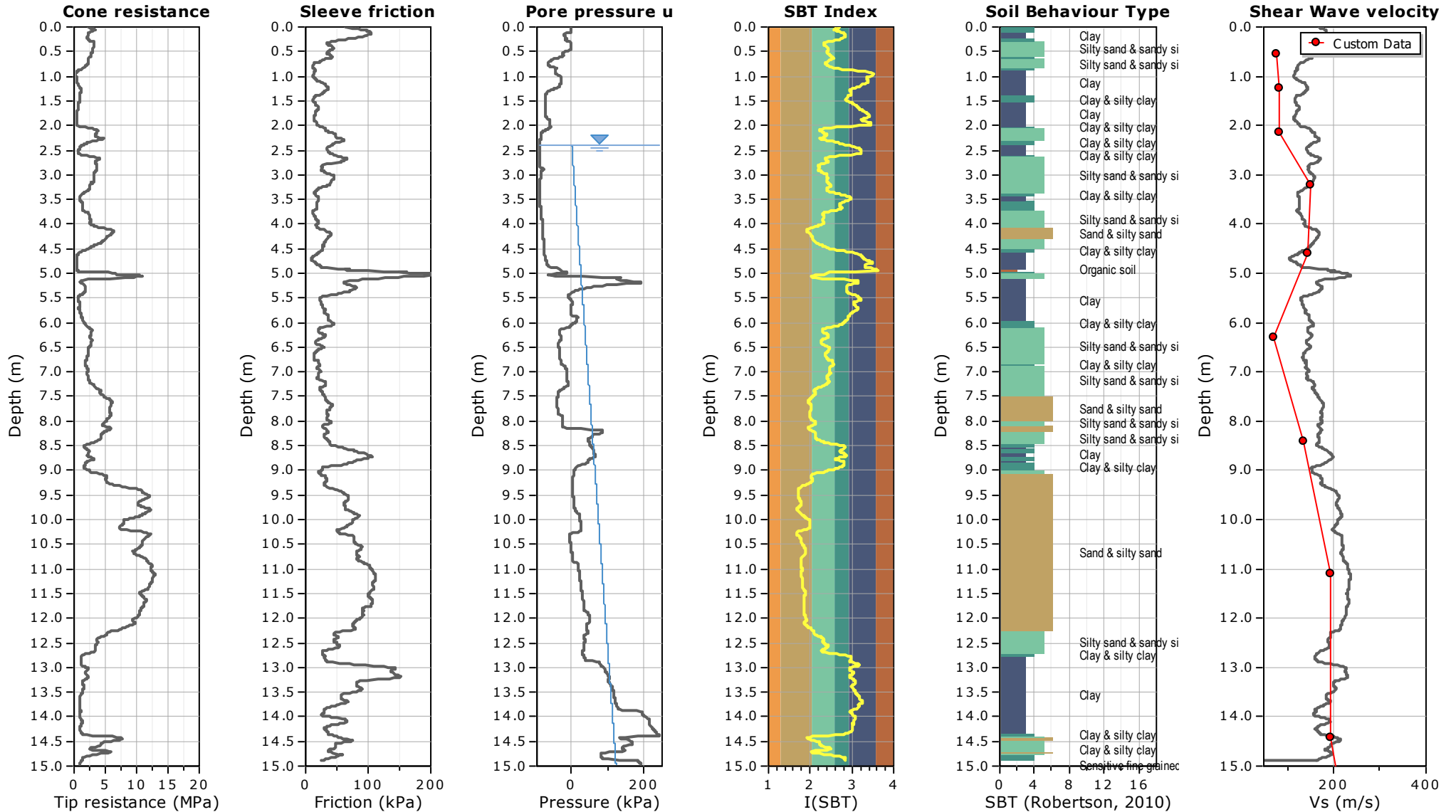




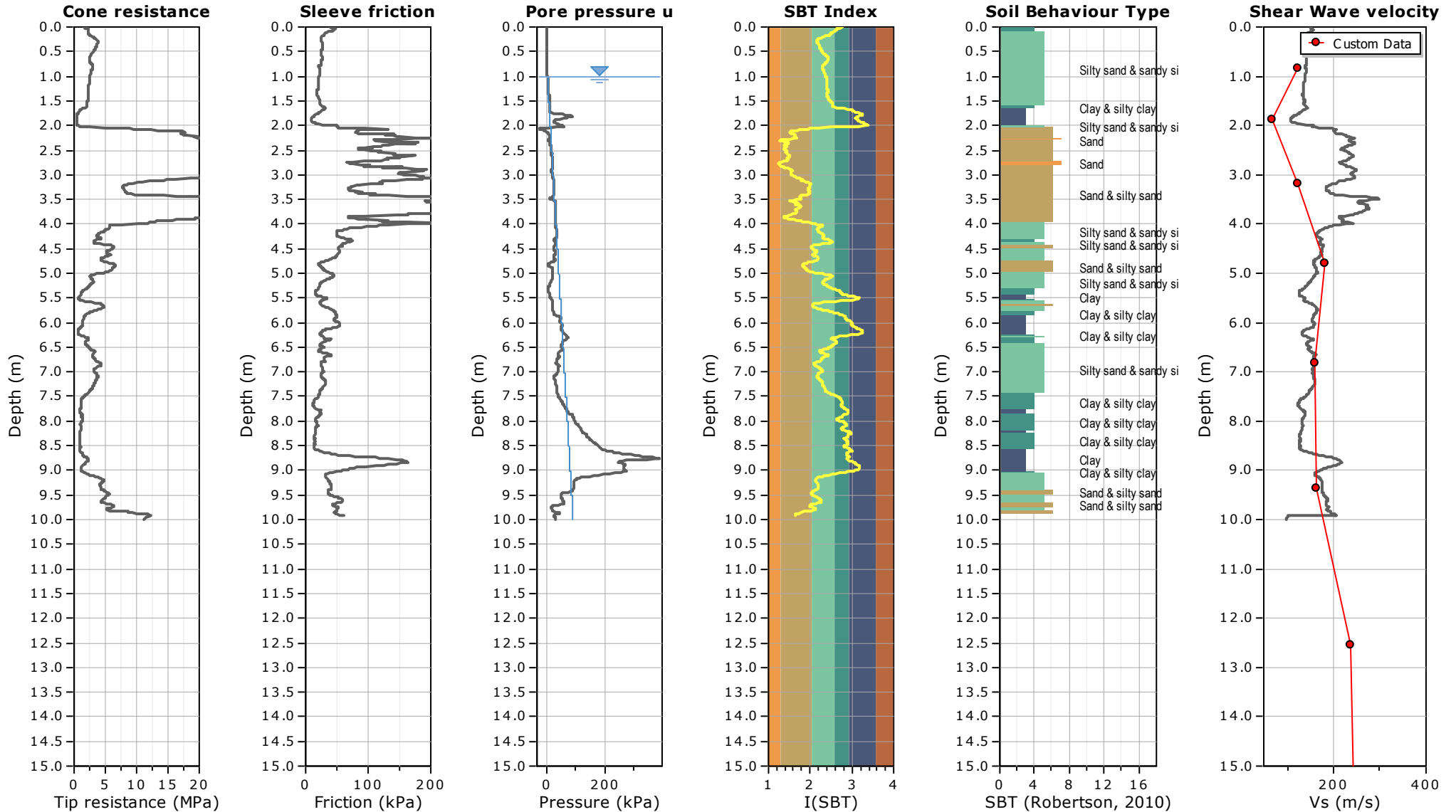
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



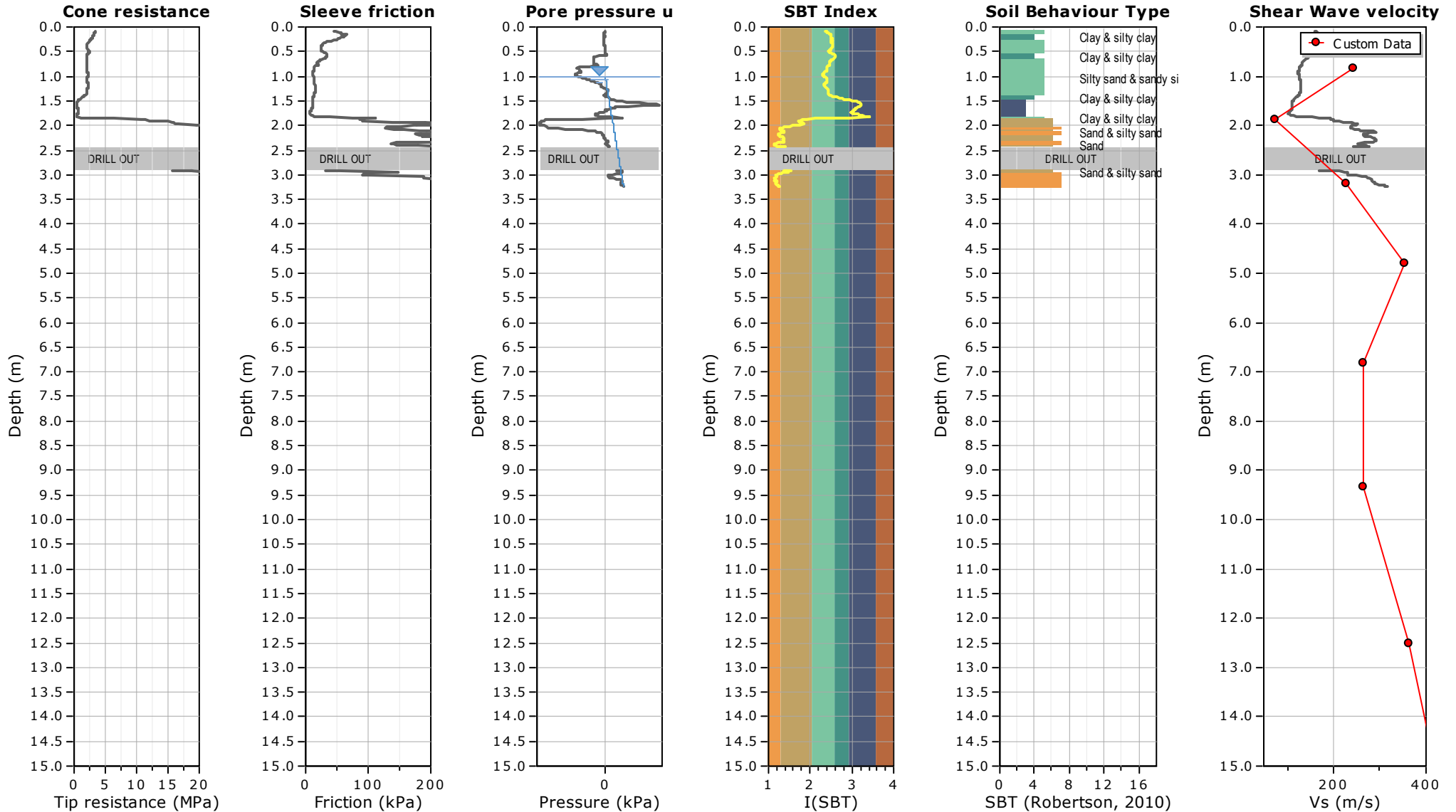
Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



Project: MINZ200357 - Geotechnical Investigation and Assessment  
 Location: 2 & 4 Glovers Road Subdivision, Halswell, Christchurch



# **CONE PENETRATION TEST (CPT) REPORT**

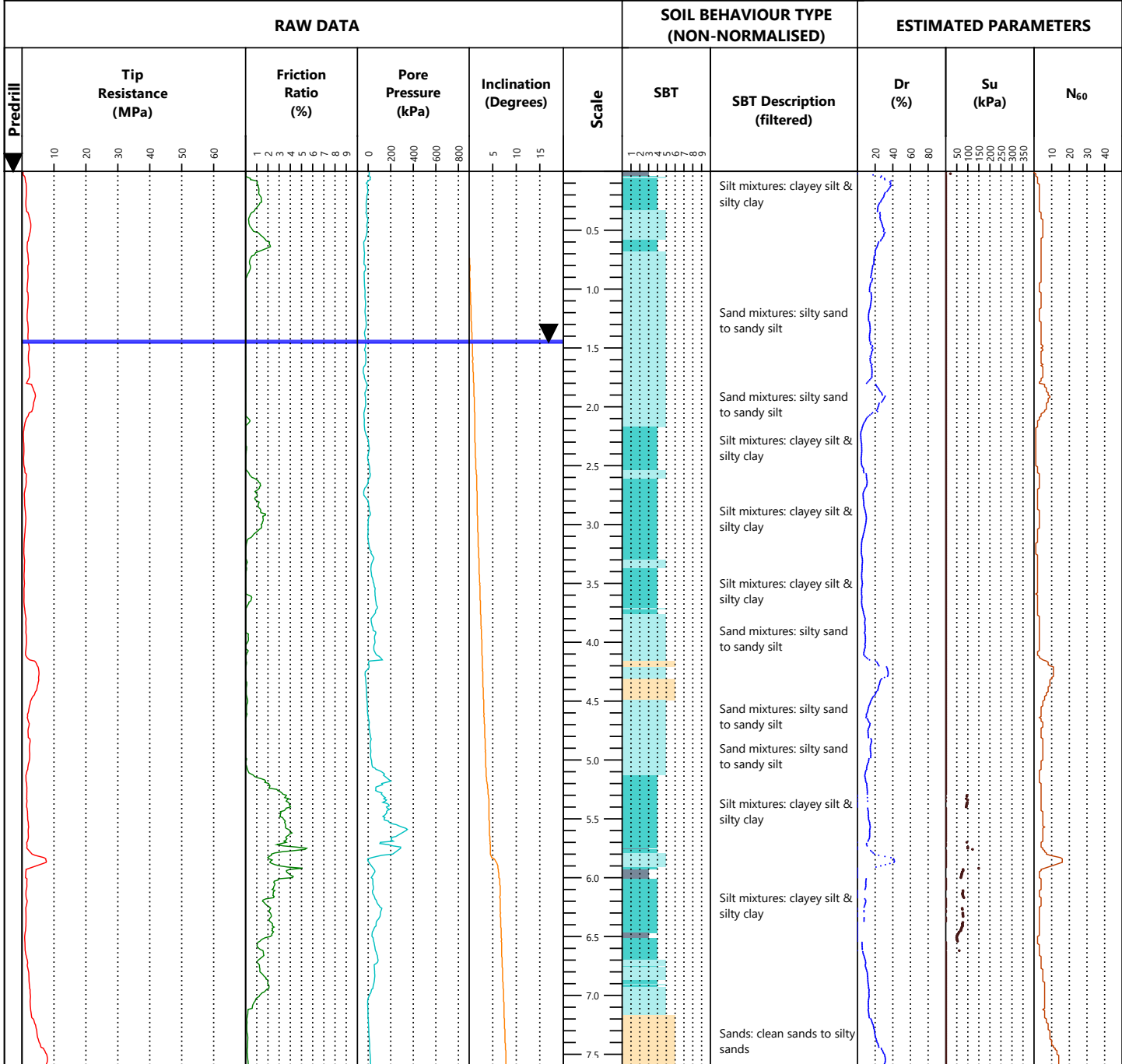


**Client: Miyamoto International NZ**

**Location: 2 Glovers Road, Christchurch**

**Printed: 20/08/2020**

**Site Location:** 2 Glovers Road, Christchurch **Date:** 18/8/2020  
**Grid Reference:** 1564920.46m E, 5173116.23m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150

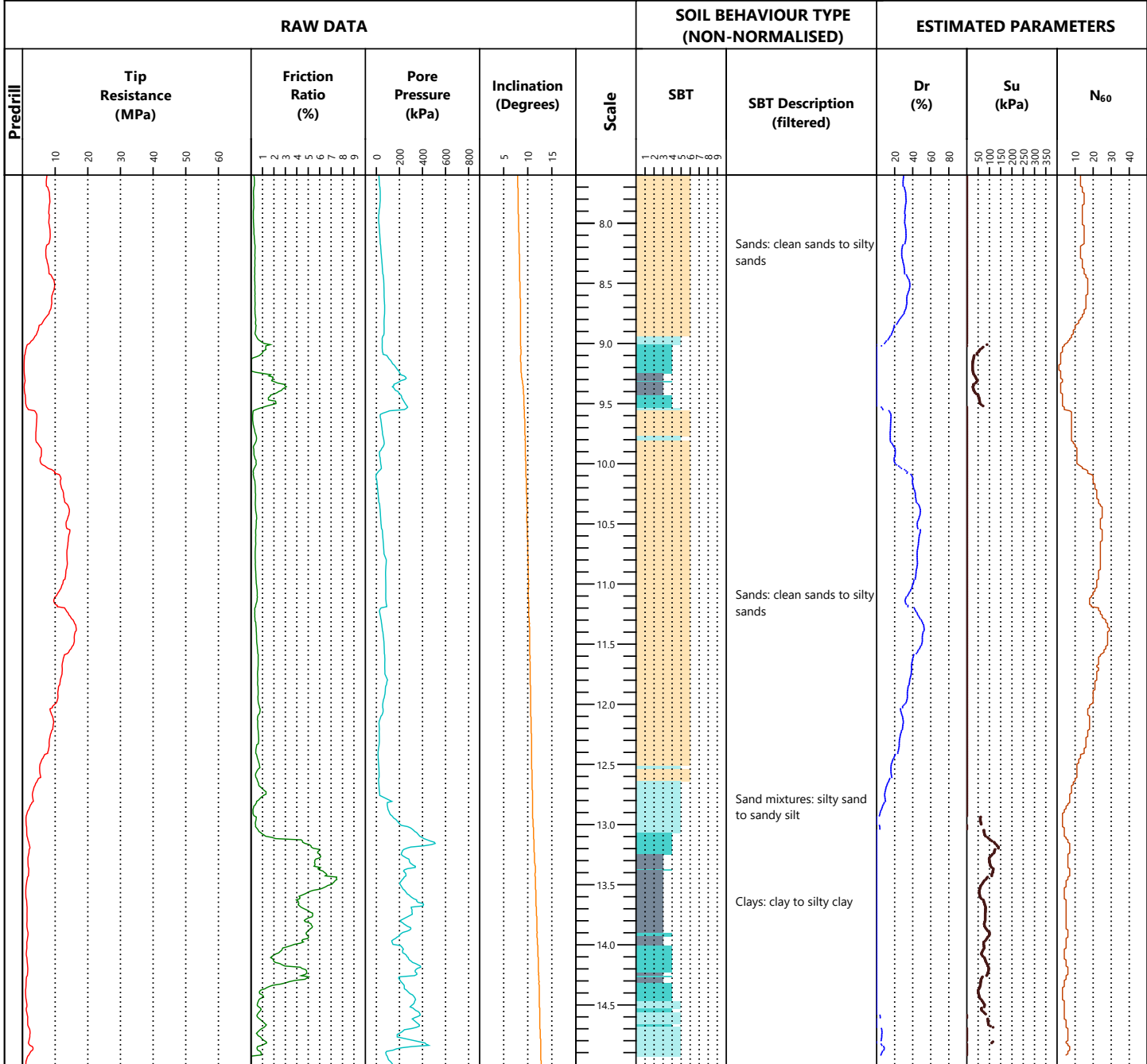


<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKS711	<b>Water Level:</b> 1.45m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 1.60m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	20.4528	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.2535		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	3.0597		<b>6</b> Sands: clean sands to silty sands
			<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

**Site Location:** 2 Glovers Road, Christchurch **Date:** 18/8/2020  
**Grid Reference:** 1564920.46m E, 5173116.23m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



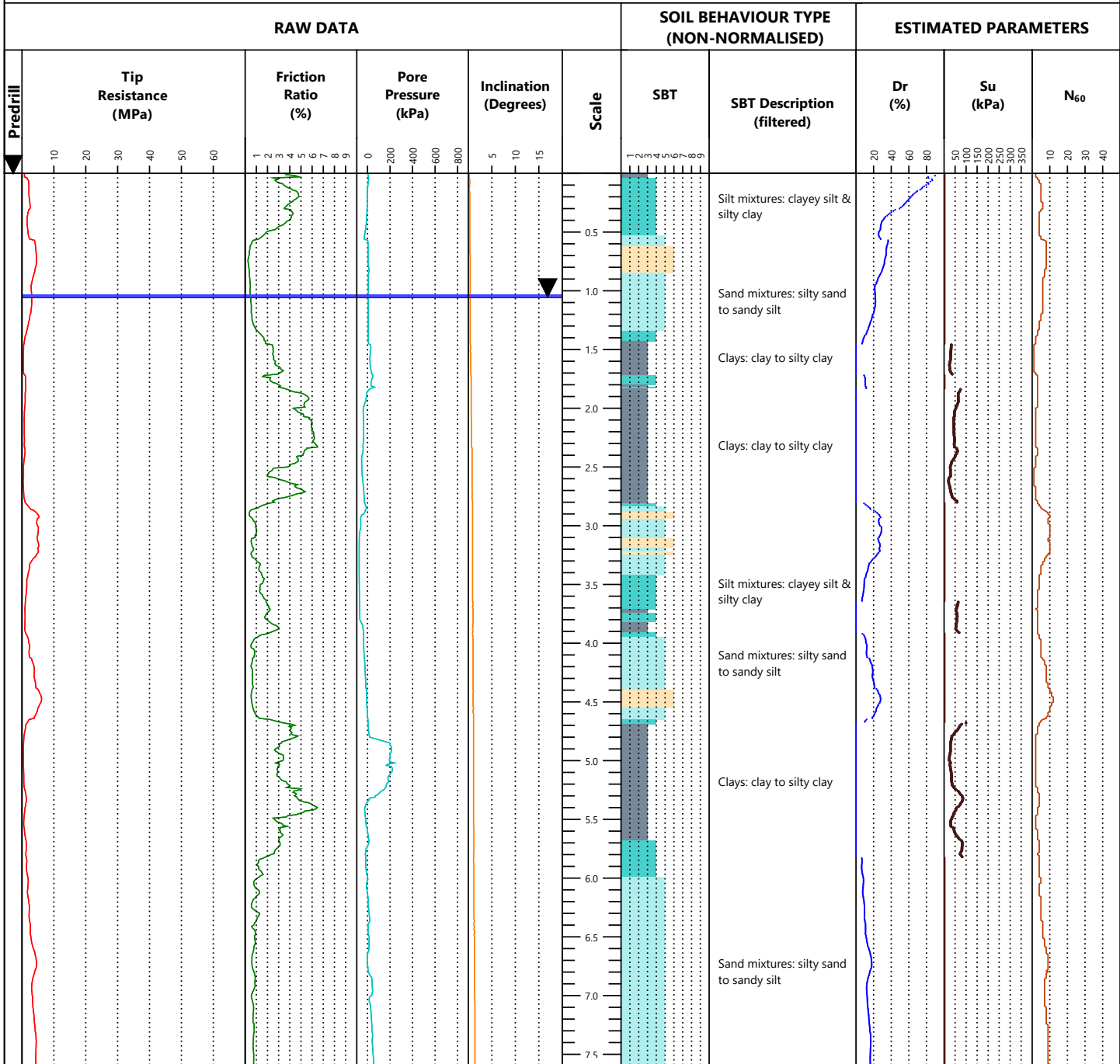
<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKS711	<b>Water Level:</b> 1.45m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 1.60m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	20.4528	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.2535		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	3.0597		<b>6</b> Sands: clean sands to silty sands
			<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
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**Remarks**

Sheet 2 of 2

**Site Location:** 2 Glovers Road, Christchurch **Date:** 17/8/2020  
**Grid Reference:** 1564969.32m E, 5173033.19m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



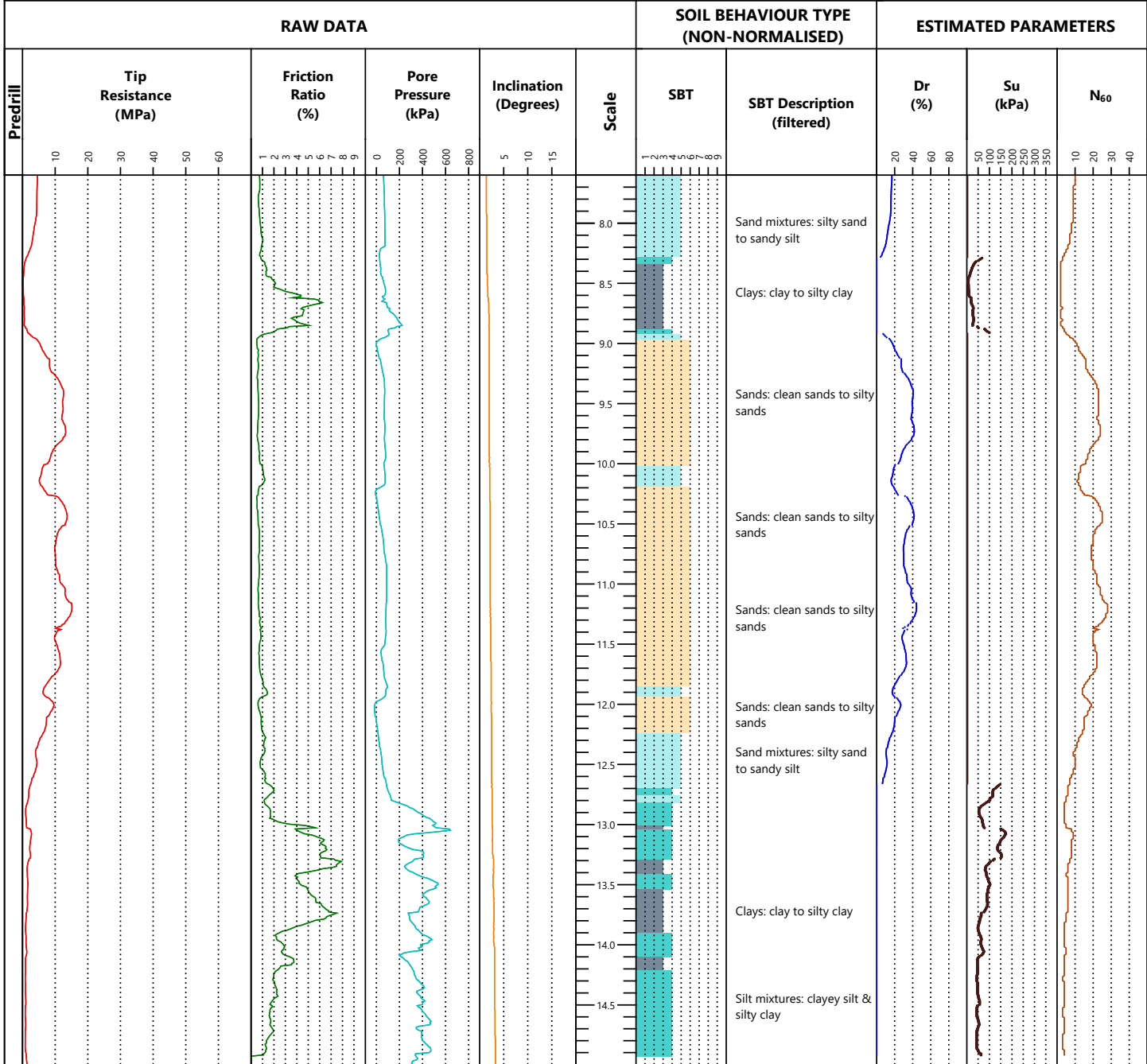
<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKS711	<b>Water Level:</b> 1.05m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 2.45m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	<b>After test</b>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	20.4004	20.348	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.2537	0.2536	<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	3.0612	3.0605	<b>6</b> Sands: clean sands to silty sands
			<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**



**Site Location:** 2 Glovers Road, Christchurch **Date:** 17/8/2020  
**Grid Reference:** 1564969.32m E, 5173033.19m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150

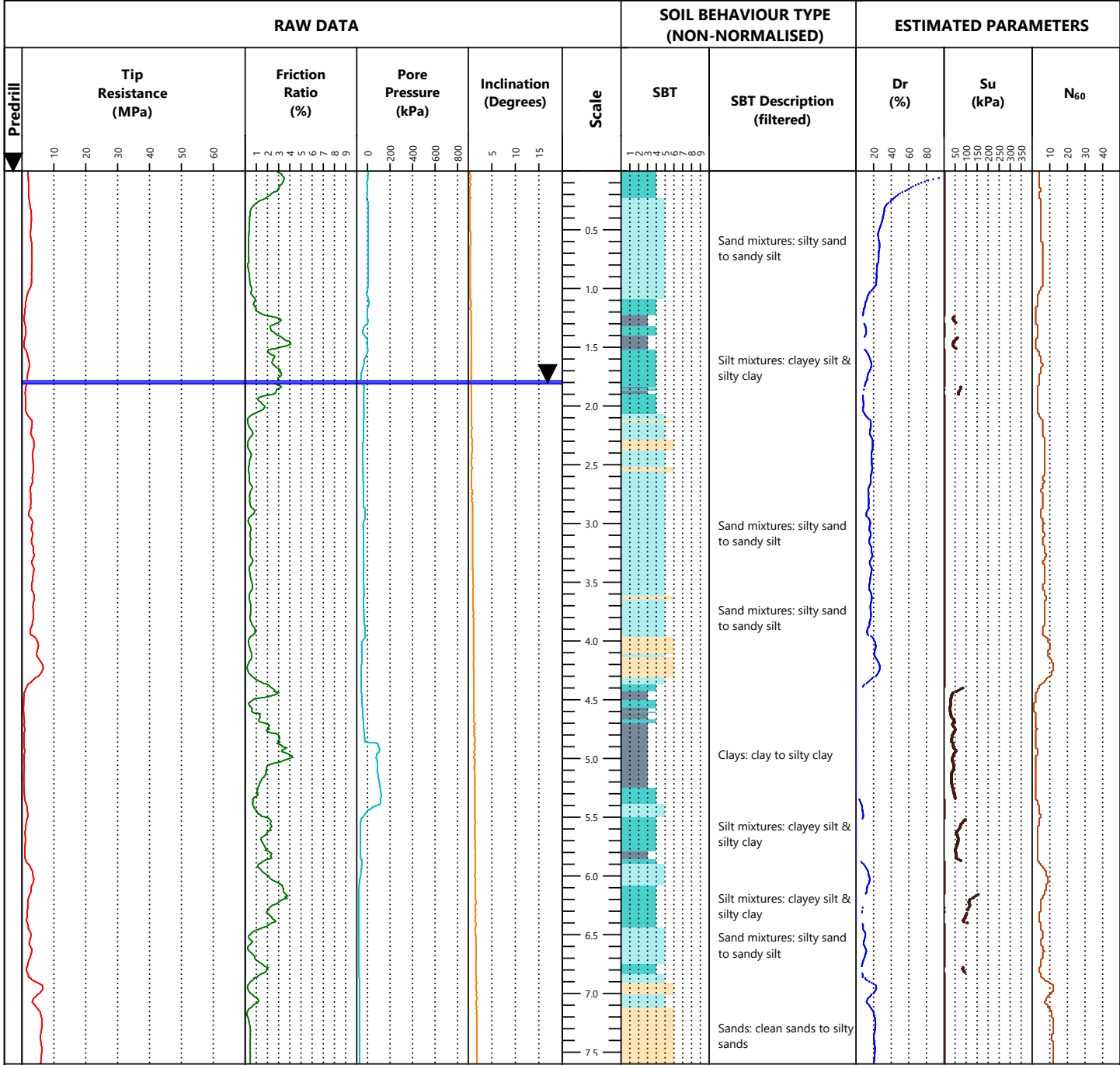


<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKS711	<b>Water Level:</b> 1.05m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 2.45m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	20.4004	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.2537		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	3.0612		<b>6</b> Sands: clean sands to silty sands
	3.0605		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

**Site Location:** 2 Glovers Road, Christchurch **Date:** 13/8/2020  
**Grid Reference:** 1564902m E, 5172941.77m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



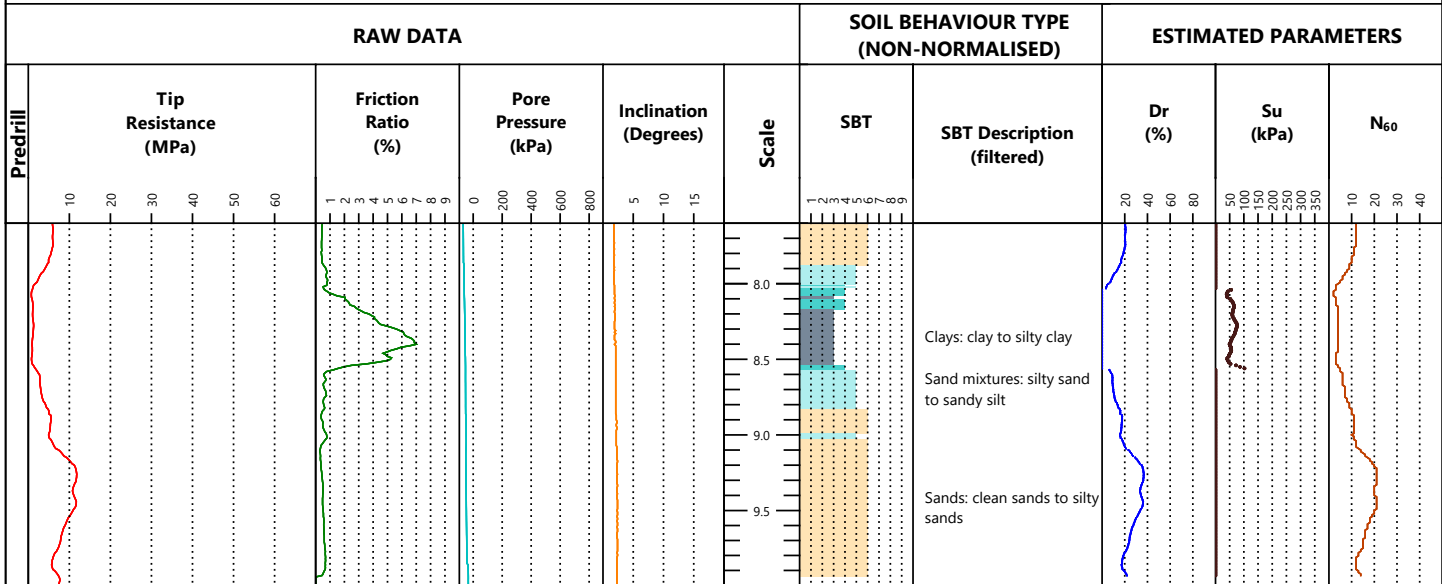
<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 1.8m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 2.70m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3554	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1187		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9596		<b>6</b> Sands: clean sands to silty sands
	0.9557		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu003</b>
<b>Project:</b>	2 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

<b>Site Location:</b> 2 Glovers Road, Christchurch	<b>Date:</b> 13/8/2020
<b>Grid Reference:</b> 1564902m E, 5172941.77m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> B. Wilson
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150

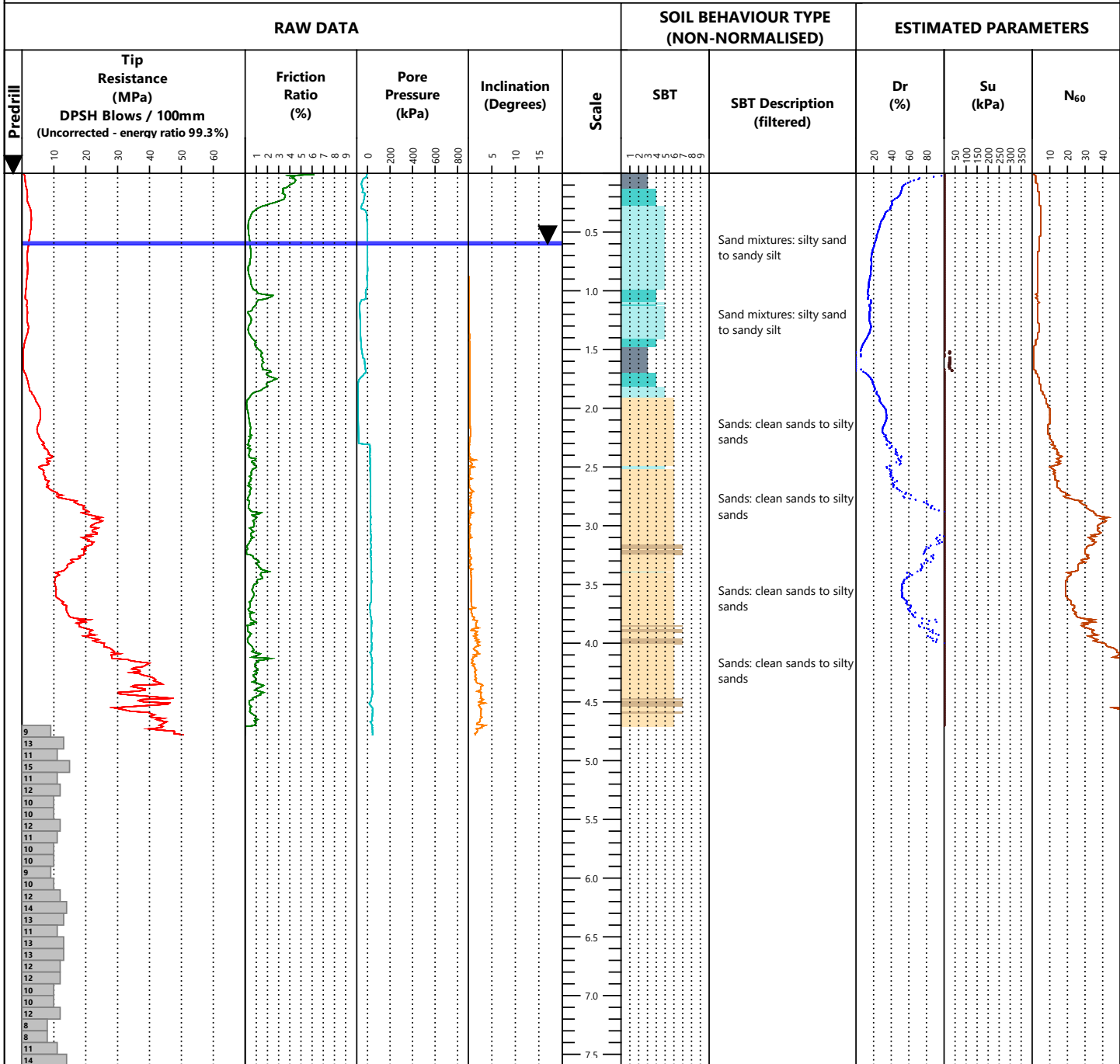


EOH: 10m

<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ328 <b>Cone Area Ratio:</b> 0.80 <b>Standards:</b> ISO 22476-1:2012	<b>Predrill:</b> - <b>Water Level:</b> 1.8m <b>Collapse:</b> 2.70m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="0"> <tr> <td>0 Undefined</td> <td>5 Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td>1 Sensitive fine-grained</td> <td>6 Sands: clean sands to silty sands</td> </tr> <tr> <td>2 Clay - organic soil</td> <td>7 Dense sand to gravelly sand</td> </tr> <tr> <td>3 Clays: clay to silty clay</td> <td>8 Stiff sand to clayey sand</td> </tr> <tr> <td>4 Silt mixtures: clayey silt &amp; silty clay</td> <td>9 Stiff fine-grained</td> </tr> </table>	0 Undefined	5 Sand mixtures: silty sand to sandy silt	1 Sensitive fine-grained	6 Sands: clean sands to silty sands	2 Clay - organic soil	7 Dense sand to gravelly sand	3 Clays: clay to silty clay	8 Stiff sand to clayey sand	4 Silt mixtures: clayey silt & silty clay	9 Stiff fine-grained
0 Undefined	5 Sand mixtures: silty sand to sandy silt												
1 Sensitive fine-grained	6 Sands: clean sands to silty sands												
2 Clay - organic soil	7 Dense sand to gravelly sand												
3 Clays: clay to silty clay	8 Stiff sand to clayey sand												
4 Silt mixtures: clayey silt & silty clay	9 Stiff fine-grained												
<b>Zero load outputs (MPa)</b> <b>Tip Resistance</b> 11.3554 <b>Before test</b> <b>After test</b> <b>Local Friction</b> 0.1187    0.1186 <b>Pore Pressure</b> 0.9596    0.9557	<b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>												

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>  Sheet 2 of 2
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<b>Site Location:</b> 2 Glovers Road, Christchurch	<b>Date:</b> 19/8/2020
<b>Grid Reference:</b> 1564993.47m E, 5172892.27m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> B. Wilson
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.6m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.95m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3452	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1186		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9595		<b>6</b> Sands: clean sands to silty sands
	0.9554		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>
	Sheet 1 of 2



<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu004</b>
<b>Project:</b>	2 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

**Site Location:** 2 Glovers Road, Christchurch **Date:** 19/8/2020  
**Grid Reference:** 1564993.47m E, 5172892.27m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150

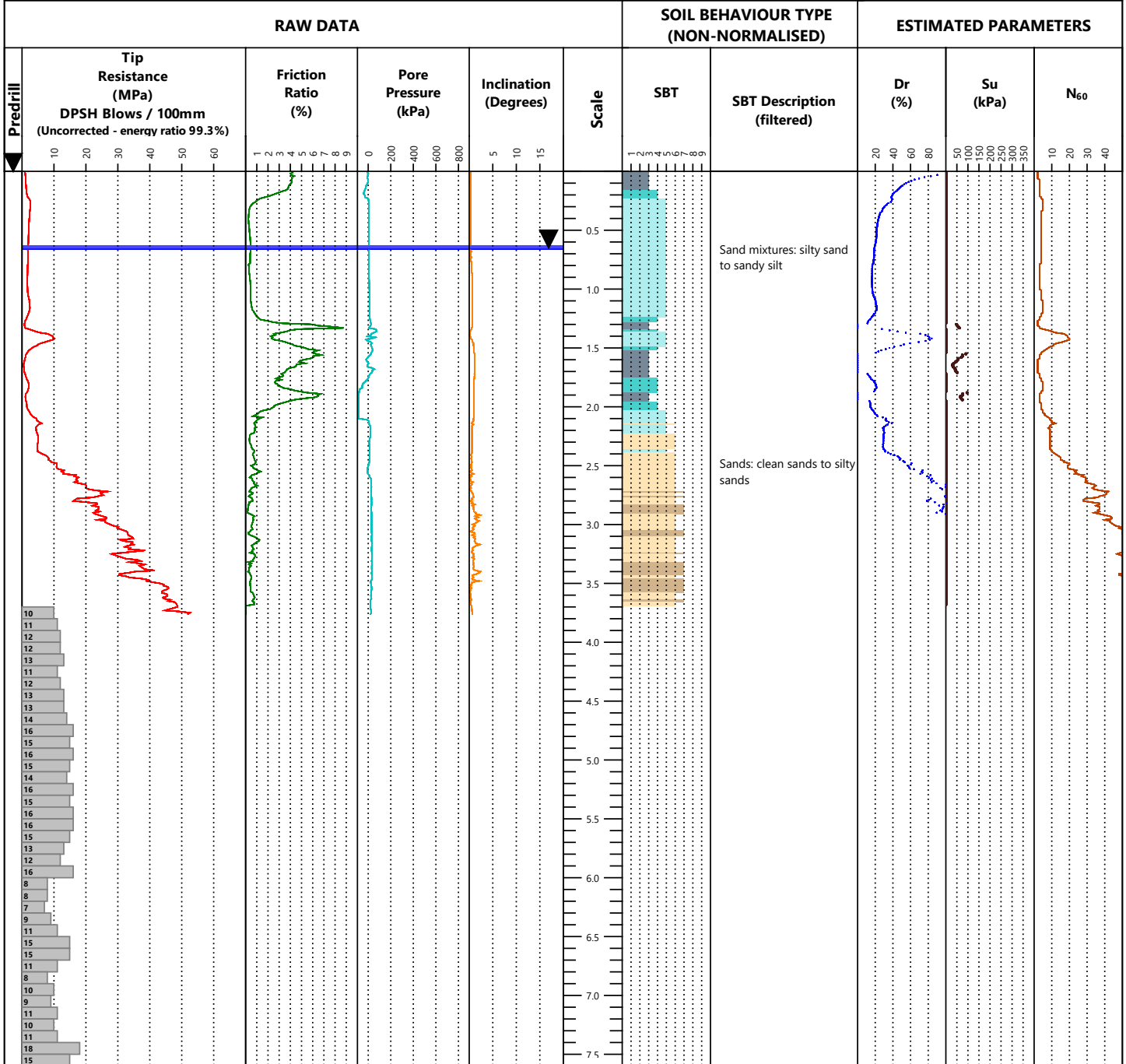
RAW DATA					SOIL BEHAVIOUR TYPE (NON-NORMALISED)		ESTIMATED PARAMETERS			
Predrill	Tip Resistance (MPa) DPSH Blows / 100mm (Uncorrected - energy ratio 99.3%)	Friction Ratio (%)	Pore Pressure (kPa)	Inclination (Degrees)	Scale	SBT	SBT Description (filtered)	ESTIMATED PARAMETERS		
								Dr (%)	Su (kPa)	N <sub>60</sub>
9	10	1	0	5	8.0	0		20	50	10
12	10	1	0	5	8.0	0		20	50	10
13	10	1	0	5	8.0	0		20	50	10
12	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
7	10	1	0	5	8.0	0		20	50	10
6	10	1	0	5	8.0	0		20	50	10
3	10	1	0	5	8.0	0		20	50	10
1	10	1	0	5	8.0	0		20	50	10
2	10	1	0	5	8.0	0		20	50	10
2	10	1	0	5	8.0	0		20	50	10
2	10	1	0	5	8.0	0		20	50	10
3	10	1	0	5	8.0	0		20	50	10
3	10	1	0	5	8.0	0		20	50	10
3	10	1	0	5	8.0	0		20	50	10
4	10	1	0	5	8.0	0		20	50	10
6	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
7	10	1	0	5	8.0	0		20	50	10
8	10	1	0	5	8.0	0		20	50	10
11	10	1	0	5	8.0	0		20	50	10
11	10	1	0	5	8.0	0		20	50	10
9	10	1	0	5	8.0	0		20	50	10
10	10	1	0	5	8.0	0		20	50	10
9	10	1	0	5	8.0	0		20	50	10
7	10	1	0	5	8.0	0		20	50	10
7	10	1	0	5	8.0	0		20	50	10
8	10	1	0	5	8.0	0		20	50	10
4	10	1	0	5	8.0	0		20	50	10
4	10	1	0	5	8.0	0		20	50	10
4	10	1	0	5	8.0	0		20	50	10
6	10	1	0	5	8.0	0		20	50	10
7	10	1	0	5	8.0	0		20	50	10
4	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
10	10	1	0	5	8.0	0		20	50	10
8	10	1	0	5	8.0	0		20	50	10
8	10	1	0	5	8.0	0		20	50	10
8	10	1	0	5	8.0	0		20	50	10
7	10	1	0	5	8.0	0		20	50	10
6	10	1	0	5	8.0	0		20	50	10
8	10	1	0	5	8.0	0		20	50	10
9	10	1	0	5	8.0	0		20	50	10
9	10	1	0	5	8.0	0		20	50	10
6	10	1	0	5	8.0	0		20	50	10
6	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
3	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
6	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
6	10	1	0	5	8.0	0		20	50	10
6	10	1	0	5	8.0	0		20	50	10
6	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
5	10	1	0	5	8.0	0		20	50	10
7	10	1	0	5	8.0	0		20	50	10
7	10	1	0	5	8.0	0		20	50	10
8	10	1	0	5	8.0	0		20	50	10
11	10	1	0	5	8.0	0		20	50	10
8	10	1	0	5	8.0	0		20	50	10
9	10	1	0	5	8.0	0		20	50	10
8	10	1	0	5	8.0	0		20	50	10
7	10	1	0	5	8.0	0		20	50	10

EOH: 15m

<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.6m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.95m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3452	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1186		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9595		<b>6</b> Sands: clean sands to silty sands
	0.9554		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

<b>Notes &amp; Limitations</b>	<b>Remarks</b>
Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	

**Site Location:** 2 Glovers Road, Christchurch **Date:** 19/8/2020  
**Grid Reference:** 1564945.37m E, 5172828.71m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.65m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.45m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.4066	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1183		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9587		<b>6</b> Sands: clean sands to silty sands
			<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**



<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu005</b>
<b>Project:</b>	2 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

<b>Site Location:</b> 2 Glovers Road, Christchurch	<b>Date:</b> 19/8/2020
<b>Grid Reference:</b> 1564945.37m E, 5172828.71m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> B. Wilson
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150

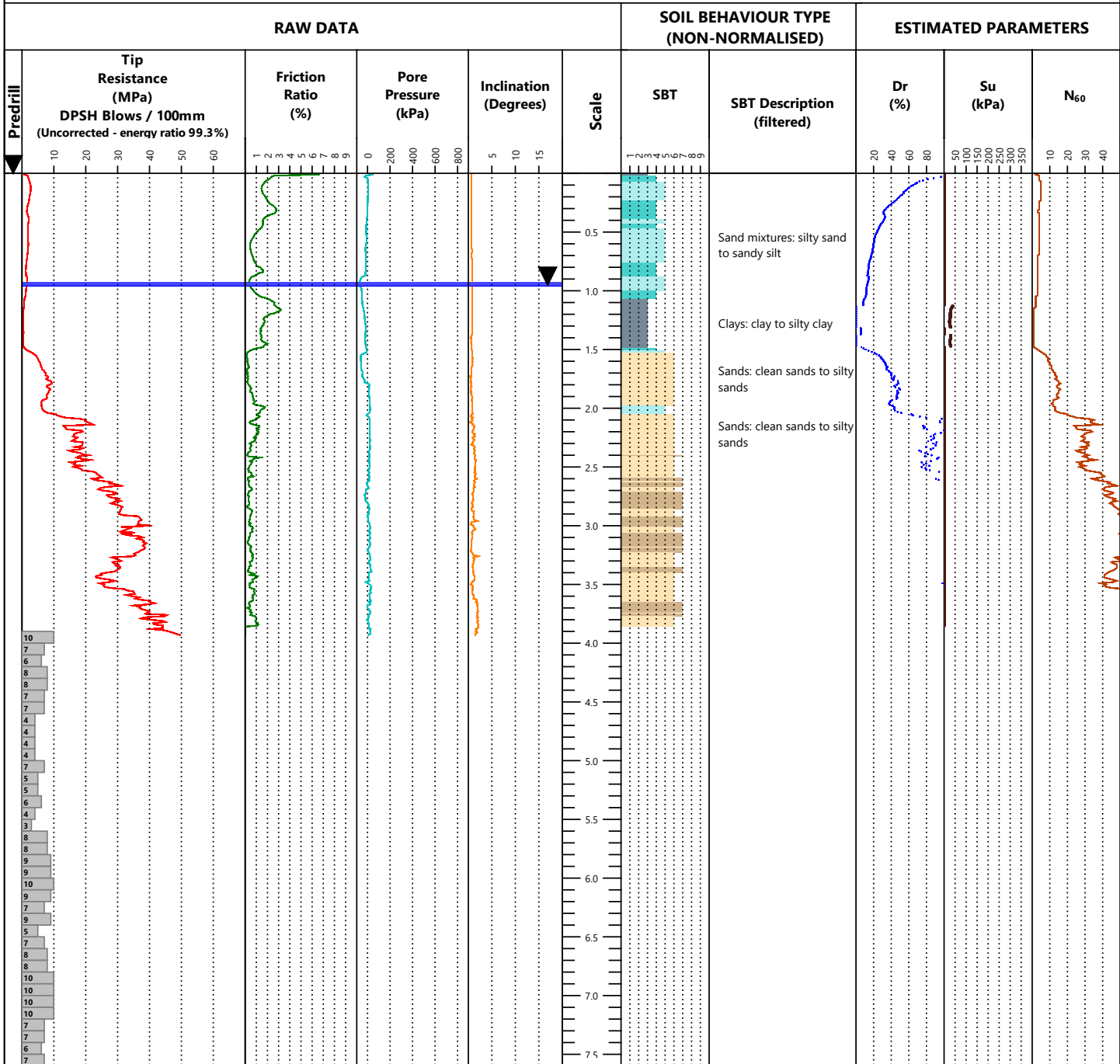
RAW DATA					SOIL BEHAVIOUR TYPE (NON-NORMALISED)		ESTIMATED PARAMETERS								
Predrill	Tip Resistance (MPa) DPSH Blows / 100mm (Uncorrected - energy ratio 99.3%)		Friction Ratio (%)	Pore Pressure (kPa)	Inclination (Degrees)	Scale	SBT	SBT Description (filtered)	Dr (%)		Su (kPa)	N <sub>60</sub>			
	10	20	1	0	5				20	40	60	80	50	10	20
13	10					8.0									
12	10														
11	10														
8	10														
4	10														
2	10														
2	10														
5	10														
4	10														
10	10					8.5									
14	10														
12	10														
12	10														
12	10														
10	10					9.0									
10	10														
9	10														
12	10														
12	10														
12	10					9.5									
14	10														
15	10														
17	10														
15	10														

EOH: 10m

<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ328 <b>Cone Area Ratio:</b> 0.80 <b>Standards:</b> ISO 22476-1:2012  <b>Zero load outputs (MPa)</b> <table border="1"> <tr> <th>Before test</th> <th>After test</th> </tr> <tr> <td><b>Tip Resistance</b> 11.4066</td> <td>11.2583</td> </tr> <tr> <td><b>Local Friction</b> 0.1183</td> <td>0.1192</td> </tr> <tr> <td><b>Pore Pressure</b> 0.9587</td> <td>0.9583</td> </tr> </table>	Before test	After test	<b>Tip Resistance</b> 11.4066	11.2583	<b>Local Friction</b> 0.1183	0.1192	<b>Pore Pressure</b> 0.9587	0.9583	<b>Predrill:</b> - <b>Water Level:</b> 0.65m <b>Collapse:</b> 1.45m	<b>Termination</b> <b>Target Depth:</b> <input type="checkbox"/>  <b>Effective Refusal</b> Tip: <input checked="" type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="1"> <tr> <td>0</td> <td>Undefined</td> <td>5</td> <td>Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td>1</td> <td>Sensitive fine-grained</td> <td>6</td> <td>Sands: clean sands to silty sands</td> </tr> <tr> <td>2</td> <td>Clay - organic soil</td> <td>7</td> <td>Dense sand to gravelly sand</td> </tr> <tr> <td>3</td> <td>Clays: clay to silty clay</td> <td>8</td> <td>Stiff sand to clayey sand</td> </tr> <tr> <td>4</td> <td>Silt mixtures: clayey silt &amp; silty clay</td> <td>9</td> <td>Stiff fine-grained</td> </tr> </table>	0	Undefined	5	Sand mixtures: silty sand to sandy silt	1	Sensitive fine-grained	6	Sands: clean sands to silty sands	2	Clay - organic soil	7	Dense sand to gravelly sand	3	Clays: clay to silty clay	8	Stiff sand to clayey sand	4	Silt mixtures: clayey silt & silty clay	9	Stiff fine-grained
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<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>   <p style="text-align: right;">Sheet 2 of 2</p>
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**Site Location:** 2 Glovers Road, Christchurch **Date:** 13/8/2020  
**Grid Reference:** 1565008.77m E, 5172744.63m N (NZTM) - Map or aerial photograph **Rig Operator:** B. Wilson  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.95m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.40m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3708	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1178		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9592		<b>6</b> Sands: clean sands to silty sands
			<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**





<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu006</b>
<b>Project:</b>	2 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

<b>Site Location:</b> 2 Glovers Road, Christchurch	<b>Date:</b> 13/8/2020
<b>Grid Reference:</b> 1565008.77m E, 5172744.63m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> B. Wilson
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150

RAW DATA					SOIL BEHAVIOUR TYPE (NON-NORMALISED)		ESTIMATED PARAMETERS			
Predrill	Tip Resistance (MPa) DPSH Blows / 100mm (Uncorrected - energy ratio 99.3%)	Friction Ratio (%)	Pore Pressure (kPa)	Inclination (Degrees)	Scale	SBT	SBT Description (filtered)	ESTIMATED PARAMETERS		
								Dr (%)	Su (kPa)	N <sub>60</sub>
5	10	1	0	5	8.0	5		20	50	10
6	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
11	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
11	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
10	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
6	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
10	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
4	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
9	10	1	0	5	8.0	5		20	50	10
6	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
7	10	1	0	5	8.0	5		20	50	10
8	10	1	0	5	8.0	5		20	50	10
12	10	1	0	5	8.0	5		20	50	10
12	10	1	0	5	8.0	5		20	50	10
12	10	1	0	5	8.0	5		20	50	10
10	10	1	0	5	8.0	5		20	50	10
11	10	1	0	5	8.0	5		20	50	10
14	10	1	0	5	8.0	5		20	50	10
13	10	1	0	5	8.0	5		20	50	10
16	10	1	0	5	8.0	5		20	50	10
17	10	1	0	5	8.0	5		20	50	10
14	10	1	0	5	8.0	5		20	50	10
15	10	1	0	5	8.0	5		20	50	10
17	10	1	0	5	8.0	5		20	50	10
16	10	1	0	5	8.0	5		20	50	10
17	10	1	0	5	8.0	5		20	50	10
21	10	1	0	5	8.0	5		20	50	10

EOH: 12.7m

<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ328	<b>Water Level:</b> 0.95m	<b>Target Depth:</b> <input type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.80	<b>Collapse:</b> 1.40m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.3708	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1178		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	0.9592		<b>6</b> Sands: clean sands to silty sands
	0.9542		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>
	Sheet 2 of 2

## TEST DETAIL

PointID: CPTu001  
Sounding: 1

**Operator:** E. Diaz  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKS711  
**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	20.4528	20.369
<b>Local Friction</b>	0.2535	0.2535
<b>Pore Pressure</b>	3.0597	3.0579

**Date:** 18/8/2020  
**Predrill:** -  
**Water Level:** 1.45m  
**Collapse:** 1.60m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu002  
Sounding: 1

**Operator:** E. Diaz  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKS711  
**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	20.4004	20.348
<b>Local Friction</b>	0.2537	0.2536
<b>Pore Pressure</b>	3.0612	3.0605

**Date:** 17/8/2020  
**Predrill:** -  
**Water Level:** 1.05m  
**Collapse:** 2.45m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu003  
Sounding: 1

**Operator:** B. Wilson  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKJ328  
**Cone Area Ratio:** 0.80

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.3554	11.3094
<b>Local Friction</b>	0.1187	0.1186
<b>Pore Pressure</b>	0.9596	0.9557

**Date:** 13/8/2020  
**Predrill:** -  
**Water Level:** 1.8m  
**Collapse:** 2.70m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu004  
Sounding: 1

**Operator:** B. Wilson  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKJ328  
**Cone Area Ratio:** 0.80

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.3452	11.2685
<b>Local Friction</b>	0.1186	0.1191
<b>Pore Pressure</b>	0.9595	0.9554

**Date:** 19/8/2020  
**Predrill:** -  
**Water Level:** 0.6m  
**Collapse:** 1.95m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

PointID: CPTu005  
Sounding: 1

**Operator:** B. Wilson  
**Cone Type:** Pagani Piezocone - Compression  
**Cone Reference:** MKJ328  
**Cone Area Ratio:** 0.80

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.4066	11.2583
<b>Local Friction</b>	0.1183	0.1192
<b>Pore Pressure</b>	0.9587	0.9583

**Date:** 19/8/2020  
**Predrill:** -  
**Water Level:** 0.65m  
**Collapse:** 1.45m

**Termination**  
**Target Depth:**   
**Effective Refusal**  
Tip:   
Gauge:   
Inclinometer:

# TEST DETAIL

---

PointID: CPTu006

Sounding: 1

**Operator:** B. Wilson

**Cone Type:** Pagani Piezocone - Compression

**Cone Reference:** MKJ328

**Cone Area Ratio:** 0.80

**Date:** 13/8/2020

**Predrill:** -

**Water Level:** 0.95m

**Collapse:** 1.40m

**Termination**

**Target Depth:**

**Effective Refusal**

Tip:

Gauge:

Inclinometer:

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.3708	11.2634
<b>Local Friction</b>	0.1178	0.119
<b>Pore Pressure</b>	0.9592	0.9542

# CPT CALIBRATION AND TECHNICAL NOTES

These notes describe the technical specifications and associated calibration references pertaining to the Pagani piezocone types measuring cone resistance, sleeve friction, inclination and pore pressure (piezocone, 10cm<sup>2</sup>)

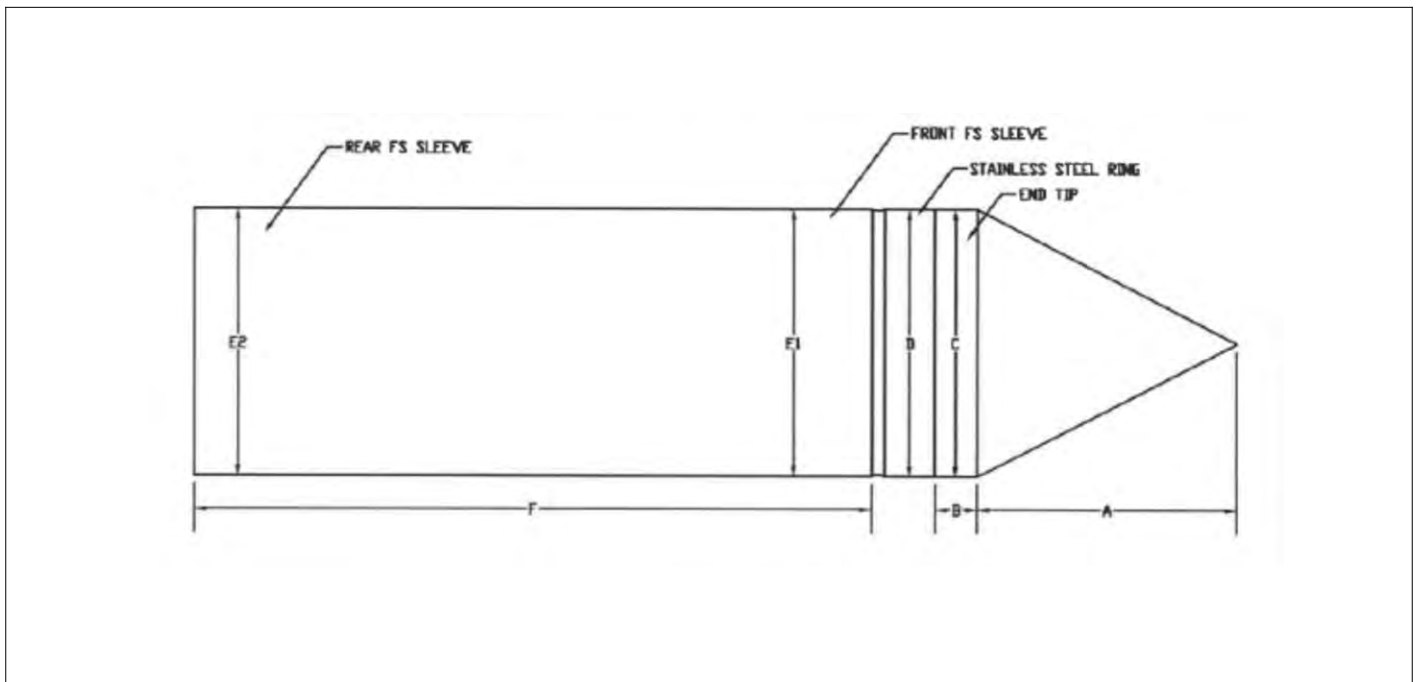
## Dimensions

Dimensional specifications are detailed below. All tolerances are routinely checked prior to testing and measurements taken are electronically recorded. All records are kept on file and available on request.

## Technical specifications

	Tip	Friction	Pore Pressure	Inclination
<b>Maximum Measuring Range:</b>	50 - 100 MPa	1.60 MPa	2.50 MPa	0° - 20°
<b>Resolution:</b>	24 bit	24 bit	24 bit	12 bit
<b>Accuracy:</b>	0.005 MPa	0.04 MPa	0.04 MPa	0.5°

<b>Length:</b>	320 mm	<b>Weight:</b>	1.8 kg
<b>Diameter:</b>	35.8 mm	<b>Opening angle of bit:</b>	60°
<b>Cone base area:</b>	10 cm <sup>2</sup>	<b>Side sleeve surfaces:</b>	150 cm <sup>2</sup>
<b>Cone area ratio:</b>	0.80	<b>Tip and Local Friction sensor displacement:</b>	80 mm



# CONE CERTIFICATES



## CONE CALIBRATION CERTIFICATE N° Z087/19

Calibrated system (Sistema tarato):  
 Serial number **Mkj328**  
 Sensor  
 Max. Capacity [MPa]: **100**  
 Scaling Factor: **195500**  
 Tip net area ratio ( $a_p$ ): **0,80**  
 Sleeve net ratio ( $b_p$ ): **0,00**

Addressee (destinatario):  
 LANDTEST  
 307 Cashel street, Christchurch  
 New Zealand

Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 200 kN  
 Serial Number 138913  
 Power press:  
 Manufacturer Easydur Italiana  
 Model Aura 20T  
 Serial Number 29084

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)

Last verification date: 15/01/2019  
 Certificate N. LAT 091 2019-014  
 Temperature of calibration 22°C  
 Humidity 53%

Factory calibration in accordance with ASTM D5778-13



## CONE CALIBRATION CERTIFICATE N° Z087/19

Calibrated system (Sistema tarato):  
 Serial number **Mkj328**  
 Sensor  
 Max. Capacity [kPa]: **1600**  
 Scaling Factor: **30696**

Addressee (destinatario):  
 LANDTEST  
 307 Cashel street, Christchurch  
 New Zealand

Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 50 kN  
 Serial Number 65495  
 Power press:  
 Manufacturer Easydur Italiana  
 Model Aura 10T  
 Serial Number 29002

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)

The adapted calibration procedure has been developed according to the suggestions given by Prof. Paul W. Mayne (Georges Institute of Technology) and Prof. Diego La Presti (University of Pisa)

Cone calibrated by **Cludio**

Date of issue 27/06/2019



## CONE CALIBRATION CERTIFICATE N° Z087/19

Calibrated system (Sistema tarato):  
 Serial number **Mkj328**  
 Sensor  
 Max. Capacity [kPa]: **2500**  
 Scaling Factor: **16963**

Addressee (destinatario):  
 LANDTEST  
 307 Cashel street, Christchurch  
 New Zealand

Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Pressure Generator:  
 Manufacturer AEP transducers  
 Model GPM500  
 Digital Indicator:  
 Manufacturer AEP transducers  
 Model LAB DMM  
 Serial Number 301796

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)

The adapted calibration procedure has been developed according to the suggestions given by Prof. Paul W. Mayne (Georges Institute of Technology) and Prof. Diego La Presti (University of Pisa)

Date of issue 27/06/2019

# CONE CERTIFICATES



## CONE CALIBRATION CERTIFICATE N° Z024/20

Calibrated system (Sistema tarato):  
 Serial number **Mks711**  
 Sensor  
 Max. Capacity [MPa]: **100**  
 Sealing Factor: **190780**  
 Tip net area ratio (a<sub>b</sub>): **0,79**  
 Sleeve net ratio (b<sub>s</sub>): **0,00**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 200 kN  
 Serial Number 138913  
 Power press: Easydur Italiana  
 Model Aura 20T  
 Serial Number 29084

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 Certificate N. LAT 091 2020-015  
 Temperature of calibration 22°C  
 Humidity 45%  
 Factory calibration in accordance with ASTM D5778-12



## CONE CALIBRATION CERTIFICATE N° Z024/20

Calibrated system (Sistema tarato):  
 Serial number **Mks711**  
 Sensor  
 Max. Capacity [kPa]: **1600**  
 Sealing Factor: **31343**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 50 kN  
 Serial Number 65495  
 Power press: Easydur Italiana  
 Model Aura 10T  
 Serial Number 29002

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 The adopted calibration procedure has been developed acc Prof. Paul W. Mayne (Georgia Institute of technology) and  
 Cone calibrated by



## CONE CALIBRATION CERTIFICATE N° Z024/20

Calibrated system (Sistema tarato):  
 Serial number **Mks711**  
 Sensor  
 Max. Capacity [kPa]: **2500**  
 Sealing Factor: **10298**  
 Sensor  
 Max. Inclination [°]: **20**  
 Sealing Factor: **280277**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Pressure Generator:  
 Manufacturer MENSOR  
 Model CPC 4000  
 Serial Number 41000V56  
 Sensor Descri Silicon Pressure Transducer  
 Sensor Serial Number 41000SYF

The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 28/02/2019  
 Certificate N. 162632  
 Temperature of calibration 22°C  
 Humidity 45%  
 Factory calibration in accordance with ASTM D5778-12

# **CONE PENETRATION TEST (CPT) REPORT**

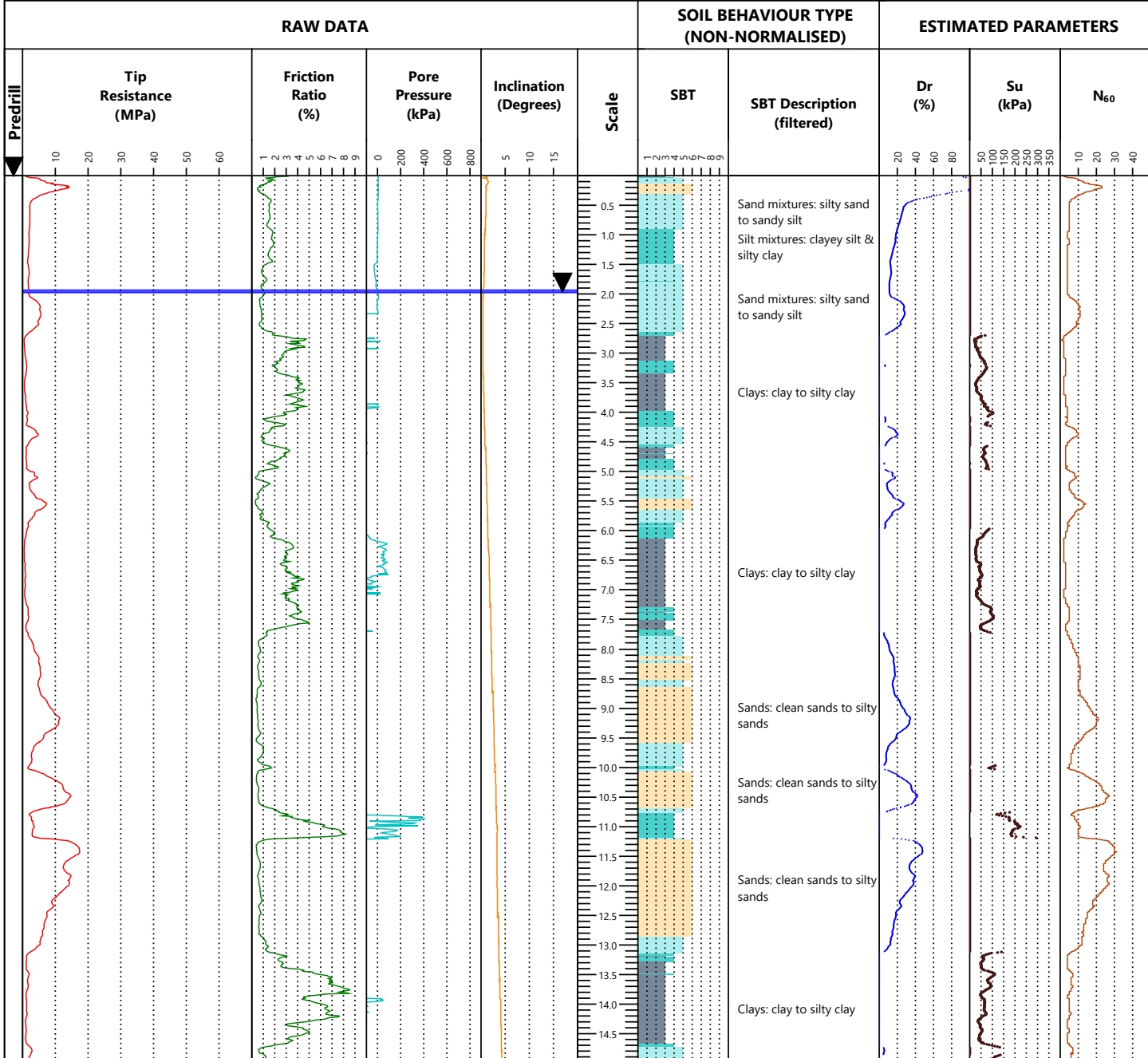


**Client: Miyamoto International NZ**

**Location: 2-4 Glovers Road, Christchurch**

**Printed: 29/09/2020**

**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 24/9/2020  
**Grid Reference:** 1564970.4m E, 5173158.32m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



EOH: 15m

<b>Cone Type:</b> Pagani Piezocone - Compression		<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>	
<b>Cone Reference:</b> MKJ329		<b>Water Level:</b> 1.96m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined	<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Cone Area Ratio:</b> 0.79		<b>Collapse:</b> 2.0m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained	<b>6</b> Sands: clean sands to silty sands
<b>Standards:</b> ISO 22476-1:2012			Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil	<b>7</b> Dense sand to gravelly sand
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	<b>After test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay	<b>8</b> Stiff sand to clayey sand
<b>Tip Resistance</b>	11.9412	11.8737	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay	<b>9</b> Stiff fine-grained
<b>Local Friction</b>	0.1606	0.161			
<b>Pore Pressure</b>	1.4594	1.262			

**Notes & Limitations**  
Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

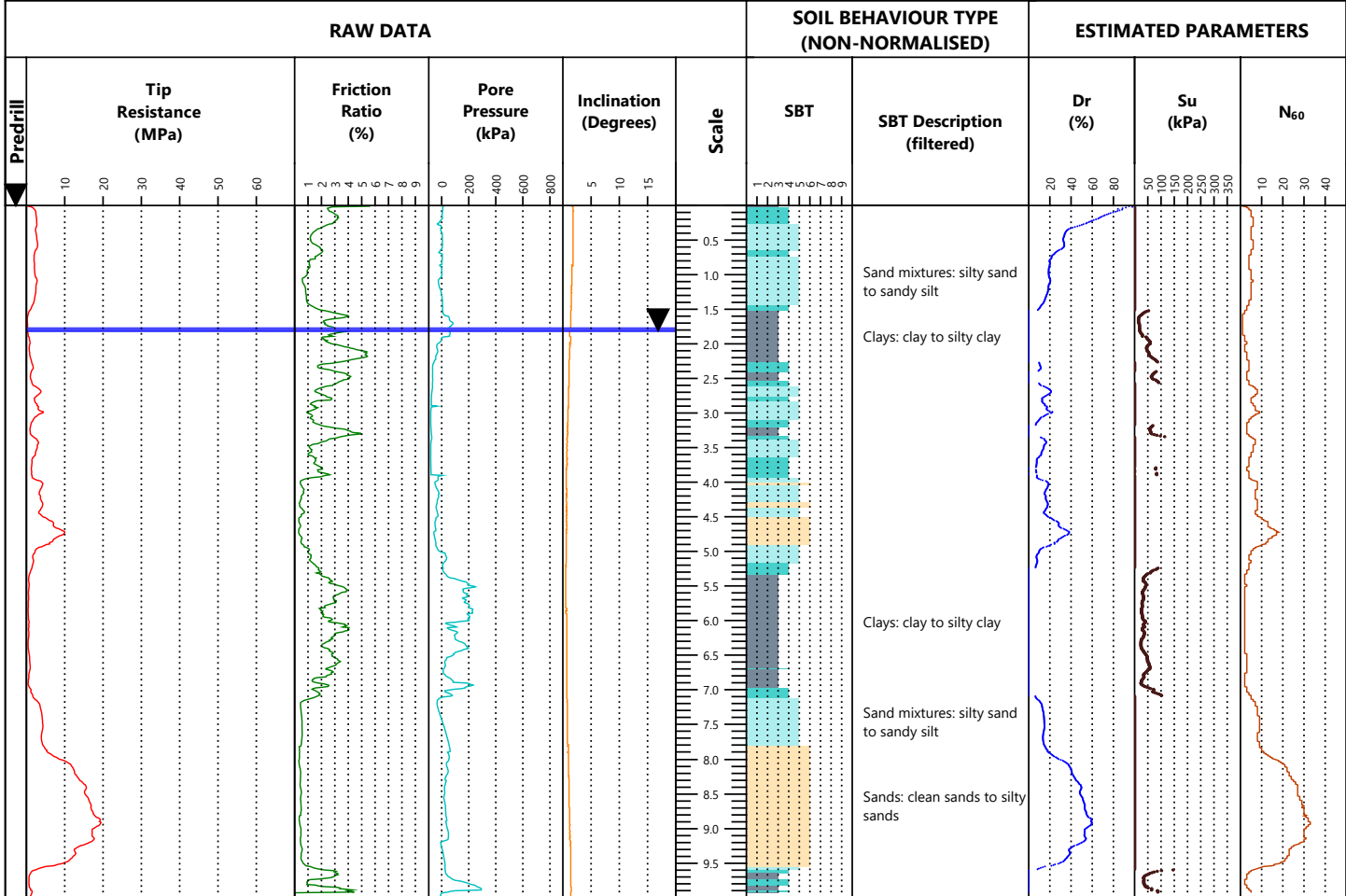
**Remarks**  
Invalid pore water pressure data from 2.33m.

Sheet 1 of 1



<b>Client:</b>	Miyamoto International NZ	<b>Bore No.:</b>	<b>CPTu008</b>
<b>Project:</b>	2-4 Glovers Road, Christchurch	<b>Job No.:</b>	<b>19096</b>

**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 24/9/2020  
**Grid Reference:** 1565034.78m E, 5173124.87m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



EOH: 10m

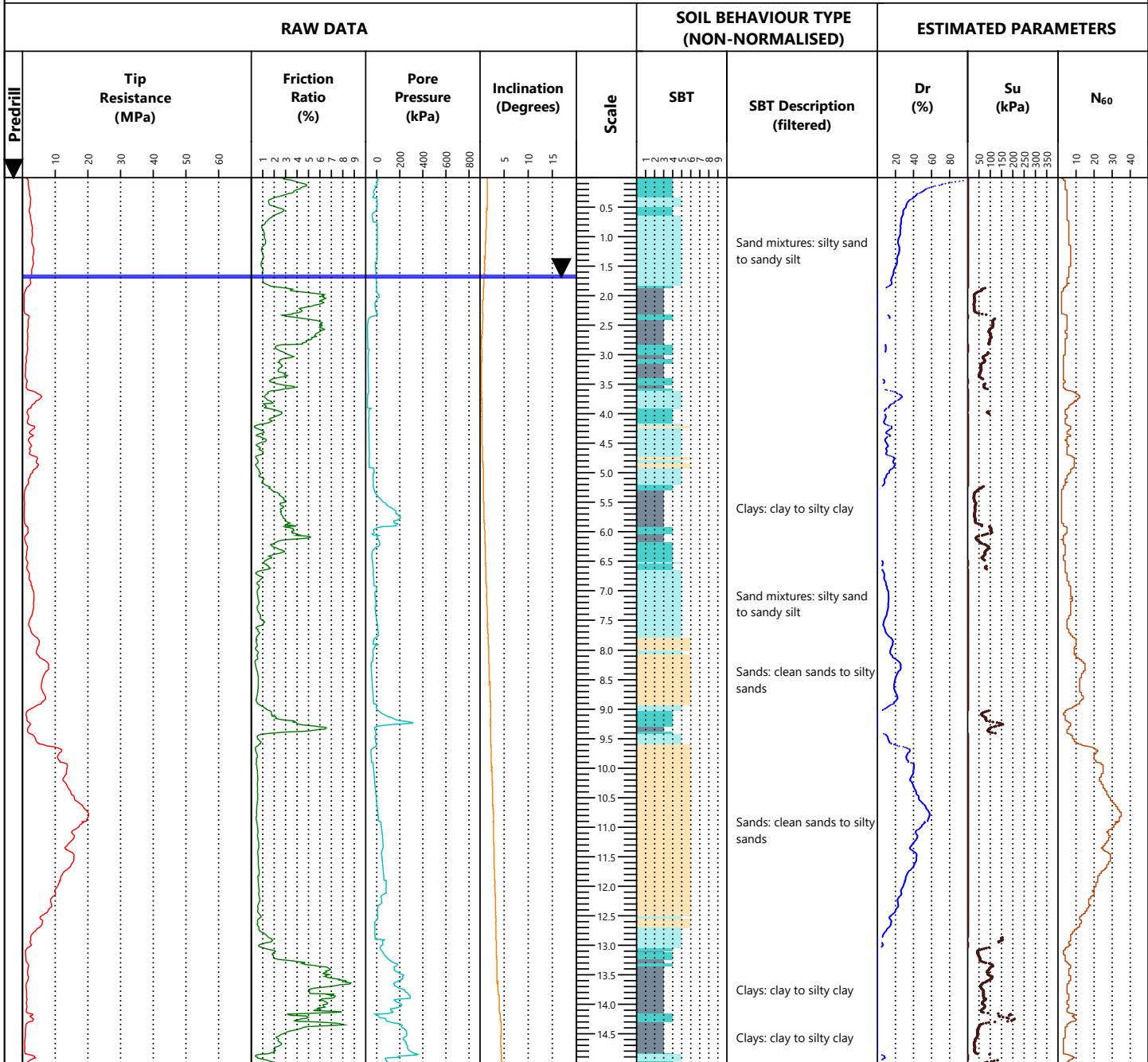
<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ329 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012	<b>Predrill:</b> - <b>Water Level:</b> 1.8m <b>Collapse:</b> 2.2m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> 0 Undefined 1 Sensitive fine-grained 2 Clay - organic soil 3 Clays: clay to silty clay 4 Silt mixtures: clayey silt & silty clay 5 Sand mixtures: silty sand to sandy silt 6 Sands: clean sands to silty sands 7 Dense sand to gravelly sand 8 Stiff sand to clayey sand 9 Stiff fine-grained
<b>Zero load outputs (MPa)</b> <b>Tip Resistance</b> 11.9516 <b>Local Friction</b> 0.1609 <b>Pore Pressure</b> 1.459	<b>Before test</b> 11.8425 0.1614 1.4561	<b>After test</b> 11.8425 0.1614 1.4561	<b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

Sheet 1 of 1

**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 24/9/2020  
**Grid Reference:** 1564969.64m E, 5173086.81m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



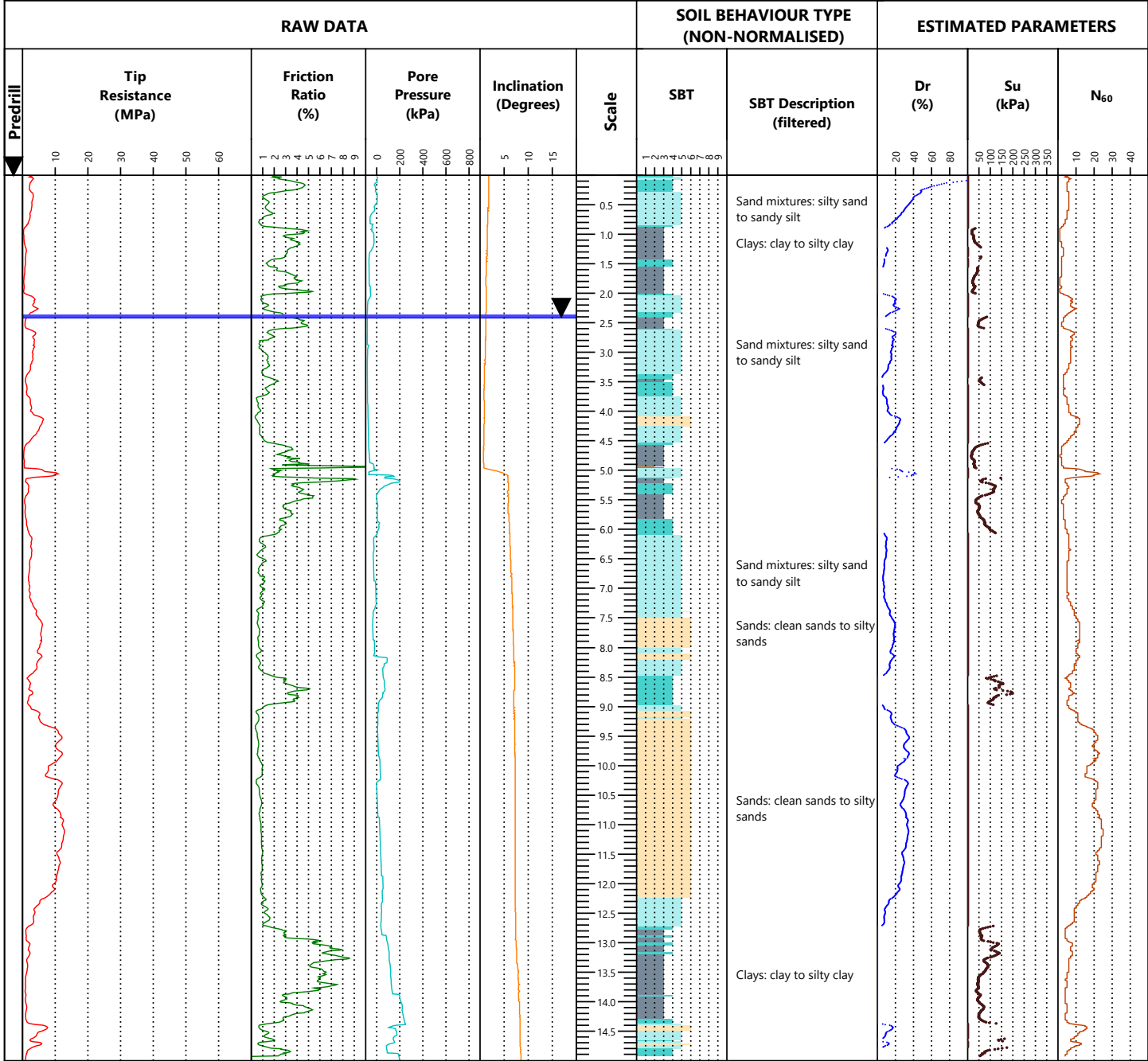
<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> -	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ329	<b>Water Level:</b> 1.68m	<b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>0</b> Undefined
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 1.80m	<b>Effective Refusal</b>	<b>1</b> Sensitive fine-grained
<b>Standards:</b> ISO 22476-1:2012		Tip: <input type="checkbox"/>	<b>2</b> Clay - organic soil
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	Gauge: <input type="checkbox"/>	<b>3</b> Clays: clay to silty clay
<b>Tip Resistance</b>	11.9464	Inclinometer: <input type="checkbox"/>	<b>4</b> Silt mixtures: clayey silt & silty clay
<b>Local Friction</b>	0.1604		<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Pore Pressure</b>	1.4592		<b>6</b> Sands: clean sands to silty sands
	1.4568		<b>7</b> Dense sand to gravelly sand
			<b>8</b> Stiff sand to clayey sand
			<b>9</b> Stiff fine-grained

**Notes & Limitations**  
 Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.

**Remarks**

Sheet 1 of 1

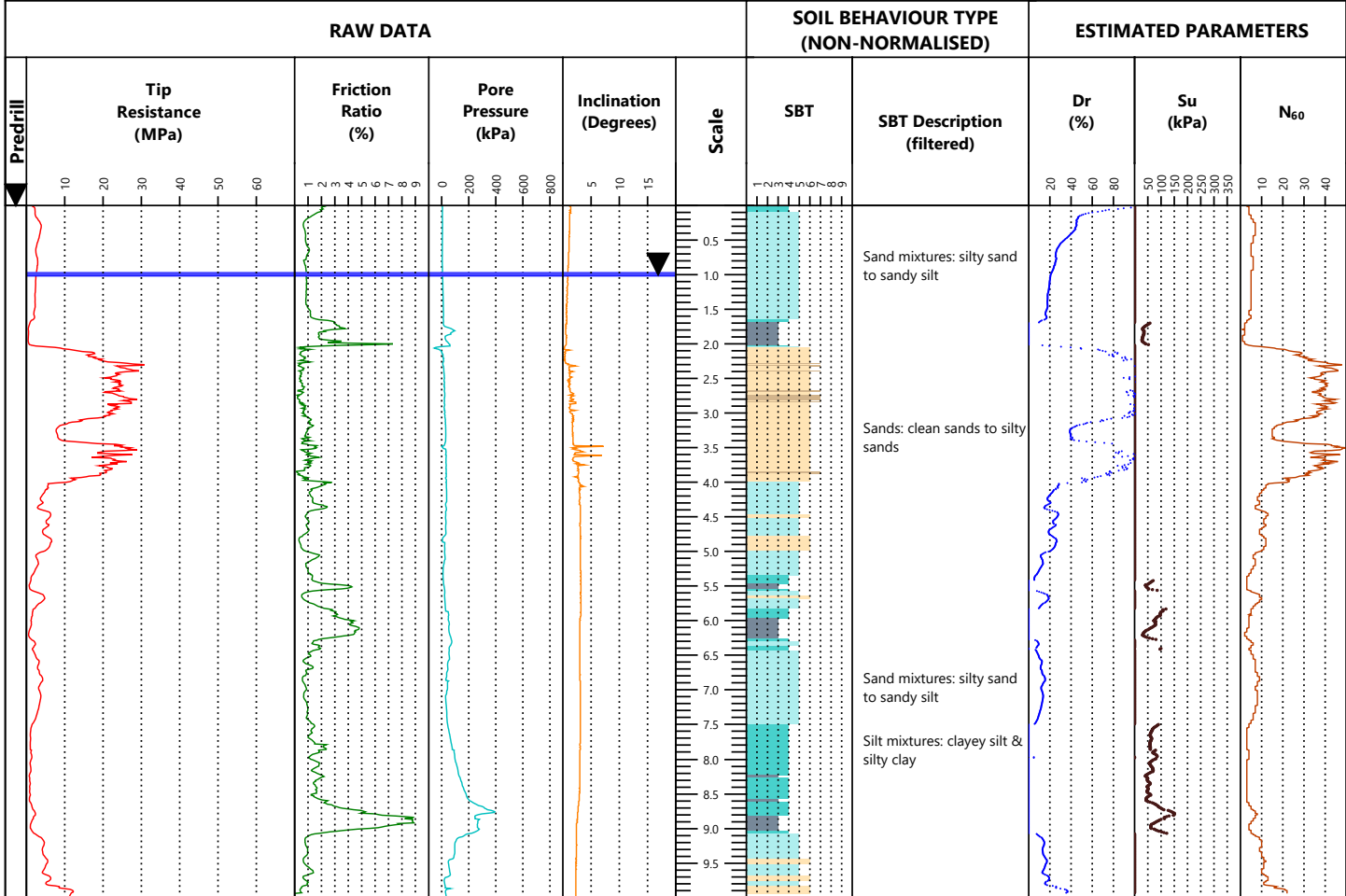
**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 25/9/2020  
**Grid Reference:** 1565043.16m E, 5173036.65m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150



<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ329 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012  <table border="1" style="width:100%; border-collapse: collapse;"> <thead> <tr> <th>Zero load outputs (MPa)</th> <th>Before test</th> <th>After test</th> </tr> </thead> <tbody> <tr> <td><b>Tip Resistance</b></td> <td>11.9568</td> <td>11.8166</td> </tr> <tr> <td><b>Local Friction</b></td> <td>0.1618</td> <td>0.1622</td> </tr> <tr> <td><b>Pore Pressure</b></td> <td>1.4599</td> <td>1.4582</td> </tr> </tbody> </table>	Zero load outputs (MPa)	Before test	After test	<b>Tip Resistance</b>	11.9568	11.8166	<b>Local Friction</b>	0.1618	0.1622	<b>Pore Pressure</b>	1.4599	1.4582	<b>Predrill:</b> - <b>Water Level:</b> 2.4m <b>Collapse:</b> 2.50m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <table border="1" style="width:100%; border-collapse: collapse;"> <tr> <td style="background-color: black; color: white;">0</td> <td>Undefined</td> <td style="background-color: #90EE90;">5</td> <td>Sand mixtures: silty sand to sandy silt</td> </tr> <tr> <td style="background-color: #FF0000;">1</td> <td>Sensitive fine-grained</td> <td style="background-color: #FFD700;">6</td> <td>Sands: clean sands to silty sands</td> </tr> <tr> <td style="background-color: #FF8C00;">2</td> <td>Clay - organic soil</td> <td style="background-color: #8B4513;">7</td> <td>Dense sand to gravelly sand</td> </tr> <tr> <td style="background-color: #4682B4;">3</td> <td>Clays: clay to silty clay</td> <td style="background-color: #808080;">8</td> <td>Stiff sand to clayey sand</td> </tr> <tr> <td style="background-color: #00CED1;">4</td> <td>Silt mixtures: clayey silt &amp; silty clay</td> <td style="background-color: #404040;">9</td> <td>Stiff fine-grained</td> </tr> </table>	0	Undefined	5	Sand mixtures: silty sand to sandy silt	1	Sensitive fine-grained	6	Sands: clean sands to silty sands	2	Clay - organic soil	7	Dense sand to gravelly sand	3	Clays: clay to silty clay	8	Stiff sand to clayey sand	4	Silt mixtures: clayey silt & silty clay	9	Stiff fine-grained
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<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>   <div style="text-align: right;">Sheet 1 of 1</div>
--	--

**Site Location:** 2-4 Glovers Road, Christchurch **Date:** 25/9/2020  
**Grid Reference:** 1565055.15m E, 5172937.04m N (NZTM) - Map or aerial photograph **Rig Operator:** E. Diaz  
**Elevation:** 0.00m **Datum:** Ground **Equipment:** Pagani TG63-150

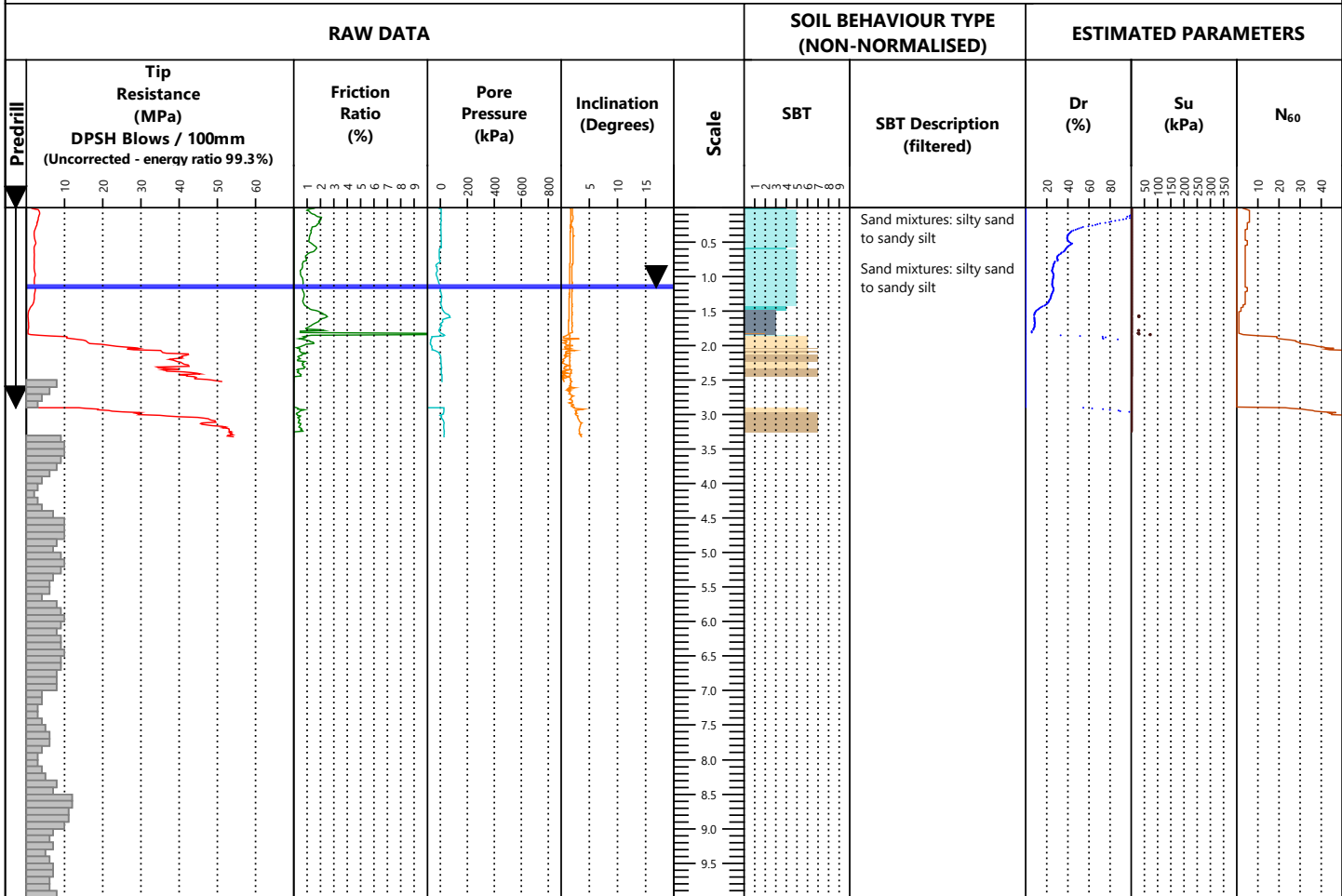


EOH: 10m

<b>Cone Type:</b> Pagani Piezocone - Compression <b>Cone Reference:</b> MKJ329 <b>Cone Area Ratio:</b> 0.79 <b>Standards:</b> ISO 22476-1:2012	<b>Predrill:</b> - <b>Water Level:</b> 1m <b>Collapse:</b> 5.1m	<b>Termination</b> <b>Target Depth:</b> <input checked="" type="checkbox"/>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b> <b>0</b> Undefined <b>1</b> Sensitive fine-grained <b>2</b> Clay - organic soil <b>3</b> Clays: clay to silty clay <b>4</b> Silt mixtures: clayey silt & silty clay <b>5</b> Sand mixtures: silty sand to sandy silt <b>6</b> Sands: clean sands to silty sands <b>7</b> Dense sand to gravelly sand <b>8</b> Stiff sand to clayey sand <b>9</b> Stiff fine-grained
<b>Zero load outputs (MPa)</b> <b>Tip Resistance</b> 11.9464 <b>Local Friction</b> 0.1615 <b>Pore Pressure</b> 1.4598	<b>Before test</b> 11.8166 0.1621 1.455	<b>After test</b> 11.8166 0.1621 1.455	<b>Effective Refusal</b> Tip: <input type="checkbox"/> Gauge: <input type="checkbox"/> Inclinator: <input type="checkbox"/>

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>  Sheet 1 of 1
--	------------------------------------

<b>Site Location:</b> 2-4 Glovers Road, Christchurch	<b>Date:</b> 29/9/2020
<b>Grid Reference:</b> 1565058.83m E, 5172852.91m N (NZTM) - Map or aerial photograph	<b>Rig Operator:</b> E. Diaz
<b>Elevation:</b> 0.00m	<b>Datum:</b> Ground
	<b>Equipment:</b> Pagani TG63-150



EOH: 10m

<b>Cone Type:</b> Pagani Piezocone - Compression	<b>Predrill:</b> 2.9m	<b>Termination</b>	<b>Soil Behaviour Type (SBT) - Robertson et al. 1986</b>
<b>Cone Reference:</b> MKJ329	<b>Water Level:</b> 1.15m	<b>Target Depth:</b> <input type="checkbox"/>	<b>5</b> Sand mixtures: silty sand to sandy silt
<b>Cone Area Ratio:</b> 0.79	<b>Collapse:</b> 2.2m	<b>Effective Refusal</b>	<b>6</b> Sands: clean sands to silty sands
<b>Standards:</b> ISO 22476-1:2012		Tip: <input checked="" type="checkbox"/>	<b>7</b> Dense sand to gravelly sand
<b>Zero load outputs (MPa)</b>	<b>Before test</b>	<b>After test</b>	<b>8</b> Stiff sand to clayey sand
<b>Tip Resistance</b>	11.8737	11.8321	<b>9</b> Stiff fine-grained
<b>Local Friction</b>	0.1612	0.1611	
<b>Pore Pressure</b>	1.4542	1.4556	
		Gauge: <input type="checkbox"/>	
		Inclinometer: <input type="checkbox"/>	

<b>Notes &amp; Limitations</b> Data shown on this report has been assessed to provide a basic interpretation in terms of Soil Behaviour Type (SBT) and various geotechnical soil and design parameters using methods published in P. K. Robertson and K.L. Cabal (2010), Guide to Cone Penetration Testing for Geotechnical Engineering, 4th Edition. The interpretations are presented only as a guide for geotechnical use, and should be carefully reviewed by the user. No warranty is provided as to the correctness or the applicability of any of the geotechnical soil and design parameters shown and does not assume any liability for any use of the results in any design or review. The user should be fully aware of the techniques and limitations of any method used to derive data shown in this report.	<b>Remarks</b>
	Sheet 1 of 1

## TEST DETAIL

PointID: CPTu007

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9412	11.8737
Local Friction	0.1606	0.161
Pore Pressure	1.4594	1.262

Date: 24/9/2020

Predrill: -

Water Level: 1.96m

Collapse: 2.0m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu008

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9516	11.8425
Local Friction	0.1609	0.1614
Pore Pressure	1.459	1.4561

Date: 24/9/2020

Predrill: -

Water Level: 1.8m

Collapse: 2.2m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu009

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9464	11.801
Local Friction	0.1604	0.1611
Pore Pressure	1.4592	1.4568

Date: 24/9/2020

Predrill: -

Water Level: 1.68m

Collapse: 1.80m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu010

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9568	11.8166
Local Friction	0.1618	0.1622
Pore Pressure	1.4599	1.4582

Date: 25/9/2020

Predrill: -

Water Level: 2.4m

Collapse: 2.50m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

PointID: CPTu011

Sounding: 1

Operator: E. Diaz

Cone Type: Pagani Piezocone - Compression

Cone Reference: MKJ329

Cone Area Ratio: 0.79

Zero load outputs (MPa)	Before test	After test
Tip Resistance	11.9464	11.8166
Local Friction	0.1615	0.1621
Pore Pressure	1.4598	1.455

Date: 25/9/2020

Predrill: -

Water Level: 1m

Collapse: 5.1m

Termination

Target Depth:

Effective Refusal

Tip:

Gauge:

Inclinometer:

## TEST DETAIL

---

PointID: CPTu012

Sounding: 1

**Operator:** E. Diaz

**Cone Type:** Pagani Piezocone - Compression

**Cone Reference:** MKJ329

**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.9568	11.8062
<b>Local Friction</b>	0.1607	0.1609
<b>Pore Pressure</b>	1.4567	1.4562

**Date:** 29/9/2020

**Predrill:** -

**Water Level:** -

**Collapse:** -

**Termination**

**Target Depth:**

**Effective Refusal**

Tip:

Gauge:

Inclinometer:

Sounding: 2

**Operator:** E. Diaz

**Cone Type:** Pagani Piezocone - Compression

**Cone Reference:** MKJ329

**Cone Area Ratio:** 0.79

Zero load outputs (MPa)	Before test	After test
<b>Tip Resistance</b>	11.8737	11.8321
<b>Local Friction</b>	0.1612	0.1611
<b>Pore Pressure</b>	1.4542	1.4556

**Date:** 29/9/2020

**Predrill:** 2.9m

**Water Level:** 1.15m

**Collapse:** 2.2m

**Termination**

**Target Depth:**

**Effective Refusal**

Tip:

Gauge:

Inclinometer:

# CPT CALIBRATION AND TECHNICAL NOTES

These notes describe the technical specifications and associated calibration references pertaining to the Pagani piezocone types measuring cone resistance, sleeve friction, inclination and pore pressure (piezocone, 10cm<sup>2</sup>)

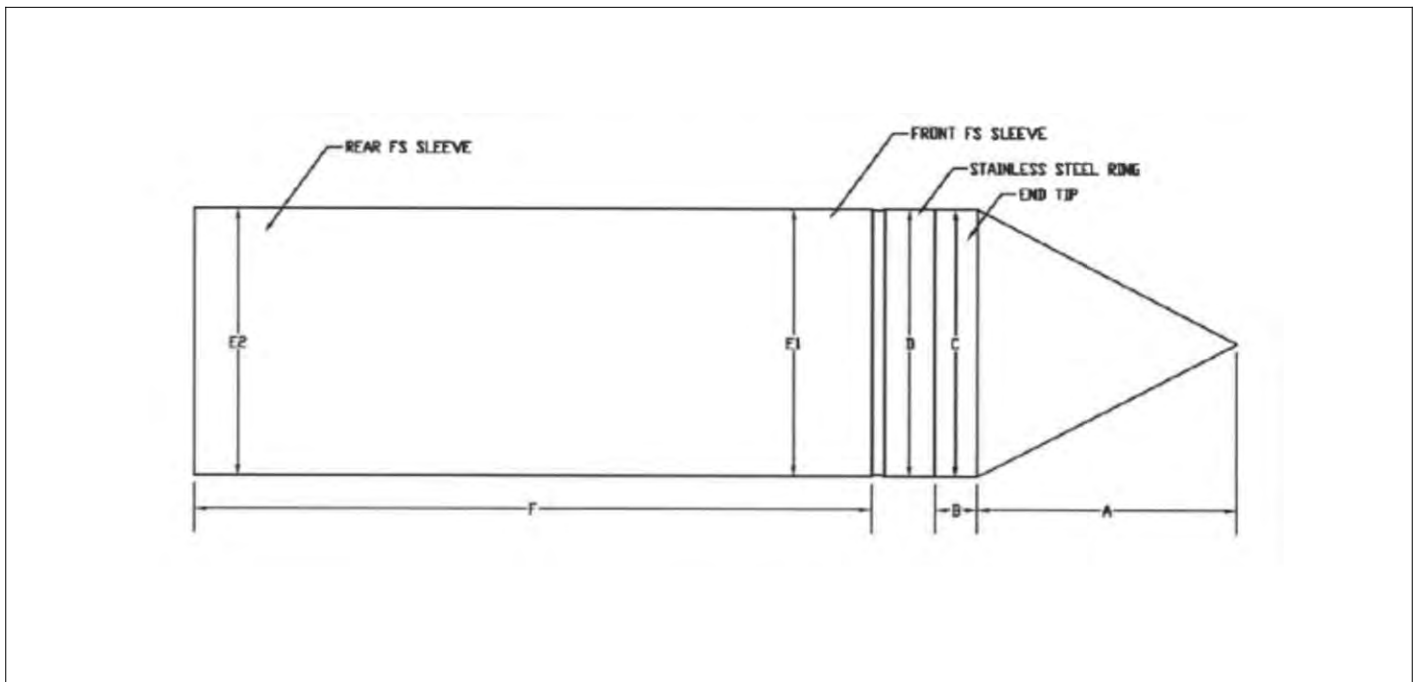
## Dimensions

Dimensional specifications are detailed below. All tolerances are routinely checked prior to testing and measurements taken are electronically recorded. All records are kept on file and available on request.

## Technical specifications

	Tip	Friction	Pore Pressure	Inclination
<b>Maximum Measuring Range:</b>	50 - 100 MPa	1.60 MPa	2.50 MPa	0° - 20°
<b>Resolution:</b>	24 bit	24 bit	24 bit	12 bit
<b>Accuracy:</b>	0.005 MPa	0.04 MPa	0.04 MPa	0.5°

<b>Length:</b>	320 mm	<b>Weight:</b>	1.8 kg
<b>Diameter:</b>	35.8 mm	<b>Opening angle of bit:</b>	60°
<b>Cone base area:</b>	10 cm <sup>2</sup>	<b>Side sleeve surfaces:</b>	150 cm <sup>2</sup>
<b>Cone area ratio:</b>	0.80	<b>Tip and Local Friction sensor displacement:</b>	80 mm







**CONE CALIBRATION CERTIFICATE**  
N° Z023/20

Calibrated system (Sistema tarato):  
 Serial number **Mkj329**  
 Sensor **TIP RESISTANCE**  
 Max. Capacity [MPa]: **100**  
 Scaling Factor: **192610**  
 Tip net area ratio ( $a_t$ ): **0,79**  
 Sleeve net ratio ( $b_s$ ): **0,00**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 200 KN  
 Serial Number 138913  
 Power press: Easydur Italiana  
 Model Aura 20T  
 Serial Number 29084  
 The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 Certificate N. LAT 091 2020-015  
 Temperature of calibration 22°C  
 Humidity 45%  
 Factory calibration in accordance with ASTM D5778-12



**CONE CALIBRATION CERTIFICATE**  
N° Z023/20

Calibrated system (Sistema tarato):  
 Serial number **Mkj329**  
 Sensor **SLEEVE FRICTION**  
 Max. Capacity [kPa]: **1600**  
 Scaling Factor: **30794**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Load cell:  
 Manufacturer AEP transducers  
 Model KAL 50 kN  
 Serial Number 65495  
 Power press: Easydur Italiana  
 Model Aura 10T  
 Serial Number 29002  
 The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 16/01/2020  
 The adopted calibration procedure has been developed according to the suggestions given by Prof. Paul W. Mayne (Georgia Institute of Technology) and Prof. Diego Lo Presti (University of Pisa)

*PLS*



**CONE CALIBRATION CERTIFICATE**  
N° Z023/20

Calibrated system (Sistema tarato):  
 Serial number **Mkj329**  
 Sensor **PORE PRESSURE**  
 Max. Capacity [kPa]: **2500**  
 Scaling Factor: **10657**  
 Sensor **TILT ANGLE**  
 Max. Inclination [°]: **20**  
 Scaling Factor: **151152**

Addressee (destinatario):  
 McMillan Drilling Ltd  
 36 Hickory Place, Islington  
 Christchurch 8042, New Zealand  
 Applied load measurement system:  
 (Sistema di rilevamento del carico applicato)

Pressure Generator:  
 Manufacturer MENSOR  
 Model CPC 4000  
 Serial Number 41000V56  
 Sensor Descr Silicon Pressure Transducer  
 Sensor Serial Number 41000SYF  
 The measurement system is periodically checked in a SIT calibration center. (Il sistema di rilevamento è sottoposto a verifica periodica presso un centro SIT)  
 Last verification date: 28/02/2019

Date of issue 05/02/2020

## D. Southern Geophysical MASW and GPR Report



October 2020

# Geophysical Site Investigation:

2-4 Glovers Road, Christchurch

Report prepared for Miyamoto International NZ Ltd

# GEOPHYSICAL REPORT



**Southern**  
**Geophysical**

3/28 Tanya St, Bromley, Christchurch 8062

Ph: 03 384 4302

Web: [www.southerngeophysical.com](http://www.southerngeophysical.com)

Data collected and report prepared for Southern Geophysical Ltd by:

Christian Ruegg, MSc, Geophysicist

Nick McConachie, BSc, Geologist

Report internally reviewed for Southern Geophysical by:

Mike Finnemore, PhD, Senior Geophysicist

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Results: .....	3
Conclusions:.....	3
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SGL Reference: 2050

Report Version 1



## **Summary:**

Southern Geophysical Ltd was contracted to undertake a geophysical survey using Multi-channel Analysis of Surface Waves (MASW) at 2-4 Glovers Road, Christchurch. The geophysical survey was conducted on September 24<sup>th</sup>, 2020 and includes three MASW lines (Figure 1). The aim of the survey was to assess the shear-wave velocities and structure of the subsurface to a depth of over 20 m. The MASW results show low shear-wave velocities to a depth of 10 m in the northern part of the site (100 m/s to 150 m/s), with higher velocities to the south (100 m/s to 300 m/s). The boundary between these two zones is a feature characteristic of the edge of a paleochannel, buried valley, or dipping volcanic strata, crossing the site east to west and dipping to the north. It is possible that high velocities imaged by the MASW survey to the south (>500 m/s from approximately 20 m depth) are associated with volcanic rock, but there are no boreholes available for ground truthing to that depth.

## **Methodology:**

MASW is a geophysical technique that uses the dispersive nature of surface waves to model shear-wave velocity versus depth.

A MASW survey is undertaken as a series of lines or points across the surface of the site. The MASW points in this survey were collected using a 24-channel towed seismic array, with 4.5 Hz geophones. The geophone spacing was 1 m and the source offset was 10 m. The seismic source was a 16 lb sledgehammer impacting an aluminium plate. Recording parameters for the MASW survey were set with a 0.125 ms sample interval, 1.5 s record length, 24 dB gains, and a geophone trigger system.

The field records were processed using the Kansas Geological Survey software package SurfSeis6++ ©. The geometry for each point was set according to the survey parameters and the dispersion curves were generated and edited. The inversions were run using a 10 layer variable depth model. The velocity data was interpolated into 2D profiles showing  $V_s$  variations with depth (Figures 2 to 3). The output shear-wave velocity data is included as data files (CSV format), supplementary to this report.

Supplementary to the MASW profiles, a series of Ground Penetrating Radar lines were acquired with a GSSI 200 MHz antenna (Figure 1). The radargrams are included in (Figures 4 and 5).

Survey positions were recorded using a Geo 7X Trimble GNSS system with a Tornado antenna. The GNSS positions were differentially corrected using a local GeoNet base station. The GNSS points were output in NZTM2000, with heights in Mean Sea Level (MSL). The accuracy of the survey positions is +/- 0.1 m. The site had no significant topographic changes, and the lines have not been corrected for elevation.

### **Results:**

A total of three MASW lines were acquired at the site with a total MASW survey length of approximately 1 km (Figure 1). The ground surface was well compacted farm tracks and farm yards. A series of GPR lines were acquired along each MASW line to provide a high resolution image of the substrate (Figures 4 and 5).

In homogenous soils, with gradually increasing shear-wave velocities and no sharp lateral discontinuities, the accuracy of the shear-wave velocities derived from the MASW processing is considered to be +/- 10%.<sup>1</sup> The quality of the seismic data and the dispersion curves used in this report is very good, with a good signal-to-noise ratio. If there is a velocity inversion present in the shear-wave profile (decreasing velocity with depth), the shear-wave velocity of the reduced velocity zone and the thickness of that zone can often be underestimated by the inversion process.

### **Conclusions:**

The MASW survey was considered to be of good quality, with modelled shear-wave velocities accurate to +/- 10%. The velocities in the top 5 m are likely to be more accurate than the deeper velocities, due to the presence of multiple velocity inversions. The MASW survey indicates a horizontal layer defined by a sharp increase in shear-wave velocity (180 m/s to 220 m/s) at around 5 m depth in the southern part of the site, consistent with the surface of dense gravels or sands. In the northern part of the site a similar 180 m/s to 220 m/s surface was observed at 20 m depth. There is a well-defined dipping surface dividing the south and the north, possibly associated with a buried valley edge, paleochannel, or

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<sup>1</sup> Stephenson, W.J., Louie, J.N., Pullammanappallil, S., Williams, R.A., and Odum, J.K. 2005. Blind Shear-wave Velocity Comparison of ReMi and MASW Results with Boreholes to 200 m in Santa Clara Valley: Implications for Earthquake Ground-Motion Assessment. *Bulletin of the Seismological Society of America*, Vol. 95, pp. 2506-2516.

bedrock interface. This edge feature is apparent in both MASW 1 and MASW 3, as well as GPR 4 and GPR 10.

While the limitations of the MASW method should be considered when evaluating these results, the quality of the data collected at the site and the confidence in the shear-wave velocities derived from the MASW data is good.

**Disclaimer:**

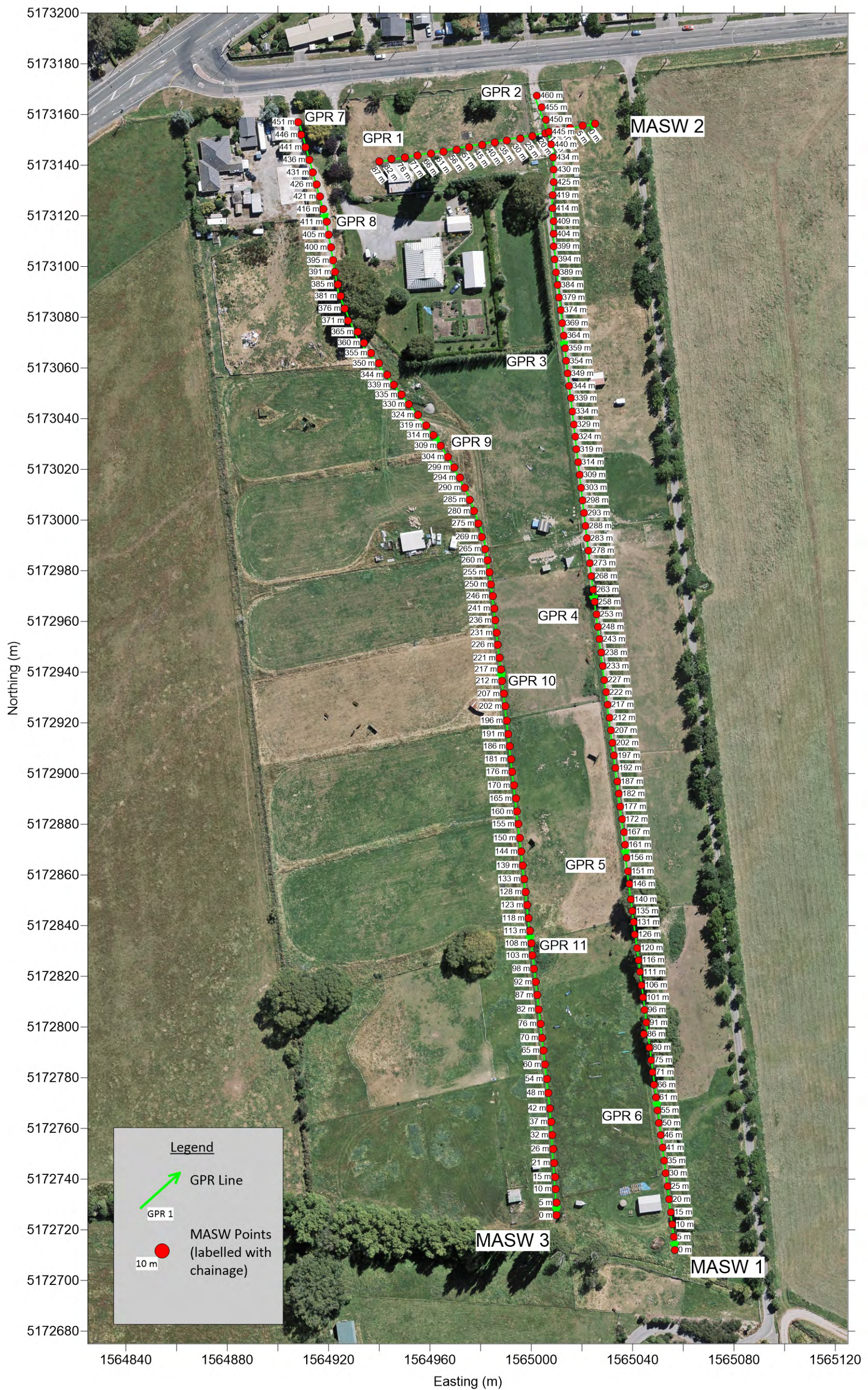
This document has been provided by Southern Geophysical Ltd subject to the following:

Non-invasive geophysical testing has limitations and is not a complete source of testing. Often there is a need to couple non-invasive methods with invasive testing methods, such as drilling, especially in cases where the non-invasive testing indicates anomalies.

This document has been prepared for the particular purpose outlined in the project proposal and no responsibility is accepted for the use of this document, in whole or in part, in other contexts or for any other purpose. Southern Geophysical Ltd did not perform a complete assessment of all possible conditions or circumstances that may exist at the site. Conditions may exist which were undetectable given the limited nature of the enquiry Southern Geophysical Ltd was retained to undertake with respect to the site. Variations in conditions often occur between investigatory locations, and there may be special conditions pertaining to the site which have not been revealed by the investigation and which have not therefore been taken into account. Accordingly, additional studies and actions may be required by the client.

We collected our data and based our report on information which was collected at a specific point in time. The passage of time affects the information and assessment provided by Southern Geophysical Ltd. It is understood that the services provided allowed Southern Geophysical Ltd to form no more than an opinion of the actual conditions of the site at the time the site was visited and cannot be used to assess the effect of any subsequent changes for whatever reason. Where data is supplied by the client or other sources, including where previous site investigation data have been used, it has been assumed that the information is correct. No responsibility is accepted by Southern Geophysical Ltd for incomplete or inaccurate data supplied by others. This document is provided for sole use by the client and is confidential to that client and its professional advisers. No responsibility whatsoever for the contents of this document will be accepted to any person other than the client. Any use which a third party makes of this document, or any reliance on or decisions to be made based on it, is the responsibility of such third parties. Southern Geophysical Ltd accepts no responsibility for damages, if any, suffered by any third party as a result of decisions made or actions based on this document.

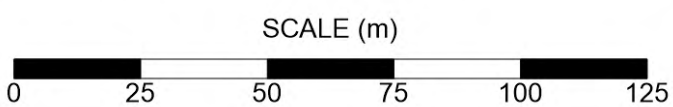




**Figure 1: Site Map**

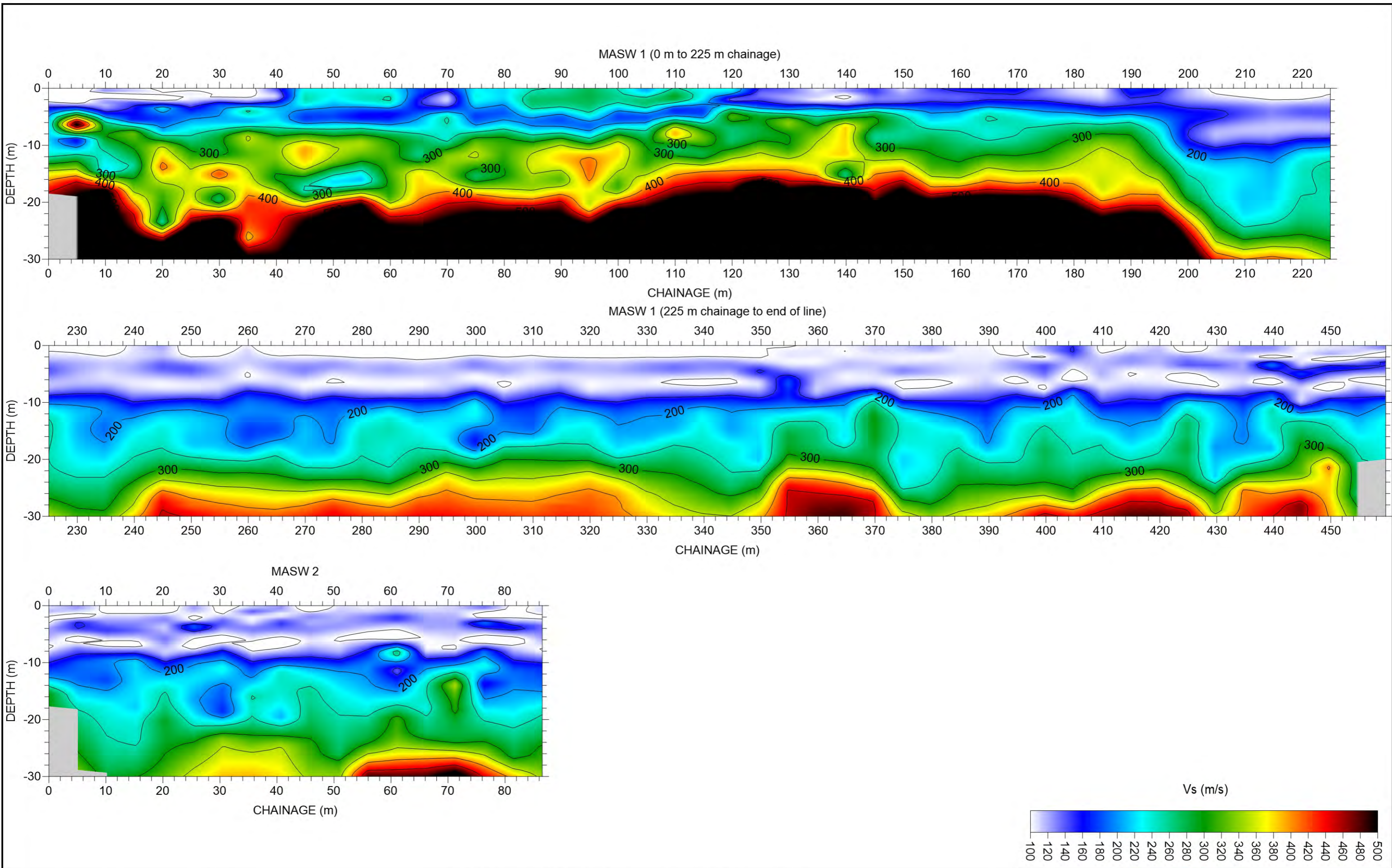
**2-4 Glovers Road, Christchurch**

Coordinates NZ2000 TM Grid.  
 NOTES- Aerial photograph sourced from LINZ, Crown Copyright ©



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DRAWING- **Figure 2: MASW 1 and 2**

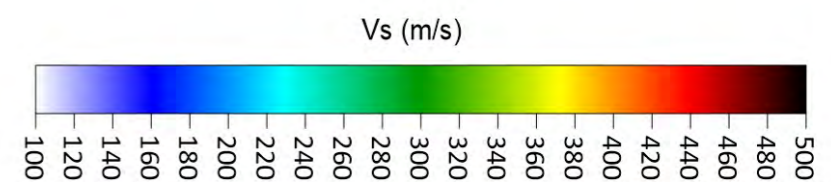
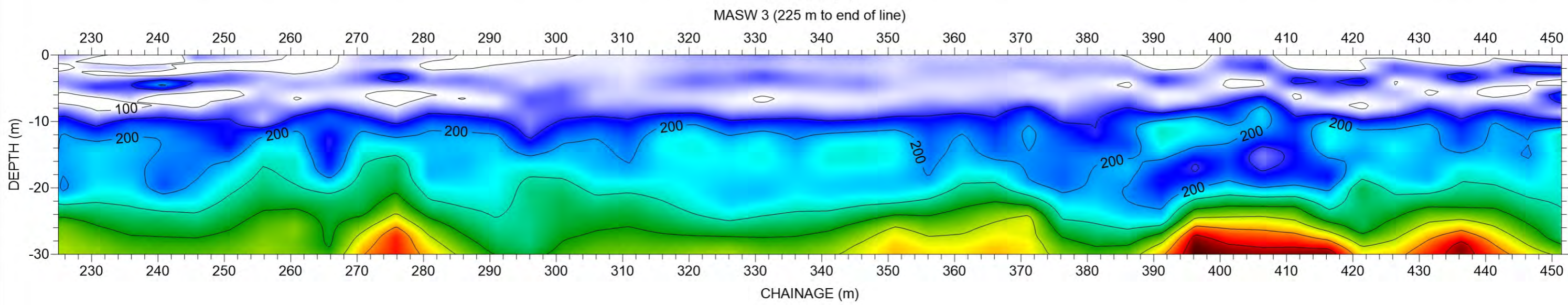
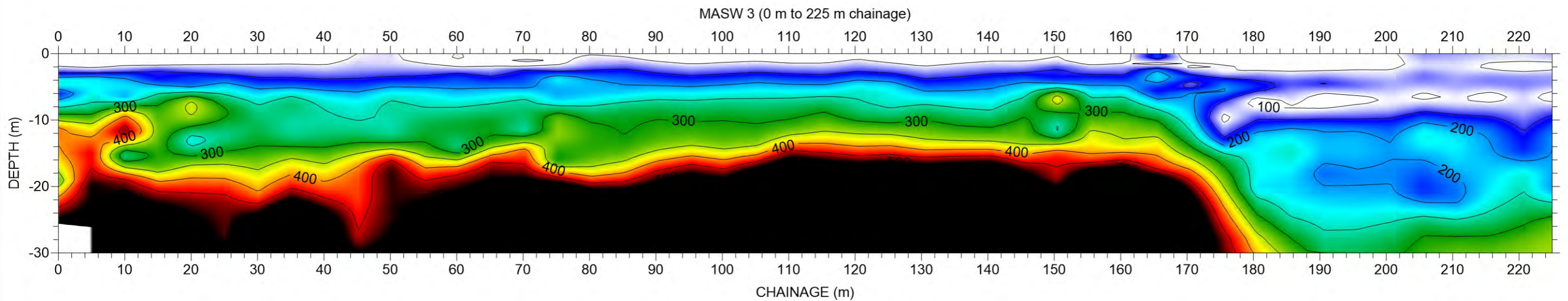
LOCATION- **2-4 Glovers Road, Christchurch**

NOTES MASW Vs profile has contour intervals of 50 m/s (Vs).

See site map for location of points.

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DRAWING- **Figure 3: MASW 3**

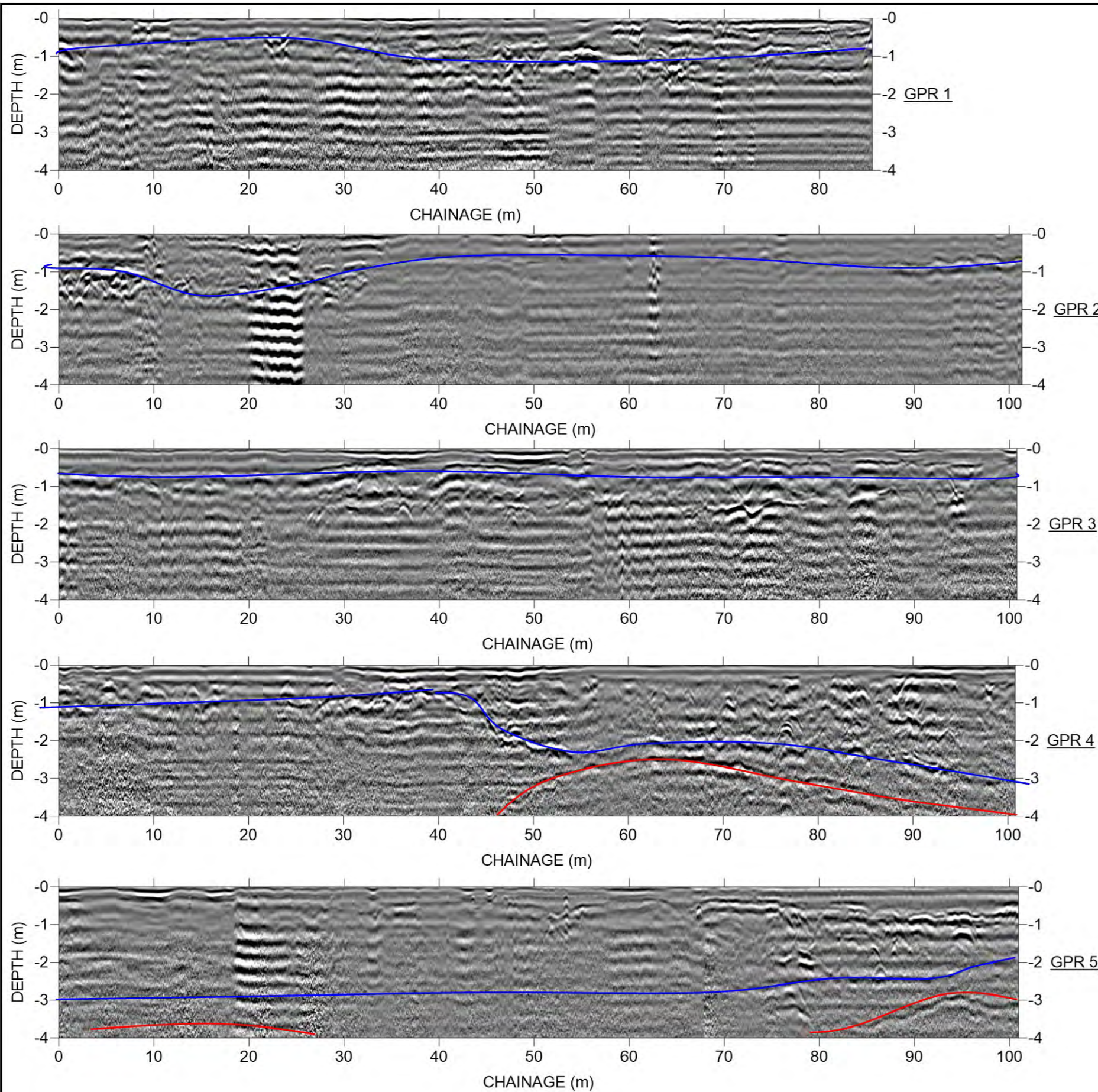
LOCATION- **2-4 Glover Street, Christchurch**

NOTES MASW Vs profile has contour intervals of 50 m/s (Vs).

See site map for location of points.

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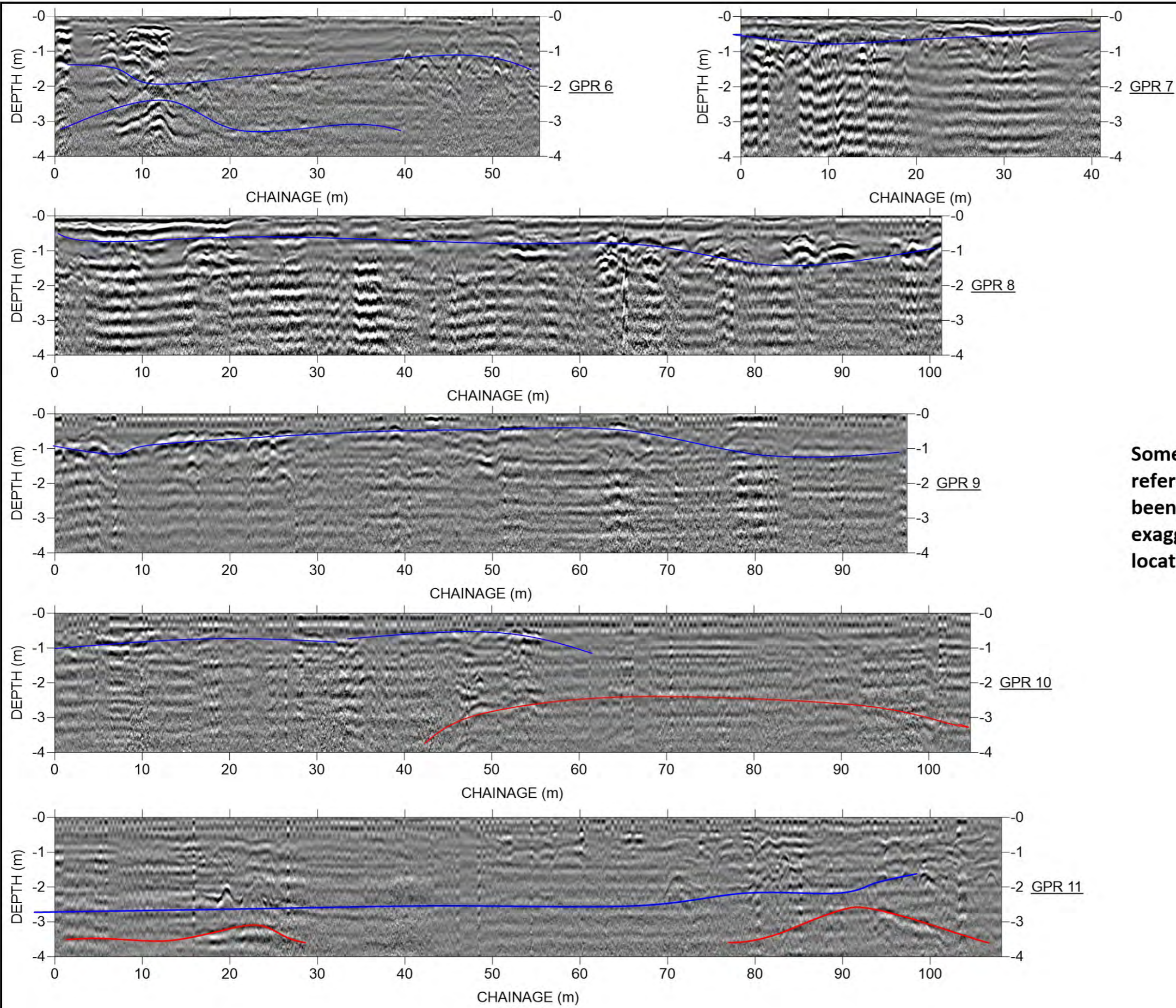


Some reflectors are annotated for reference. Note the profiles have been plotted with a 4:1 vertical exaggeration. See site map for line locations.

DRAWING- **Figure 4: GPR Radargrams 1 to 5**

LOCATION- **2-4 Glover Street, Christchurch**

NOTES



Some reflectors are annotated for reference. Note the profiles have been plotted with a 4:1 vertical exaggeration. See site map for line locations.

DRAWING- **Figure 5: GPR Radargrams 6 to 11**

LOCATION- **2-4 Glover Street, Christchurch**

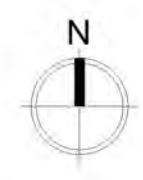
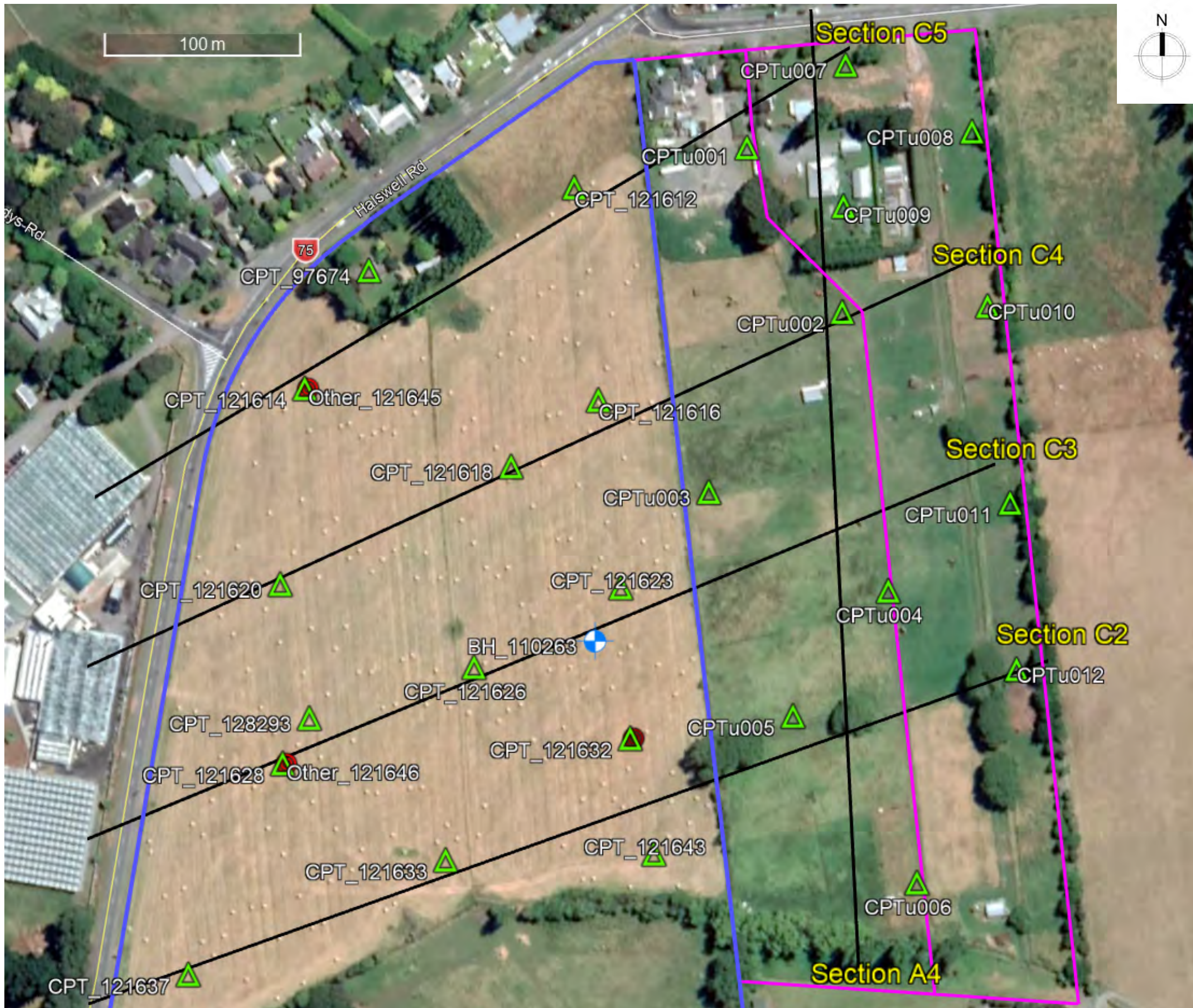
NOTES

## E. Geotechnical Cross Sections



## PROJECT No: 200357 GEOTECHNICAL CROSS SECTIONS FOR 2&4 GLOVERS ROAD, HALSWELL, CHRISTCHURCH 8025

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SHEET N°	SHEET NAME	REV.
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S2.1	GEOTECHNICAL CROSS-SECTION 1	1
S2.2	GEOTECHNICAL CROSS-SECTION 2	1
S2.3	GEOTECHNICAL CROSS-SECTION 3	1



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**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**

REVISION HISTORY		
REV	DATE	DESCRIPTION
1	19/10/20	FINAL

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PROJECT No.:	200357
VERSION DATE:	16/10/2020
DRAWN:	CG
ENGINEER:	CG
APPROVED:	AG

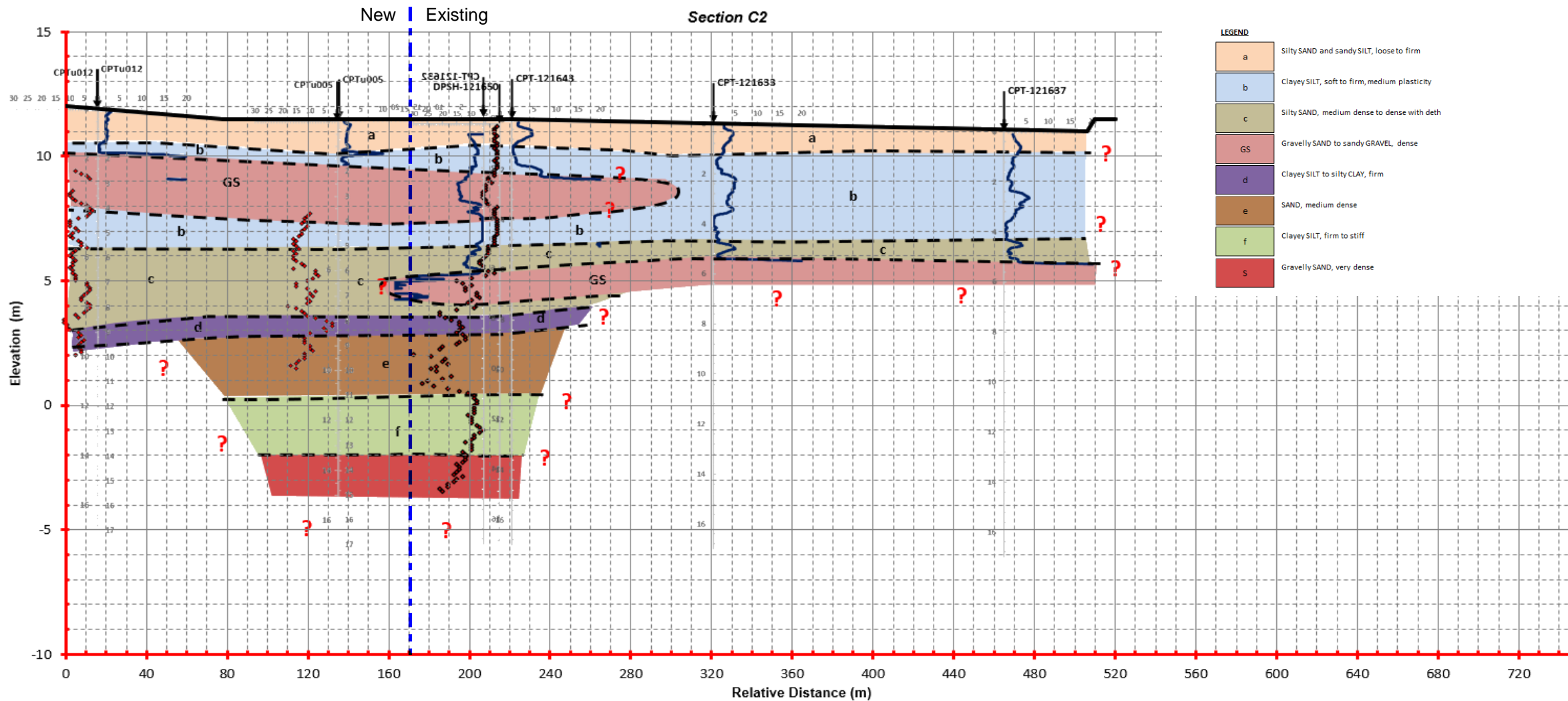
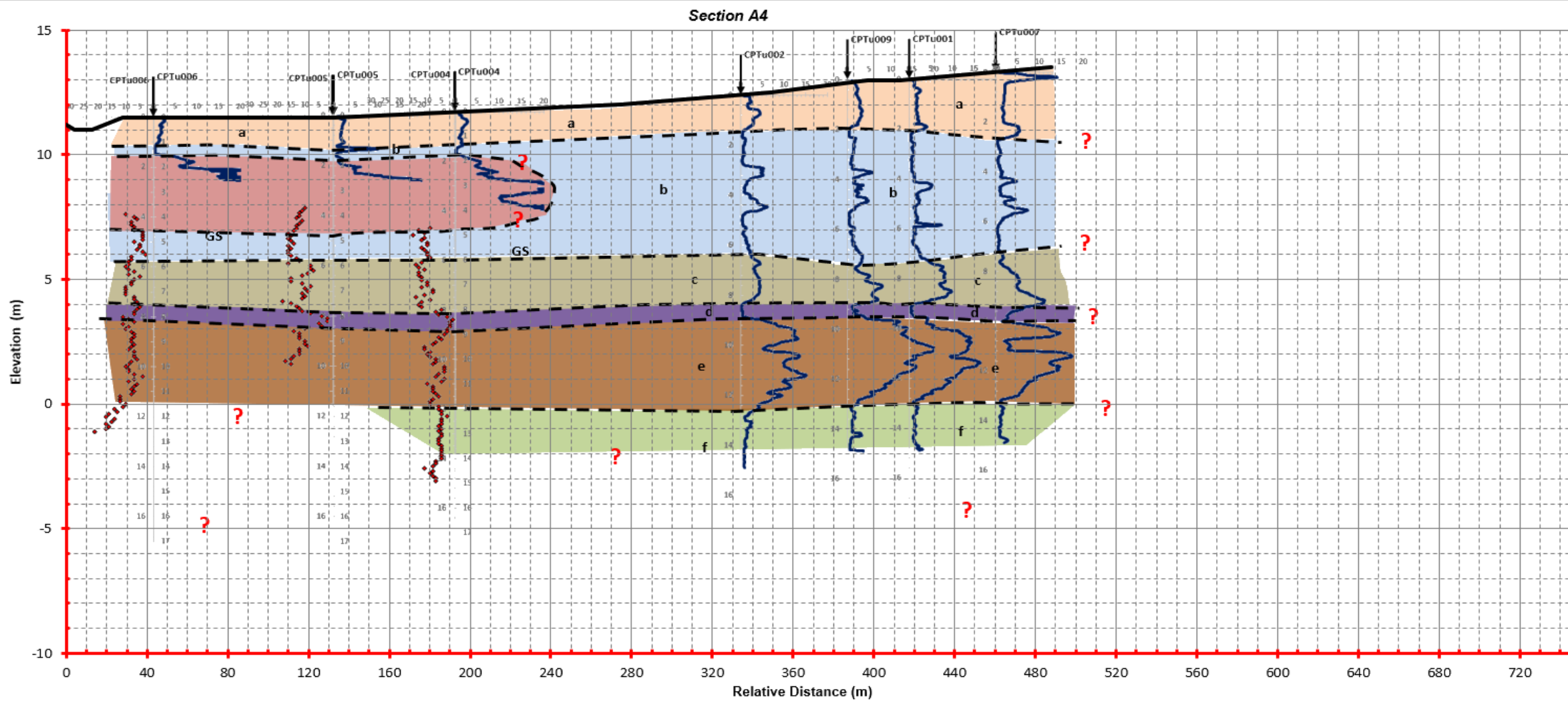
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LOCATION PLAN

SHEET No.: S1 REV. 1

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**LEGEND**

a	Silty SAND and sandy SILT, loose to firm
b	Clayey SILT, soft to firm, medium plasticity
c	Silty SAND, medium dense to dense with deth
GS	Gravelly SAND to sandy GRAVEL, dense
d	Clayey SILT to silty CLAY, firm
e	SAND, medium dense
f	Clayey SILT, firm to stiff
s	Gravelly SAND, very dense

**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**

**REVISION HISTORY**

REV	DATE	DESCRIPTION
1	19/10/20	FINAL

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 PROJECT No.: 200357  
 VERSION DATE: 16/10/2020  
 DRAWN: CG  
 ENGINEER: CG  
 APPROVED: AG

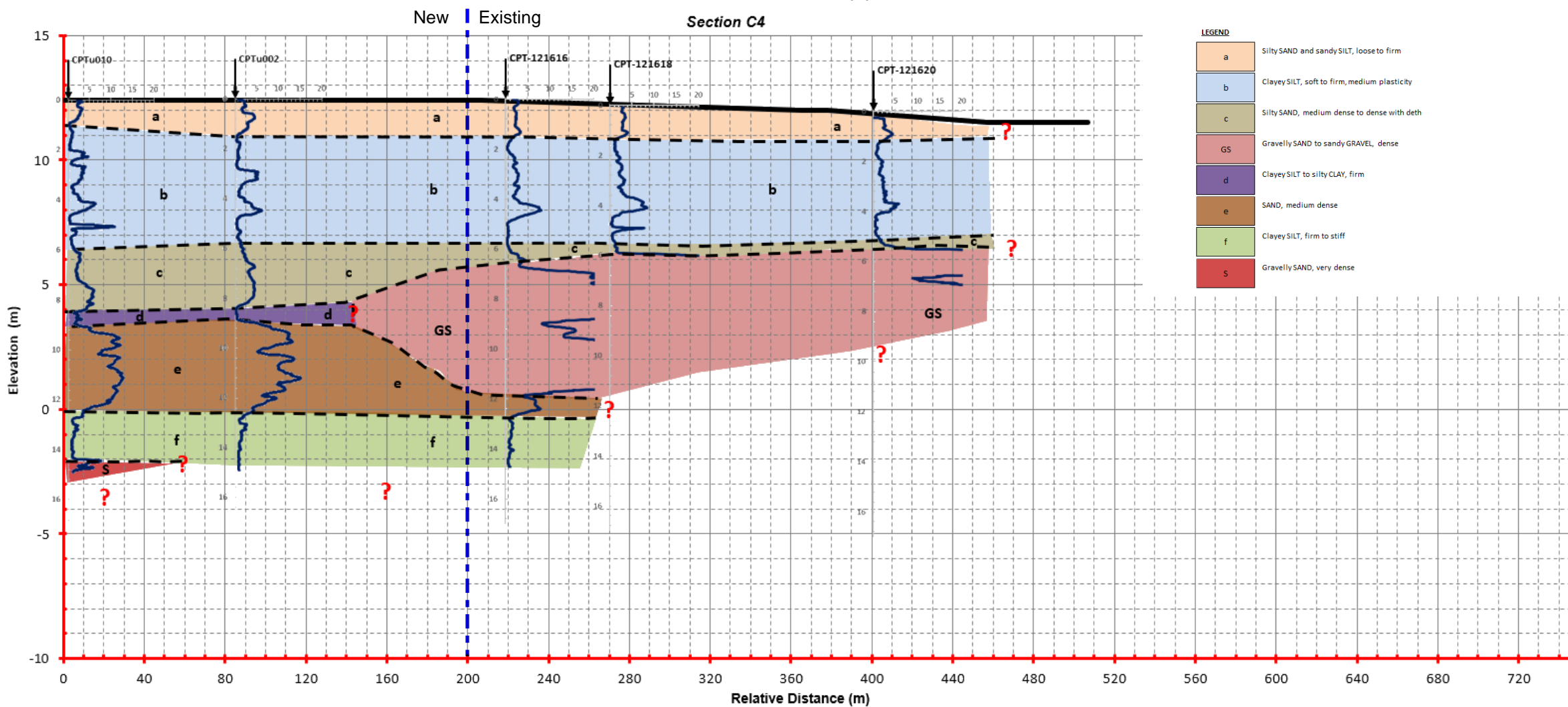
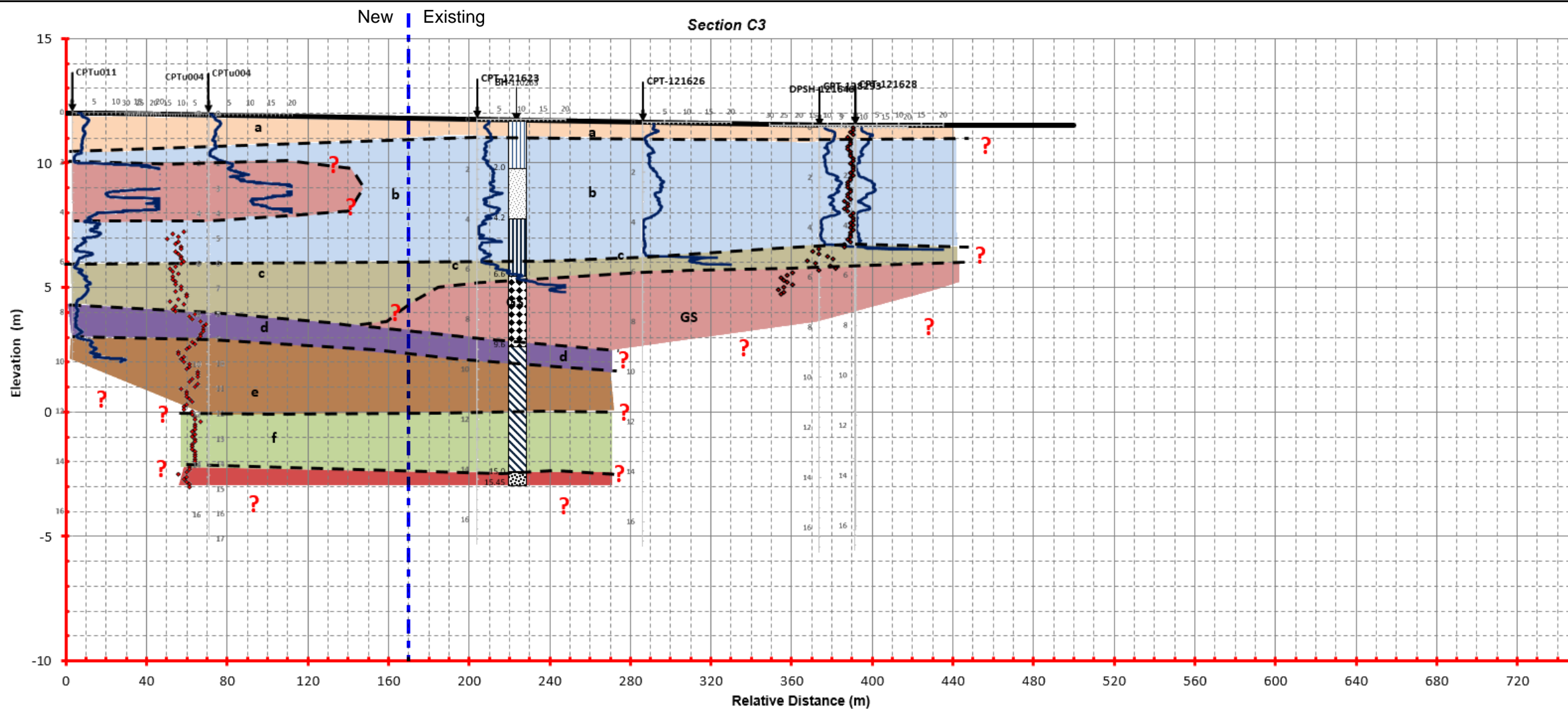
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**GROUND MODEL SHEET 1**

SHEET No.: S2.1 REV. 1

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**SITE SURVEY DRAWINGS FOR**  
**2&4 GLOVERS ROAD,**  
**HALSWELL,**  
**CHRISTCHURCH 8025**



**LEGEND**

a	Silty SAND and sandy SILT, loose to firm
b	Clayey SILT, soft to firm, medium plasticity
c	Silty SAND, medium dense to dense with deth
GS	Gravelly SAND to sandy GRAVEL, dense
d	Clayey SILT to silty CLAY, firm
e	SAND, medium dense
f	Clayey SILT, firm to stiff
s	Gravelly SAND, very dense

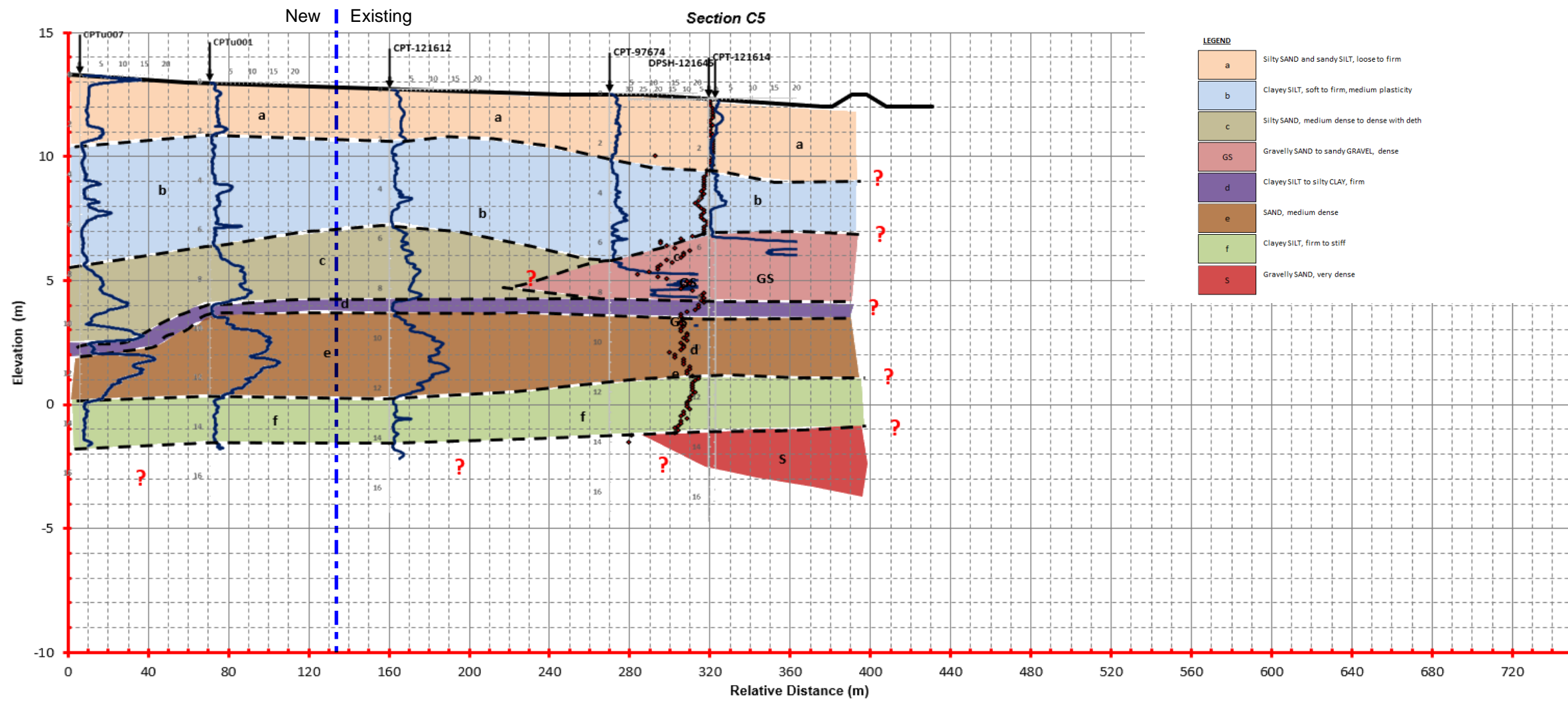
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PROJECT No.: 200357  
VERSION DATE: 16/10/2020  
DRAWN: CG  
ENGINEER: CG  
APPROVED: AG

SIZE: A3  
**GROUND MODEL SHEET 2**

SHEET No.: S2.2 REV. 1



**LEGEND**

a	Silty SAND and sandy SILT, loose to firm
b	Clayey SILT, soft to firm, medium plasticity
c	Silty SAND, medium dense to dense with deth
GS	Gravelly SAND to sandy GRAVEL, dense
d	Clayey SILT to silty CLAY, firm
e	SAND, medium dense
f	Clayey SILT, firm to stiff
S	Gravelly SAND, very dense

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**SITE SURVEY DRAWINGS FOR**  
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**CHRISTCHURCH 8025**

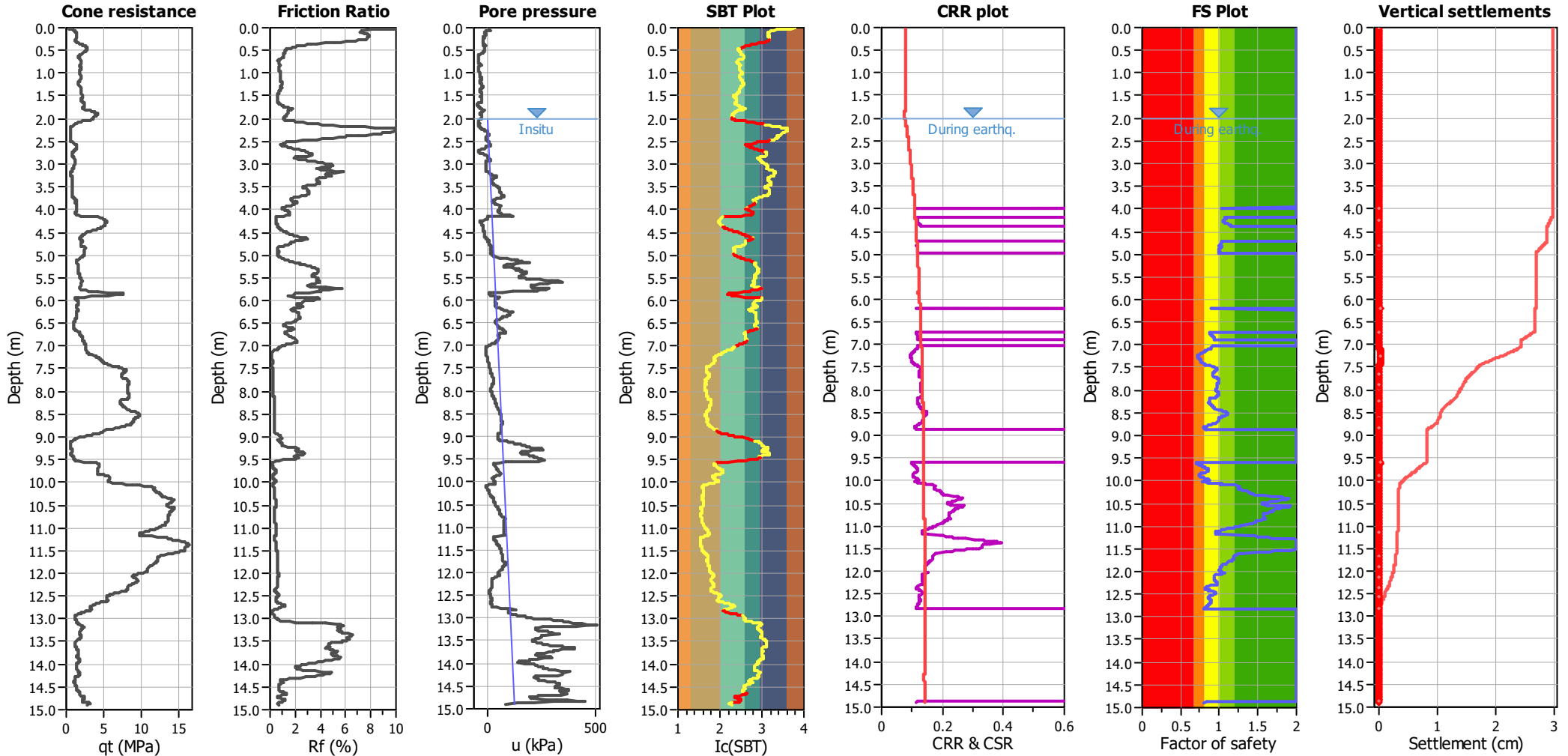
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VERSION DATE:	16/10/2020
DRAWN:	CG
ENGINEER:	CG
APPROVED:	AG

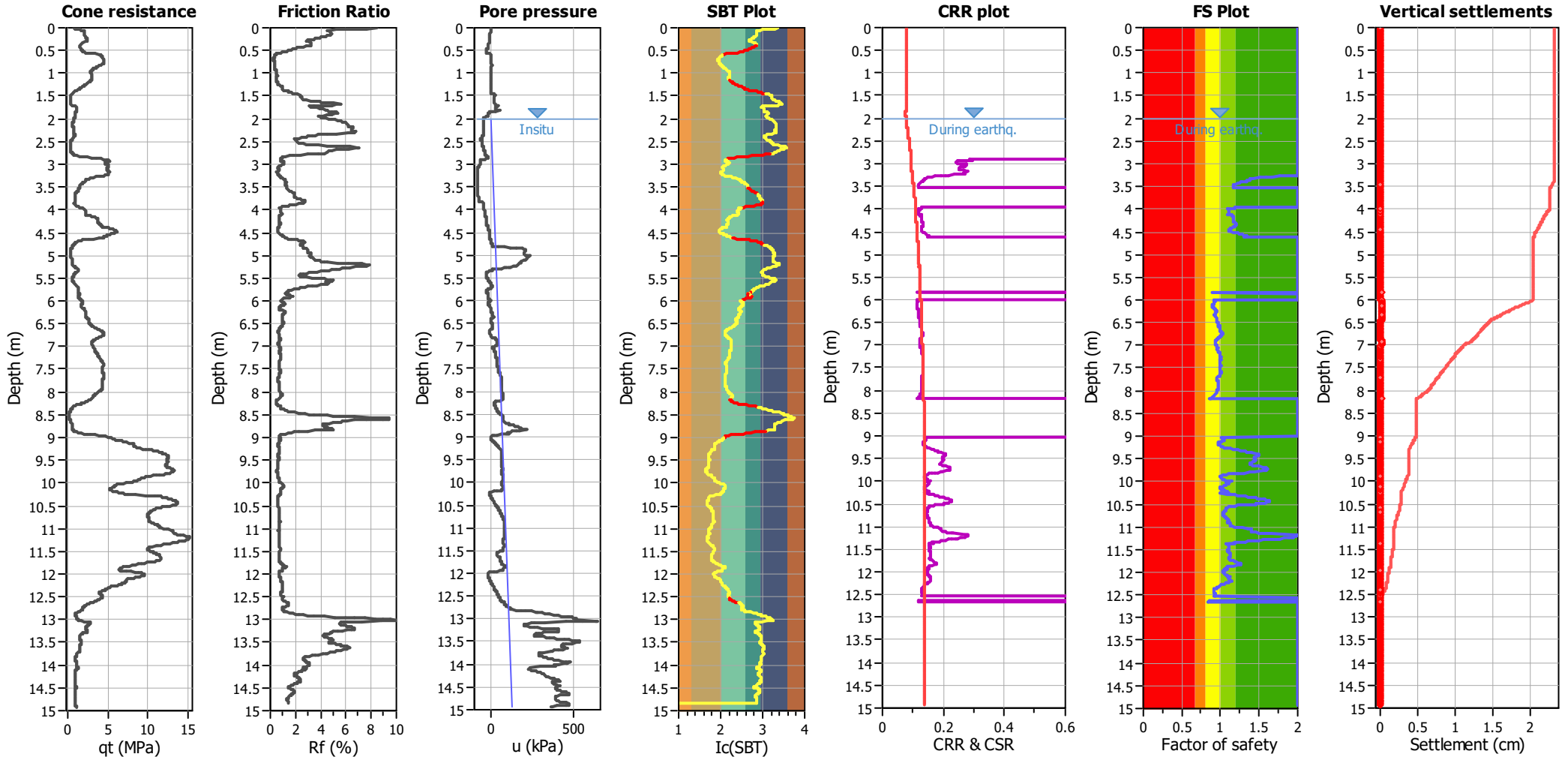
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## F. Liquefaction Analyses

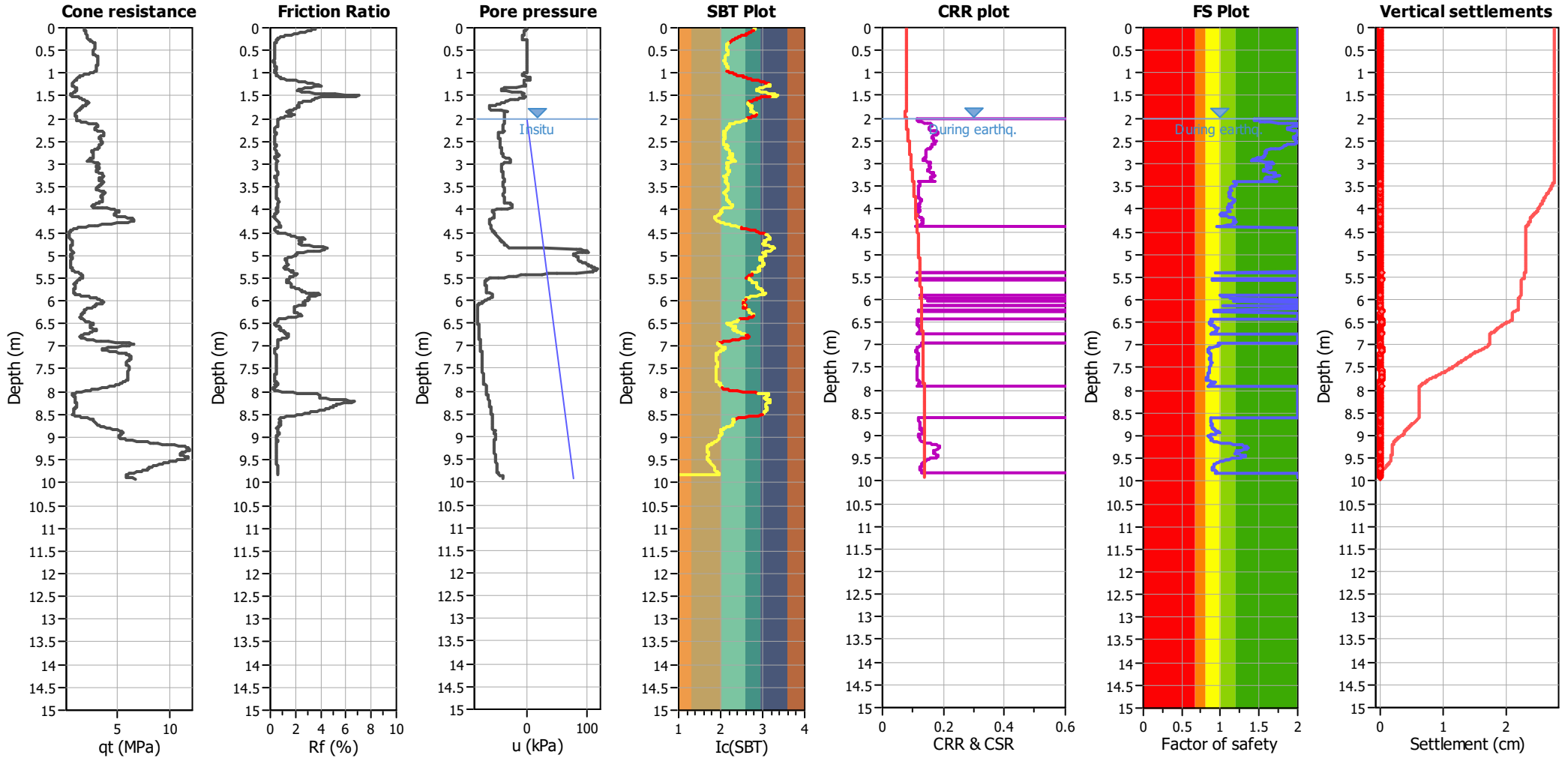




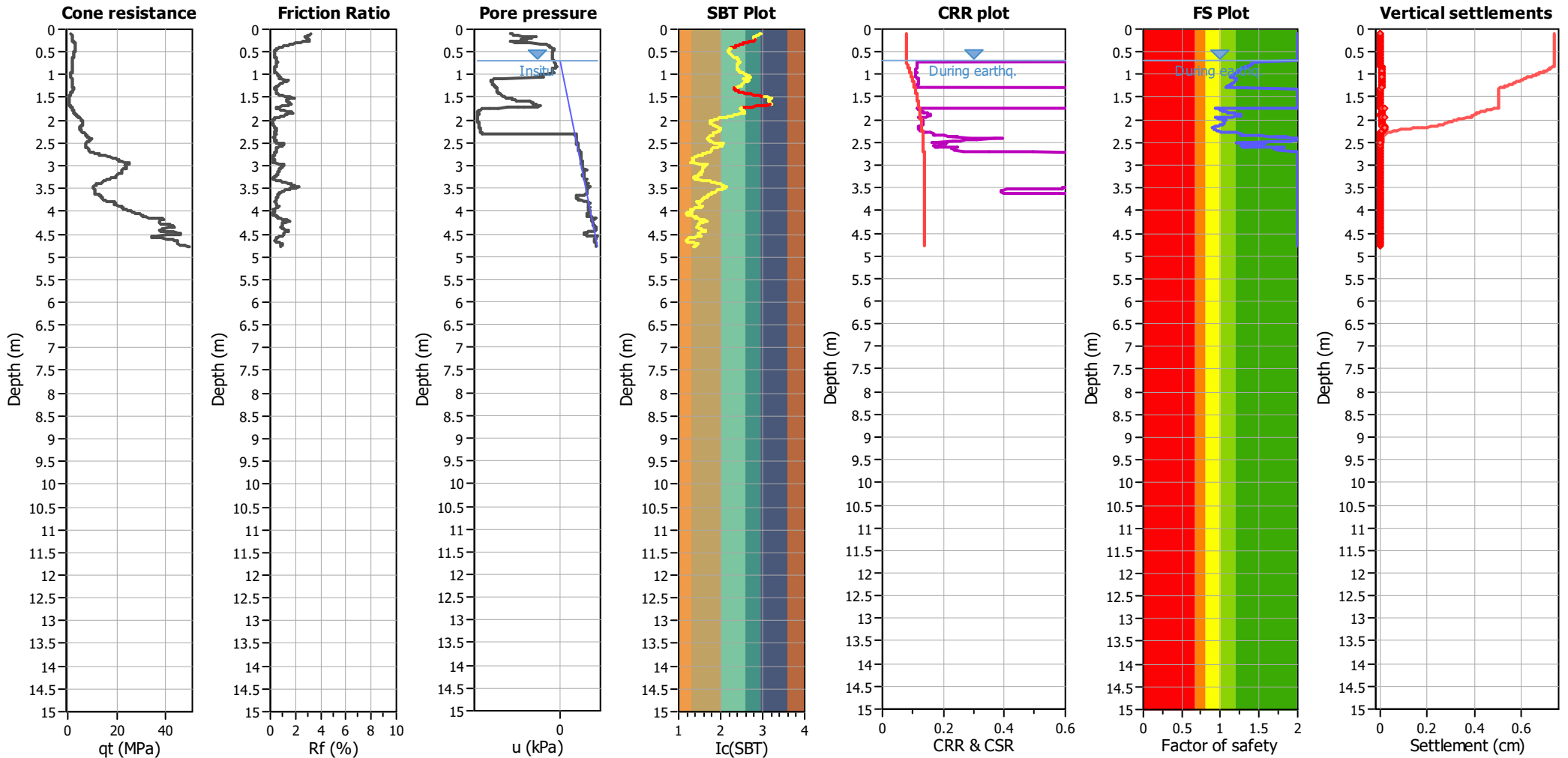
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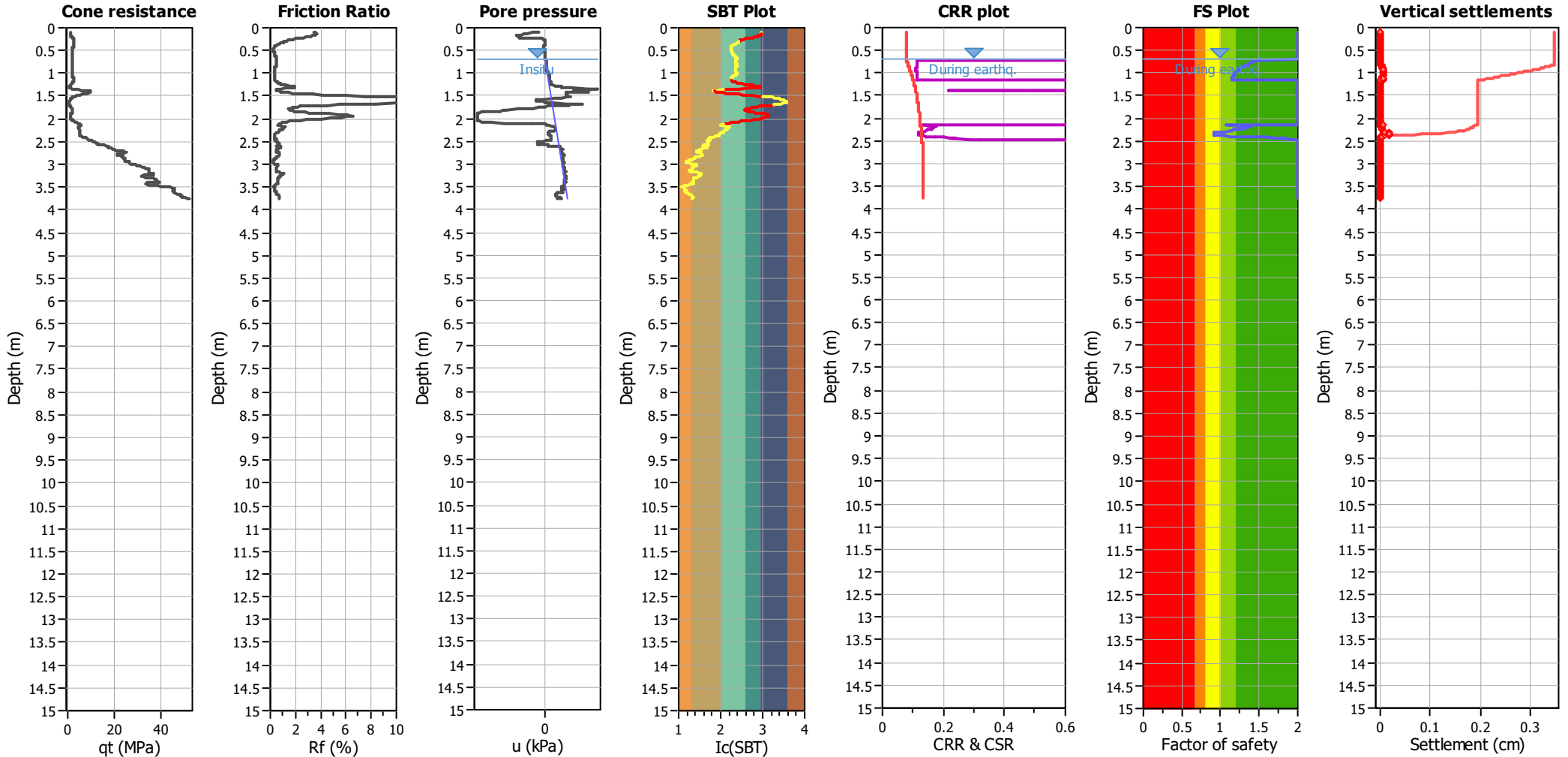


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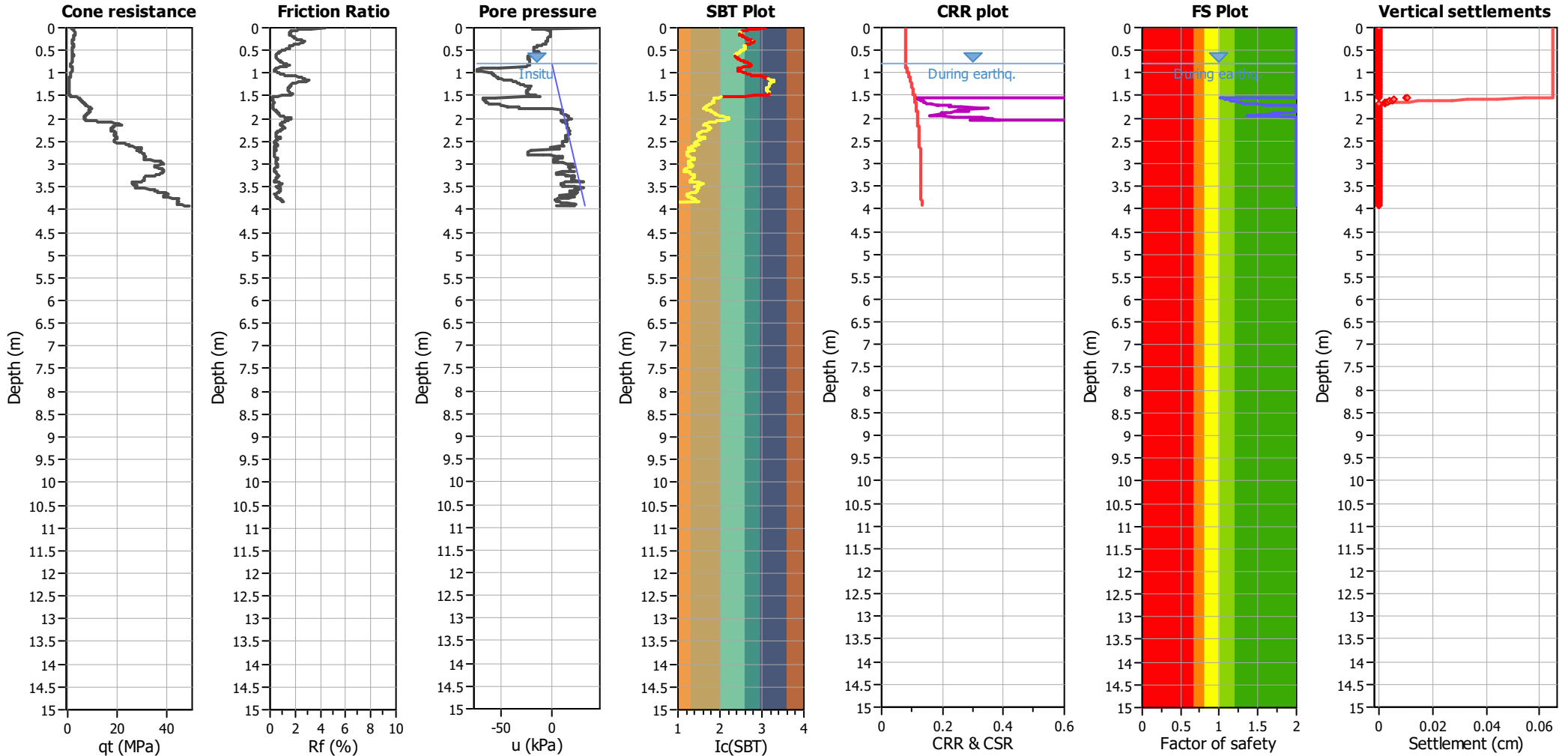


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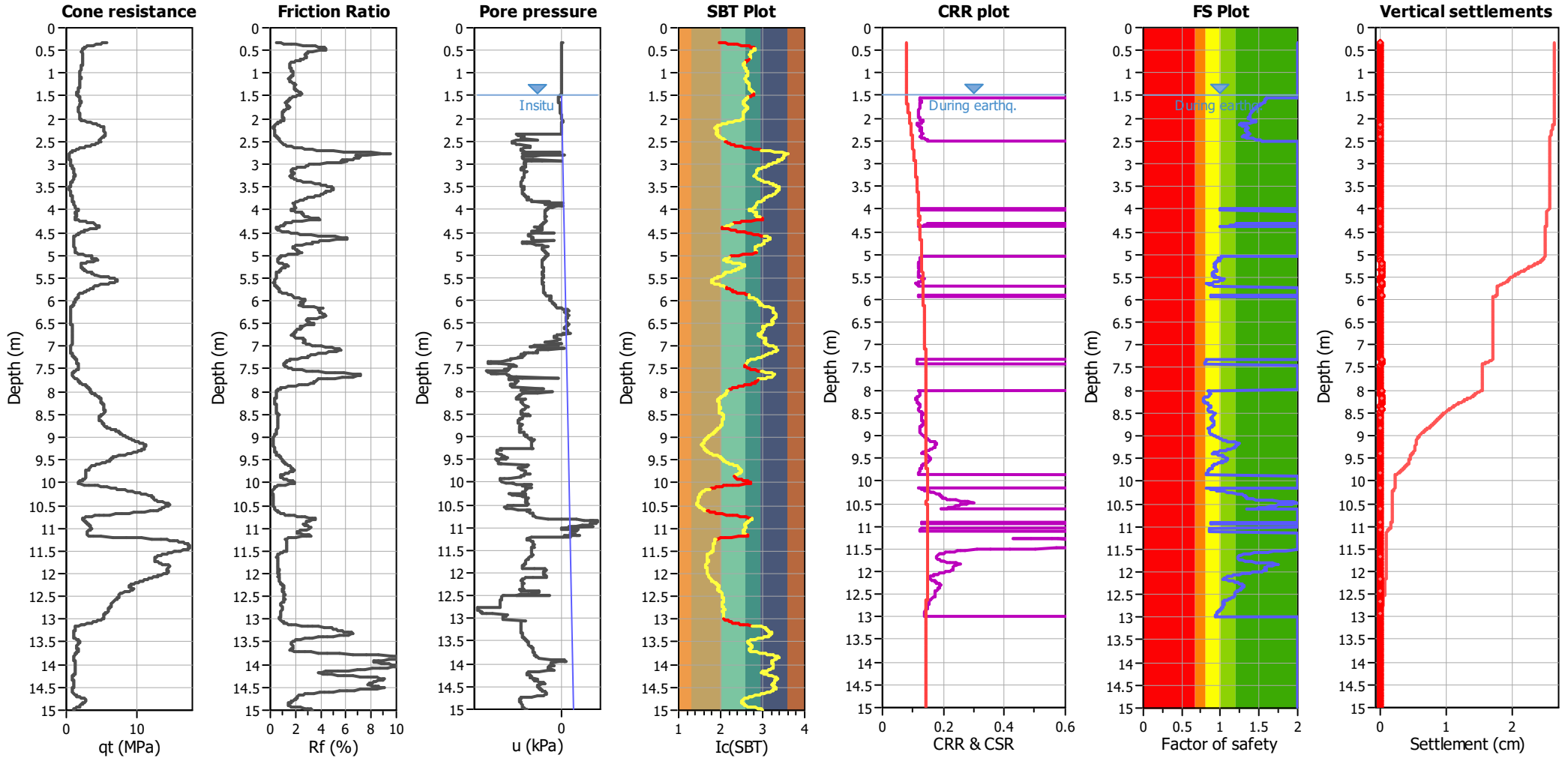




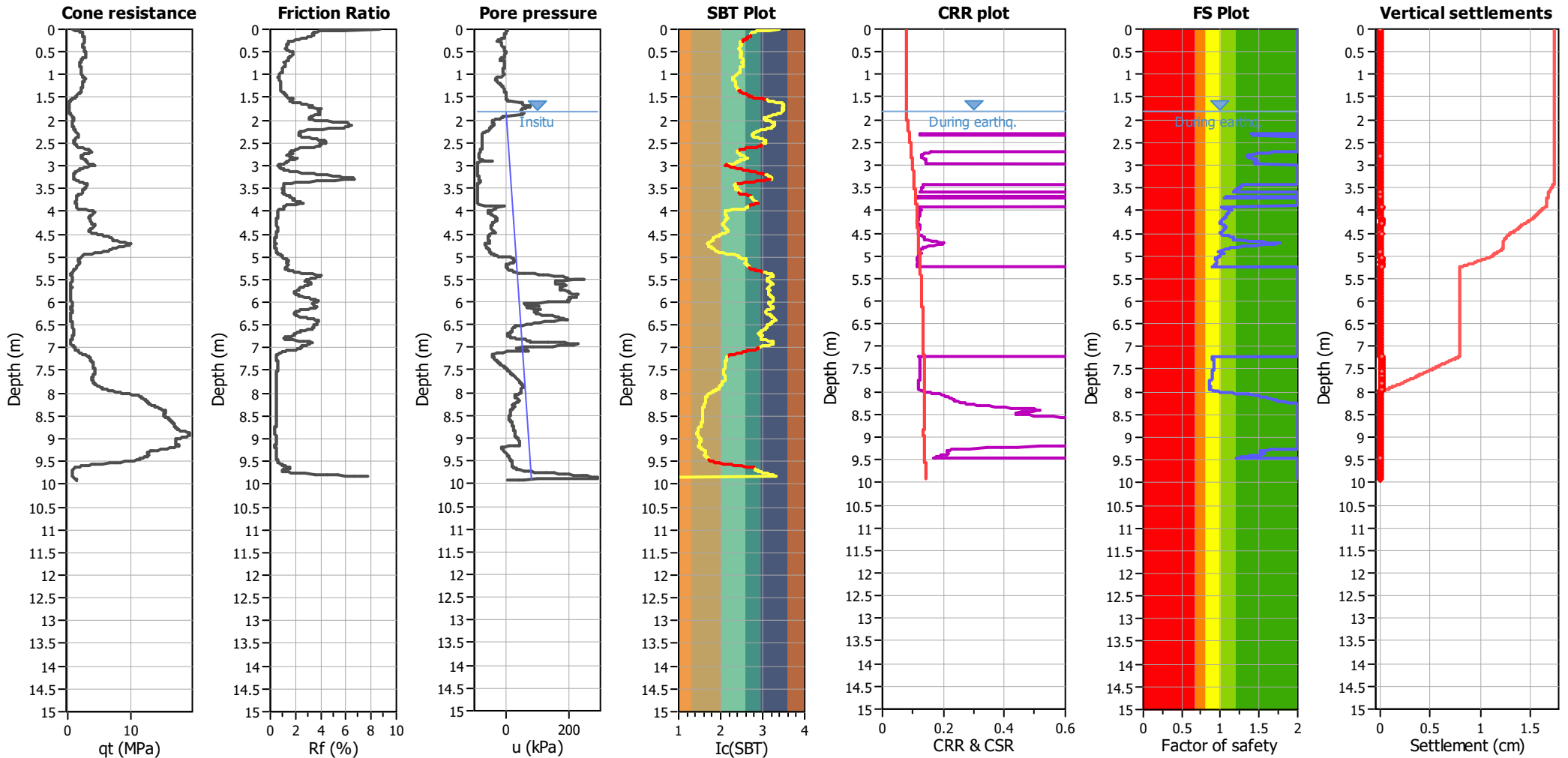
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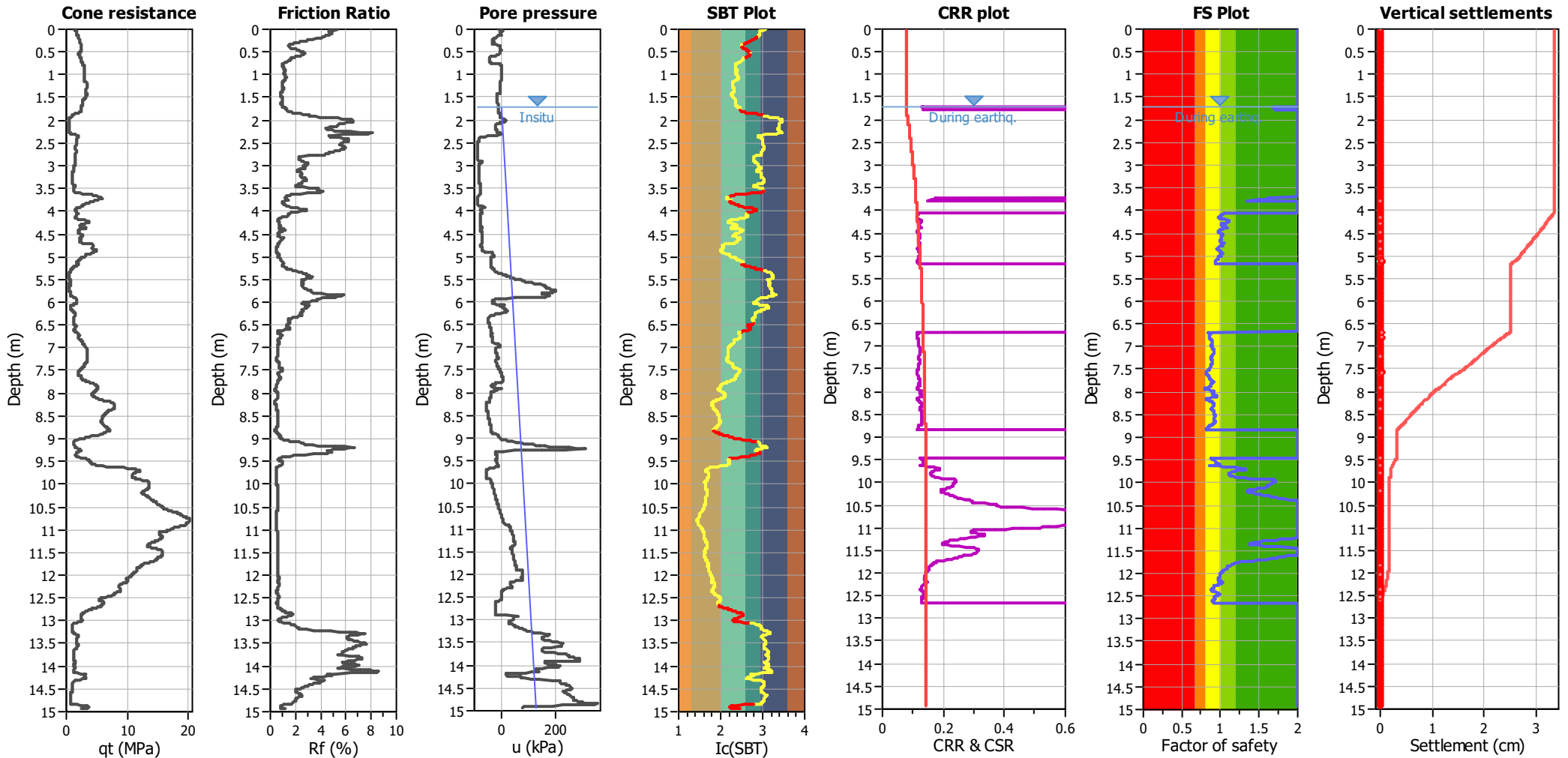
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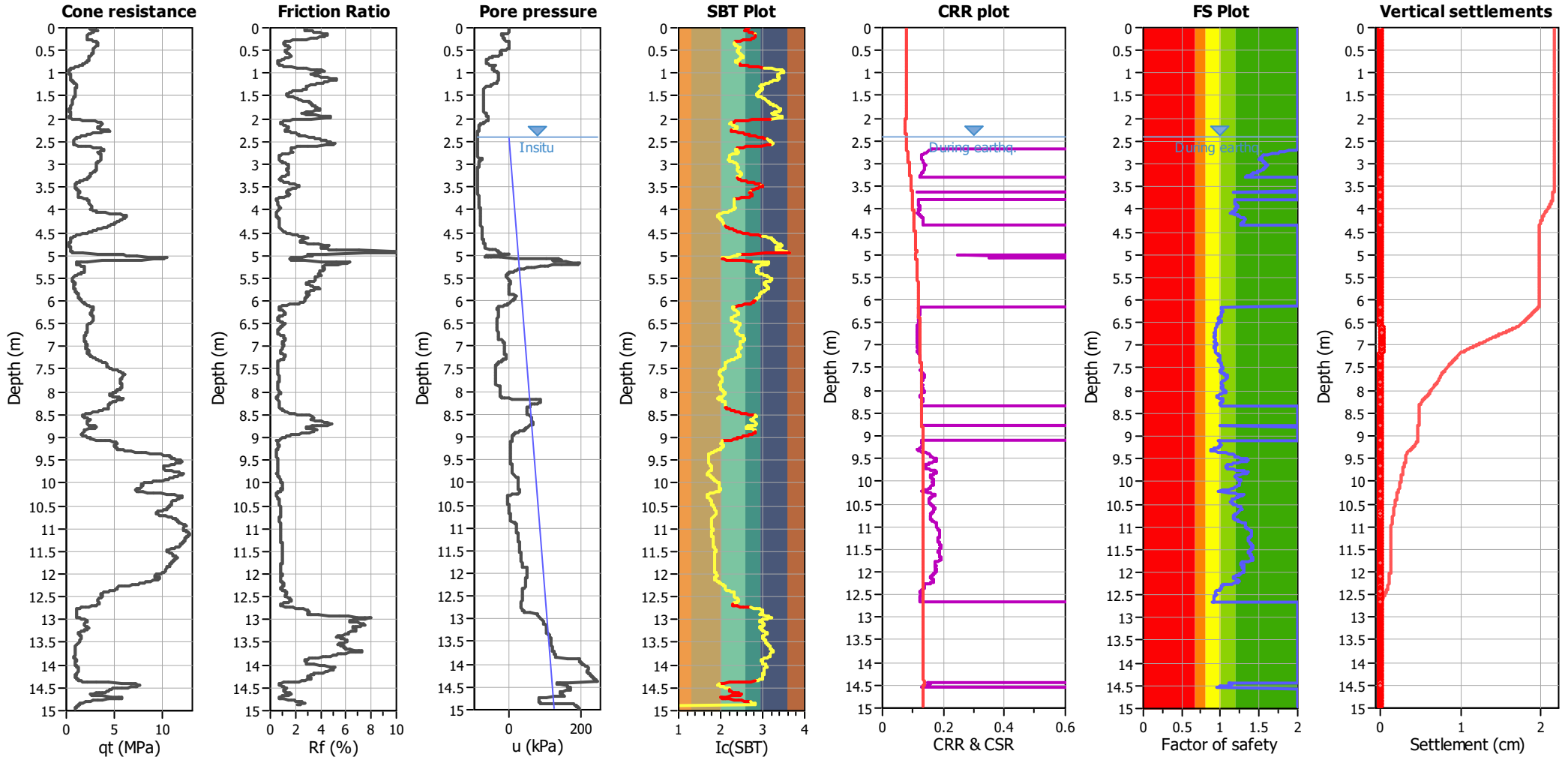
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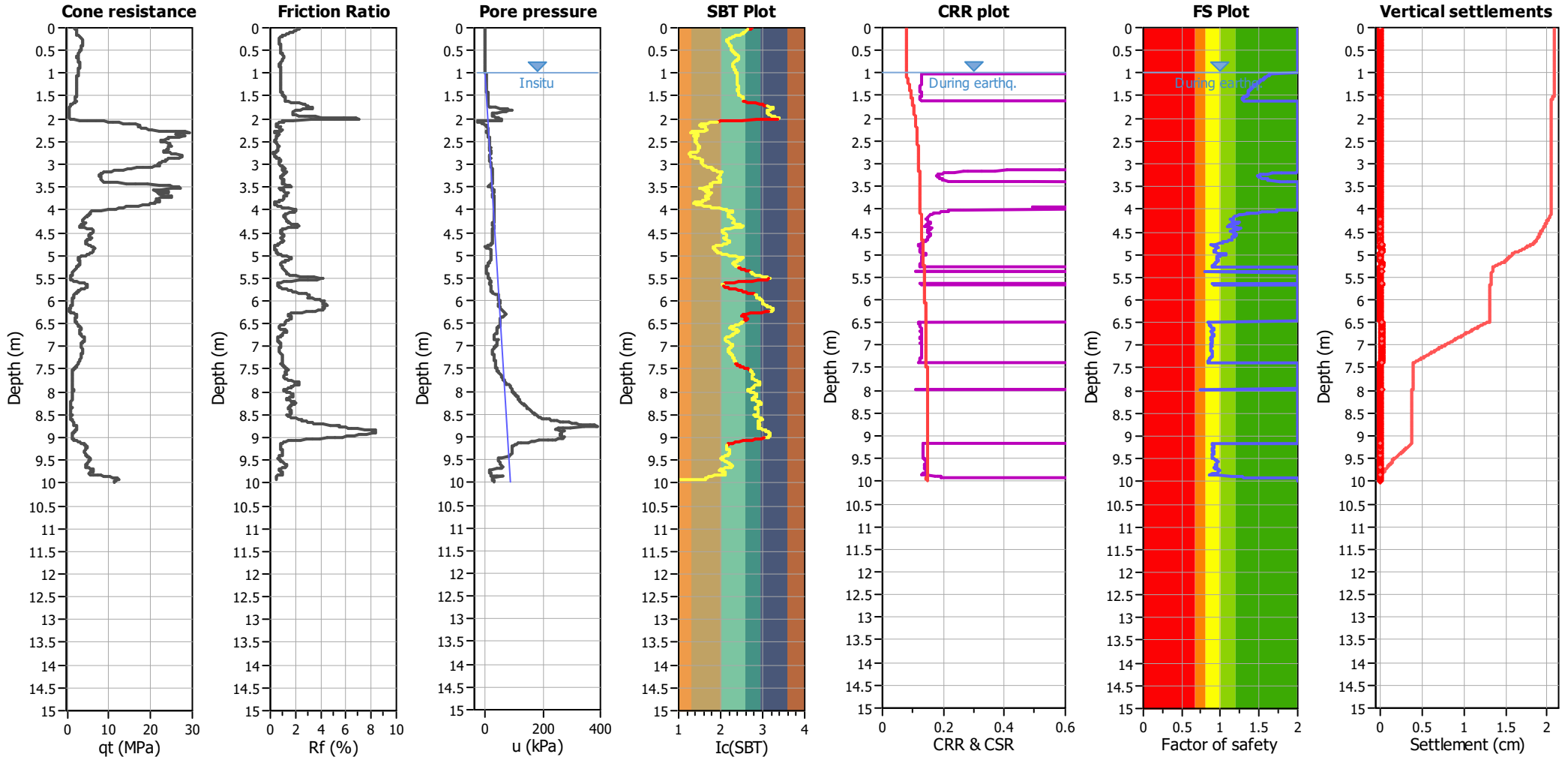
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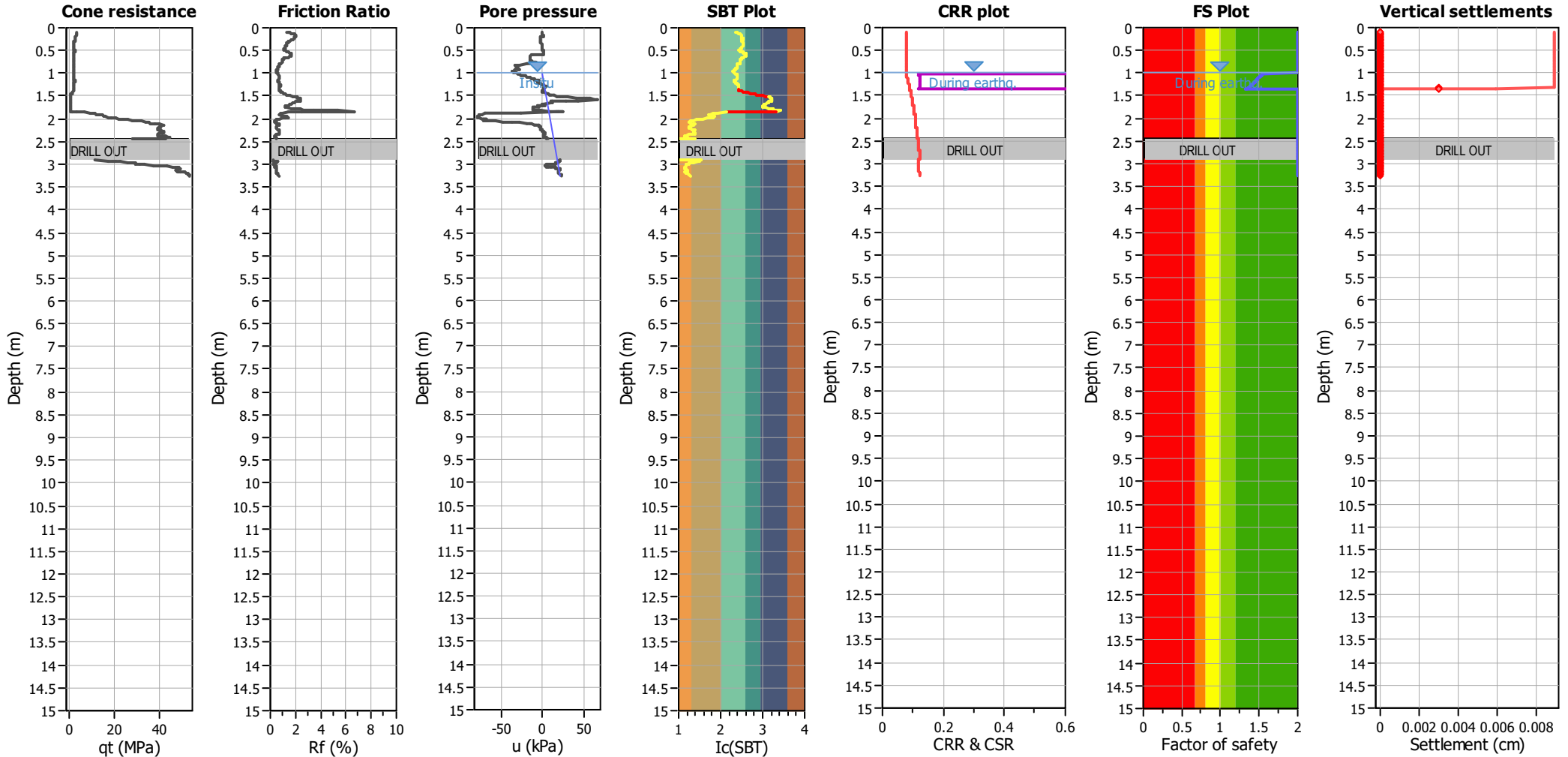
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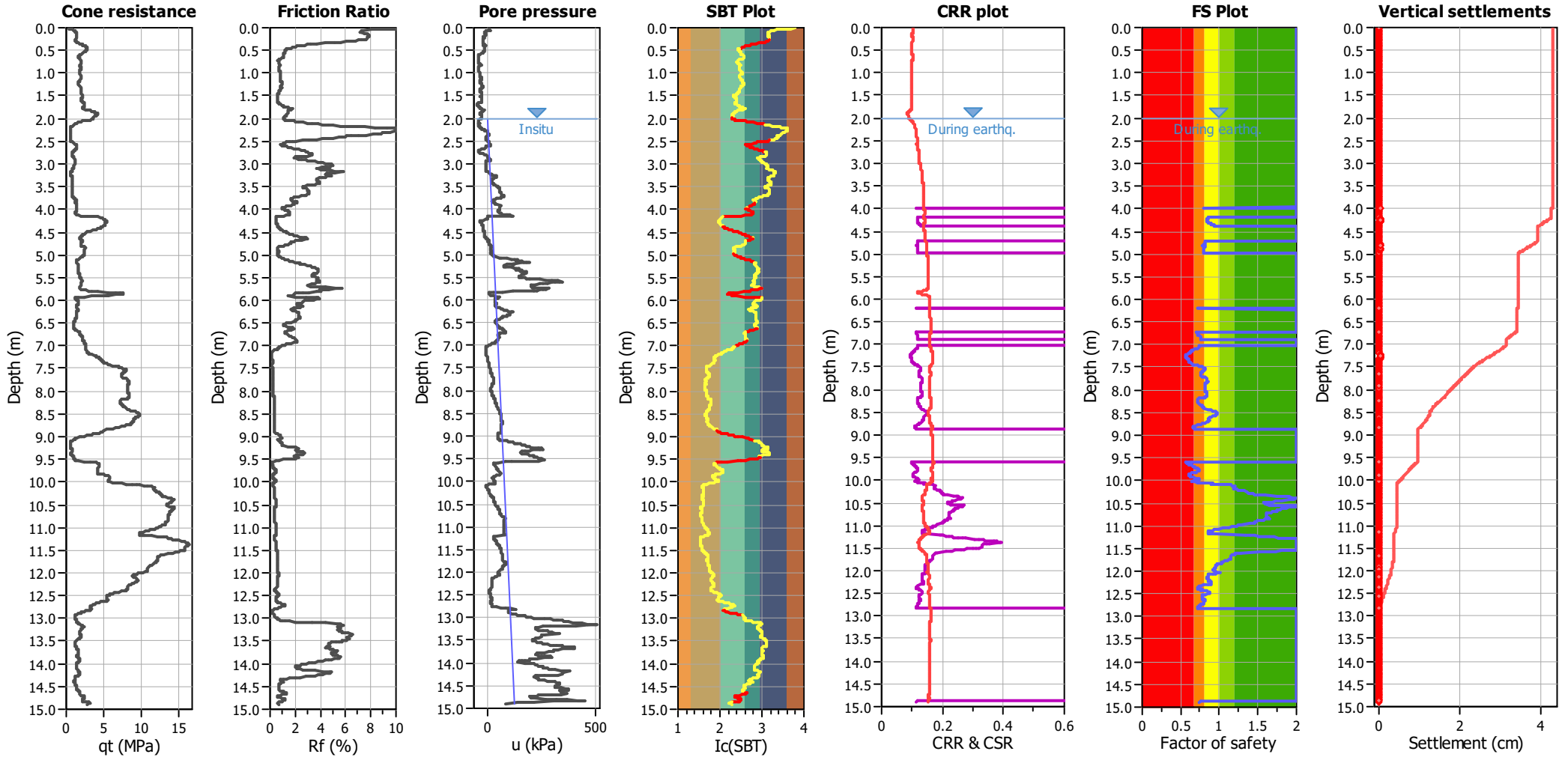


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Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

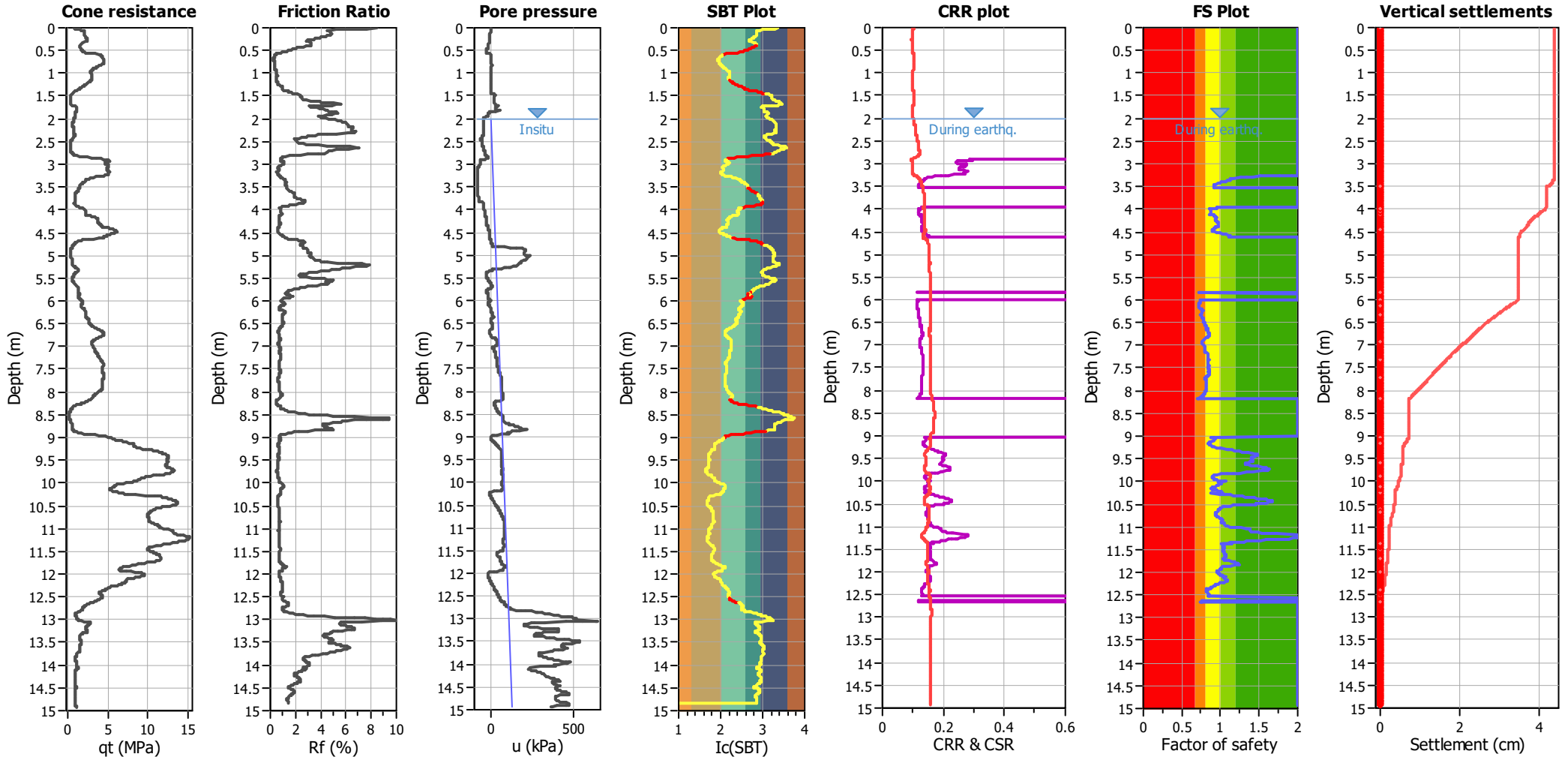


Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.13	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

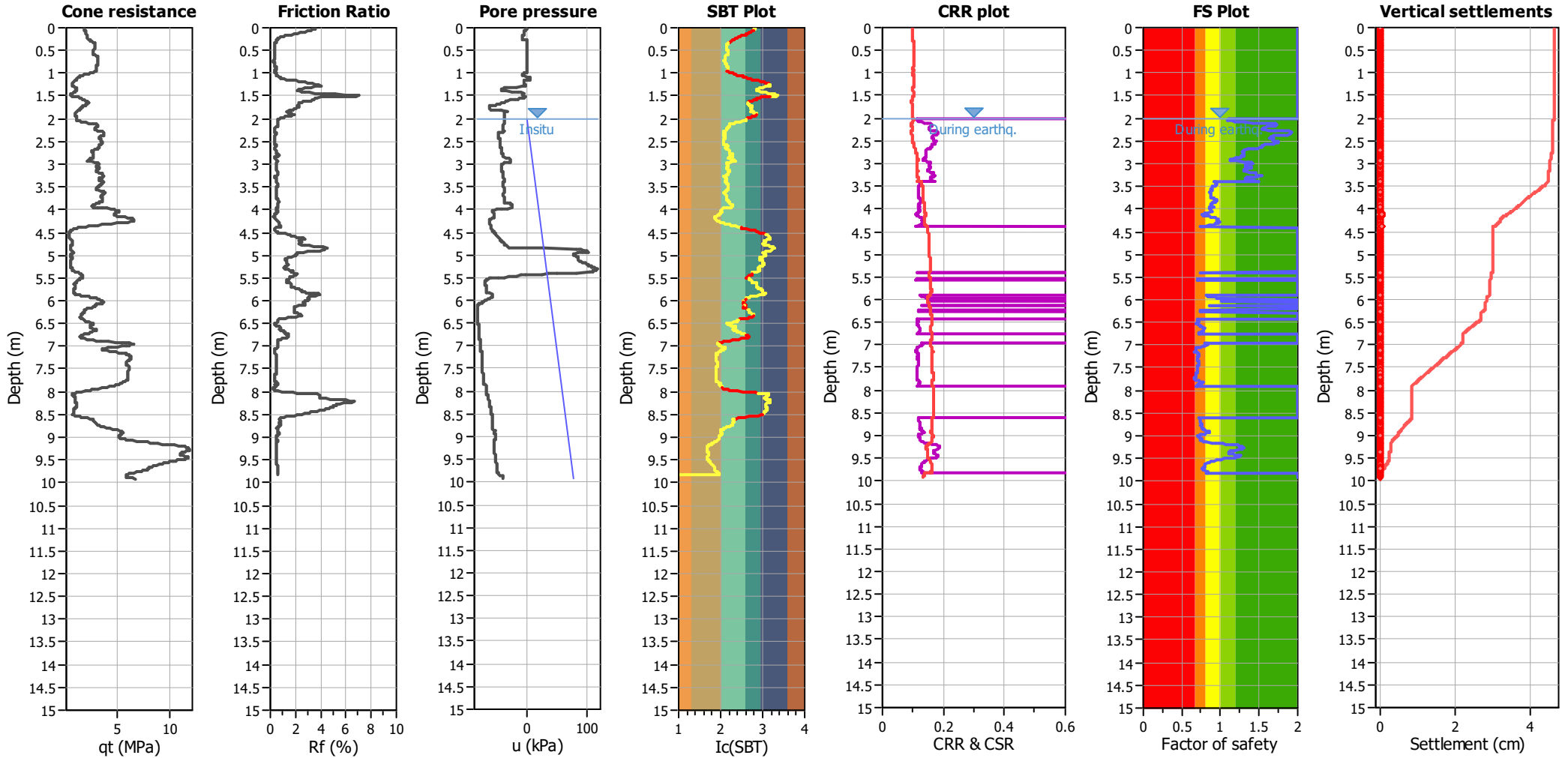




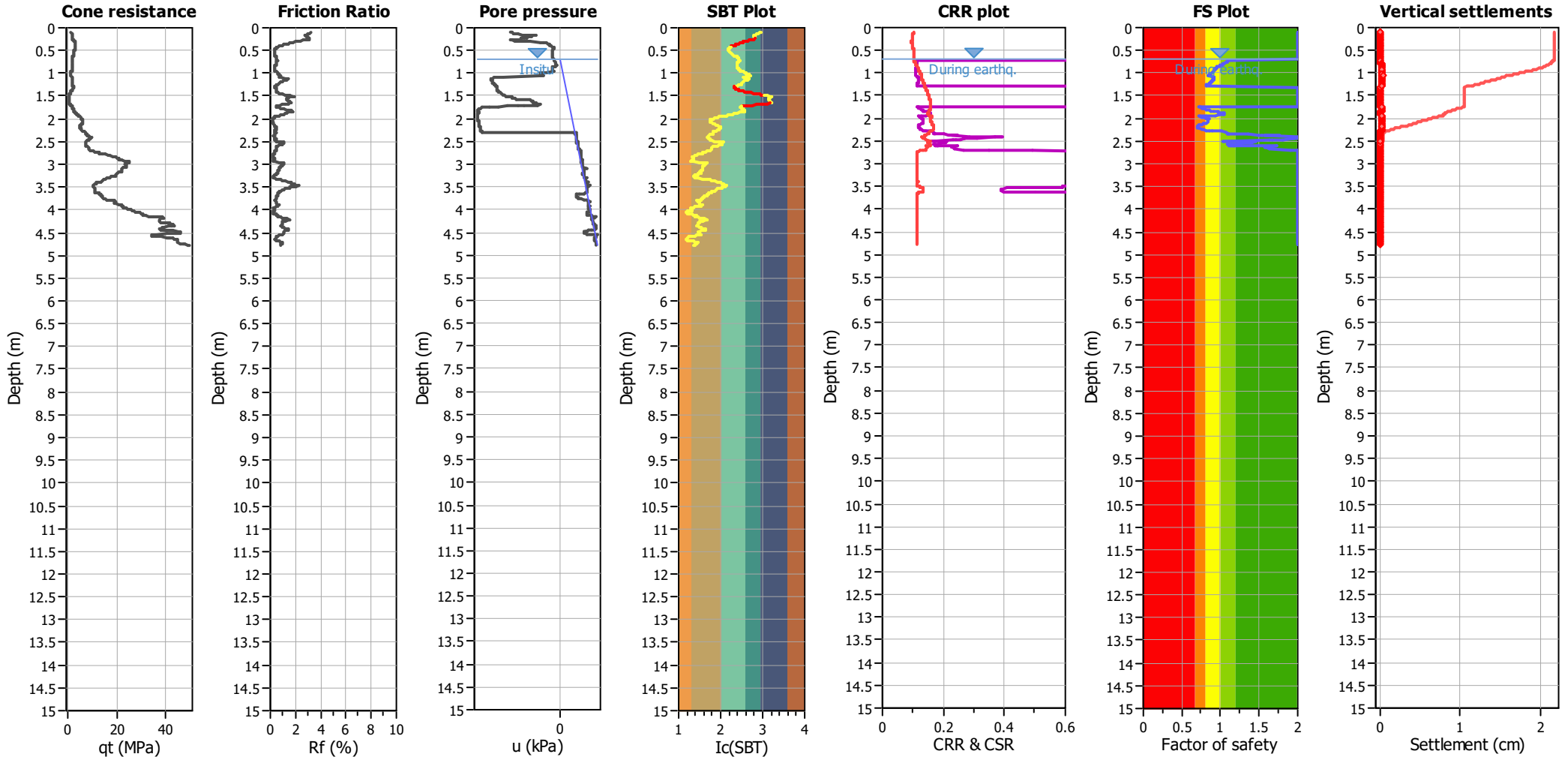
Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



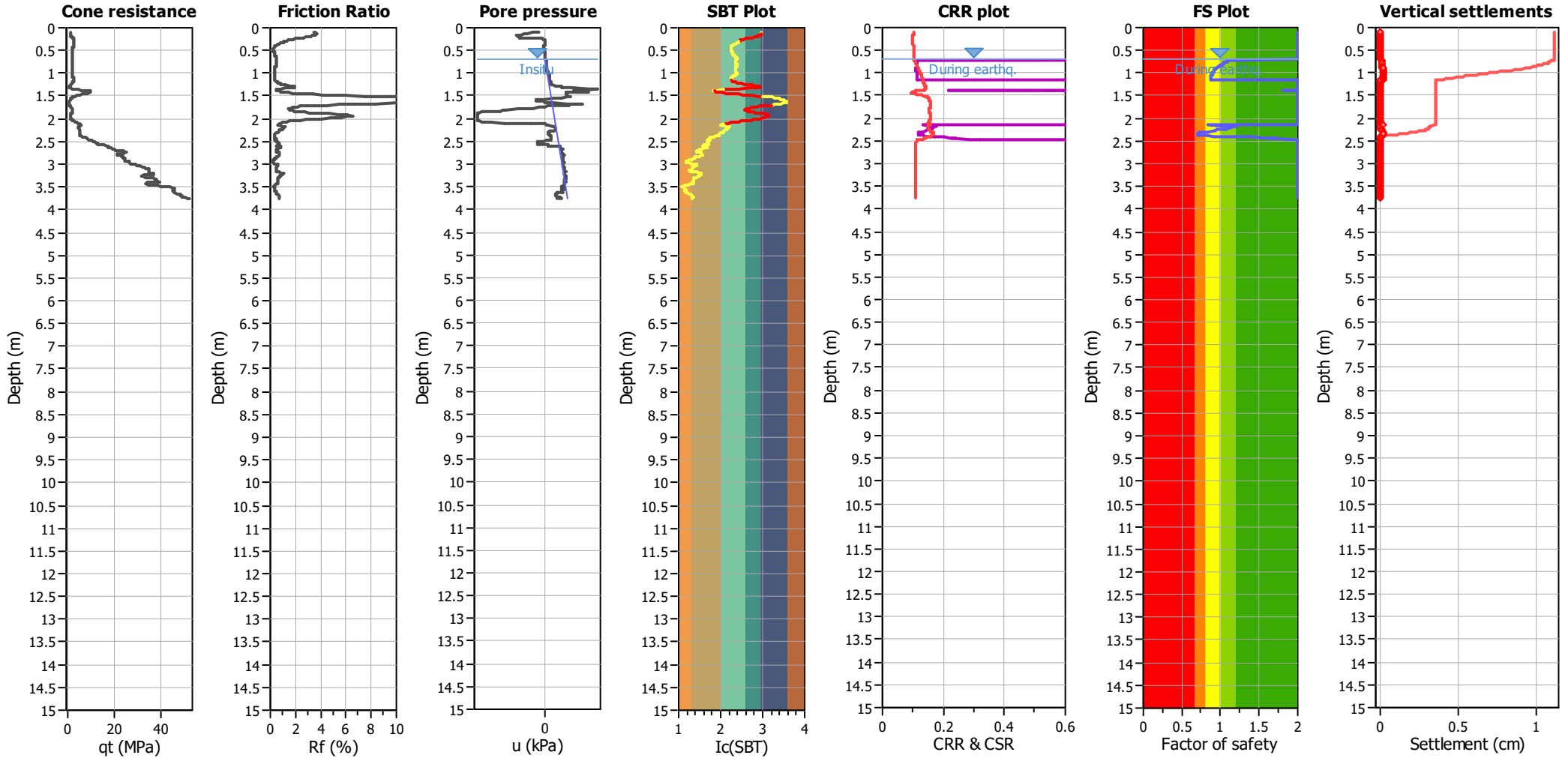
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



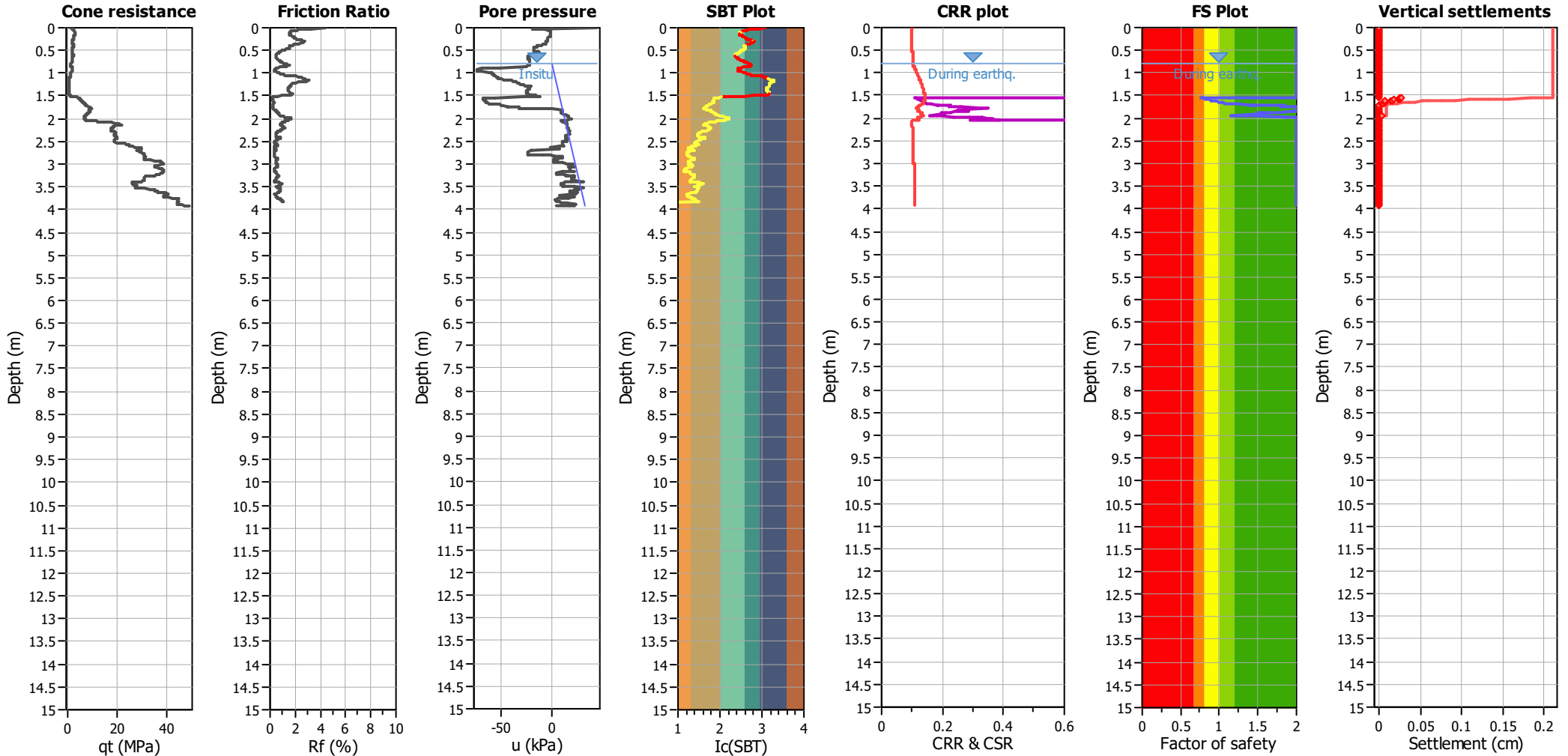
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_\sigma$ applied:	Yes	MSF method:	Method based



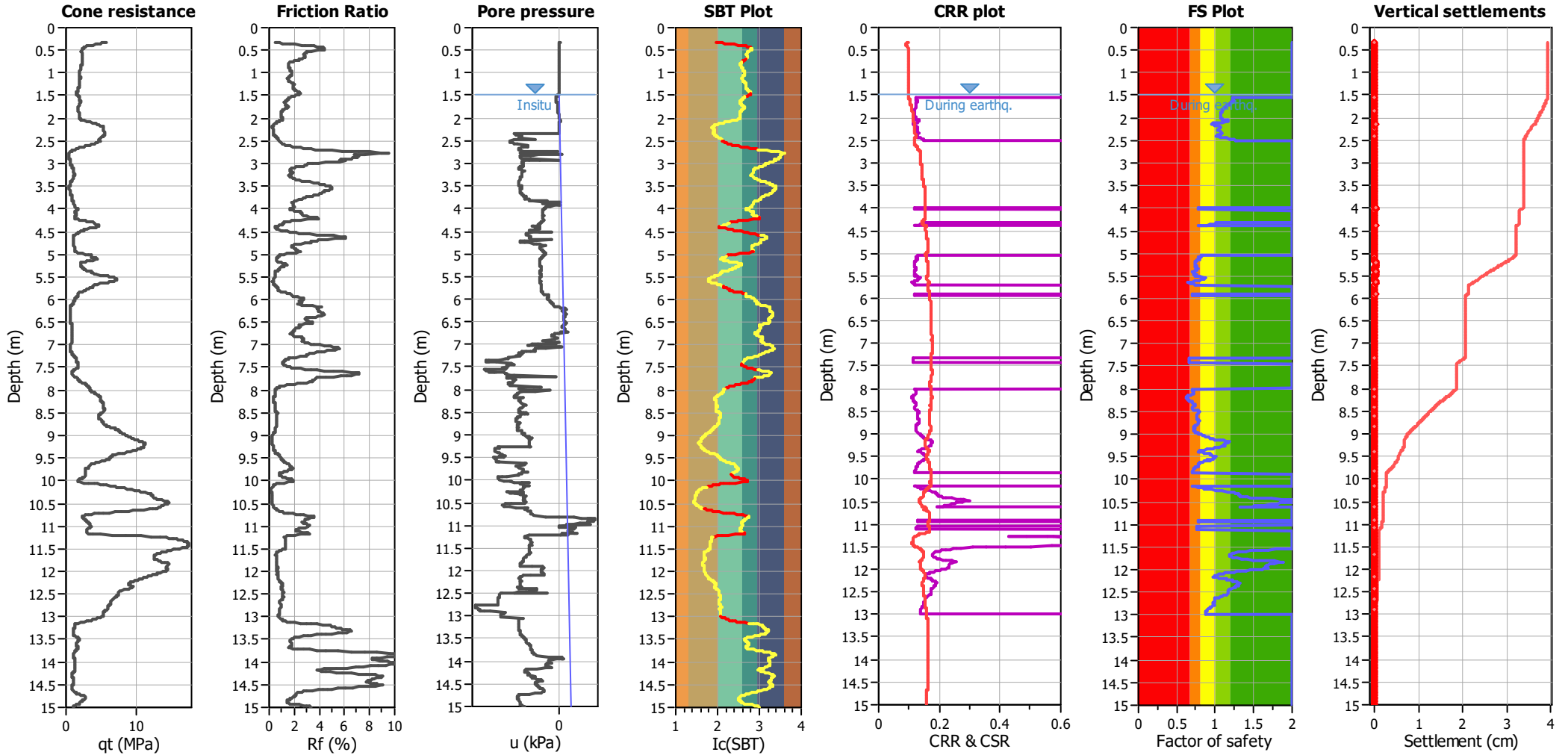
Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



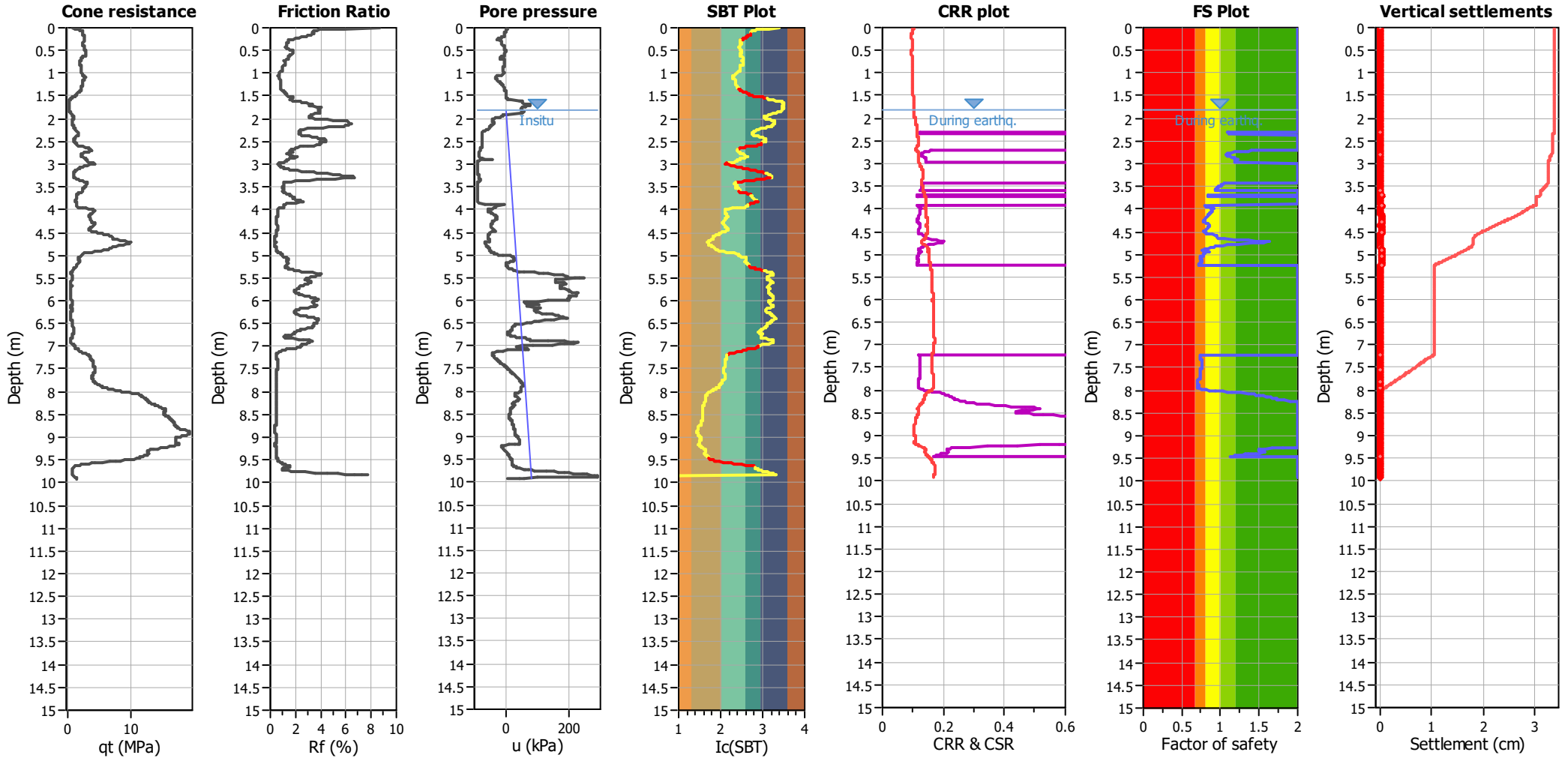
Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.80 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

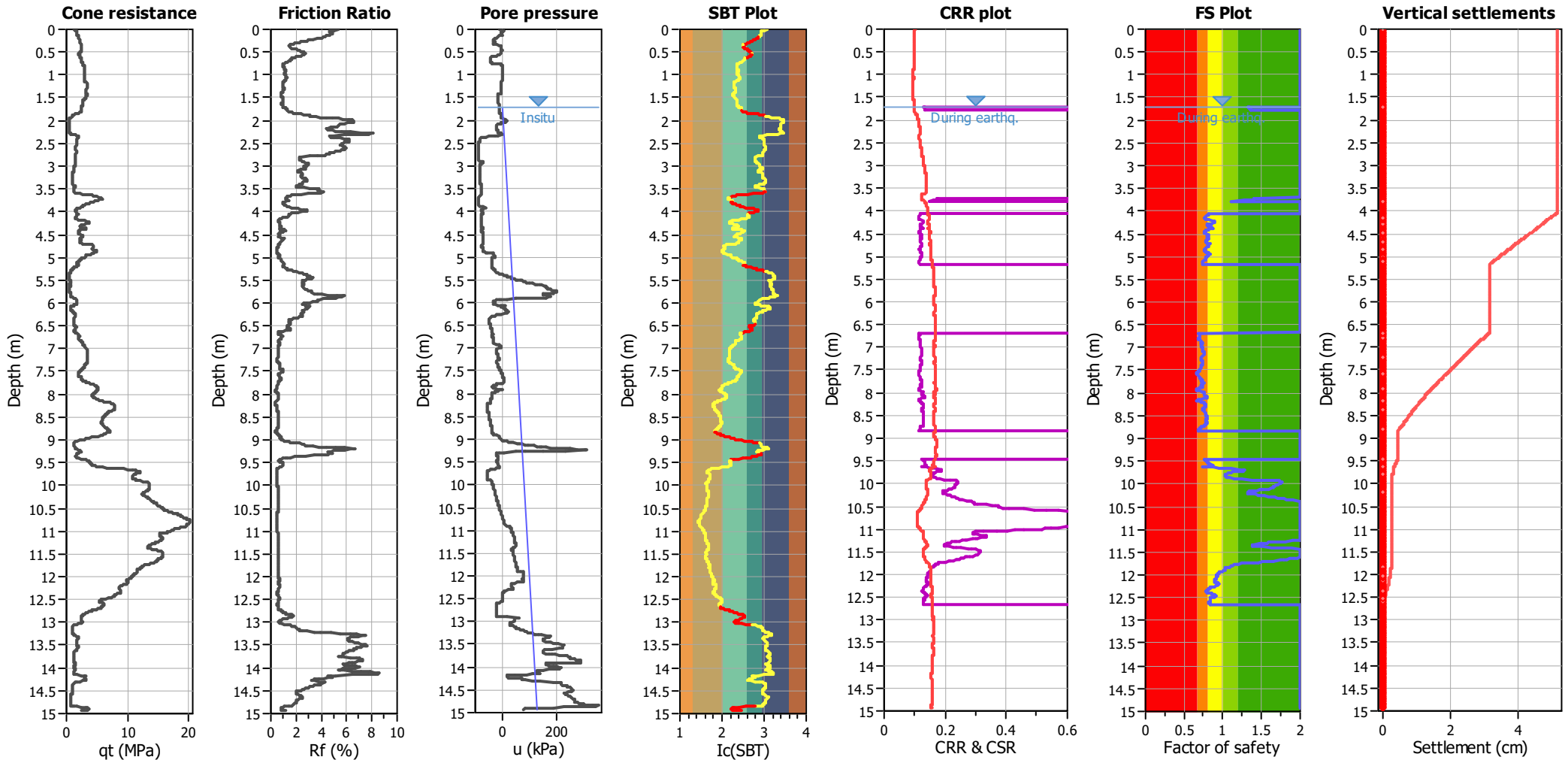


Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.50 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.50 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

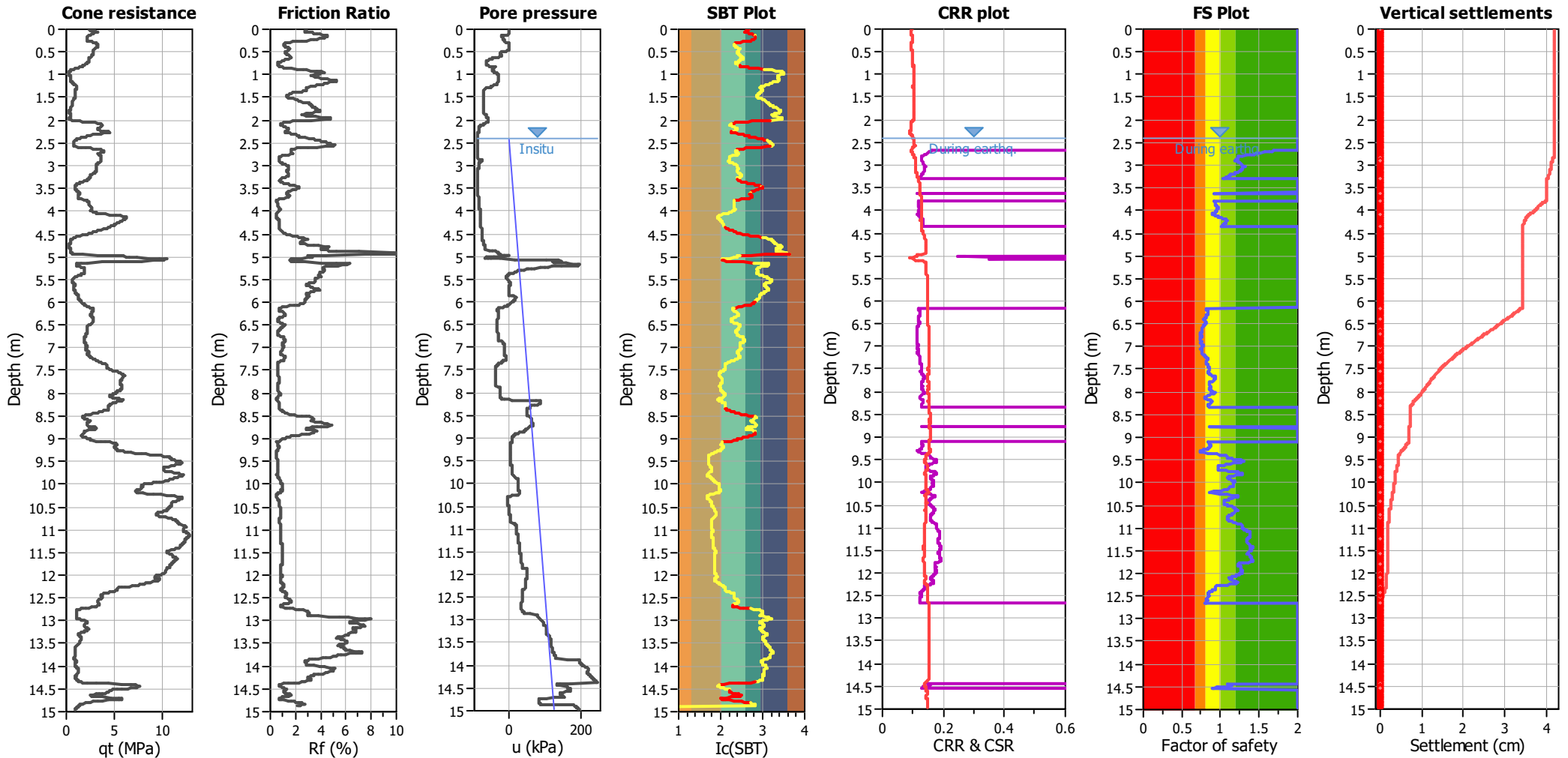


Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.80 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

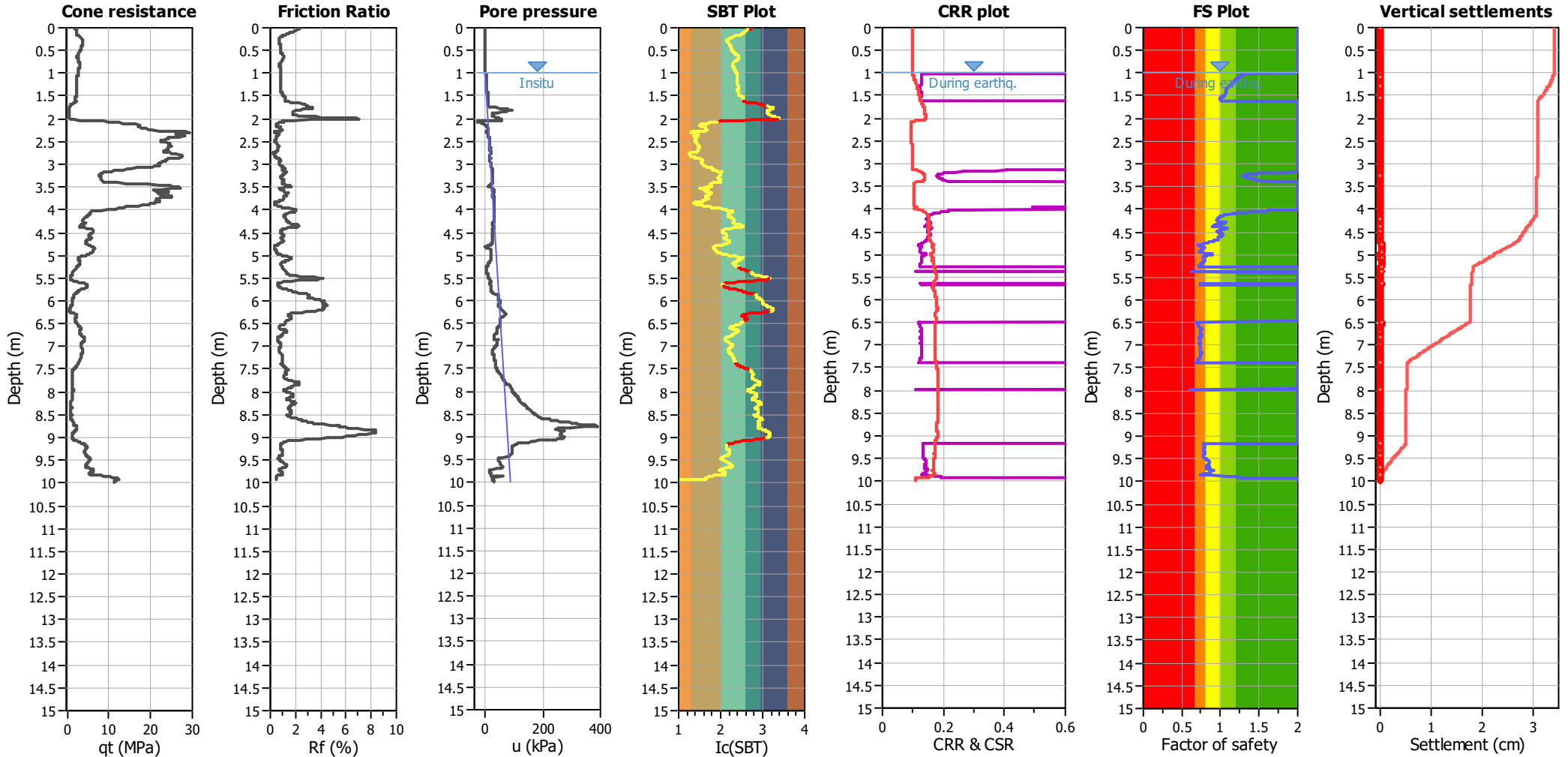




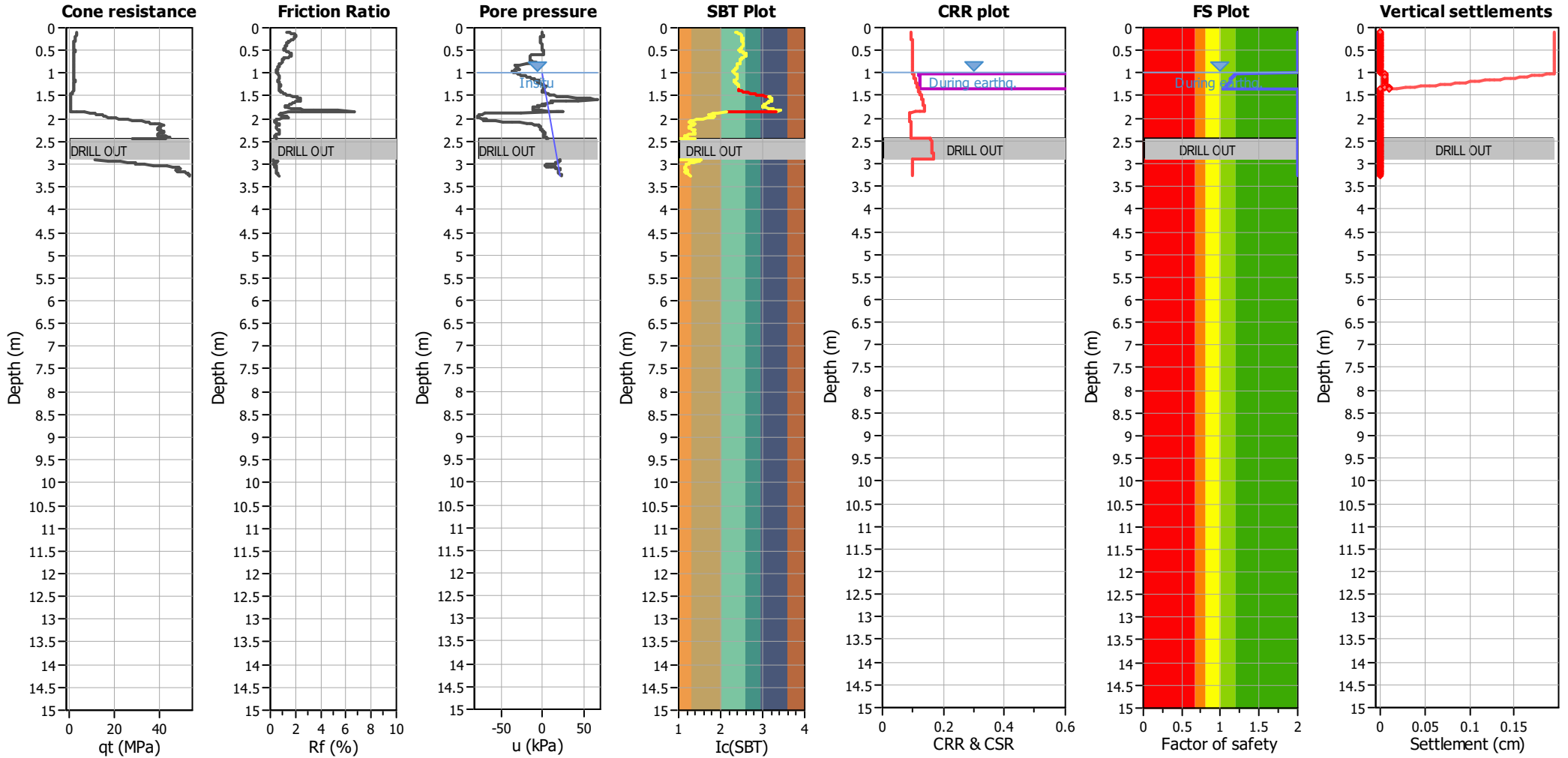
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



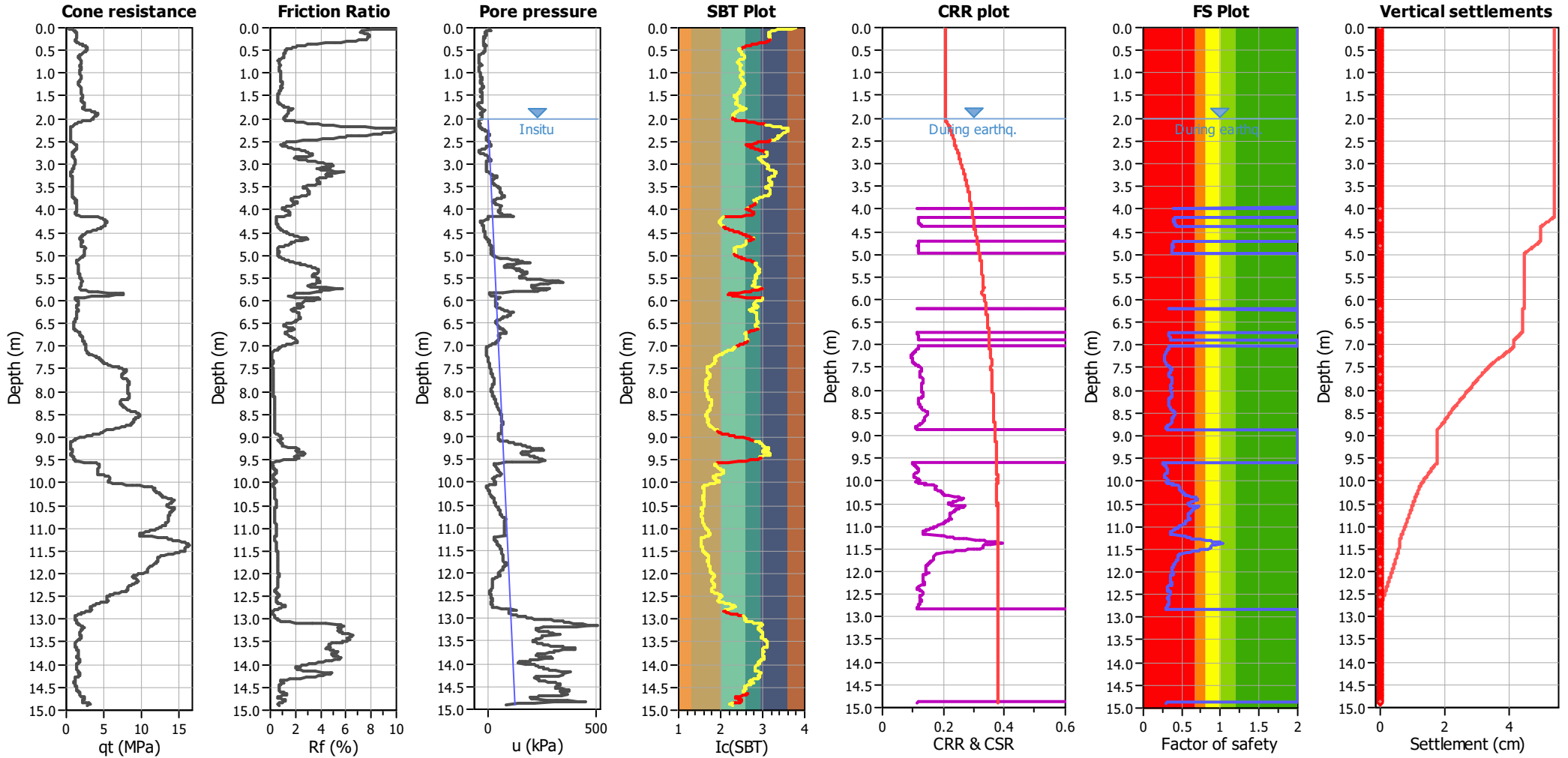
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.40 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



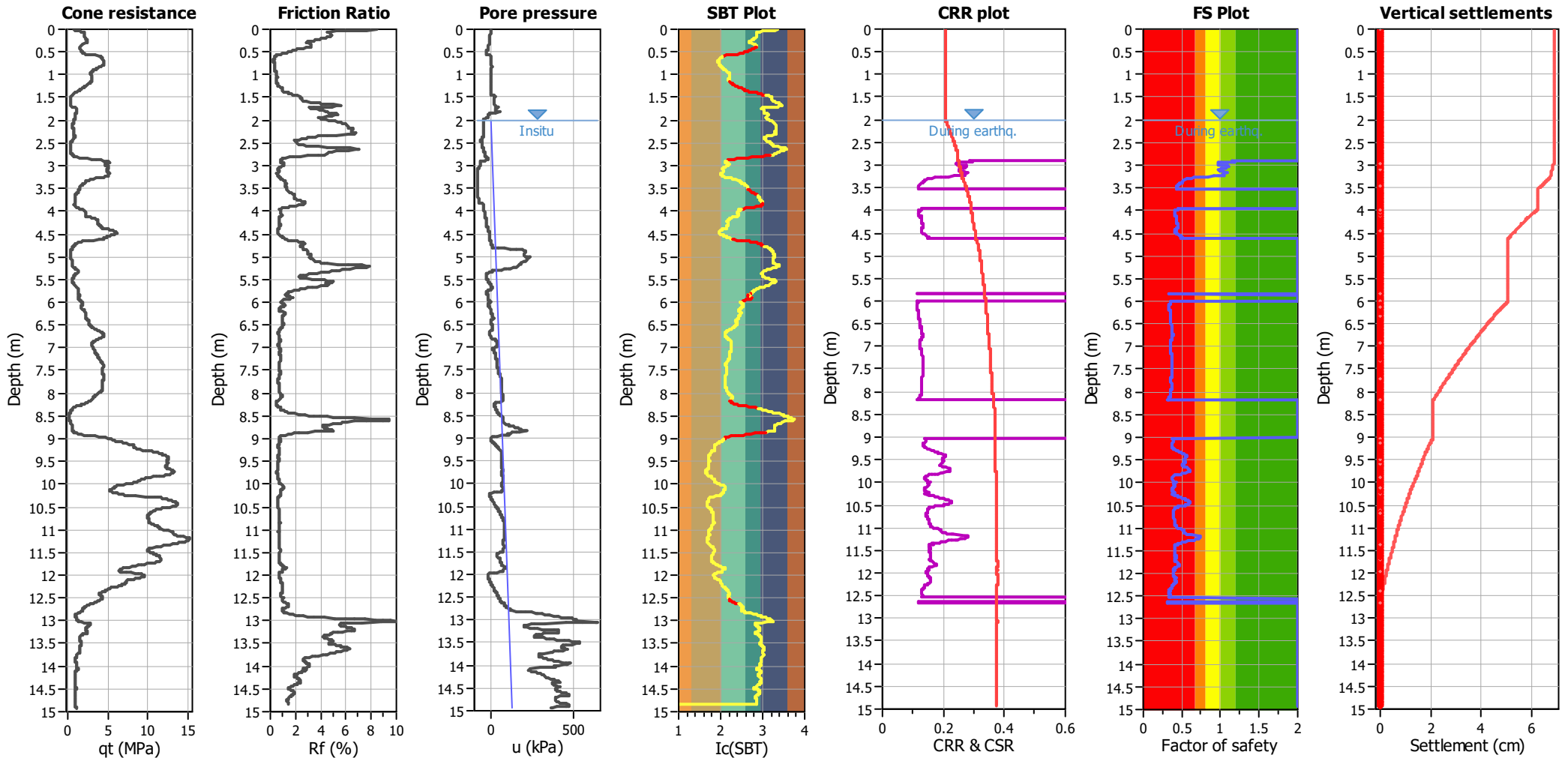
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



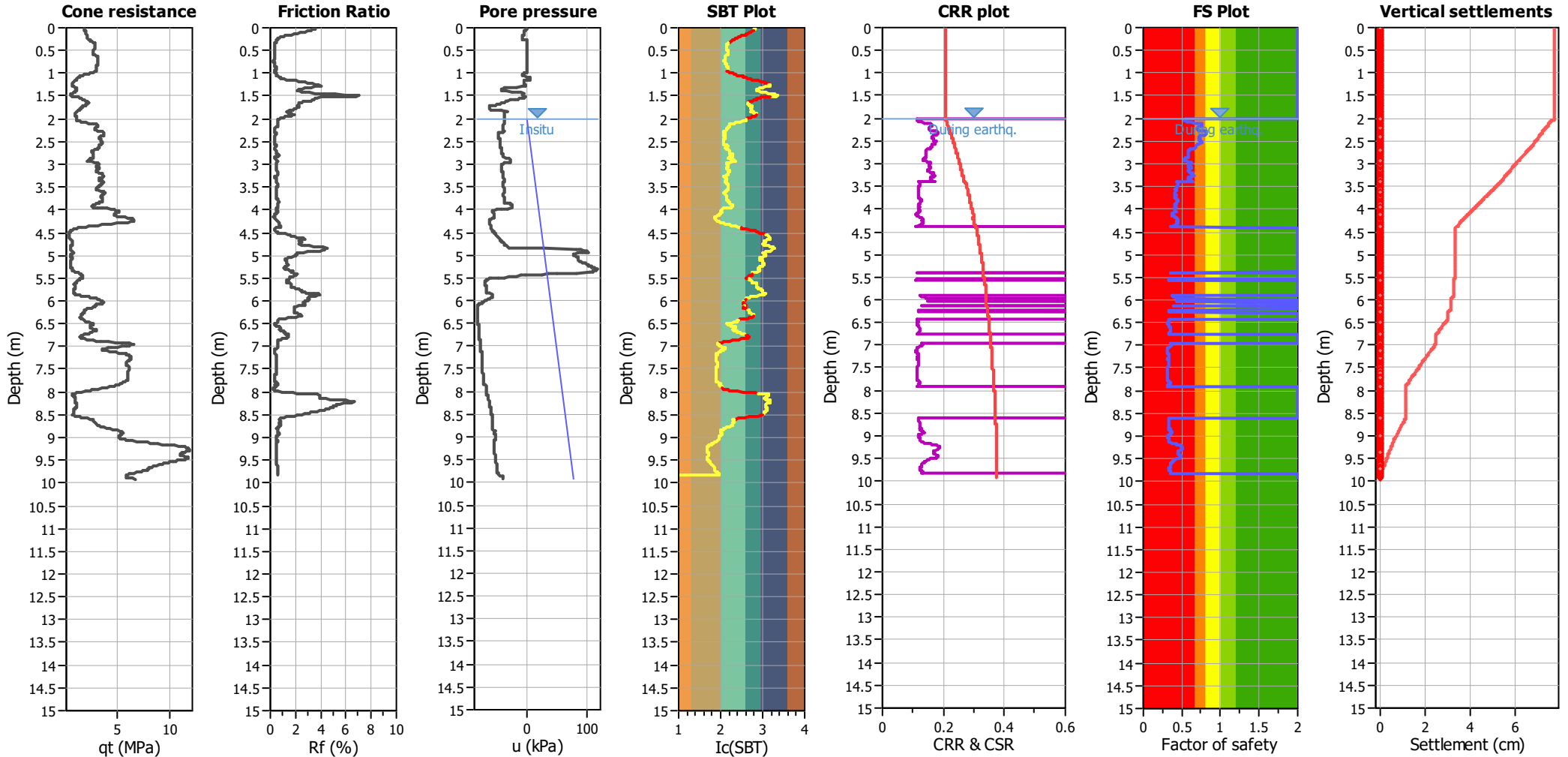
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	6.00	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.19	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



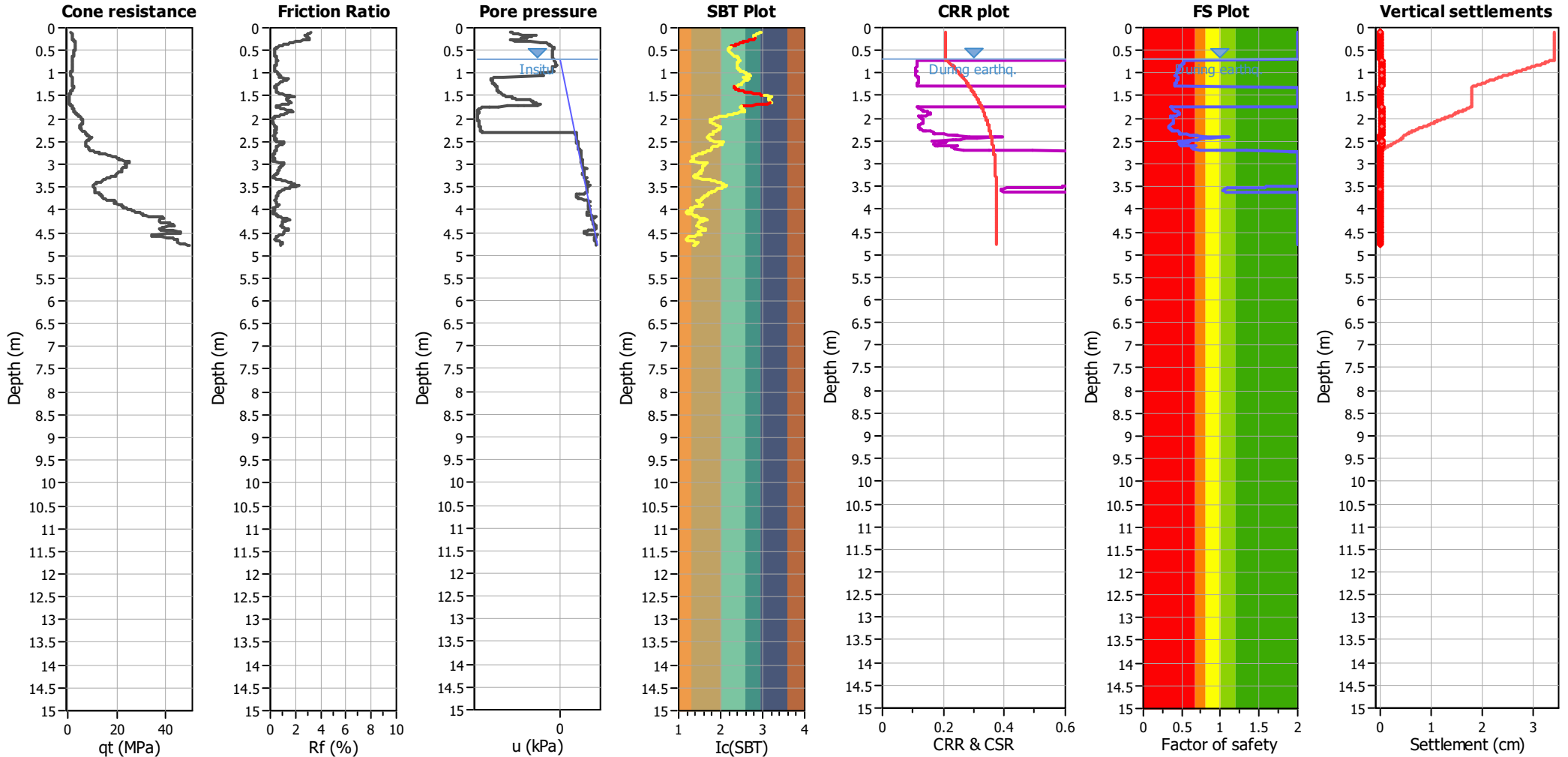
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	2.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

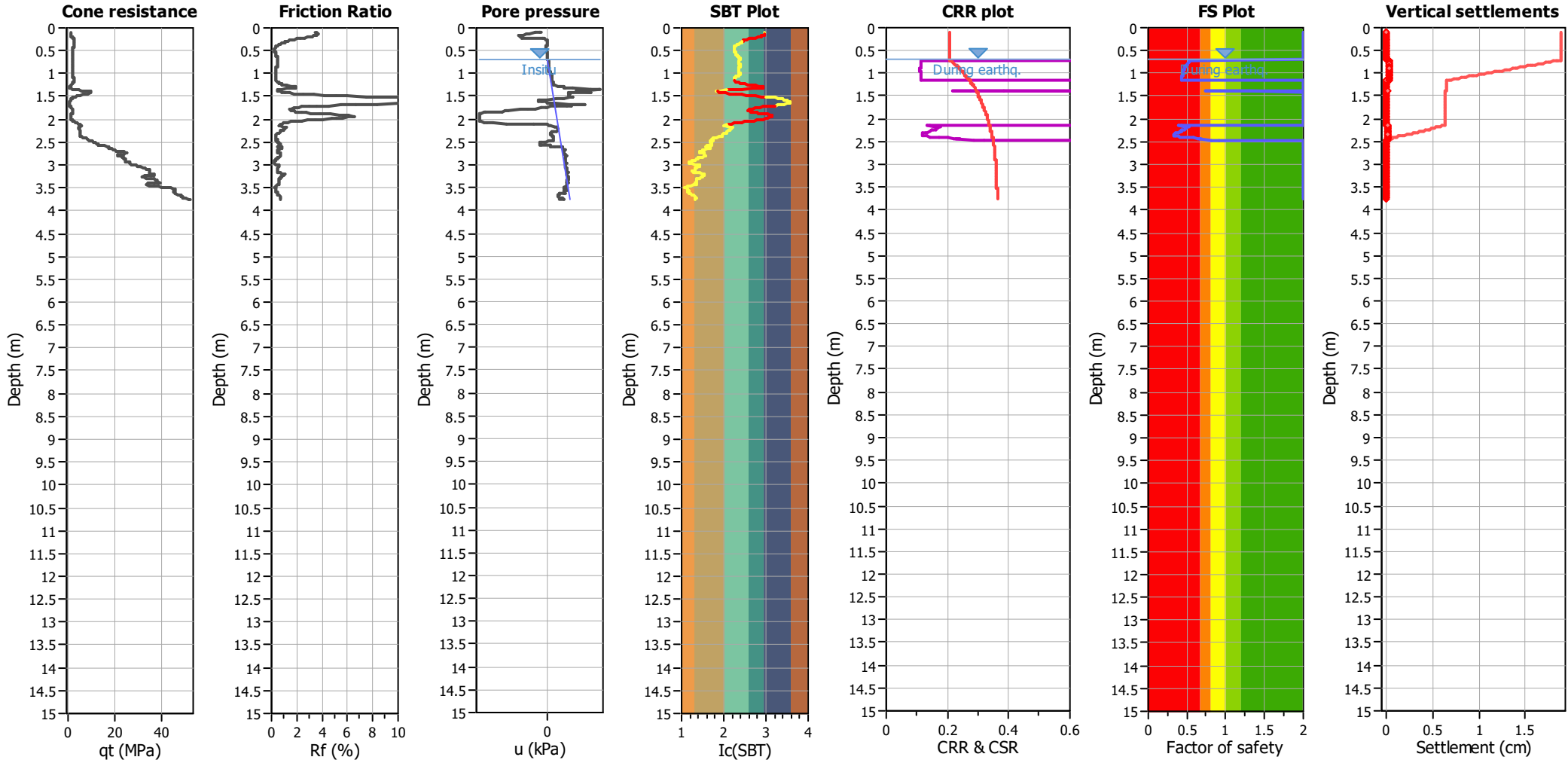


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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

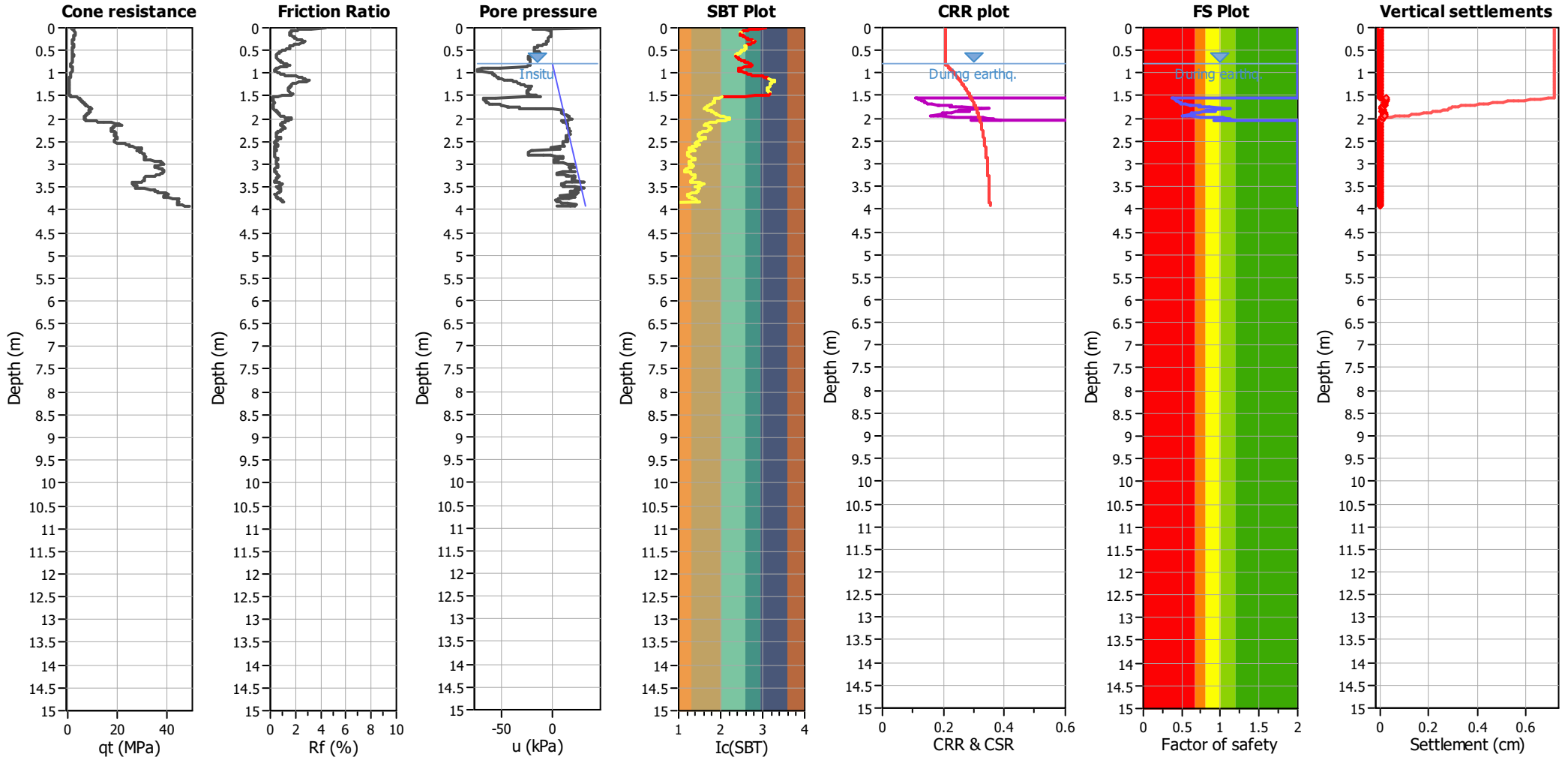


Analysis method:	B&I (2014)	G.W.T. (in-situ):	0.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

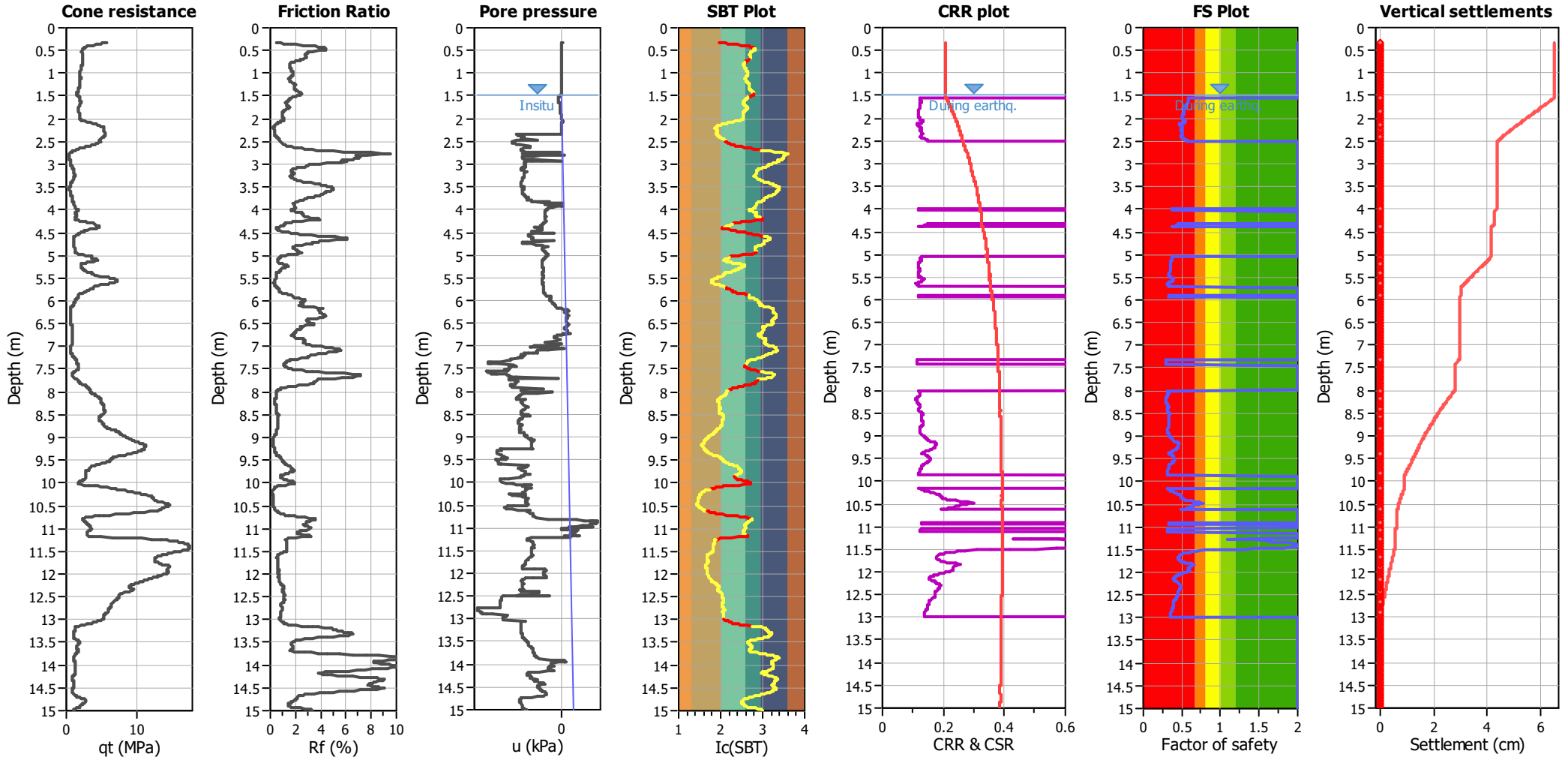




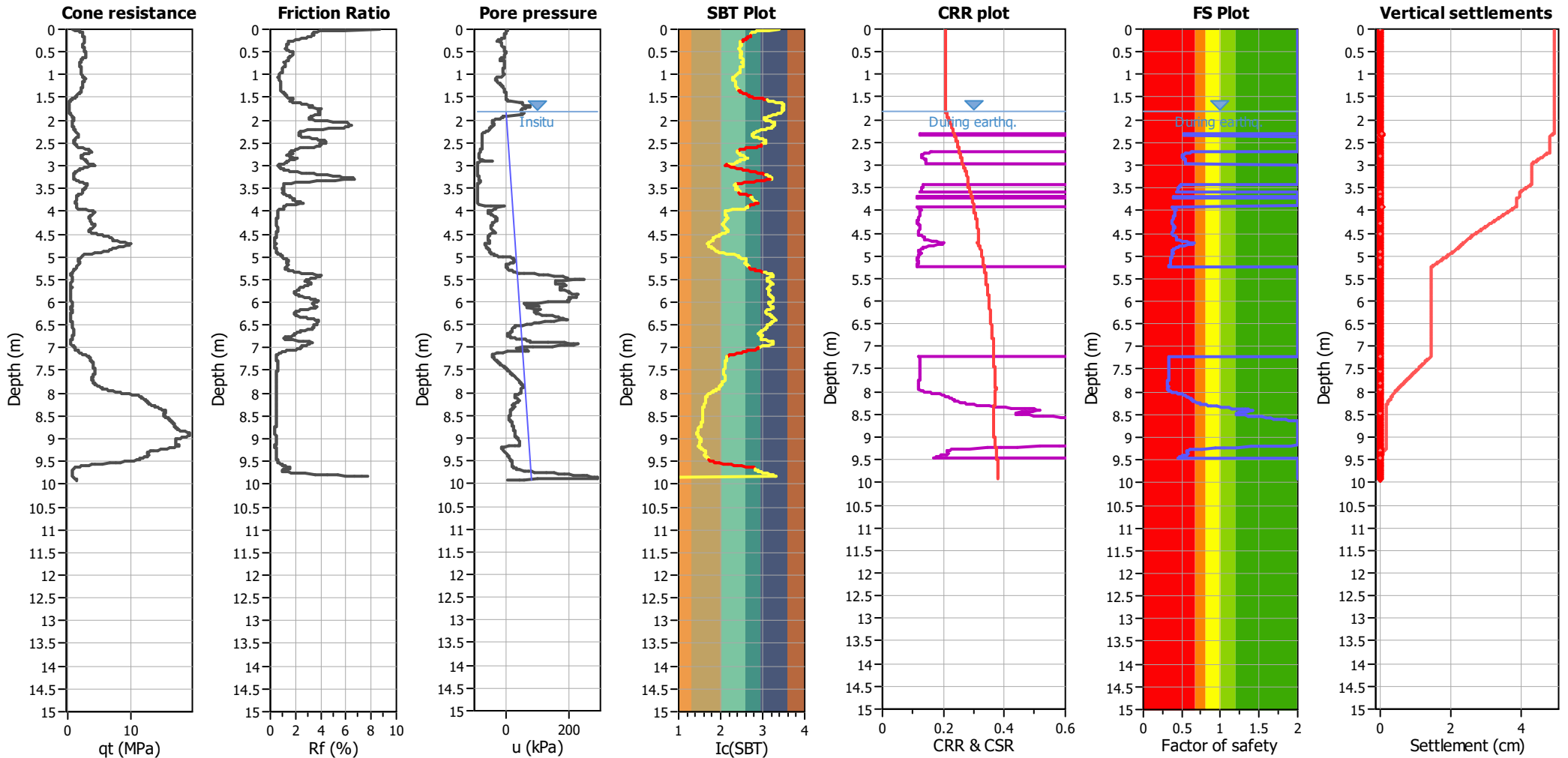
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



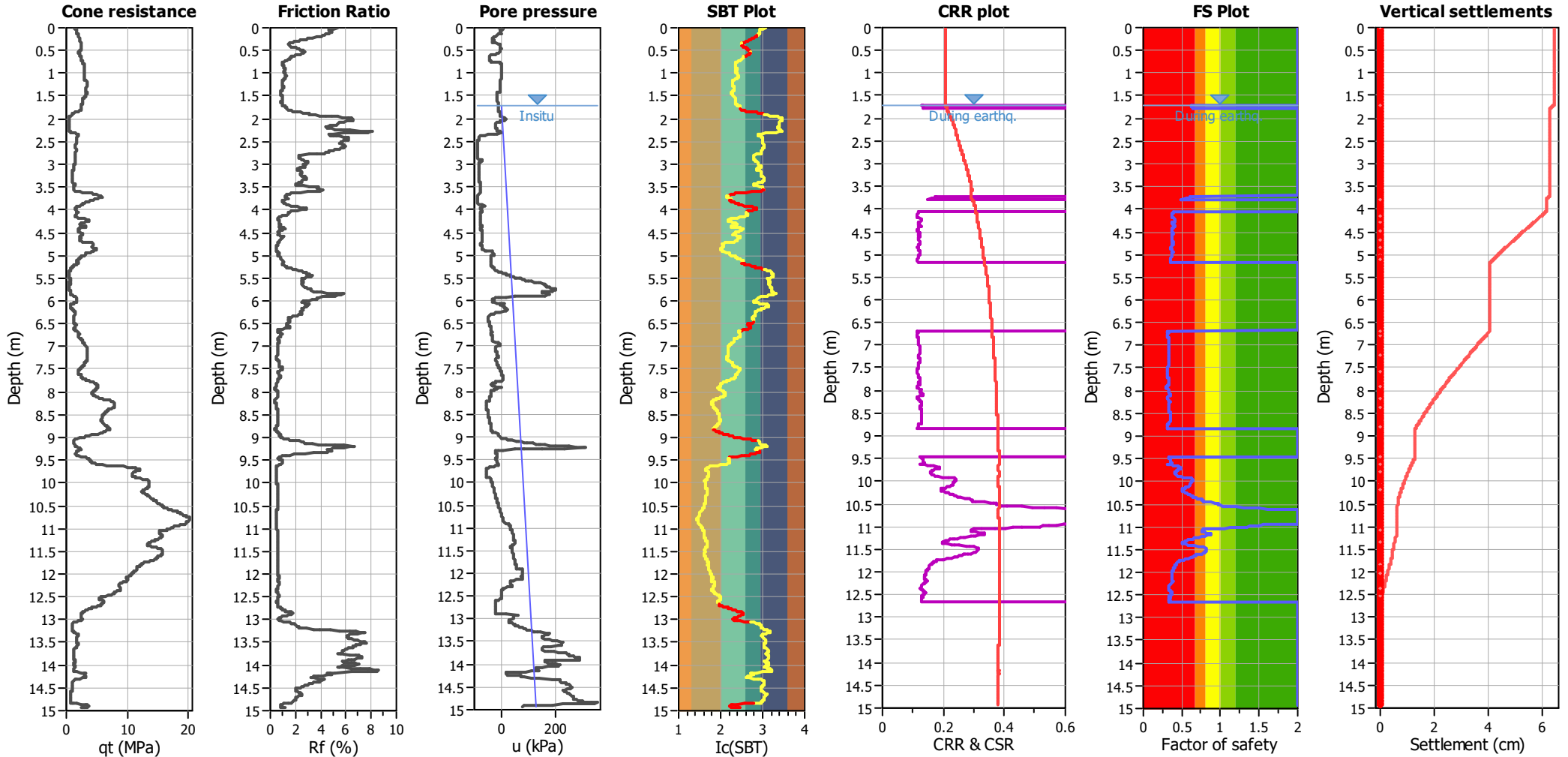
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	0.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



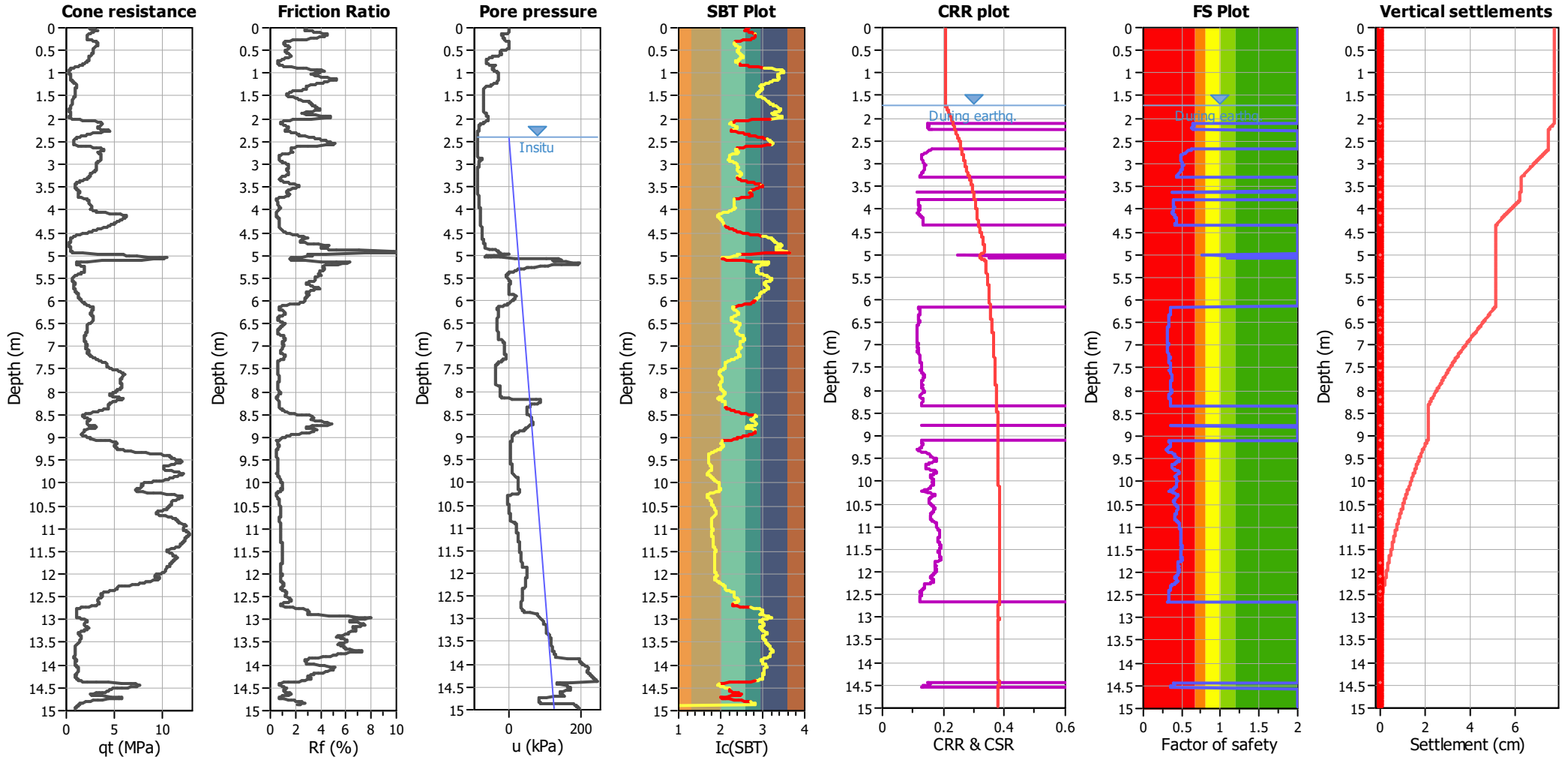
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Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



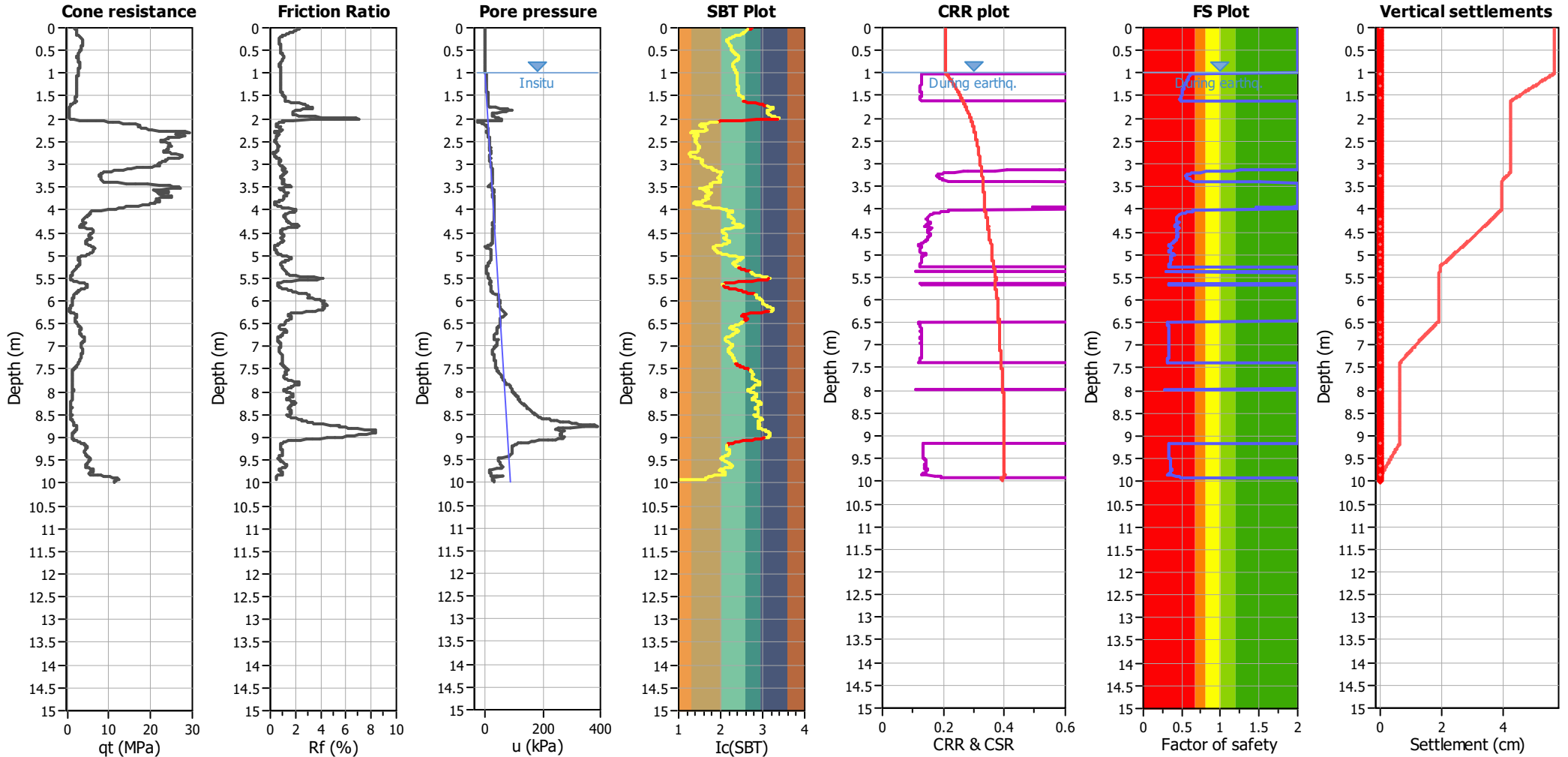
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Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.80 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



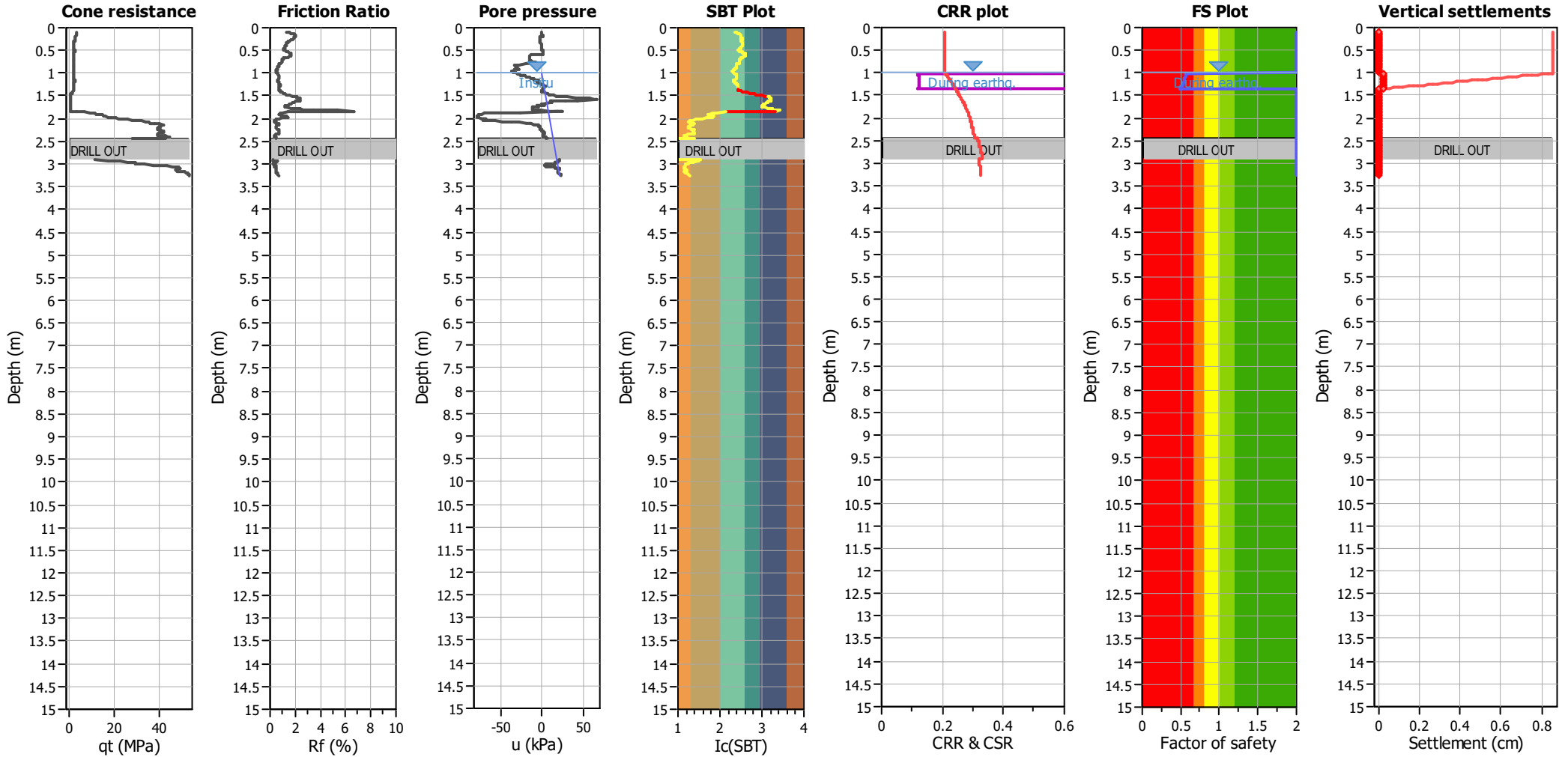
Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.70 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	2.40 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.70 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	No
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	N/A
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based

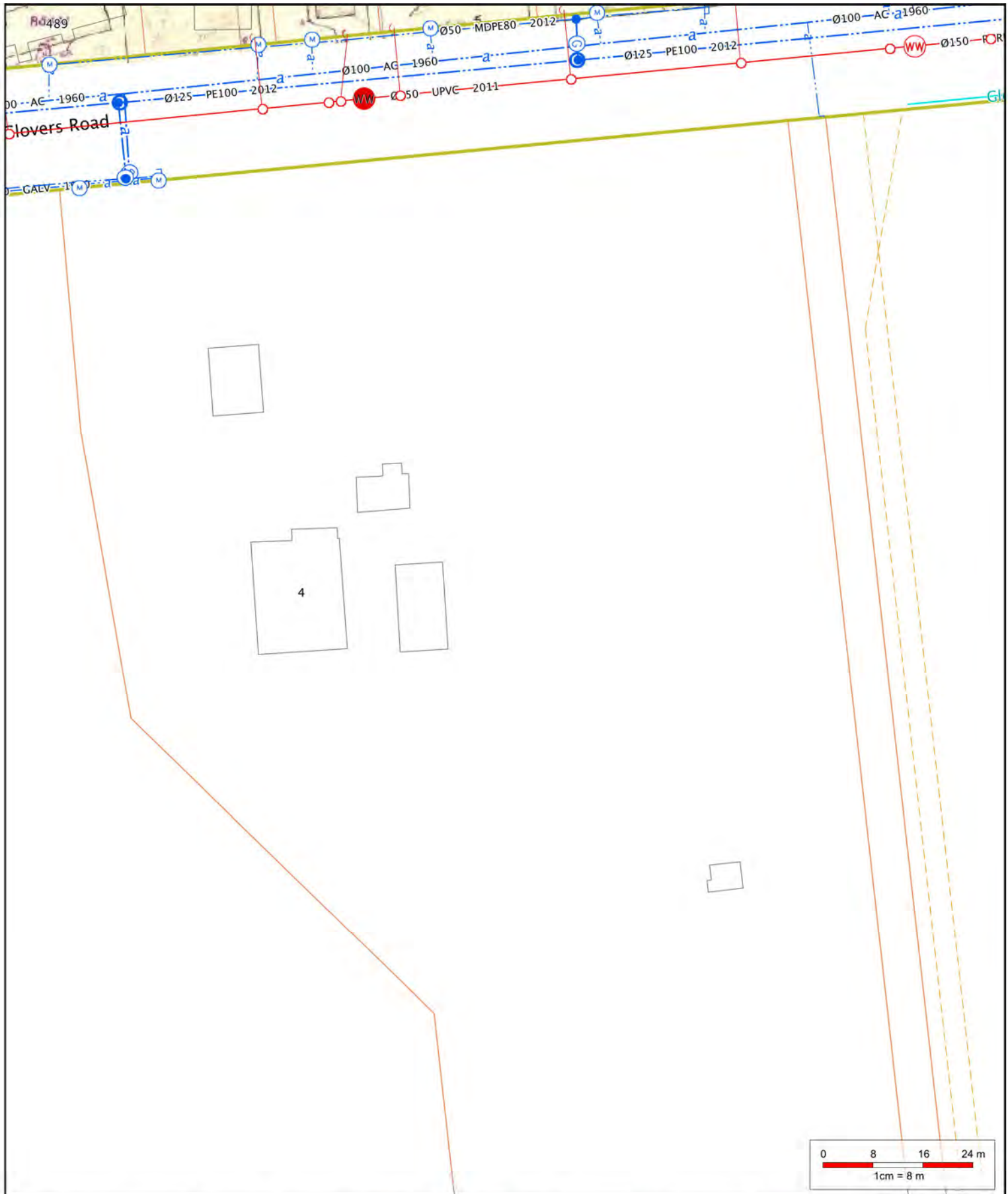


Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based



Analysis method:	B&I (2014)	G.W.T. (in-situ):	1.00 m	Use fill:	No	Clay like behavior	
Fines correction method:	B&I (2014)	G.W.T. (earthq.):	1.00 m	Fill height:	N/A	applied:	.
Points to test:	Based on Ic value	Average results interval:	3	Fill weight:	N/A	Limit depth applied:	Yes
Earthquake magnitude $M_w$ :	7.50	Ic cut-off value:	2.60	Trans. detect. applied:	Yes	Limit depth:	10.00 m
Peak ground acceleration:	0.35	Unit weight calculation:	Based on SBT	$K_0$ applied:	Yes	MSF method:	Method based






**1 : 800 on A4**  
 18/06/2021 10:43:50 AM  
  
 ph: 941-8300 fax: 941-8385

**Private Drainage**

**Standard Infrastructure**

- Bio Gas
- Condensate Trap
- End Cap
- Inlet
- Outlet
- Valve
- Main
- Cable

**Water Intake/Supply**

- Connector
- Ballows
- Connector
- Hydrant

**Water Intake/Supply**

- Inlet
- Meter
- Outlet
- Pump
- Restrictor
- Valve
- Air Release
- Butterfly
- Flow restriction
- Gate
- Pressure Activated
- Sluice
- Valve
- Reservoir
- Structure
- Lateral
- Main
- Sub Main

**Wastewater**

- End Cap
- Valve
- Air Gap Separator
- Vent
- Eye
- Eye (Vertical)
- Outfall
- Pump
- Junction
- Access
- Flush Manhole
- Inspection Point
- Standard Manhole
- Trap
- Vented Manhole
- Lateral
- Main
- Pressure Main

**Wastewater**

- Lateral Fitting
- Local Pressure:**
- Control Panel
- Boundary Kit
- Tank System
- Site
- Vacuum Chamber
- Vacuum Breather

**Stormwater**

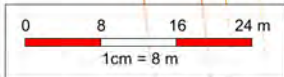
- Bend
- Change
- Eye
- Flow Restriction
- Inlet
- Dome Sump
- Double Sump
- Gross Debris Trap

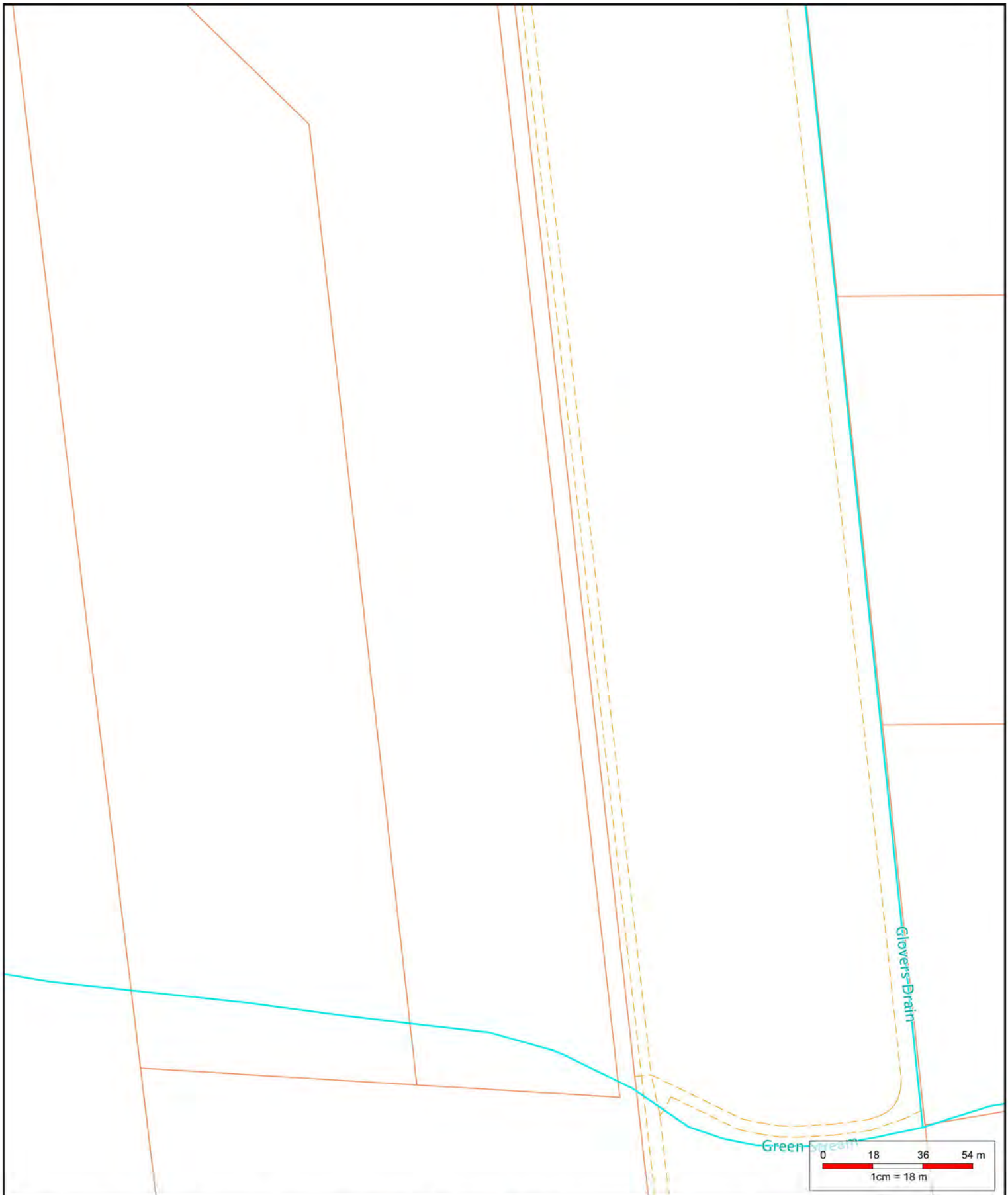
**Stormwater**

- Inlet
- Inlet Headwall
- Pipe End
- Silt Trap
- Single Sump
- Soak Pit
- Triple Sump
- Junction
- Standard Manhole
- Outlet
- Pump
- Structure
- Lateral
- Main
- Lateral Fitting
- Double Sump

**Stormwater**

- Lateral Fitting
- Single Sump
- Soak Pit
- Inspection point
- Manhole
- All services**
- Pipe Protection
- Abandoned
- Proposed point
- Out of service
- Landbase**
- Easement







 1 : 1,800 on A4  
 18/06/2021 10:45:41 AM  
  
 ph: 941-8300 fax: 941-8385

**Private Drainage**

**Standard Infrastructure**

-  Bio Gas
-  Condensate Trap
-  End Cap
-  Inlet
-  Outlet
-  Valve
-  Main
-  Cable

**Water Intake/Supply**

-  Connector
-  Ballows
-  Connector
-  Hydrant

**Water Intake/Supply**

-  Inlet
-  Meter
-  Outlet
-  Pump
-  Restrictor
-  Valve
-  Air Release
-  Butterfly
-  Flow restriction
-  Gate
-  Pressure Activated
-  Sluice
-  Valve
-  Reservoir
-  Structure
-  Lateral
-  Main
-  Sub Main









**Wastewater**

-  End Cap
-  Valve
-  Air Gap Separator
-  Vent
-  Eye
-  Eye (Vertical)
-  Outfall
-  Pump
-  Junction
-  Access
-  Flush Manhole
-  Inspection Point
-  Standard Manhole
-  Trap
-  Vented Manhole
-  Lateral
-  Main
-  Pressure Main


**Wastewater**

-  Lateral Fitting
- Local Pressure**
-  Control Panel
-  Boundary Kit
-  Tank System
-  Site
-  Vacuum Chamber
-  Vacuum Breather






**Stormwater**

-  Bend
-  Change
-  Eye
-  Flow Restriction
-  Inlet
-  Dome Sump
-  Double Sump
-  Gross Debris Trap





**Stormwater**

-  Inlet
-  Inlet Headwall
-  Pipe End
-  Silt Trap
-  Single Sump
-  Soak Pit
-  Triple Sump
-  Junction
-  Standard Manhole
-  Outlet
-  Pump
-  Structure
-  Basin
-  Lateral
-  Main
-  Lateral Fitting
-  Double Sump

**Stormwater**

-  Lateral Fitting
-  Single Sump
-  Soak Pit
-  Inspection point
-  Manhole

**All services**

-  Pipe Protection
-  -a- Abandoned
-  -p- Proposed
-  -os- Out of service

**Landbase**

-  Easement

Accuracy not guaranteed. Onsite verification required. Display of data scale dependent, full detail available at 1:500.

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CHRISTCHURCH CITY COUNCIL - DRAINAGE PICK UP

KED



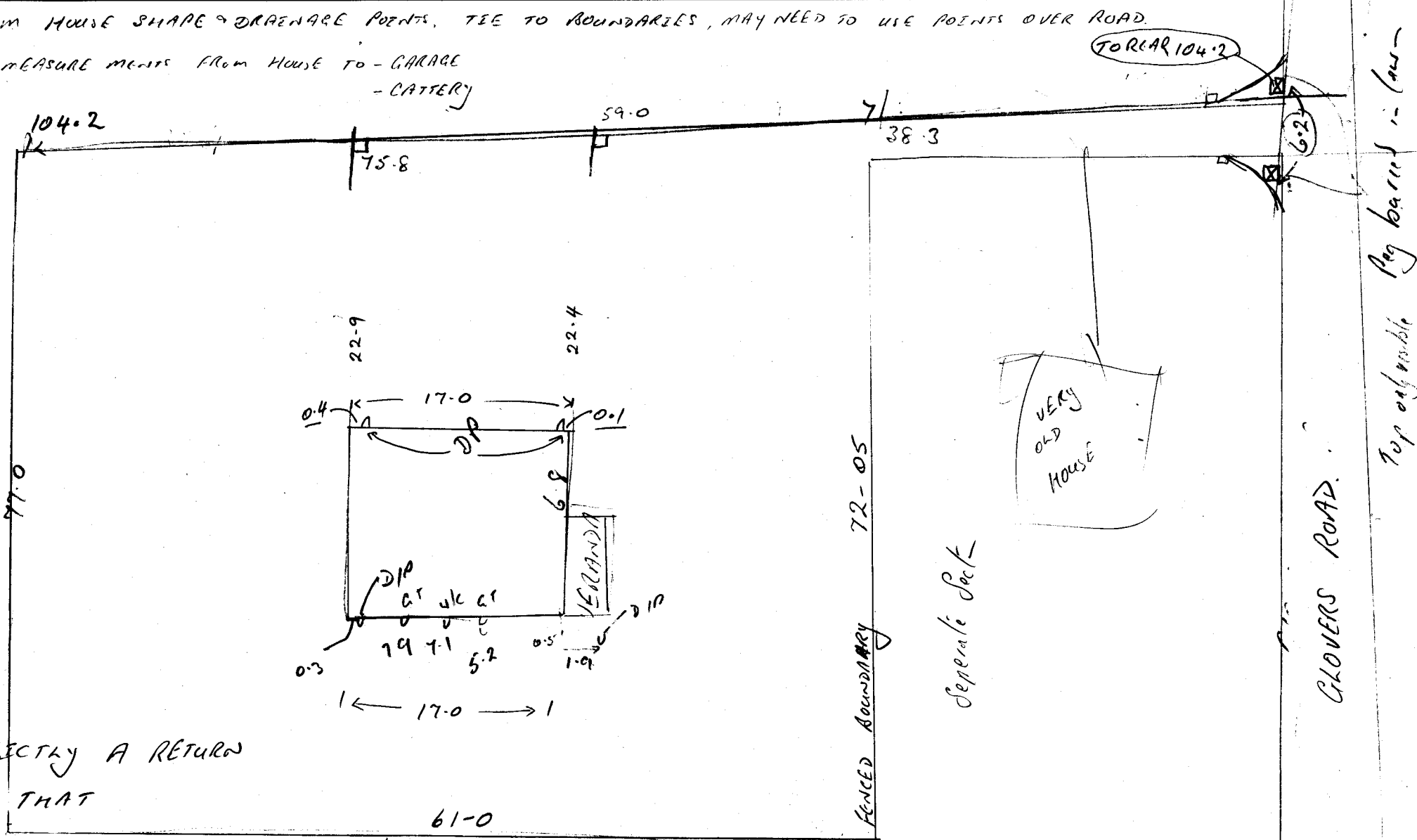
ADDRESS: 24 GLOVERS ROAD  
 LEGAL DESCRIPTION:  
 PROJECT No.:  
 DATE: 3/4/95

OWNER: CATTERY  
 DRAINLAYER:  
 PLUMBER:  
 FIELD OFFICER:

RECEIVED:  
 BLOCK PLAN:  
 PLOTTED: / /  
 EYE BOOK:

CONNECTION NUMBER

- CONFIRM HOUSE SHAPE & DRAINAGE POINTS, TIE TO BOUNDARIES, MAY NEED TO USE POINTS OVER ROAD.
- CHECK MEASURE MENTS FROM HOUSE TO - GARAGE - CATTERY



NOT STRICTLY A RETURN  
 JUST THAT

THIS PROPERTY IS OUTSIDE THE AREA COVERED BY OUR BLOCK PLANS

PHONE 898-7011R.

# W. G. GULLEFORD

BUILDING CONTRACTOR

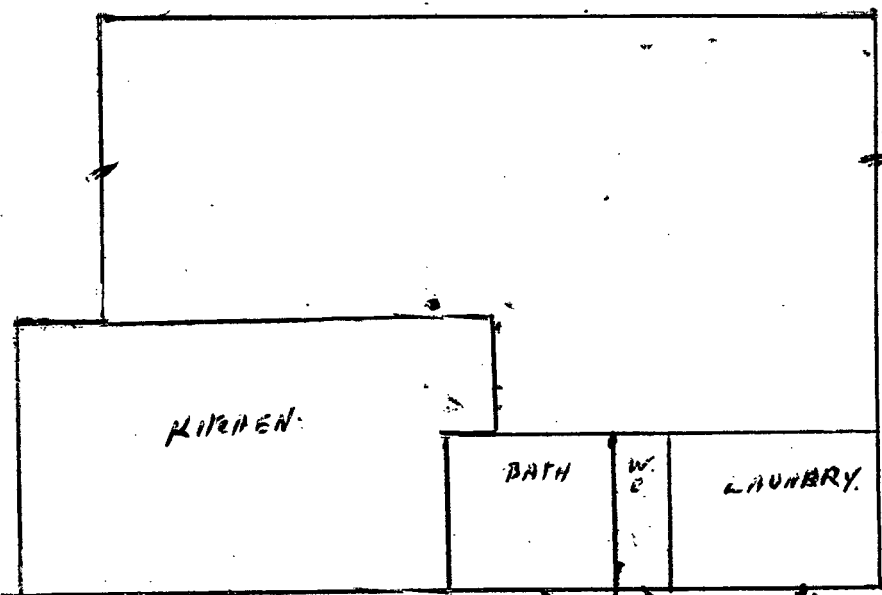
448 HALSWELL RD.  
~~69A JERROLD STREET~~  
CHRISTCHURCH  
S. W. 1.

HALSWELL RD.

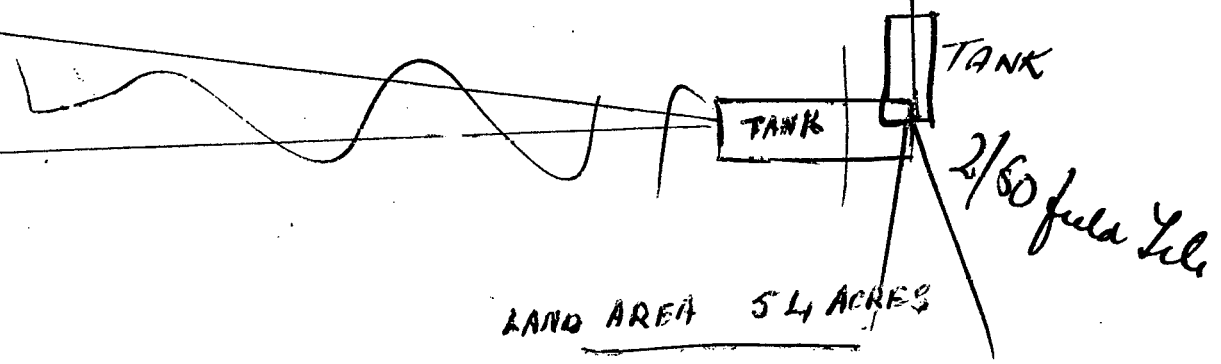
GLOVERS RD.

Per. R CAESAR ESQ

BOUNDARY



SINK      MV.      BATH BASIN      W.C.      TUB. 3'0"



LAND AREA 5 1/4 ACRES

# Your guide to the pressure wastewater system



**For alarms call**

**Christchurch  
City Council**



**(03) 941 8999**

# If the alarm sounds

1. The alarm noise can be turned off by pressing the button underneath the alarm panel. The alarm light on the panel will remain on.

If your pressure wastewater system has had a short term build up of wastewater then the system will automatically clean itself and the alarm light will go out.

2. If the alarm light is still on after one hour (1 hr) then call the Christchurch City Council on (03) 941 8999. The Council number is also on the alarm panel.
3. The Council call centre operator will ask you a series of questions to help determine the urgency and nature of any repairs that may be required.
4. The Council call centre operator will ask for your name and contact number so that the maintenance contractor can call you regarding any repairs.
5. The system has a 24hr emergency storage capacity. However, while waiting for any repairs you should try to minimise the amount of wastewater going through the system.
6. If the alarm sounded because of a short term build up of wastewater and then cleared you should consider what might have made this happen (for example flushing inappropriate items) and avoid this happening again.
7. If you notice any irregularity with the system (for example the alarm sounding often), contact the Christchurch City Council on (03) 941 8999.



Press the button located under the alarm panel. This will turn off the sound but the light will remain on.

Wait an hour and then check to see if the light on the alarm panel is still on.

If the light on the alarm panel is no longer lit then no further action is required.

If the light on the alarm panel is still on then call the Christchurch City Council on (03) 941 8999.

The call centre operator will ask for your address, name and contact number.

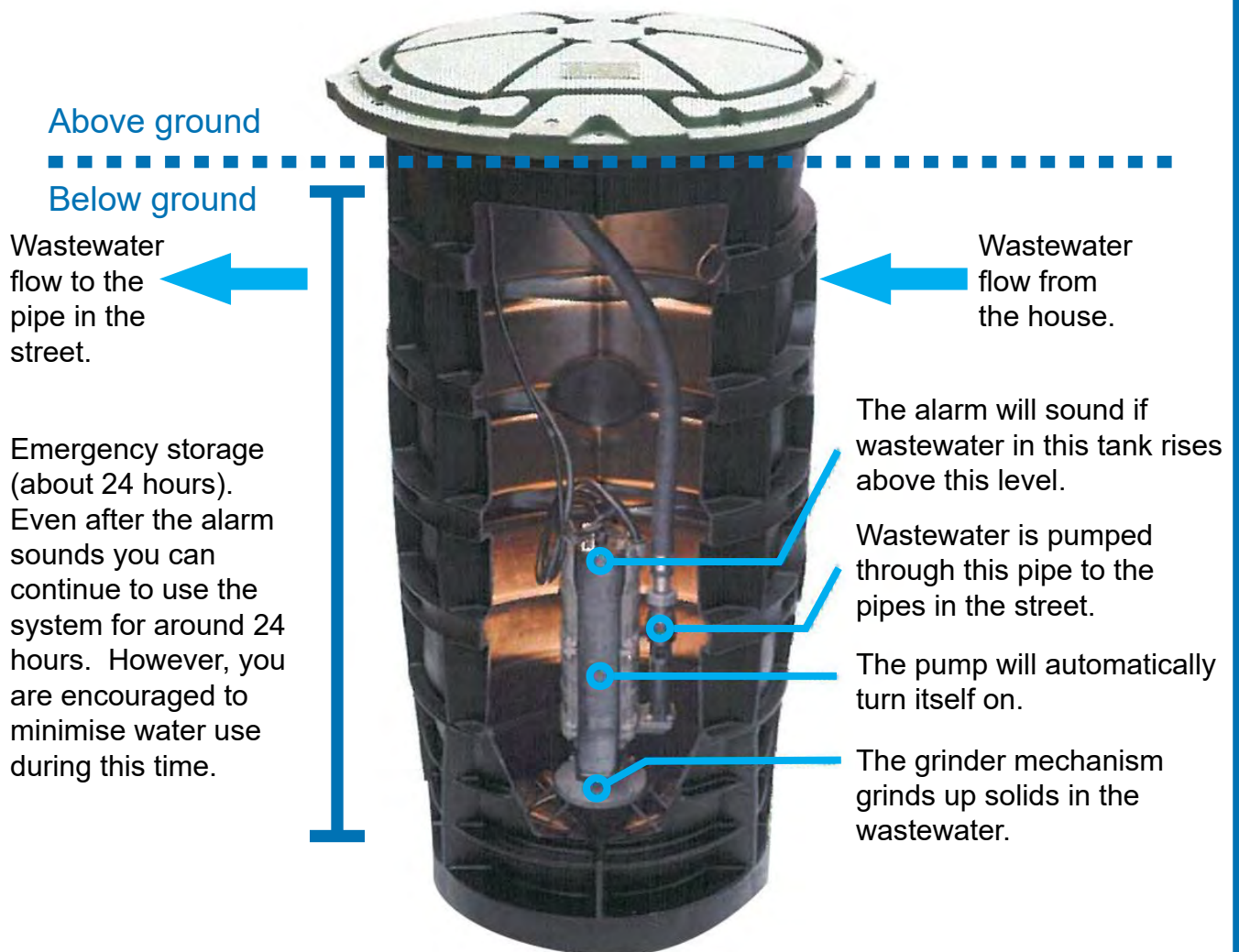
# The pressure wastewater system

**The wastewater system for this property is a pressure wastewater system.**

A pressure wastewater system includes an individual pump and tank. The pump is located within the tank. The tank is located underground and you will only see the lid at the surface. Wastewater from your house flows through a pipe (a private lateral) to the tank. The tank then pumps the wastewater to the pipes in the street. From the street the wastewater goes to the wastewater treatment plant.

The pressure wastewater system is very reliable and robust. There is very little you need to do and very little that can go wrong.

## The pressure wastewater system



# Using the system

There are a few things you need to know to ensure that the pressure wastewater system runs smoothly. The system operates like a normal wastewater system. It takes wastewater from your toilet, sink, shower, bath, dishwasher, and washing machine and transfers it to the wastewater pipes in the street, and onto the wastewater treatment plant.

To avoid blockages and damage to the pressure wastewater system there are a number of items that should not be disposed of via the system.

**The following items should not be flushed down the toilet or sink:**

- **glass**
- **metal**
- **gravel or sand, including stone from fish tanks**
- **seafood shells**
- **socks, rags, clothes**
- **plastic**
- **nappies, sanitary napkins, tampons, 'wet' wipes**
- **kitty litter**
- **explosives**
- **flammable materials**
- **lubricating oil and grease**
- **strong chemicals**
- **petrol, diesel**
- **stormwater runoff**

## Before you go on holiday

Before you go on holiday, even if it is just for a few days, you should flush the pressure wastewater system before you go. This is to avoid the possibility of the system becoming smelly while you are away. **To flush the system simply run a tap in the kitchen or bathroom sink for about five minutes before you go.**



# Taking care of the system

- **Do not flush any inappropriate items through the system.**
- **Do not put heavy weights on the lid of the tank. The lid can be walked on, but this should be avoided.**
- **Do not touch the valves in the boundary kit.**
- **Do not turn off the power to the pump unless evacuating in an emergency or if there is a broken wastewater pipe.**
- **Do not cover the unit in any way. This includes covering it with dirt, garden mulch, or concrete.**
- **Ensure access to the unit is available at all times.**
- **If you are going on holiday, even for just a few days, you should flush the system before you go. Simply run clean water down your kitchen or bathroom sink for five minutes (5 mins).**
- **If you do accidentally break a pipe under the ground contact the Christchurch City Council on (03) 941 8999 immediately and tell them what happened. While waiting for the pipe to be repaired minimise the amount of wastewater going through the system.**
- **Contact the Christchurch City Council on (03) 941 8999 if you install a swimming or spa pool.**
- **Contact the Christchurch City Council on (03) 941 8999 if you are making any modifications to your home which may affect the system (for example a house addition).**
- **Do not attempt to repair the system yourself. Always call the Christchurch City Council on (03) 941 8999.**

# Trouble shooting

## What happens if...

### 1. The system is damaged and needs repair?

The alarm will go off. Follow the alarm procedure on page 2.

### 2. You notice a bad smell around the tank

When operating normally there should be no noticeable odours coming from the unit. If it is smelly, the unit may just need flushing. Just run clean water down your kitchen or bathroom sink for about five minutes. If the unit remains smelly contact the Christchurch City Council on (03) 941 8999.

### 3. You notice wet spots around the unit or wastewater pipes

The pumping unit and pipes are sealed. If you notice wet spots and there hasn't been any recent heavy rain contact the Christchurch City Council on (03) 941 8999.

### 4. The alarm keeps going off when it rains

This means that rainwater may be getting into the system and overloading it. Contact the Christchurch City Council on (03) 941 8999.

### 5. The neighbours alarm goes and they are away

Do not investigate yourself. Contact the Christchurch City Council on (03) 941 8999.

### 6. There is a power failure

If there is a power failure the pump will not run. The tank has 24 hours of emergency storage so minimise the amount of wastewater going through the system. When the power comes on again the system will reset itself.

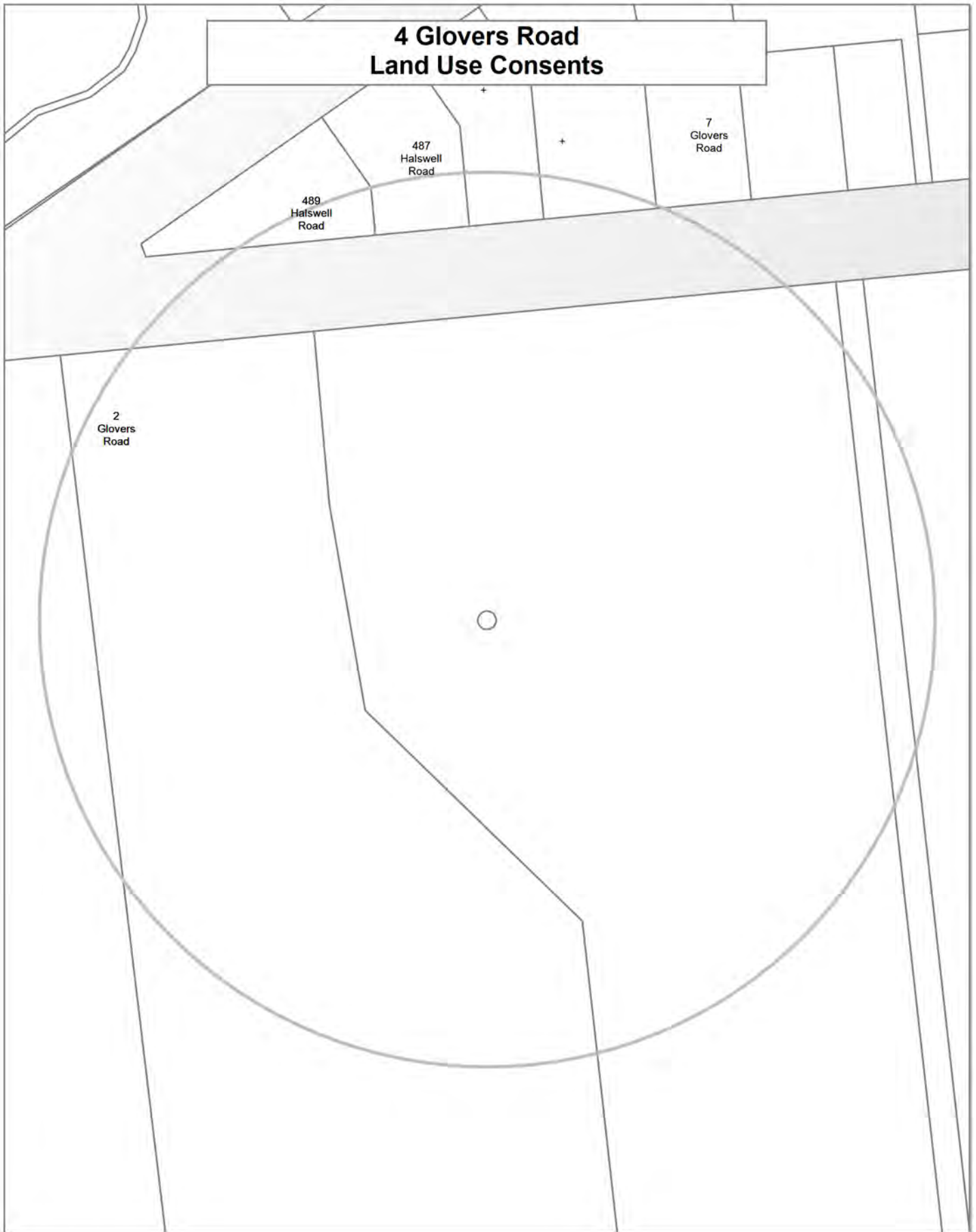
### 7. There is a flood

If you can safely stay in your home in a flood then simply minimise the amount of wastewater going through the system.

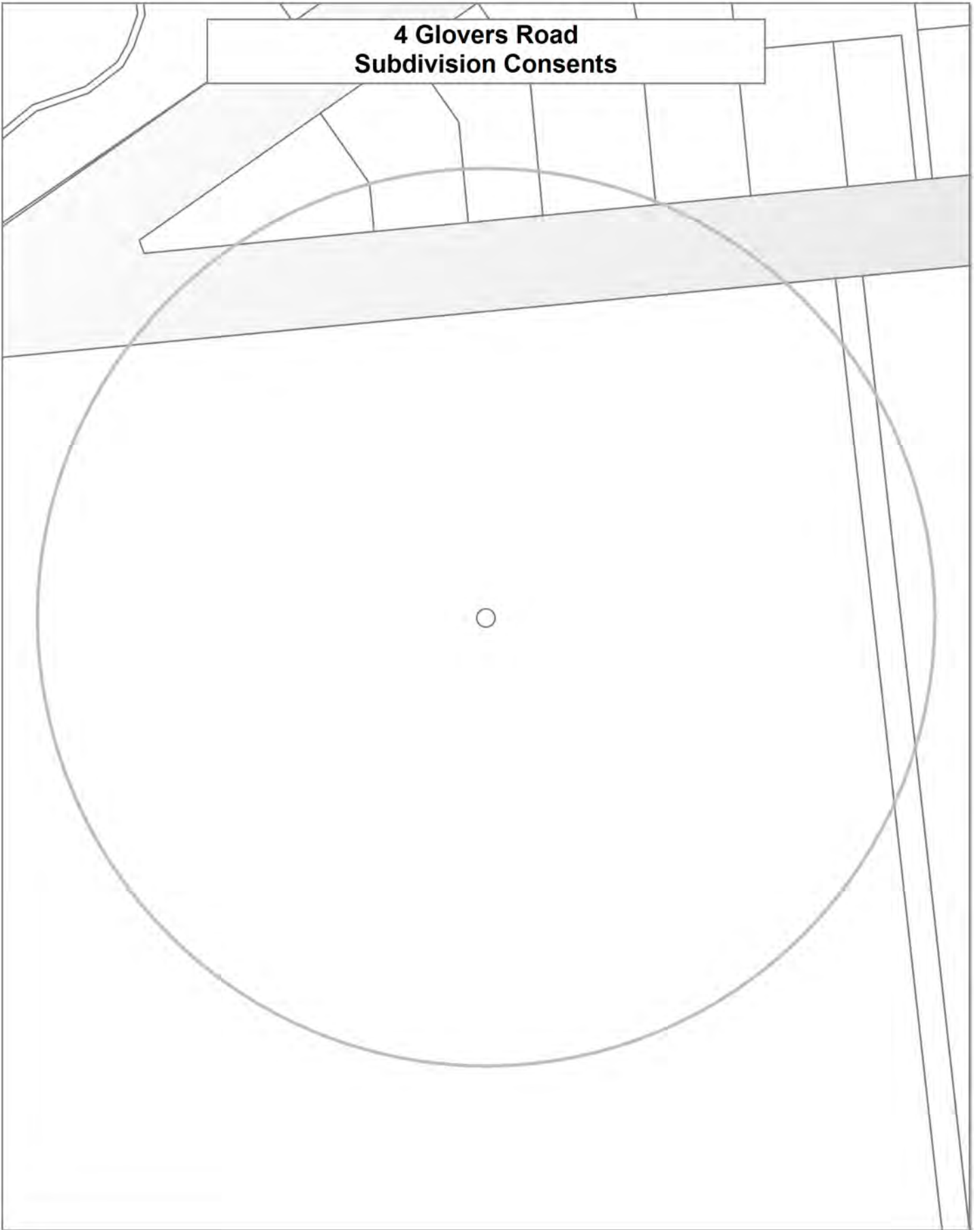
### 8. You need to evacuate due to an emergency (such as an earthquake)

If you can, flush out the system by running water down your kitchen or bathroom sink for about five minutes. Turn off the power to the pump. The on/off switch is located by the alarm panel.

## 4 Glovers Road Land Use Consents



**4 Glovers Road  
Subdivision Consents**



## Land Use Resource Consents within 100 metres of 4 Glovers Road

Note: This list does not include subdivision Consents and Certificates of Compliance issued under the Resource Management Act.

---

### 10 Glovers Road

RMA/2002/1305

Application to erect a new implement shed - Historical Reference RMA20010309

Processing complete

Applied 06/06/2002

Decision issued 03/07/2002

Granted 02/07/2002

### 2 Glovers Road

RMA/1974/419

To permit a subdivision less than the area permitted under the District planning scheme. - Historical Reference RES955313

Processing complete

Applied 21/10/1974

Decision issued 21/10/1974

Granted 21/10/1974

RMA/1989/257

4.6m side yard instead of the required 10m - Historical Reference RES9206551

Processing complete

Applied 17/08/1989

Decision issued 23/08/1989

Granted 23/08/1989

RMA/1993/1160

The erection of a boarding cattery in the rural 2 zone at Glovers Road. - Historical Reference RES94101932

Processing complete

Applied 12/03/1993

Decision issued 19/05/1993

Granted 19/05/1993

RMA/1998/1327

Application for a temporary additional rural dwelling a proposed dwelling is to be constructed which is to replace an existing cottage on - Historical Reference RES981500

Processing complete

Applied 08/06/1998

Decision issued 17/07/1998

Granted 17/07/1998

RMA/1998/1529

Application for a dwelling addition which intrudes the 10m setback in terms of both the Proposed and Transitional Plans.  
- Historical Reference RES981736

Processing complete

Applied 01/07/1998

Decision issued 08/07/1998

Granted 08/07/1998

RMA/1999/2499

Application to subdivide a 5261m<sup>2</sup> allotment, including an existing dwelling, garage and cattery, from a 12.3192 ha property. - Historical Reference RES991246

Processing complete

Applied 30/04/1999

Decision issued 09/09/1999

Declined 09/09/1999

RMA/2020/2557

Remediation of contaminated soils

Processing complete

Applied 06/11/2020

Decision issued 09/12/2020

Granted 09/12/2020

RMA/2020/2770

To conduct earthworks and stockpiling on site

Processing complete

Applied 27/11/2020

Decision issued 27/01/2021

Granted 27/01/2021

RMA/2020/3076

To subdivide 4 allotments to create 87 residential allotments. Land use consent for earthworks and under the NES for contaminated land.

On hold - waiting for response from applicant

Applied 22/12/2020

## 26 Glovers Road

RMA/2004/670

To subdivide a site into 2 allotments of 6.4489ha and 1 .3460ha and to retain an existing dwelling on the small er allotment. - Historical Reference RMA20016252

Processing complete

Applied 04/03/2004

Decision issued 11/10/2004

Granted 07/10/2004

RMA/2012/543

ESTABLISH AND UTILISE A RESIDENTIAL UNIT AND ACCESSORY BUILDINGS FOR 252 LOTS ASSOCIATED TO A SUBDIVISION SUB - RMA92019884 - Historical Reference RMA92019883

On hold - waiting for response from applicant

Applied 17/04/2012

RMA/2021/1513

Global consent for earthworks within 5 metres of a street tree

Processing

Applied 25/05/2021

RMA/2021/199

Fee simple subdivision - 207 lots, eight roads, recreation reserve and three local purpose reserves and associated land use.

On hold - processing suspended by applicant

Applied 02/02/2021

## **487 Halswell Road**

RMA/1994/527

Consent to erect a garage over 40m<sup>2</sup> in the front yard, and to erect a studio in the front yard. - Historical Reference RES94001092

Processing complete

Applied 30/06/1994

Decision issued 25/07/1994

Granted 25/07/1994

## **489 Halswell Road**

RMA/1995/2290

Application for reduced setback for garage - Historical Reference RES953485

Processing complete

Applied 16/08/1995

Decision issued 07/09/1995

Granted 07/09/1995

RMA/2001/351

Appication for a garage addition to be attached to the existing dwelling with non compliances with street setback; length of wall and queuing space - Historical Reference RMA20004203

Processing complete

Applied 09/02/2001

Decision issued 01/03/2001

Granted 01/03/2001

## 511 Halswell Road

RMA/2020/163

Earthworks for residential development

Processing complete

Applied 29/01/2020

Decision issued 10/02/2020

Granted 10/02/2020

RMA/2020/2770

To conduct earthworks and stockpiling on site

Processing complete

Applied 27/11/2020

Decision issued 27/01/2021

Granted 27/01/2021

RMA/2020/3076

To subdivide 4 allotments to create 87 residential allotments. Land use consent for earthworks and under the NES for contaminated land.

On hold - waiting for response from applicant

Applied 22/12/2020

RMA/2021/733

Earthworks - Associated with the formation of vehicle crossings

Processing complete

Applied 24/03/2021

Decision issued 11/06/2021

Granted 11/06/2021

## 7 Glovers Road

RMA/1978/147

Extension to dwelling with garage less than 3m from dwelling - Historical Reference RES9206552

Processing complete

Applied 19/12/1978

Decision issued 12/01/1979

Declined 12/01/1979

## Data Quality Statement



## Land Use Consents

All resource consents are shown for sites that have been labelled with an address. For sites that have been labelled with a cross (+) no resource consents have been found. Sites that have no label have not been checked for resource consents. This will be particularly noticeable on the margins of the search radius. If there are such sites and you would like them included in the check, please ask for the LIM spatial query to be rerun accordingly. This will be done free of charge although there may be a short delay. Resource consents which are on land occupied by roads, railways or rivers are not, and currently cannot be displayed, either on the map or in the list. Resource consents that relate to land that has since been subdivided, will be shown in the list, but not on the map. They will be under the address of the land as it was at the time the resource consent was applied for. Resource consents that are listed as Non-notified and are current, may in fact be notified resource consents that have not yet been through the notification process. If in doubt. Please phone (03)941 8999.

The term “resource consents” in this context means land use consents. Subdivision consents and certificates of compliance are excluded.

## Subdivision Consents

All subdivision consents are shown for the sites that have been labelled with consent details. For Sites that have been labelled with a cross (+) no records have been found. Sites that have no label have not been checked for subdivision consents. This will be particularly noticeable on the margins of the search radius. If there are such sites and you would like them included in the check, please ask for the LIM spatial query to be rerun accordingly. This will be done free of charge although there may be a short delay.

The term “subdivision consents” in this context means a resource consent application to subdivide land. Non subdivision land use resource consents and certificates of compliance are excluded.

This report will only record those subdivision applications which have not been completed i.e once a subdivision has been given effect to and the new lots/properties have been established the application which created those lots will not be shown

All subdivision consent information is contained on the map and no separate list is supplied